# CAMBRIA STEEL

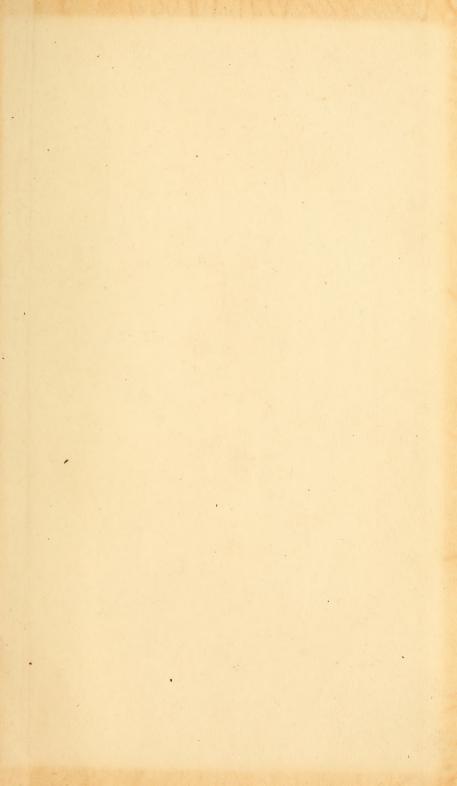
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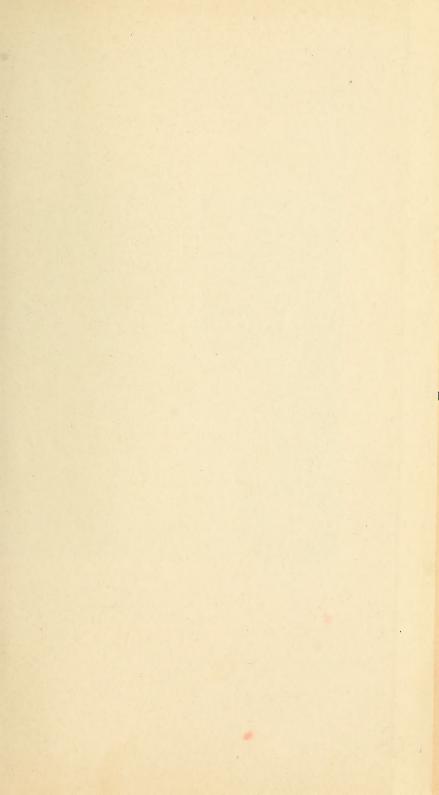
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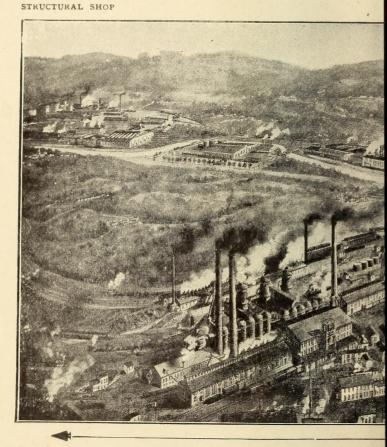




NEW OPEN HEARTH STEEL WORKS
BLOOMING MILL
SLABBING MILL
PLATE MILL
CAR PLANT
COKE OVENS

COAL MINES

POLISHED



BLAST FURNACES
BOILER HOUSES

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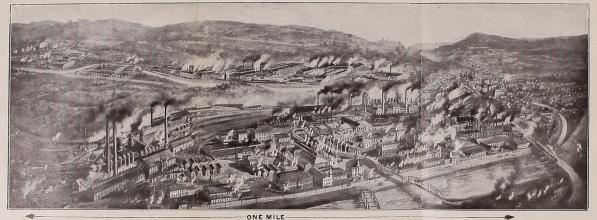


NEW OPEN HEARTH STEEL WORKS
RLOOMING MILL
SLABBING MILL
PLATE MILL
CAR FLANT
COKE OVENS
STRUCTURAL SHOP

#### ROLLING MILLS FOR MERCHANT BAK, AGRICULTURAL, PLOW AND COLD-ROLLED STEEL

POLISHED STEEL DEPT. SHEAR SHOP RAKE SHOP HARROW DISC PLANT
HAMMER SHOP MACHINE SHOP SHAFTING WAREHOUSE

OFFICE



BLAST FURNACES
BOILER HOUSES

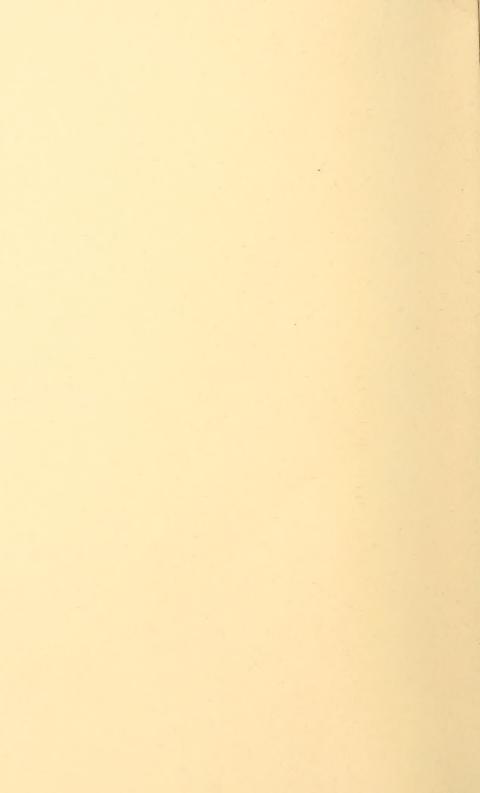
PATTERN HOUSES WAREHOUSE, FOUNDRY, ROLLING MILLS

ROOFING DEPT. BOILER SHOPS

AXLE PLANT

BLAST FURNACES
BLOOMING MILL BRAM, BILLET AND SLAB MILLS
BESSHMER STEEL WORKS OLD OPEN HEARTH STEEL WORKS

WORKS OF CAMBRIA STEEL COMPANY
AT JOHNSTOWN, PENNA.
GENERAL OFFICE, PHILADELPHIA, PENNA.
1903



# CANBRA STREET

A handbook of information relating to

### STRUCTURAL STEEL

Manufactured by the

# CAMBRIA STEEL CO.

containing useful tables, rules, data and formulæ for the use of Engineers, Architects,

BUILDERS AND MECHANICS.

GENERAL OFFICE, PHILADELPHIA.

Works, Johnstown, Pa.

THE L SPARY OF CONGRESS.

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PRICE, \$1.00

PRESS OF
MACCALLA & COMPANY
PHILADELPHIA, PA

#### PREFACE TO SIXTH EDITION.

This, the sixth edition of our hand book, contains all of the data of the fourth and fifth editions, which, however, have been corrected where necessary and revised to conform to our present practice.

The present edition also contains a considerable amount of new matter relating to new sections of angles and T-Bars, and additional sizes of billets, blooms, ingots, edged and sheared plates.

The weights of angles, Z-Bars and T-Bars now given are those adopted as standards by the Association of American Steel Manufacturers.

Other new matter, which has been introduced, consists of tables of safe loads and dimensions for plate and angle columns and for Z-Bar columns with side plates. Tables have been added showing the section moduli and moments of inertia for all of the built-up columns for which the safe loads are tabulated, which values will be of special assistance in cases where it is necessary to consider the effect of eccentric loads in figuring the strength of the columns.

Tables of safe loads for angles, T-Bars and Z-Bars acting as beams with uniformly distributed loads, have been inserted, and in the case of angles with unequal legs the safe loads are given for both positions, that is, with the long leg vertical and with the short leg vertical.

The matter relating to fire-proof construction has been revised, and some changes have been made in the information relating to wood.

Special attention is called to the list of sheared plates which we can now furnish in widths up to 126 inches.

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#### GENERAL INFORMATION.

Our product is almost exclusively steel, made by the Bessemer or Open Hearth process as required, and of all qualities from the softest rivet stock to high carbon special spring material.

Our Beams and Channels are made to conform to the American Standards, adopted January, 1896, in which the flanges have a uniform slope of one to six, and the dimensions, proportions and weights are determined by a regular schedule, as shown on the diagrams on pages 22 and 23. The standard proportions of beams and channels are further shown on Plate 24.

The principal structural angles now made are limited in number to conform to the American Standards, adopted December, 1895, and include twelve base, or a total of eighty-four, sizes for equal leg angles, and nine base, or a total of eighty-six, sizes of unequal leg angles, all varying in thickness by one-sixteenth inch, as shown on Plates 12 and 14 and tables herein. It is believed that these standard angles include a sufficient range of sizes to meet all usual structural requirements, but at the same time we will continue the manufacture of angles of special sizes and proportions for those who require them, as shown on Plates 13 and 15.

The weights of angles, Z-Bars and T-Bars now given, are those adopted as American Standards in July, 1902.

The method of increasing the sectional area of shapes from the minimum or base sizes to intermediate and maximum sizes, is shown on page 21. For beams and channels the increase from the minimum adds equally to the web thickness and flange width, the weight of the increase being equal to that of a plate of the same depth as the section, and of a thickness equal to the increase of the dimensions stated.

The method of increasing the thickness of angles and Z-Bars from

the minimum has the effect of adding to the length of the legs, as shown on page 21, so that for intermediate and maximum sizes the legs will be somewhat longer than the minimum or nominal dimensions, except in the cases for which we have finishing grooves. The plates of drawings of sections, pages 2 to 20 inclusive, show the minimum or base sizes of the various shapes. Sections shown on the plates or lists for which more than one weight is stated can be rolled of different thicknesses to produce the stated weights. Others for which only one weight is given cannot be varied. Each section shown herein is numbered, both in the plates and tables, for convenience in reference and ordering.

I-Beams and Channels should be ordered of weights shown in the tables.

Orders for angles and plates should specify either the thickness or weight, but not both.

All weights are stated in pounds per lineal foot of section, except in the table of rails on page 184 in which the weights are given in pounds per yard as customary. Weights of rolled sections are calculated on the basis of 489.6 pounds per cubic foot of steel, and 3.4 times the sectional area in square inches equals the weight in pounds per lineal foot. In calculating the weights, areas and properties of I-Beams, Channels, and structural angles for the lists and tables herewith, the fillets and smaller rounded corners were not considered.

Structural material, unless otherwise ordered, will be cut to length with variation not to exceed  $\frac{3}{8}$  inch more or less than that specified. For cutting to exact lengths or with less variation than  $\frac{3}{8}$  inch an extra price will be charged.

All sections shown herein are steel.

### OFFICES FOR SALE OF CAMBRIA STEEL CO.'S PRODUCTS.

GENERAL OFFICES, Arcade Building, Corner Fifteenth and Market Streets. (Connected by bridge with P. R. R. Terminal Station.)

NEW YORK ..... Empire Building, 71 Broadway.

CHICAGO ..........Western Union Building, Corner of Clark and Jackson Streets.

CINCINNATI .......Union Trust Building, Corner of Fourth and
Walnut Streets.

Boston ...... Mason Building, 70 Kilby Street.

St. Louis..........Chemical Building, Corner of Eighth and Olive
Streets.

TOLEDO ...........Nasby Building, Corner of Huron and Madison Streets.

PITTSBURG. ........Park Building, Corner of Fifth Avenue and Smithfield Street.

ATLANTA ...........Austell Building, 10 N. Forsyth Street.

SAN FRANCISCO.....17-23 Beale Street.

WORKS AT JOHNSTOWN, PA.

#### STRUCTURAL STEEL WORK.

Finished Steel Work for Buildings, including Beams, Girders, Columns, Roof Trusses, etc., fitted complete and ready for erection.

#### STEEL FREIGHT CARS.

Gondola, Hopper-Gondola, Hopper, Flat, etc.

#### STEEL RAILS.

Steel T-Rails, 8 lbs. to 100 lbs. per yard.
Angle and Plain Splice Bars.
Standard and Special Track Bolts and Nuts.
For detailed information, see T-Rail Catalogue.

#### STEEL AXLES.

Passenger Car, Freight Car, Tender Truck, Engine Truck, Driving, Street Car, Mine Car, etc.

#### CRANK PINS, PISTON RODS.

Crank Pins and Piston Rods made to any requirement.

#### FORGINGS.

Axles, Crank Pins, Piston Rods and Forgings will be furnished of carbon steel or nickel steel as required and are annealed, or treated by our Coffin toughening process (patented) as specified.

Particular attention is called to our Coffin Process of treatment for toughening Axles, Crank Pins, Piston Rods and other forgings.

Crank Pins and Piston Rods are oil-tempered and other small Forgings will be if desired.

See special list for description and specifications of our various classes of steel forgings.

#### GAUTIER DEPARTMENT

#### OF

#### CAMBRIA STEEL CO.

#### MERCHANT BAR STEEL,

Including Tire, Toe Calk, Machinery, Carriage Spring, Baby Carriage Spring, Railroad Spring, Hoe, Rake, Fork, Forging, Bolt, Rivet, etc.

#### AGRICULTURAL STEEL AND SHAPES,

Finger Bars, Knife Backs, Rake Teeth, Bundle Carrier Teeth, Tedder Forks and Springs, Spring Harrow Teeth, Harrow (Drag) Teeth, Seat Springs, etc.

#### PLOW STEEL,

Bars and Slabs (Penn and Pernot), Flat and Finished Plow Shapes, Digger Blades, Hammered Lay, Rolled Lay, etc.

#### COLD ROLLED STEEL,

Rounds, Squares, Flats, Shafting and Special Shapes.

#### STEEL DISCS WITH ROLLED BEVEL,

10" to 20" diameter for Harrows, Drills, Cultivators, etc. 23" to  $28\frac{1}{4}$ " diameter for Plows.

#### PRESSED STEEL SEATS FOR AGRICULTURAL IMPLEMENTS.

For Gautier Steel Department Products not listed herein, see special Catalogue, or address,

#### GAUTIER DEPARTMENT, Cambria Steel Company, Johnstown, Pa.

## **PLATES**

OF

STRUCTURAL STEEL SHAPES

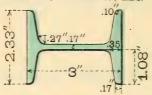
MANUFACTURED BY

CAMBRIA STEEL CO.

#### STANDARD BEAMS.

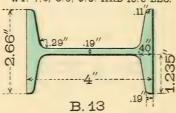
B. 5

WT. 5.5, 6.5 AND 7.5 LBS.

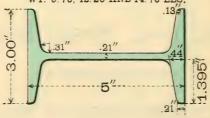


B. 9

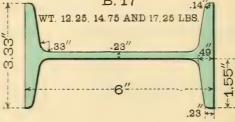
WT. 7.5, 8.5, 9.5. AND 10.5 LBS.

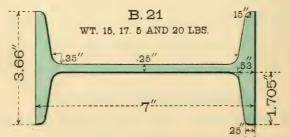


WT. 9.75, 12.25 AND 14.75 LBS.

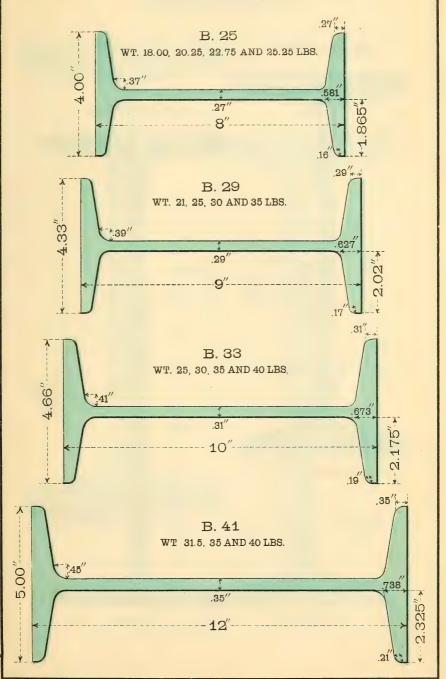


B. 17



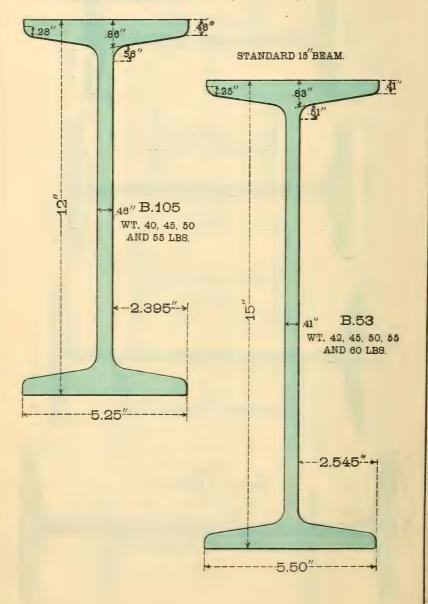


#### STANDARD BEAMS.

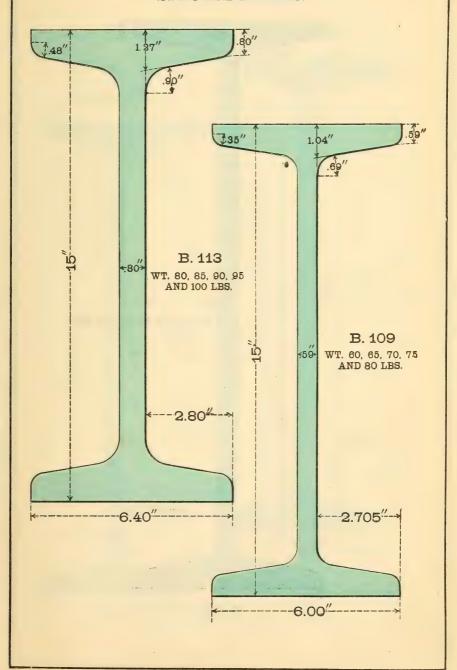


#### BEAMS.

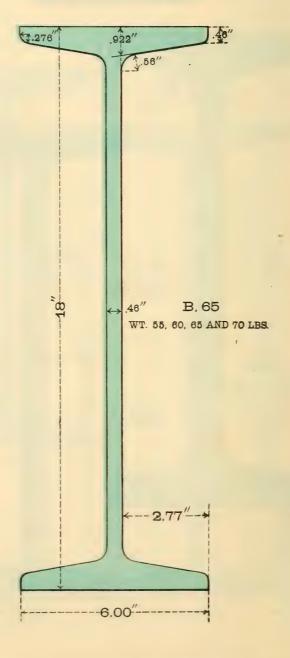
SPECIAL 12 BEAM.



#### SPECIAL BEAMS.

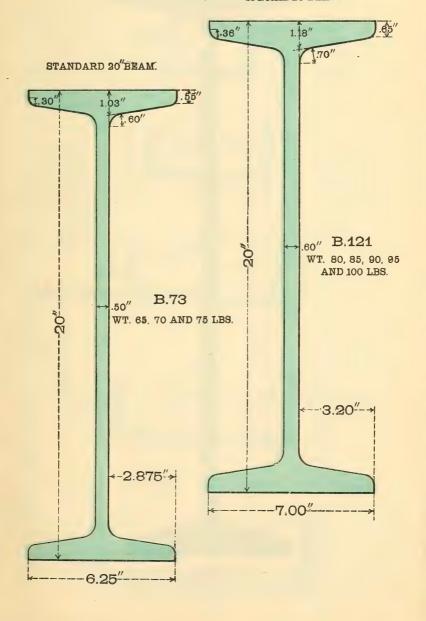


#### STANDARD BEAMS.

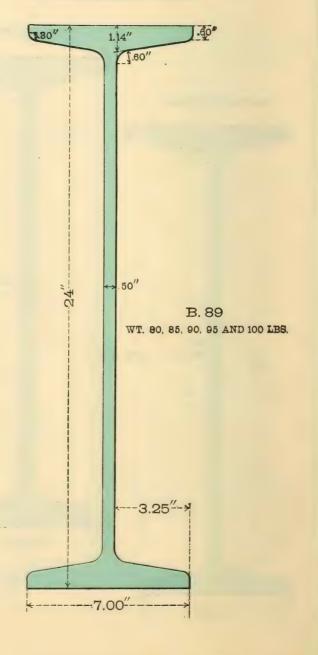


#### BEAMS.

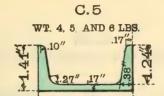
SPECIAL 20"BEAM.

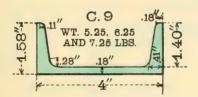


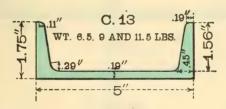
#### STANDARD BEAMS.

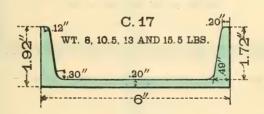


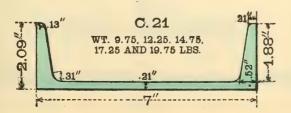
#### STANDARD CHANNELS.



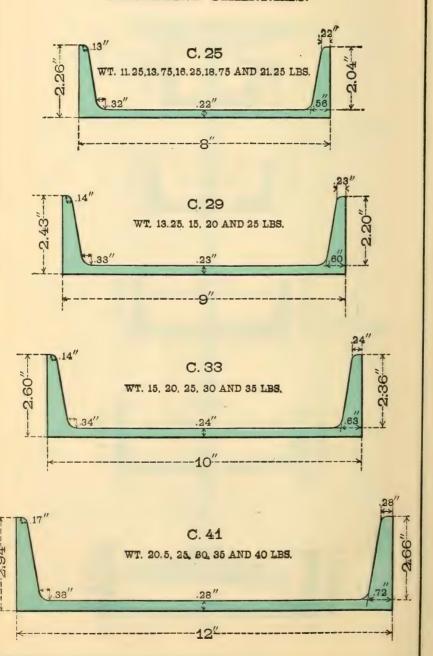




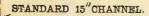


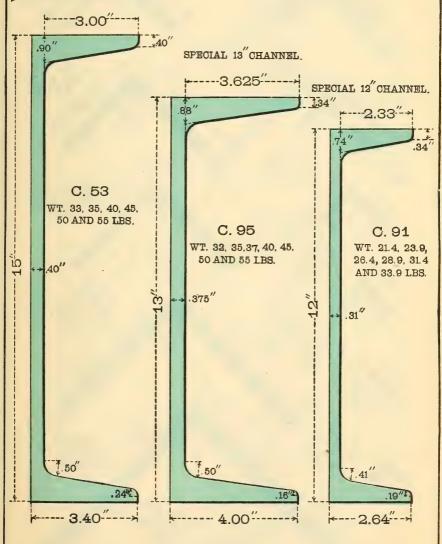


#### STANDARD CHANNELS.

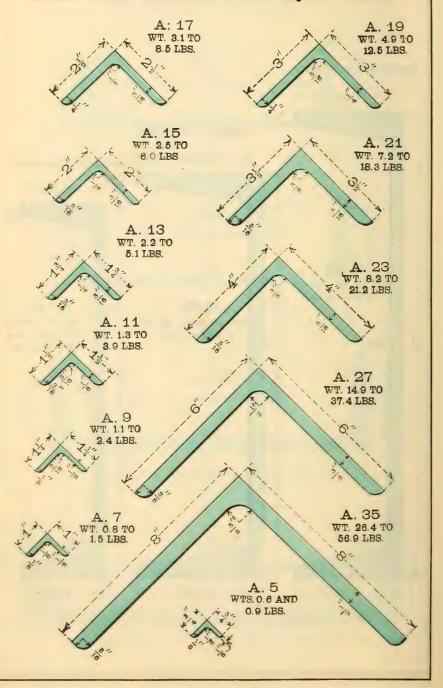


#### CHANNELS.

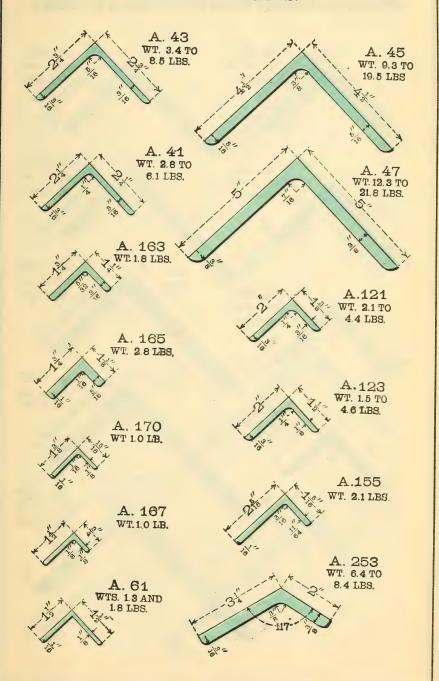




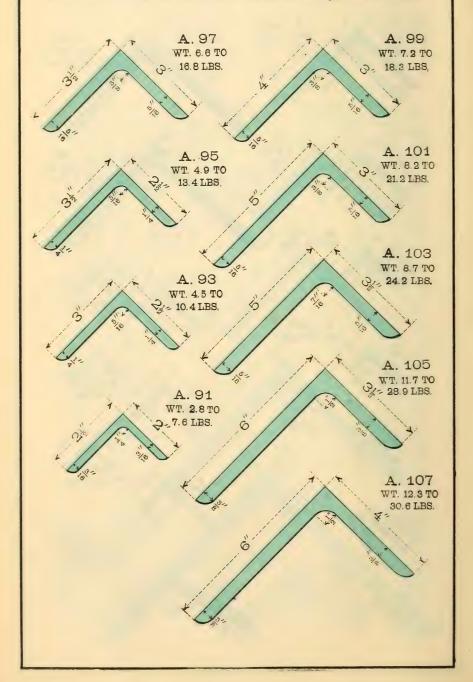
#### STANDARD ANGLES WITH EQUAL LEGS.



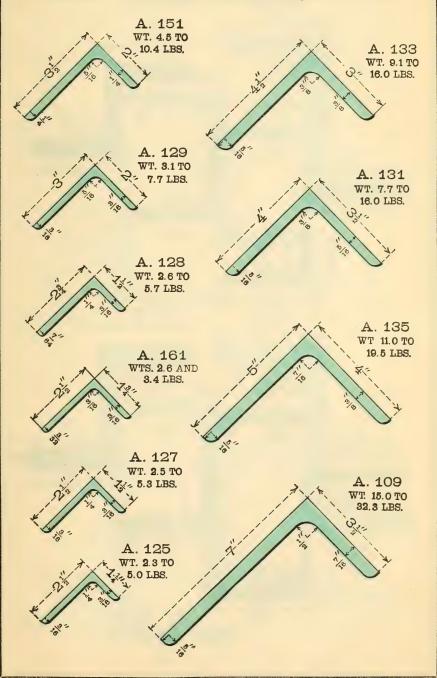
#### SPECIAL ANGLES.



#### STANDARD ANGLES WITH UNEQUAL LEGS.

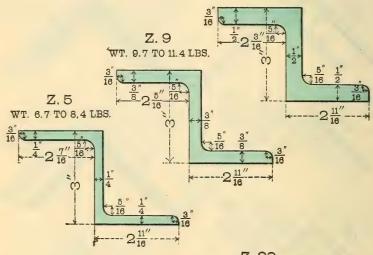


#### SPECIAL ANGLES WITH UNEQUAL LEGS.

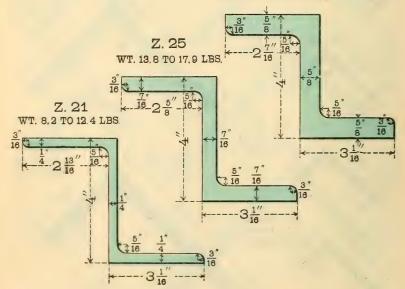


#### STANDARD Z-BARS.

Z. 13 WT. 12.5 TO 14.2 LBS.



Z. 29 WT. 18.9 TO 23.0 LBS.



# STANDARD Z-BARS. Z. 45

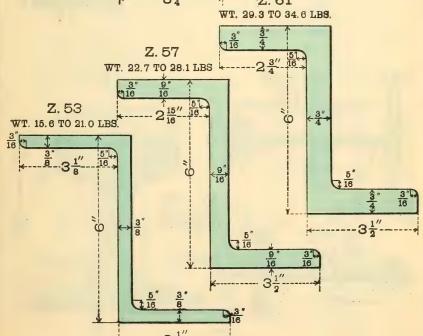
WT. 17.9 TO 22.6 LBS.

2. 41

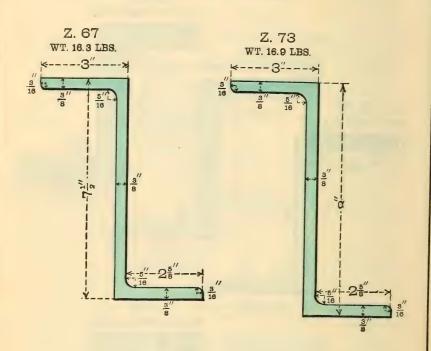
WT. 17.9 TO 22.6 LBS.

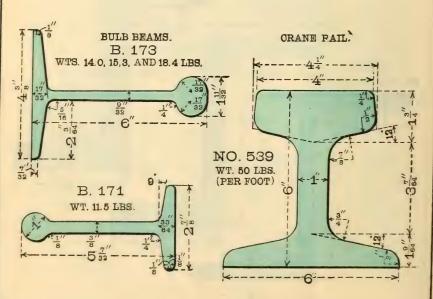
2.  $\frac{3''}{16}$ WT. 11.6 TO 16.4 LBS.

2.  $\frac{3''}{16}$ 2.  $\frac{3''}{16}$ 3.  $\frac{5''}{16}$ 2.  $\frac{11''}{16}$ 3.  $\frac{1}{16}$ 3.  $\frac{1}{16}$ 3.  $\frac{1}{16}$ 3.  $\frac{1}{16}$ 3.  $\frac{1}{16}$ 3.  $\frac{1}{16}$ 2. 61

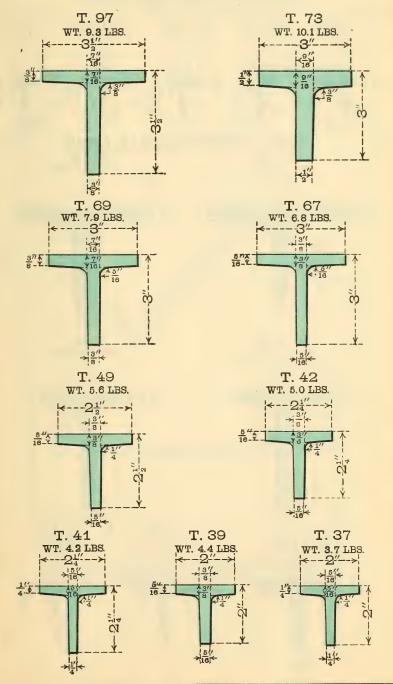


# SPECIAL Z-BARS.

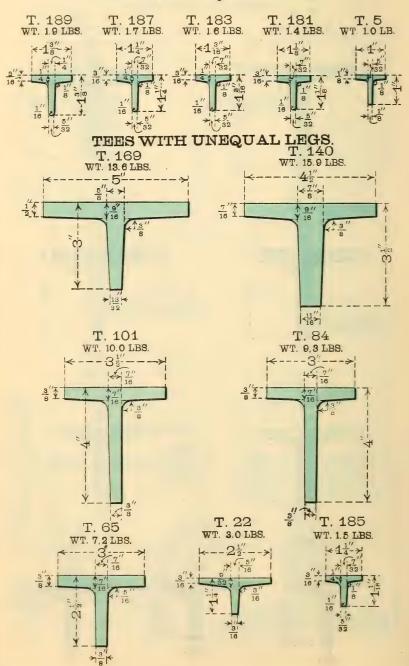




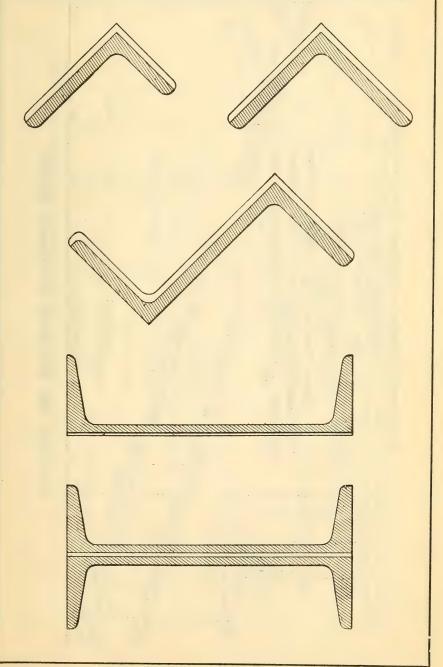
# TEES WITH EQUAL LEGS.



# TEES WITH EQUAL LEGS.



# METHOD OF INCREASING SECTIONAL AREAS.



# STANDARD BEAMS.

50

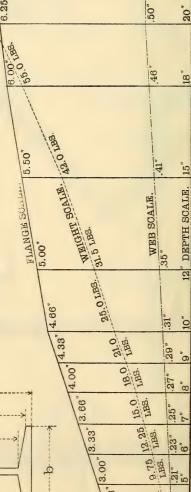
The following Formulas and Diagram relate to the Properties of I-Beams:

Weight per foot = Area  $\times$  3.4. Area = td + 2s (b-t) +  $\frac{(b-t)^2}{12}$ . Section Modulus = s =  $\frac{21}{d}$ .

Slope of Flange =  $g = \frac{h-l}{b-t} = \frac{3}{6}$  for Standard Beams.

I = M ement of Inertia, Neutral Axis (1-1) parallel to flange.  $I = \frac{1}{13} \left[ \text{ bd}^3 - \frac{1}{4g} \left( \text{hd-l4} \right) \right] \text{ or } \frac{\text{bd}^3}{12} - \frac{1}{3} \left( \text{hd-l4} \right) \text{ for Standard Beams.}$ 

7.00"



3.00"

# DIAGRAM FOR MINIMUM STANDARD BEAMS.

6.23

5,12

5.5 LB3

# STANDARD CHANNELS.

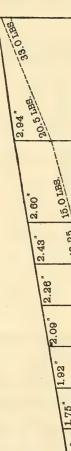
The following Formulas and Diagram relate to the Properties of Channels:

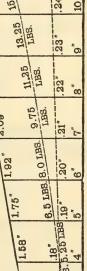
Weight per foot = Area  $\times 3.4$ . Area = td + 2s (b-t) +  $\frac{(b-t)^2}{6}$ 

Section Modulus =  $s = \frac{2I}{d}$ .

Slope of Flange =  $g = \frac{h-1}{2(b-t)}$ , or  $\frac{1}{6}$  for Standard Channels.

I = Moment of Inertia, Neutral Axis (1-1) parallel to flange.  $I = \frac{1}{12} \left[ bd^3 - \frac{1}{8g} \left( h^4 - l^4 \right) \right] \text{ or } \frac{bd^3}{12} - \frac{h^4 - l^4}{16} \text{ for Standard Channels.}$ 





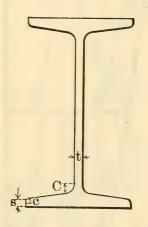
FLANGE SCALE [1.41"

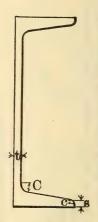
WEB SCALE
WEIGHT SCALE 7
DEPTH SCALE 3

40

# DIAGRAM FOR MINIMUM STANDARD CHANNELS.

### STANDARD BEAMS AND CHANNELS.





The following data are common to all I-Beams and Channels, with the exceptions stated:

 $c = \frac{6}{10}$  Minimum Web.

 $C = Minimum Web + \frac{1}{10} inch.$ 

s = Minimum Thickness of Web = t Minimum for all Channels and Beams, except 20" I and 24" I.

For  $20^{\prime\prime}$  Standard I s = .55 $^{\prime\prime}$  t Minimum = .50 $^{\prime\prime}$ .

For  $24^{\prime\prime}$  Standard I s =  $.60^{\prime\prime}$  t Minimum =  $.50^{\prime\prime}$ .

For  $20^{\prime\prime}$  Special I  $s = .65^{\prime\prime}$  t Minimum  $= .60^{\prime\prime}$ .

The Slope of Flange of all Beams and Channels is  $16\frac{2}{3}\%$ =  $9^{\circ} - 27' - 44'' = 2''$  per foot.

# TABLES OF BARS, BILLETS, BLOOMS, INGOTS AND PLATES.

# STEEL SQUARES.

All sizes from  $\frac{1}{4}$ " to  $3\frac{3}{8}$ " increasing by  $\frac{1}{16}$ ". All sizes from  $3\frac{1}{2}$ " to  $5\frac{1}{2}$ " increasing by  $\frac{1}{8}$ ".

### STEEL HAND ROUNDS.

All sizes from  $\frac{3}{8}$ " to  $3\frac{1}{8}$ " increasing by  $\frac{1}{16}$ " All sizes from  $3\frac{1}{4}$ " to  $7\frac{1}{8}$ " increasing by  $\frac{1}{8}$ "

### STEEL GUIDE ROUNDS.

All sizes from  $\frac{3}{16}$ " to 1" increasing by  $\frac{1}{64}$ " All sizes from 1" to  $1\frac{1}{2}$ " increasing by  $\frac{3}{32}$ " All sizes from  $1\frac{1}{2}$ " to 3" increasing by  $\frac{1}{16}$ "

### REGULAR FLATS.

WID	TH,	THICK	NESS.
Inches.	Increasing by Inches.	Inches.	Increasing by Inches.
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1 64 66 66 66 66 66 66 66 66 66 66 66 66	3 to 3 8 1 6 0 8 1 6 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 64 66 66 66 66 66

# THIN FLATS OR LIGHT BANDS.

½ to 6	1 16	No. 10 to No. 16 ga.	by gauges.

## EDGED PLATES.

357. 7/2						THICK	NESS 1	IN INC	HES.					
Width in Inches.	3 16	$\frac{1}{4}$	<del>5</del> <del>16</del>	<u>3</u>	7 16	$\frac{1}{2}$	$\frac{9}{16}$	<u>5</u>	$\frac{1}{1}\frac{1}{6}$	34	$\frac{13}{16}$	7/8	$\frac{1}{1}\frac{5}{6}$	1
Inonos.						LEN	GTH I	N FEE	T.					
4	50	50	50	50	50	50	40	40	30	30	30	28	28	28
5	30	42	42	42	42	40	30	30	30	30	30	30	30	30
6	30	42	42	42	42	40	35	30	30	30	30	30	30	30
7	25	42	42	42	42	40	35	30	30	30	30	30	30	30
8	25	42	42	42	42	42	38	36	32	30	29	28	26	25
9	25	42	42	42	42	42	38	34	32	30	29	28	26	25
10	25	42	42	42	42	42	38	33	32	30	29	28	26	25
11	25	42	42	42	42	42	38	33	31	29	28	27	25	24
12	25	42	42	42	42	42	37	32	30	28	27	26	24	23
13		42	42	42	42	42	37	32	30	27	25	24	22	20
14		42	42	42	42	40	35	30	28	26	25	23	22	20
$14\frac{1}{2}$		42	42	42	42	36	33	30	28	25				

Intermediate widths varying by  $\frac{1}{4}$ " can be furnished.

# STEEL BILLETS, BLOOMS AND SLABS.

WIDTH Inches.	THICKNESS Inches.	WIDTH Inches.	THICKNESS Inches.	WIDTH Inches.	THICKNESS Inches.
3	3	13	2 to 13	24	2 to 20
$3\frac{1}{2}$	$3\frac{1}{2}$	14	2 " 14	25	2 " 20
4	4	15	2 " 15	26	2 " 20
5	3½ to 5	16	2 " 16	27	2 " 20
6	2 " 6	17	2 " 17	28	2 " 20
7	2 " 7	18	2 " 18	35	3 " 15
8	2 " 8	19	2 " 19	36	3 " 15
9	2 " 9	20	2 " 20	37	3 " 15
10	2 " 10	21	2 " 20	48	5 " 15
11	2 " 11	22	2 " 20	49	5 " 15
12	2 " 12	23	2 " 20	50	5 " 15

Sections larger than 4" x 4" can be furnished in thicknesses vary-

ing by  $\frac{1}{2}$ ".

Billets, Blooms and Slabs, of sections given in above table, can be furnished within the following limits of length, provided the weight does not exceed the maximum given for the different sizes:

SECTION.	WIDTH.	SECTIONAL AREA.	LENGTHS. MINIMUM MAXIMUM	MAXIMUM WEIGHTS.
	Inches.	Sq. Ins.	Feet. Ins. Feet.	Pounds.
Billets and Slabs.	3 to 7	9 to 16	1 6 10	300 to 600
66 66 66	4 " 17	16 " 36	3 0 30	1600 " 3600
Blooms and Slabs.	6 " 28	36 and over	66 66 66	3600 " 20000
66 66	35 " 37	105 " "	66 66 66	11000 66 18000
"	48 " 50	240 " "	" " 27	22000

# STEEL BILLETS, SQUARE CORNERS.

 $1'' \times 1''$  to  $3\frac{1}{4}'' \times 3\frac{1}{4}''$  increasing by  $\frac{1}{16}''$ .

### STEEL INGOTS.

DIMENS		WEIG	нт				
BUTT.	TOP.	A DIG	HI.		GRADE.		
Inches	Inches.	Pound	is.				
22 x 19½	20 x 16	6000 to	7000	Open	Hearth	or	Bess.
$25 \times 20^{\circ}$	23 x 17	7700 "	8700	-66	66	66	6.6
27 x 22	23 x 18	8800 "	9800	66	66	66	66
29 x 25	$27\frac{1}{5} \times 22$	12000 "	13000	Open	Hearth.		
39 x 25	$37\frac{1}{2} \times 22$	17000 "	18000	6.6	66		
$52 \times 25\frac{1}{2}$	$50\frac{1}{2} \times 22\frac{1}{2}$	23000 "	24000	6.6	66		
$29\frac{1}{2} \times 29\frac{1}{2}$	28 x 28	21000 "	22000	66	66		
29 x 29	261 x 261	15000 "	16000	6.6	66		
0							
SPEC	IAL.	Ì					
15" to 36" squ	are or round.	7000 "	40000	66	66		
Maximum L							

# SHEARED PLATES.

				-		Ť	THICK	NESS	(N)	NCHI	ES.		the Young's	k private			
Width in	3 16																
Inches.						!	LEN	GTH I	IN IN	CHES			-		-		
4.5	240	990	400	500	500	EEO	500	AITE	AME	APE	105	400	חייור	260	200	ൈ	900
15 16 17	240	320	400 400 400	500	500	550	500	475	475	475	425	400	375	360	300	280	280
18 19	240	360	$\frac{400}{400}$	500	500	500	500	550	550	550	500	500	450	400	400	400	350
20 21			400 400														
22 23 24	216 204	$\begin{array}{c} 360 \\ 360 \end{array}$	400 400 400	500 500	525 525	525 525	525 525	550 550	550 550	550 550	$\begin{array}{c} 500 \\ 500 \end{array}$	$\begin{array}{c} 500 \\ 500 \end{array}$	$\frac{450}{450}$	$\frac{400}{400}$	$\begin{array}{c} 400 \\ 400 \end{array}$	$\frac{400}{400}$	350 350
25	204	360	400	500	525	550	550	550	550	550	500	475	425	400	350	350	325
26 27 28	168	340	$\frac{400}{400}$	500	500	550	550	500	500	500	450	450	400	380	330	300	300
29	156																
30 to 35 36 " 41 42 " 47		360	$\frac{400}{400}$	500	500	500	500	550	550	550	500	500	450	400	400	400	350
48 " 53 54 " 59		360	400 400	500	525	550	550	550	550	550	500	475	425	400	350	350	325
60 " 65 66 " 71		300	400 350	430	450	475	425	425	425	410	375	340	330	320	280	260	260
72 " 77 78 " 83 84 " 89		240	300 275 250	380	400	420	375	375	375	370	325	300	300	300	240	220	220
90 " 95		180	230	330	340	350	350	325	325	325	275	260	260	260	220	200	200
96 "101 102 "107 108 "113		120	175 150	200	230	230 200	250 220	250 225	250 225	250 225	230 220	230 220	210 200	$\frac{210}{200}$	190 180	170 160	170 160
114 "119 120 "125								210 150									
2100	1																

# WEIGHTS AND DIMENSIONS OF STANDARD I-BEAMS.

Section Number.	Depth of Beam. Inches.	Weight per Foot.  Pounds,	Area of Section.	Thickness of Web.	Width of Flange. Inches.	Page Number of Section,
B 5 "	3 "	5.5 6.5 7.5	1.63 1.91 2.21	.17 .26 .36	2.33 2.42 2.52	2 "
B 9 " "	4 "	7.5 8.5 9.5 10.5	2.21 2.50 2.79 3.09	.19 .26 .34 .41	2.66 2.73 2.81 2.88	2 "
B 13	5 "	9.75 12.25 14.75	2.87 3.60 4.34	.21 .36 .50	3.00 3.15 3.29	2 "
B 17	6 "	12.25 14.75 17.25	3.61 4.34 5.07	.23 .35 .47	3.33 3.45 3.57	2 "
B 21	7 "	15.0 17.5 20.0	4.42 5.15 5.88	.25 .35 .46	3.66 3.76 3.87	2 "
B 25	8 " " " "	18.0 20.25 22.75 25.25	5.33 5.96 6.69 7.43	.27 .35 .44 .53	4.00 4.08 4.17 4.26	3 "
B 29	9 " " "	21.0 25 0 30.0 35.0	6.31 7.35 8.82 10.29	.29 .41 .57 .73	4.33 4.45 4.61 4.77	3
B 33	10	25.0 30.0 35.0 40.0	7.37 8.82 10.29 11.76	.31 .45 .60 .75	4.66 4.80 4.95 5.10	3
B 41	12	31.5 35.0 40.0	9.26 10.29 11.76	.35 .44 .56	5.00 5.09 5.21	3
B 53	15	42.0 45.0 50.0 55.0 60.0	12.48 13.24 14.71 16.18 17.65	.41 .46 .56 .66 .75	5.50 5.55 5.65 5.75 5.84	4 66 66

# WEIGHTS AND DIMENSIONS OF STANDARD I-BEAMS.

Section	Depth	Weight per	Area of	Thickness	Width	Page
Number.	Beam.	Foot.	Section.	Web.	Flange.	Number of
Number,	Inches.	Pounds.	Sq. In.	Inches.	Inches.	Section.
B 65	18	55.0	15.93	.46	6.00	6
66	66	60.0	17.65	.56	6.10	16
66	66	65.0	19.12	.64	6.18	66
66	"	70.0	20.59	.72	6.26	66
B 73	20	65.0	19.08	.50	6.25	7
66	66	70.0	20.59	.58	6.33	66
66	66	75.0	22.06	.65	6.40	"
B 89	24	80.0	23.32	.50	7.00	8
"	66	85.0	25.00	.57	7.07	66
"	66	90.0	26.47	.63	7.13	66
66	66	95.0	27.94	.69	7.19	66
"	66	100.0	29.41	.75	7.25	"

# WEIGHTS AND DIMENSIONS OF SPECIAL I-BEAMS.

Section	Depth of Beam.	Weight per Foot.	Area of Section.	Thickness of Web.	Width of Flange.	Page Number of
Number.	Inches.	Pounds.	Sq. Inches.	Inches.	Inches.	Section.
B 105	12	40.0	11.84	.46	5.25	4
"	66	45.0	13.24	.58	5.37	66
66	66	50.0	14.71	.70	5.49	66
66	66	55.0	16.18	.82	5.61	66
B 109	15	60.0	17.67	.59	6.00	5
"	66	65.0	19.12	.69	6.10	"
66	66	70.0	20.59	.78	6.19	66
66	66	75.0	22.06	.88	6.29	66
66	66	80.0	23.53	.98	6.39	66
B 113	15	80.0	23.57	.80	6.40	5
46	66	85.0	25.00	.90	6.50	66
66	66	90.0	26.47	.99	6.59	"
"	66	95.0	27.94	1.09	6.69	66
"	66	100.0	29.41	1.19	6.79	"
B 121	20	80.0	23.73	.60	7.00	7
"	66	85.0	25.00	.66	7.06	"
66	66	90.0	26.47	.74	7.14	66
66	66	95.0	27.94	.81	7.21	66
66	66	100.0	29.41	.88	7.28	66

# WEIGHTS AND DIMENSIONS OF STANDARD CHANNELS.

2-11-	Depth	Weight	Area of	Thickness	Width	Page
Section	Channel.	per Foot.	Section.	Web.	Flange.	
Number.				-		Number of
	Inches.	Pounds,	Sq. In.	Inches.	Inches,	Section.
			•			
0 5	3	4.0	1.19	.17	1.41	9
"	"	5.0	1.47	.26	1.50	"
66	66	6.0	1.76	.36	1.60	66
0 9	4	5.25	1.55	.18	1.58	9
"	66	6.25	1.84	.25	1.65	"
66	66	7.25	2.13	.33	1.73	66
C 13	5	6.50	1.95	.19	1.75	9
"	66	9.00	2.65	.33	1.89	66
66	66	11.50	3.38	.48	2.04	66
0 17	6	8.00	2.38	.20	1.92	9
66	66	10.50	3.09	.32	2.04	"
66	66	13.00	3.82	.44	2.16	66
		15.50	4.56	.56	2.28	
0,21	7	9.75 12.25	2.85	.21	2.09 2.20	9
66	66	12.25	3.60 4.34	.52	2.30	66
"	66	17.25	5.07	.53	2.41	66
66	66	19.75	5.81	.63	2.51	66
C 25	8	11.25	3.35	.22	2.26	10
"	"	13.75	4.04	.31	2.35	66
66	66	16.25	4.78	.40	2.44	6.6
66	66	18.75	5.51	.49	2.53	66
66	"	21.25	6.25	.58	2.62	66
C 29	9	13.25	3.89	.23	2.43	10
"	66	15.00	4.41	.29	2.49	66
"	66	20.00 25.00	5.88 7.35	.45	2.65 2.81	66
	1	15.0		1	2.60	}
0.33	10	20.0	4.46 5.88	.24	2.74	10
"	66	25.0	7.35	.53	2.89	66
66	66	30.0	8.82	.68	3.04	66
66	66	35.0	10.29	.82	3.18	66
C 41	12	20.5	6.03	.28	2.94	10
"	66	25.0	7.35	.39	3.05	66
66	66	30.0	8.82	.51	3.17	66
"	66	35.0	10.29	.64	3.30	"
	1	40.0	11.76	.76	3.42	

# WEIGHTS AND DIMENSIONS OF STANDARD CHANNELS.

Section Number.	Depth of Channel.	Weight per Foot. Pounds.	Area of Section, Sq. Ins.	Thickness of Web.	Width of Flange.	Page Number of Section.
0.53	15	33 35 40 45 50 55	9.90 10.29 11.76 13.24 14.71 16.18	.40 .43 .52 .62 .72 .82	3.40 3.43 3.52 3.62 3.72 3.82	11

# WEIGHTS AND DIMENSIONS OF

# SPECIAL CHANNELS.

Section Number.	Depth of Channel.	Weight per Foot.	Area of Section.	Thickness of Web.	Width of Flange,	Thickness  of  Flange.	Increase in Web and Flange for each pound increase of Weight.	Page Number of Section.
	Inches.	Pounds.	Sq. Ins.	Inches.	Inches.	Inches.	Inches.	
C 91	12	21.4 23.9 26.4 28.9 31.4 33.9	6.30 7.03 7.77 8.50 9.24 9.97	.31 .37 .44 .50 .56	2.64 2.70 2.76 2.82 2.89 2.95	.34	.024	11
0,95	13	32 35	9.30 10.29	.38 .45	4.00 4.08	.34	.023	11
66	66	37	10.88	.50	4.12	66	66	66
66	66	40	11.76	.56	4.19	66	66	66
66	66	45	13.24	.68	4.30	66	"	66
66	66	50	14.71	.79	4.42	66	66	66
66	66	55	16.18	.90	4.53	66	66	66

# WEIGHTS AND DIMENSIONS OF STANDARD ANGLES.

# EQUAL LEGS.

Section Num- ber,	Dimensions.	Thick- ness.	Weight per Foot.	Area of Section.	Section Num- ber.	Dimensions.	Thick- ness.	Weight per Foot.	Area of Section,
	Inches	Inches.	Pounds	Sq. Ins.		Inches.	Inches.	Pounds,	Sq. Ins.
A 5	3 X 3 4 X 3 3 X 3	$\frac{\frac{1}{8}}{\frac{3}{16}}$	.6	.18	A 17	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3 87 16 12 9 16	5.9 6.8 7.7	1.74 2.00 2.25
A.7	1 x 1 1 x 1 1 x 1	$\frac{\frac{1}{8}}{\frac{3}{16}}$	.8 1.2 1.5	.24 .34 .44	" A 19	3 x 3		8.5 4.9	2.50
A 9 "	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c} \frac{1}{8} \\ \frac{3}{16} \\ \frac{1}{4} \\ \frac{5}{16} \end{array} $	1.1 1.5 2.0 2.4	.30 .44 .57 .69	ee ee ee	3 x 3 3 x 3 3 x 3 3 x 3 3 x 3 3 x 3	145 6 3 007 6 1040 15 00 1/6	6.1 7.2 8.3 9.4 10.4	1.78 2.11 2.44 2.75 3.06
A 11	1½ x 1½ x 1½ 1 x 1	103 T145 6 13007 T6	1.3 1.8 2.4	.36 .53 .69	"			11.5 12.5	3.36 3.66
66		16 16 28 7 16	2.9 3.4 3.9	.84 .99 1.13	A 21	3½ X	16 387 16	7.2 8.5 9.8 11.1	2.09 2.49 2.88 3.25
A 13	134 x 1343143143143143143143143143143143143143	3 14 5 16 13 18 7 16 12	2.2 2.8 3.4 4.0 4.6 5.1	.63 .82 1.00 1.18 1.34 1.50	(( (( ((	163 - 163 -		12.4 13.6 14.8 16.0 17.1 18.3	3.63 3.99 4.34 4.69 5.03 5.36
A 15	2 x 2 2 x 2 2 x 2 2 x 2 2 x 2 2 x 2 2 x 2	3 16 14 5 16 3 8 7 16 12	2.5 3.2 4.0 4.7 5.3 6.0	.72 .94 1.16 1.36 1.56 1.75	A 23	4 x 4 4 x 4 4 x 4 4 x 4 4 x 4 4 x 4 4 x 4	5 6 3 00 7 6 10 9 6 5 10 1 1 0 1 4 3 6 7 10 1 1 7 10	8.2 9.8 11.3 12.8 14.3 15.7 17.1	2.41 2.86 3.31 3.75 4.19 4.62 5.03
A 17	$\begin{array}{c} 2\frac{1}{2} \times 2\frac{1}{2} \\ 2\frac{1}{2} \times 2\frac{1}{2} \\ 2\frac{1}{2} \times 2\frac{1}{2} \end{array}$	3 16 4 5 16	3.1 4.1 5.0	.91 1.19 1.47	66	4 x 4 4 x 4 4 x 4	34 136 78	18.5 19.9 21.2	5.44 5.84 6.24

Standard Angles vary only by  $\frac{1}{16}$  inch. Sections shown on page 12.

# WEIGHTS AND DIMENSIONS OF STANDARD ANGLES.

### EQUAL LEGS.—CONTINUED.

Section Num- ber.	Dimensions.	Thick- ness,	Weight per Foot.	Area of Section.	Section Num- ber,	Dimensions.	Thick- ness.	Weight per Foot.	Area of Section.
	Inches.	Inches.	Pounds.	Sq. Ins.		Inches.	Inches.	Pounds.	Sq. Ins.
A 27 "" "" "" "" "" "" "" "" "" "" "" "" ""	6 x 6 6 x 6	3 887 16 15 6 15 8 1 1 16 15 15 15 15 15 15 15 15 15 15 15 15 15	14.9 17.2 19.6 21.9 24.2 26.5 28.7 31.0 35.3 37.4	4.36 5.06 5.75 6.44 7.11 7.78 8.44 9.09 9.74 10.38 11.00	A 35 "" "" "" "" "" "" "" "" "" "" "" "" ""	8 x 8 8 x 8	$\begin{array}{c} \frac{1}{2} \\ \frac{9}{1} \\ \frac{5}{6} \\ \frac{8}{11} \\ \frac{1}{16} \\ \frac{3}{4} \\ \frac{1}{17} \\ \frac{6}{6} \\ \frac{1}{18} \\ \end{array}$	26.4 29.6 32.7 35.8 38.9 42.0 45.0 45.0 54.0 56.9	7.75 8.69 9.61 10.53 11.44 12.34 13.24 14.13 15.00 15.88 16.74

Standard Angles vary only by  $\frac{1}{16}$  inch. Sections shown on page 12.

# WEIGHTS AND DIMENSIONS OF STANDARD ANGLES.

# UNEQUAL LEGS.

Section Num- ber.	Dimensions.  Inches.	Thick-ness.	Weight per Foot. Pounds.	Area of Section.	Section Num- ber.	Dimensions.  Inches.	Thick-ness.	Weight per Foot. Pounds.	Area of Section.
A 91 "" " " " " A 93 "" " "	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	$\frac{3}{1}\frac{6}{1}\frac{1}{4}\frac{4}{5}\frac{5}{1}\frac{6}{3}\frac{9}{100}\frac{7}{1}\frac{6}{100}\frac{1}{29}\frac{9}{10}\frac{1}{100$	2.8 3.7 4.5 5.3 6.1 6.8 7.6 4.5 5.6 6.6 7.6 8.5	.81 1.07 1.31 1.55 1.78 2.00 2.22 1.32 1.63 1.93 2.22 2.50	A 93  A 95  ""  ""  ""  ""  ""	22 1/22 1/22 1/22 1/22 1/22 1/22 1/22 1	9-10-500 14-5-10-500-7-10-10-9-10-500-1-10-514	9.5 10.4 4.9 6.1 7.2 8.3 9.4 10.4 11.5 12.5 13.4	2.78 3.05 1.44 1.78 2.11 2.44 2.75 3.06 3.36 3.66 3.94

Standard Angles vary only by  $\frac{1}{16}$  inch. Sections shown on page 14.

# WEIGHTS AND DIMENSIONS OF STANDARD ANGLES.

# UNEQUAL LEGS.—CONTINUED.

Section Num- ber.	Dimensions.	Thick- ness.	Weight per Foot.	Area of Section.	Section Num- ber.	Dimensions.	Thick- ness.	Weight per Foot. Pounds.	Area of Section.
A 97	30 1 2 X 30 30 30 1 2 X 30 30 30 1 2 X 30 30 30 30 30 30 30 30 30 30 30 30 30	5 0 3 0 - 0 10 10 10 10 10 10 10 10 10 10 10 10 1	6.6 7.9 9.1 10.2 11.4 12.5 13.6 14.7 15.8 16.8	1.94 2.30 2.66 3.00 3.34 3.68 4.00 4.32 4.63 4.93	A103	CO C	$\frac{5}{ 1 } \frac{ 0 }{ 2 } \frac{2}{ 1 } \frac{2}{ 1 } \frac{ 0 }{ 1 $	8.7 10.4 12.0 13.6 15.2 16.8 18.3 19.8 21.3 22.7 24.2	2.56 3.05 3.53 4.00 4.47 4.93 5.38 5.82 6.25 6.68 7.09
A 99	4 x 3 4 x 3	5 10 3 18 7 10 12 29 10 5 10 11 10 20 4 3 10 7 10	7.2 8.5 9.8 11.1 12.4 13.6 14.8 16.0 17.1 18.3	2.09 2.49 2.88 3.25 3.63 3.99 4.34 4.69 5.03 5.36	A105	6 x 30 30 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1	03/001-10-1000 10-04/00 1-10-01-4-01-0-100-10-10-10-10-10-10-10-10-10-10-	11.7 13.5 15.3 17.1 18.9 20.6 22.4 24.0 25.7 27.3 28.9	3.43 3.97 4.50 5.03 5.55 6.06 6.57 7.06 7.55 8.03 8.50
A101	5 x 3 5 x 3	5 6 3 8 7 6 4 9 5 6 5 8 1 1 5 8 4 3 6 7 8 1 7 8	8.2 9.8 11.3 12.8 14.3 15.7 17.1 18.5 19.9 21.2	2.41 2.86 3.31 3.75 4.19 4.61 5.03 5.44 5.84 6.24	A107 "" "" "" "" "" "" "" "" "" "" "" "" ""	6 x 4 6 x 4	308710910381109143107056	12.3 14.3 16.2 18.1 20.0 21.8 23.6 25.4 27.2 28.9 30.6	3.61 4.19 4.75 5.31 5.86 6.41 6.94 7.47 7.99 8.50 9.00

Standard Angles vary only by  $\frac{1}{16}$  inch. Sections shown on page 14.

# WEIGHTS AND DIMENSIONS OF SPECIAL ANGLES.

# EQUAL LEGS.

Section Num- ber.	Dimensions. Inches.	Thick-ness. Inches.	Weight per Foot. Pounds.	Area of Section.	Section Num- ber.	Dimensions.	Thick-ness.	Weight per Foot. Pounds.	Area of Section.
A 41 "	2 1 x 2 1 4 1 x 2 2 1 4 x 2 2 2 1 4 x 2 2 2 1 4 x 2 2 2 2 2 1 4 x 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	3 6 14 5 6 13 87 6	2.8 3.7 4.5 5.3 6.1	.81 1.07 1.31 1.55 1.78	A 45	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	5 0 3007 0 1000 0 1000 100	9.3 11.0 12.8 14.5 16.2 17.8 19.5	2.72 3.24 3.75 4.25 4.75 5.24 5.72
A 43	\$\frac{\pi_{40}}{2\cdot \pi_{40}} \rightarrow \pi_{40} \rightarrow \pi_{	3 6 145 6 3 0 7 6 1 2	3.4 4.5 5.6 6.6 7.6 8.5	1.00 1.32 1.63 1.93 2.22 2.50	A 47	5 x 5 5 x 5 5 x 5 5 x 5 5 x 5 5 x 5	3 007 6 1-29 6 1-5 811 6	12.3 14.3 16.2 18.1 20.0 21.8	3.61 4.19 4.75 5.31 5.86 6.41

Sections shown on page 13.

# WEIGHTS AND DIMENSIONS OF SPECIAL ANGLES.

# UNEQUAL LEGS.

Section Num- ber.	Dimensions, Inches,	Thick-ness.	Weight per Foot.	Area of Section.	Section Num- ber.	Dimensions, Inches,	Thick-ness.	Weight per Foot. Pounds.	Area of Section.
A170 A167 A165 A163	1\frac{3}{8} \times \frac{15}{16}  1\frac{1}{2} \times \frac{3}{4}  1\frac{3}{4} \times 1\frac{1}{8}  1\frac{3}{4} \times 1\frac{1}{4}	18 18 16	1.0 1.0 2.8 1.8	.28 .27 .81	A129	3 x 2 3 x 2 3 x 2 3 x 2 3 x 2 3 x 2 3 x 2	3 1 4 5 6 1 3 8 7 6 1 2	3.1 4.1 5.0 5.9 6.8 7.7	.91 1.19 1.47 1.74 2.00 2.25
A121	2 x 1500000000000000000000000000000000000	$ \begin{array}{c} 16 \\ 3 \\ 16 \\ \frac{1}{4} \\ 5 \\ 16 \\ 38 \\ 7 \\ 16 \end{array} $	2.1 2.7 3.3 3.9 4.4	.60 .79 .96 1.13 1.29	A151	3½ x 2 3½ x 2 3½ x 2 3½ x 2 3½ x 2 3½ x 2	1456300766 1300776	4.5 5.6 6.6 7.6 8.5	1.32 1.63 1.93 2.22 2.50
A123 "" "" "" ""	2 x 1½ 2 x 1½	1836 1456 1387 16	1.5 2.2 2.8 3.4 4.0 4.6	.43 .63 .82 1.00 1.18 1.34	"." A 131	$\begin{array}{cccccccccccccccccccccccccccccccccccc$		9.5 10.4 7.7 9.1	2.78 3.05 2.25 2.68
A125	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c} 3 \\ \hline{16} \\ 4 \\ 5 \\ \hline{16} \\ 3 \\ 8 \\ 7 \\ \hline{16} \end{array} $	2.3 3.0 3.7 4.4 5.0	.67 .88 1.08 1.27 1.45	66 66 66 66	4 x 3 <sup>1</sup> / <sub>2</sub>	5 6 6 3 8 7 6 1 2 9 7 5 8 1 6 1 6	10.6 11.9 13.3 14.7 16.0	3.09 3.50 3.91 4.30 4.69
A127	$\begin{array}{c} 2\frac{1}{2} \times 1\frac{1}{2} \\ 2\frac{1}{2} \times 1\frac{1}{2} \end{array}$	$\begin{array}{c} \frac{3}{16} \\ \frac{1}{4} \\ \frac{5}{16} \\ \frac{3}{8} \\ 7 \\ 16 \end{array}$	2.5 3.2 4.0 4.7 5.3	.72 .94 1.16 1.36 1.56	A133	$\begin{array}{c} 4\frac{1}{2} \times 3 \\ 4\frac{1}{2} \times 3 \end{array}$	387 16 29 16 8 11 16 8 11 16	9.1 10.6 11.9 13.3 14.7 16.0	2.68 3.09 3.50 3.91 4.30 4.69
A161  A128  ""  ""  ""	2 1 x 1 3 4 3 4 3 4 2 2 2 x 1 4 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 2 3 4 x 1 1 2 1 2 1 2 2 3 4 x 1 1 2 1 2 2 3 4 x 1 1 2 3 4 x 1 1 2	3 16 14 3 16 14 5 16 3 87 16	2.6 3.4 2.6 3.4 4.2 5.0 5.7	.77 1.00 .77 1.00 1.24 1.46 1.67	A135 " " " " "	5 x 4 5 x 4 5 x 4 5 x 4 5 x 4	3 867   16   16   15 8   11 6	11.0 12.8 14.5 16.2 17.8 19.5	3.24 3.75 4.25 4.75 5.24 5.72

Sections shown on pages 13 and 15.

# WEIGHTS AND DIMENSIONS OF SPECIAL ANGLES.

# UNEQUAL LEGS.—CONTINUED.

Section Num-	Dimensions.	Thick- ness.	Weight per Foot.	Area of Section.	Section Num-	Dimensions.	Thick- ness.	Weight per Foot,	Area of Section.
ber.	Inches.	Inches.	Pounds.	Sq. Ins.	ber.	Inches.	Inches.	Pounds.	Sq. Ins.
A109 " " " "	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 7 \\ 1 \\ 6 \\ 2 \\ 9 \\ \hline 1 \\ 6 \\ \underline{5} \\ 8 \\ \underline{1} \\ \underline{1} \\ 6 \\ \end{array}$	15.0 17.0 19.1 21.0 23.0	4.41 5.00 5.59 6.18 6.75	A109	7 x 3 <sup>1</sup> / <sub>2</sub> 2 <sup>1</sup> / <sub>2</sub> 2 7 x 3 <sup>1</sup> / <sub>2</sub> 2	34 136 78 155 116 1	24.9 26.8 28.7 30.5 32.3	7.32 7.88 8.43 8.97 9.50

Sections shown on page 15.

# WEIGHTS AND DIMENSIONS OF ODD ANGLES.

Section Num- ber.	 ensions.	Thick-ness. Inches.	Weight per Foot. Pounds.	of Section.	Section Num- ber.	Dimensions.  Inches.	Thick-ness.	Weight per Foot. Pounds.	Area of Section.
	$\begin{array}{c} x  1\frac{1}{2} \\ x  1\frac{1}{2} \end{array}$	$\frac{\frac{1}{8}}{\frac{3}{16}}$	1.3 1.8 2.1	.36 .53	A253 "	3½ x 2 3½ x 2 3½ x 2	$\frac{\frac{3}{8}}{\frac{7}{16}}$	6.4 7.4 8.4	1.88 2.18 2.47

Sections shown on page 13.

# WEIGHTS AND DIMENSIONS OF BULB BEAMS.

Section Number.	Depth of Beam.  Inches.	Weight per Foot. Pounds.	Area of Section. Sq. Ins.	Thickness of Web.	Width of Flange. Inches.	Diameter of Head.  Inches.	Page Number of Section.
B 171 B 173 "	$\begin{bmatrix} 5\frac{7}{32} \\ 6 \\ 6 \\ 6 \end{bmatrix}$	11.5 14.0 15.3 18.4	3.37 4.11 4.48 5.42	300000000000000000000000000000000000000	$\begin{array}{c} 2\frac{7}{8} \\ 4\frac{3}{8} \\ 4\frac{7}{16} \\ 4\frac{1}{3}\frac{9}{2} \end{array}$	1	18 18 18 18

## WEIGHTS AND DIMENSIONS OF

# REGULAR T-BARS.

# EQUAL LEGS.

Section Number.	Width of Flange.	Depth of Bar.	Thickness of Flange, Inches.	Thickness of Stem.	Weight per Foot. Pounds.	Area of Section. Sq. Ins.	Page Number of Section.
T 5 T 181 T 183 T 187 T 189 T 37 T 39 T 41 T 42 T 49 T 67 T 69 T 73 T 97	1 1 1 1 1 2 2 2 2 2 2 2 2 3 3 3 3 3 3 3	1 1100 100 1100 1100 1100 1100 1100 11	10	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1.0 1.4 1.6 1.7 1.9 3.7 4.4 4.2 5.0 5.6 6.8 7.9 10.1 9.3	.27 .41 .45 .48 .55 1.07 1.28 1.21 1.46 1.63 1.99 2.31 2.96 2.74	20 20 20 20 20 20 19 19 19 19 19 19 19

# WEIGHTS AND DIMENSIONS OF

# REGULAR T-BARS. UNEQUAL LEGS.

Section Number.	Width of Flange.	Depth of Bar.	Thickness of Flange.	Thickness of Stem.	Weight per Foot.	Area of Section.	Page Number of
	Inches.	Inches.	Inches.	Inches.	Pounds.	Sq. Ins.	Section.
T 185 T 22 T 65 T 84 T 101 T 140 T 169	144162 20 3 3	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	5 to 7 2 8 5 5 6 7 7 8 5 6 7 7 8 5 6 7 7 8 5 6 7 7 8 6 7 7 8 6 7 7 8 6 7 7 8 6 7 7 8 6 7 7 8 6 7 7 8 6 7 7 8 6 7 7 8 6 7 7 8 6 7 7 8 6 7 7 8 6 7 7 8 6 7 8 7 8	1.5 3.0 7.2 9.3 10.0 15.9 13.6	.44 .86 2.11 2.74 2.94 4.65 3.99	20 20 20 20 20 20 20 20 20

# WEIGHTS AND DIMENSIONS OF

### Z-BARS.

Section Number,	Depth of Bar. Inches.	Length of Legs.	Thickness of Web and Legs. Inches.	Weight per Foot.	Area of Section.	Page Number of Section.
Z, 5	3 3 1 6	211 213 234	1 4 5 1 6	Pounds. 6.7 8.4	Sq. In. 1.97 2.48	16
Z 9	3 3 1 6	$2\frac{1}{16}$ $2\frac{3}{4}$	3 8 7 16	9.7 11.4	2.86 3.36	16
Z 13	3 3 1 1 6	$2\frac{1}{1}\frac{1}{6}$ $2\frac{3}{4}$	10 12 9 16	12.5 14.2	3.69 4.18	16
Z 21	$\begin{array}{c} 4 \\ 4 \\ 4 \\ \frac{1}{16} \\ 4 \\ \frac{1}{8} \end{array}$	$egin{array}{cccccccccccccccccccccccccccccccccccc$		8.2 10.3 12.4	2.41 3.03 3.66	16
Z 25 "	$\begin{array}{c} 4 \\ 4 \\ \frac{1}{16} \\ 4 \\ \frac{1}{8} \end{array}$	$egin{array}{c} {f 3}_{ar{1}ar{6}} \\ {f 3}_{ar{8}}^{\ 1} \\ {f 3}_{ar{1}ar{6}}^{\ 3} \end{array}$	1 45 6 3 8 17 6 1 22 9 6	13.8 15.8 17.9	4.05 4.66 5.27	16
Z 29 · "	4 4 1 1 6 4 1 8	$egin{array}{cccccccccccccccccccccccccccccccccccc$	58 116 34	18.9 20.9 23.0	5.55 6.14 6.75	16
Z 37 "	5 5 \frac{1}{16} 5 \frac{1}{8}	3 <u>1</u> 4 3 <u>1</u> 5 6 3 <u>3</u> 8	5 16 3 8 7 16	11.6 13.9 16.4	3.40 4.10 4.81	17
Z 41	5 5 1 6 5 1 8	3 <u>1</u> 4 3 5 6 3 8	1/2 9 1/6 5/8	17.9 20.2 22.6	5.25 5.94 6.64	17
Z 45 "	5 5 \frac{1}{16} 5 \frac{1}{8}	3 1/4 5 1/6 3 8	116 34 13 16	23.7 26.0 28.3	6.96 7.64 8.33	17
Z 53 "	6 6 1 6 6 1 8	3 ½ 9 9 1 6 3 5 8	38 7 16 12	15.6 18.3 21.0	4.59 5.39 6.19	17
Z 57	$\begin{array}{c} 6 \\ 6\frac{1}{1.6} \\ 6\frac{1}{8} \end{array}$	3 1 2 9 5 1 6 5 8	9 16 5 8 11 16	22.7 25.4 28.1	6.68 7.46 8.25	17
Z 61	6 6 1 1 6 6 8	$egin{array}{c} {\bf 3} & {1\over 2} \\ {\bf 3} & {1\over 16} \\ {\bf 3} & {5\over 8} \\ \end{array}$	34 136 7	29.3 31.9 34.6	8.63 9.39 10.17	17
Z 67	7 1/2	3	x 23)00	16.3	4.78	18
Z 73	8	3	38	16.9	4.97	18

# STANDARD CONNECTION ANGLES FOR I-BEAMS AND CHANNELS.

Standard angle connections for all sizes of beams and channels are shown on page 43. These are of sufficient strength for all usual connections of the various sizes shown, figured on the basis of 10 000 pounds per square inch, as the allowable unit stress for single shear of rivets or bolts, and 20 000 pounds per square inch as the allowable unit stress for double shear and bearing value of the parts connected by the rivets.

When beams of very short spans are loaded to their full capacity, the end shear or reaction which has to be transmitted through the connections becomes so great that stronger connections than the stand-

ard should be used.

The following tables give the limits of length below which the standard connections do not apply and for which special designs should be made. For all lengths greater than those given in the tables the standard connections are sufficiently strong.

# MINIMUM SPANS OF STANDARD CHANNELS FOR WHICH STANDARD CONNECTION ANGLES MAY BE SAFELY USED WITH CHANNELS UNIFORMLY LOADED TO THEIR FULL CAPACITY, IN ACCORDANCE WITH TABLES OF SAFE LOADS, FOR FIBER STRESS OF 16 000 LBS. PER SQUARE INCH.

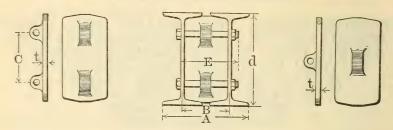
Section Number	Depth of Chan- nel.	Weight per Foot.	Mini- mum Safe Span.	Section Number	Depth of Chan- nel.	Weight per Foot.	Mini- mum Safe Span.	Section Number	Depth of Chan- nel.	Weight per Foot.	Mini- mum Safe Span.
	Inches.	Pounds.	Feet.		Inches.	Pounds.	Feet.		Inches.	Pounds.	Feet.
0,5	3	4.0 5.0	1.1	0.21	7,	12.25 14.75	2.6 2.3	0,33	10	25.0 30.0	5.5 6.2
66	66	6.0	0.8	66	66	17.25 19.75	2.6	66	66	35.0	7.0
0 9	4	5.25 6.25	1.9 1.5	C 25	8	11.25		C 41	12	20.5	5.4
"	"	7.25	1.4	66	66	13.75	3.4	66	66	25.0	4.8
C 13	5	6.5	2.8	66	66	16.25 18.75	3.0	66	66	30.0	5.4 6.0
66	66	9.0 11.5	2.1 2.5	66	66	21.25	3.6	66	66	40.0	6.6
				C 29	9	13.25	5.4	~ ~ ~		22.0	
0.17	6	8.0	3.9	46	66	15.00 20.00	4.6	0.53	15	33.0 35.0	7.4 7.1
66	66	13.0	3.5	44	66	25.00	4.7	66	66	40.0	7.0 7.5
		15.5	3.9	C 33	10	15.0	6.6	66	66	50.0	8.1
0 21	7	9.75	3.4	66	66	20.0	4.9	66	66	55.0	8.7

MINIMUM SPANS OF I-BEAMS FOR WHICH STANDARD CONNECTION ANGLES MAY BE SAFELY USED WITH I-BEAMS UNIFORMLY LOADED TO THEIR FULL CAPACITY, IN ACCORDANCE WITH TABLES OF SAFE LOADS, FOR FIBER STRESS OF 16 000 LBS.

PER SQUARE INCH.

Section Number	Depth of Beam.	Weight per Foot.	Mini- mum Safe Span.	Section Number	Depth of Beam.	Weight per Foot.	Mini- mum Safe Span.	Section Number	Depth of Beam.	Weight per Foot.	Mini- mum Safe Span.
	Inches.	Pounds.	Feet.		Inches.	Pounds.	Feet.		Inches.	Pounds.	Feet.
B 5 "	3	5.5 6.5 7.5	1.7 1.2 1.2	B29	9 "	30.0 35.0	6.8 7.5	B113	15 "	80.0 85.0 90.0	15.9 16.4 17.0
В 9	4	7.5	2.8	B33	10	25.0 30.0	9.3 8.1	"	66	95.0 100.0	17.5 18.1
и В Э	"	8.5	2.2	66	66	35.0	8,8			100.0	10.1
"	"	9.5 10.5	2.0 2.2	"	66	40.0	9.6	B65	18	55.0 60.0	13.7 11.9
		0 701		B41	12	31.5	7.3	"	66	65.0	11.8
B13	5 "	9.75	4.1	"	66	35.0	7.7	66	66	70.0	12.4
"	66	12.25 14.75	3.3 3.7	, i		40.0	8.2	B73	20	65.0	13.9
		14.(0	0.1	B105	12	40.0	9.0	" D(0	66	70.0	12.5
B17	6	12.25	5.6	"	"	45.0	9.6	66	66	75.0	12.8
66	66	14.75	4.8	66	66	50.0	10.2				
66	66	17.25	5.3	66	66	55.0	10.8	B121	20	80.0	14.8
704	194	45.00		Dro	4 2	40.0	400	"	66	85.0	15.2
B21	7 "	15.00	4.9	B53	15	42.0	10.2	"	66	90.0	15.7
66	66	17.50 20.00	3.8 3.6	"	66	45.0 50.0	9.4 9.7	"	66	95.0 100.0	16.2 16.7
		20.00	5.0	"	66	55.0	10.3			100.0	10.7
B25	8	18.00	6.2	66	66	60.0	10.8	B89	24	80.0	17.7
"	"	20.25	5.1			00.0	20,0	"	"	85.0	16.1
66	66	22.75	4.8	B109	15	60.0	12.3	"	66	90.0	16.1
46	66	25.25	5.1	46	66	65.0	12.8	66	66	95.0	16.6
				"	66	70.0	13.4	"	6.	100.0	17.1
B29	9	21.0	7.7	46	66	75.0	13.9				
	66	25.0	6.2	"	) "	80.0	14.5	1			

## CAST IRON SEPARATORS FOR I-BEAMS.



		Beams	,	,		Separato	Bolts, Square Heads and Hex Nuts.					
Section Number	Depth.	Weight per Foot.	Out to Out of Flanges of Beams.	Center to Cen- ter of Beams.	Thickness.	Weight.	Increase of Weight for each inch additional spread of Beams.	Diameter.	Center to Cen-	Ea Length.	Weight of Bolts and Nuts.	Increase of Weight of Bolts for each in addi- tional spread of Beams
	In.	Pounds.	Inches.	Inches.	In.	Pounds.	Pounds.	In.	In.	In.	Pounds.	Pounds

# SEPARATORS WITH ONE BOLT.

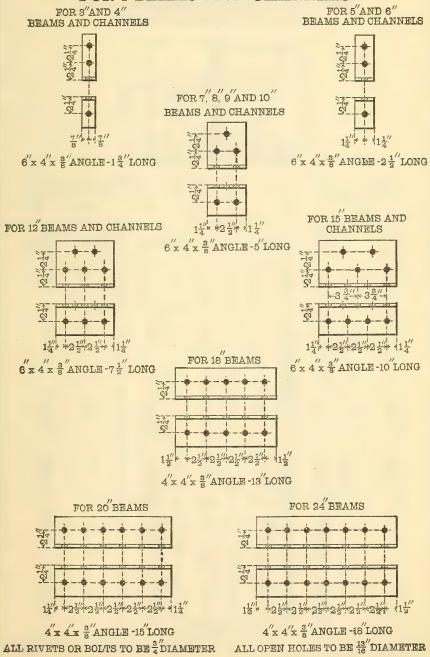
B 5	3	5.5	$5\frac{5}{1.6}$	3	3000	1.1	.29	50	$ 3\frac{7}{8} $	.94	.085
B 9	4	7.5	5 7 8	$3\frac{1}{4}$	60	1.6	.38	50034	41/4	.98	.123
B 13	5	9.75	$6\frac{1}{2}$	$3\frac{1}{2}$	66	2.0	.49	76	41/2	1.01	66
B 17	6	12.25	$\begin{array}{c c} 6\frac{1}{2} \\ 7\frac{5}{16} \end{array}$	4	$\frac{1}{2}$	3.3	.78	6.6	5	1.07	66
B 21	7	15.0	7 7 8	$4\frac{1}{4}$	เีย	3.9	.92	66	51	1.10	66
B 25	8	18.0	8 1/2	$4\frac{1}{2}$	66	4.7	1.06	66	$5\frac{1}{4}$ $5\frac{1}{8}$	1.15	66
B 29	9	21.0	$\frac{8\frac{1}{2}}{9\frac{5}{1.6}}$	5	66	5.9	1.20	66	61	1.21	66
B 33	10	25.0	97		66	6.8	1.33	66	66 667 67 67 67 67 67 67 67 67 67 67 67	1.24	66
B 41	12	31.5	$\frac{9\frac{7}{9}}{10\frac{3}{4}}$	$5\frac{1}{4}$ $5\frac{3}{4}$	66	8.8	1.61	66	$6\frac{9}{5}$	1.30	66
B105	12	40.0	11 4	6	66	8.9	1.58	66	$ 7\frac{1}{4} $	1.35	66

# SEPARATORS WTH TWO BOLTS.

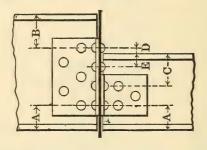
***************************************												
B 41	12	31.5	$10\frac{3}{4}$	$5\frac{3}{4}$	10	9.5	1.61	34	$ 6^{\frac{1}{2}}$	$6\frac{7}{8}$	2.61	.246
B105	12	40.0	117	6	2,	9.5	1.58	7.	66"	$ 7\frac{1}{4} $	2.70	66
B 53	15	42.0	$11\frac{1}{4}$ $11\frac{3}{4}$	$6\frac{1}{4}$	66	12.5	2.02	6.6	7	71	2.76	66
B109	15	60.0	$12\frac{3}{4}$	$6\frac{3}{4}$	66	13.0	1.97	66	66	81/8	2.92	66
B113	15	80.0	13 \$	$7\frac{1}{4}$	66	13.2	1.91	66	66	87/8	3.10	44
B 65	18	55.0	123	$6\frac{3}{4}$	50	19.8	2.41	6.6	9	8	2.89	66
B 73	20	65.0	$13\frac{1}{4}$	7	66	22.9	3.37	$\frac{7}{8}$	10	838	4.20	.334
B121	20	80.0	$14\frac{3}{4}$	73/4	44	24.6	3.34	11	1 66	91	4.49	66
B 89	24	80.0	143	$7\frac{3}{4}$	66	30.3	4.07	66	12	$9\frac{1}{8}$	4.45	66

Lengths and weights of separator bolts in above table are for girders composed of two beams of minimum section as shown. Lengths of bolts for intermediate and maximum sizes of beams may be obtained by adding twice the increase of web thickness to the lengths given.

# STANDARD CONNECTION ANGLES FOR I-BEAMS AND CHANNELS.



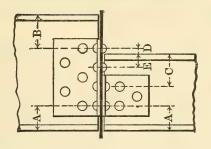
LOCATION OF CONNECTION ANGLES FOR BEAMS OF THE SAME OR DIFFERENT SIZES FRAMING OPPOSITE, BOT-TOMS OR TOPS FLUSH.



DEPTH OF	BEAMS.	A	В	C	D	E
Inch	16S,	A.				
Main Beam.	Opposite Beam.	Inches.	Inches.	Inches.	Inches,	Inches.
3	3	1½	1½	1½		
4	3 4	$\frac{1}{2}^{\frac{1}{2}}$	2½ 2	2 2	• •	
5 "	4 5	2 2½	3 2½	$\frac{2}{2\frac{1}{2}}$		
6	4 5 6	2 3	4  3	2 3 3	• •	
66	4 5 6 7	2½ " 2¼	2 '' 2 <sup>1</sup> / <sub>4</sub>	1½ 2½ 3½ 2¼	0 ::	1½ 0 1
8 "	4 5 6 7 8	2½ " " 2¾	3   2 <sup>3</sup> / <sub>4</sub>	1½ 2½ 3½ 3½ 2 2 <sup>3</sup> / <sub>4</sub>	1 0 	1½ 0 1 2
9	5 6 7 8 9	2½ "' " 3½	4 " " 3 <sup>1</sup> / <sub>4</sub>	$2\frac{1}{2}$ $3\frac{1}{2}$ $2$ $3$ $3\frac{1}{4}$	0	0 1 
10	6 7 8 9 10	2 <sup>1</sup> / <sub>2</sub> 3 <sup>3</sup> / <sub>4</sub>	5   3 <sup>3</sup> / <sub>4</sub>	$egin{array}{c} 3^{1}\!\!/_{2} \ 2 \ 3 \ 4 \ 3^{3}\!\!/_{4} \ \end{array}$		1 2 8 4

For cases where **D** is zero or **E** is 1'' or zero cut beam back  $\frac{1}{2}''$  or cope flanges back  $\frac{1}{2}''$  to clear rivet head.

### LOCATION OF CONNECTION ANGLES FOR BEAMS OF THE SAME OR DIFFERENT SIZES FRAMING OPPOSITE, BOT-TOMS OR TOPS FLUSH.



DEPTH 0	DEPTH OF BEAMS.		В	C	D	<b>JB</b>
Inc	hes.	A				
Main Beam.	Opposite Beam.	Inches.	Inches.	Inches.	Inches.	Inches.
12 " "	8 9 10 12	3½ " 3½	3 <sup>3</sup> / <sub>4</sub> " 3 <sup>1</sup> / <sub>2</sub>	$2^{1}/4$ $3^{1}/4$ $4^{1}/4$ $3^{1}/2$	1/4 : :	2½ 3½ 1¾ 1¾
15	8 9 10 12 15	3½ '' '' 3¾	4½ ;; ;; 3¾	2 <sup>1</sup> / <sub>4</sub> 3 <sup>1</sup> / <sub>4</sub> 4 <sup>1</sup> / <sub>4</sub> 3 <sup>3</sup> / <sub>4</sub> 3 <sup>3</sup> / <sub>4</sub>	1 <sup>3</sup> / <sub>4</sub> 3 <sup>3</sup> / <sub>4</sub> 	2½ 1 <sup>3</sup> ¼ 1½ 1¼
18 " " "	8 9 10 12 15 18	31/4    4	4 <sup>3</sup> / <sub>4</sub> 4	214 314 414 334 414 414	134 34 114 	$egin{array}{c} 2^{1}_{4} \\ 3^{4}_{4} \\ 1^{3}_{4} \\ 1^{3}_{4} \\ \vdots \\ \ddots \\ \end{array}$
20 " " "	8 9 10 12 15 18 20	3 <sup>1</sup> / <sub>4</sub> 3 <sup>3</sup> / <sub>4</sub>	4 <sup>1</sup> / <sub>4</sub> 3 <sup>3</sup> / <sub>4</sub>	21/4 31/4 41/4 33/4 41/4 48/4 33/4	134 134 114 114 	2 <sup>1</sup> / <sub>4</sub> 3 <sup>3</sup> / <sub>4</sub> 1 <sup>3</sup> / <sub>4</sub> 1 <sup>3</sup> / <sub>4</sub> 2 <sup>1</sup> / <sub>4</sub>
24 66 66 66 66 66 66	8 10 12 15 18 20 24	3 <sup>1</sup> / <sub>4</sub> 4 <sup>1</sup> / <sub>2</sub>	5 <sup>3</sup> / <sub>4</sub> 4 <sup>1</sup> / <sub>2</sub>	21/4 31/4 41/4 33/4 41/4 43/4 41/4 41/2	13/4 3/4 11/4 3/4 1/4 	2 <sup>1</sup> / <sub>4</sub> 1 <sup>3</sup> / <sub>4</sub> 1 <sup>1</sup> / <sub>4</sub> 1 <sup>3</sup> / <sub>4</sub> 2 <sup>1</sup> / <sub>4</sub> 1 <sup>3</sup> / <sub>4</sub>

For cases where **D** is  $\frac{1}{4}''$  or  $\frac{3}{4}''$  or **E** is  $\frac{3}{4}''$  or  $\frac{1}{4}''$  cut beam back  $\frac{1}{2}''$  or cope flanges back  $\frac{1}{2}''$  to clear rivet head.

### BEARING PLATES FOR SHAPES USED AS BEAMS.

Shapes used as beams resting on masonry walls or piers will generally require bearing plates of steel or their equivalents, set in or upon the masonry to properly distribute the load thereon with due regard to the allowable safe pressures for the

class of stonework or brickwork in question.

A table of bearing plates is presented on page 47, which gives the bearing values in pounds for plates of various sizes based on the safe unit pressure allowable on different classes of masonry. As the strength of masonry varies largely dependent upon the qualities of the material used, the workmanship and age, it is impossible to present absolute figures for safe unit pressures for all classes of work, but the values given below are believed to fairly represent these for the usual kinds of ordinary architectural masonry. The strength of ordinary masonry generally depends upon the crushing value of the mortar or cement used and does not bear any fixed relation to the ultimate strength of the brick or stone entering into the construction.

The table of bearing plates gives the bearing values of various sizes of plates when used with different classes of masonry, but the thickness of the plate should

be computed for each case.

For a plate of given length and breadth the thickness depends upon the allowable load and unit stress, and the width of the flange of the beam or channel resting upon it.

The thickness may be determined by the following formula:

$$t = .866 (1-b) \sqrt{\frac{R}{pb'l}}$$

t = thickness of plate in inches.

l = length of plate in a direction perpendicular to the axis of the beam or channel in inches.

b = width of flange of beam or channel in inches.

R = reaction at point of support in pounds. For uniformly distributed loads R = one-half of the load given in Tables of Safe Loads, pages 76 to 92 inclusive.

p = allowable stress in pounds per square inch on extreme fibre of plate. b' = width of plate in the direction of the axis of the beam or channel; *i. e.*, bearing on wall in inches.

If p = 16000 lbs. for steel we have

$$t = .00685 (l-b) \sqrt{\frac{R}{b'l}}$$

### EXAMPLES.

What is the proper size of steel bearing plate to be used in a wall of good brick laid in lime mortar to support the end of a 10-inch standard I-Beam, weighing 25 pounds per foot, of 16-foot span, subjected to its safe load uniformly distributed?

On page 79 in the Table of Safe Loads Uniformly Distributed for Cambria I-Beams, the total load is found to be 16280 pounds, and half of this, or 8140

On referring to the Table of Bearing Plates, on page 47, the proper size for this load on the class of masonry in question is found to be 6" x 10". The width of flange of a 10-inch 25 lb. standard beam is 4.66 inches.

Substituting these values in the formula for thickness gives

$$t = .00685 (10 - 4.66) \sqrt{\frac{8140}{6 \times 10}} = .426$$

The nearest commercial size above this is  $\frac{7}{16}$  inch, which is the thickness required. If a shorter plate would suit the location better it may be seen from the table that a plate  $8'' \times 8''$  will give the necessary bearing value and the thickness of this would be

$$t = .07685 (8 - 4.66) \sqrt{\frac{8140}{8 \times 8}} = .258$$

and the nearest commercial size above this is 15", which is the thickness required.

# BEARING PLATES FOR I-BEAMS AND CHANNELS.

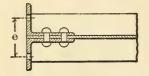
To be used on walls of different kinds of masonry.

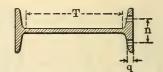
:	n Wall.  Disc.  Plate,  es.		Safe B	earing V		Plate in	Wall,	te,		Safe Bearing Value of Plate in Pounds,				
	bearing on wall. Inches.	Size of Plate, Inches,	Ordinary Stone Masonry.	Good Stone Masonry.	Brick in Lime Mortar.	Brick in Cement Mortar.	Bearing on V	Size of Plate, Inches.	Ordinary Stone Masenry.	Good Stone Masonry.	Brick in Lime Mortar,	Brick in Cement Mortar.		
	4	4x 4	2880				14	14×14	35280		29400	39200		
	4	4x 6	4320				14	14×16	40320	67200	33600	44800		
	4	4x 8	5760	9600	4800	6400	14	14x18	45360	75600	37800	50400		
	6	Gy G	6100	10800	5400	7200	14	14x20	50400	84000	42000	56000		
	6	6x 6 6x 8		14400			16	16×16	46080	76900	38400	51200		
	6	6x10		18000			16	16x18	51840		43200			
	U	0.710	10000	10000	5000	12000	16	16x20	57600		48000			
	8	8x 8	11520	19200	9600	12800	16	16x22	63360		52800	70400		
	8	8x10		24000				10-100	00000	100000	02000	10200		
	8	8x12		28800			18	18×18	58320	97200	48600	64800		
							18	18x20		108000				
	10	$10 \times 10$	18000	30000	15000	20000	18	18x22	71280	118800	59400	79200		
	10	10x12		36000			18	18x24	77760	129600	64800	86400		
	10	$10 \times 14$	25200	42000	21000	28000								
	10	10 16	05000		0.1.000	2002		$20 \times 20$	72000	120000	60000	80000		
		12x12		43200				20x22	79200	132000	66000	88000		
	12	12x14	30240	50400	25200	33600		20x24		144000				
				57600			20	$20 \times 26$	93600	156000	78000	104000		
_	12	12×18	38880	04800	32400	43200								

Bearing values are based on the following allowed pressures:

	Allowable Pressure.		
Masonry.	Pounds per Square Inch.	Tons per Square Foot.	
Ordinary Stone Good Stone Brick in Lime Mortar Brick in Cement Mortar	180 300 150 200	12.96 21.60 10.80 14.40	

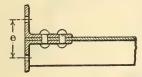
### STANDARD SPACING OF RIVET AND BOLT HOLES THROUGH FLANGES AND CON-NECTION ANGLES OF I-BEAMS, AND TANGENT DISTANCES BETWEEN FILLETS MEASURED ALONG THE WEB.

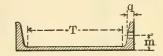




Depth of Beam.	Weight.	n	е	, <b>d</b>	T	Depth of Beam.	Weight.	n	е	q	Т
Inches.	Lbs.perFt.	Inches.	Inches.	In.	Inches.	Inches.	Lbs.perFt.	Ins.	Inches.	Inches.	Inches.
3	5.5 6.5 7.5	1 7 16 · · ·	421 43/4 47/8	1/4	1 13 66	12	55.0	3	5 5 16	11 16	9 5 6
4	7.5 8.5 9.5 10.5	11/2	4116 43/4 4277 4239 4232	9 32 16	211 (18 (1	15	42.0 45.0 50.0 55.0 60.0	3	$\begin{array}{c} 4_{\overline{3}\overline{2}}^{29} \\ 4_{\overline{3}\overline{2}}^{31} \\ 5_{\overline{1}6}^{1} \\ 5_{\overline{3}\overline{2}}^{5} \\ 5_{\overline{4}}^{1} \end{array}$	5/8   21 32	12½
5	9.75 12.25 14.75	13/4	4 <sup>23</sup> / <sub>3</sub> 4 <sup>7</sup> / <sub>8</sub> 5	5 16 16 11 32	35/8 	15	60.0 65.0 70.0	31/4	5\frac{3}{32} 5\frac{3}{32} 5\frac{9}{32} 5\frac{3}{32} 5\frac{9}{32} 5\frac{15}{32}	13 16 27 37	1134
6	12.25 14.75 17.25	2	423 427 431 431	11 32 3/8	4 7 6	66	75.0 80.0	66		66	66
7	15.00 17.50 20.00	21/4	$\begin{array}{c} 4\frac{3}{4} \\ 4\frac{27}{322} \\ 4\frac{31}{32} \end{array}$	3/8	<b>5</b> <sup>3</sup> / <sub>8</sub>	15	80.0 85.0 90.0 95.0 100.0	33/4	5 5 6 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	1 1/3/2  1 1/16	1015
8	18.00 20.25 22.75 25.25	21/4	$\begin{array}{c} 4\frac{25}{32} \\ 4\frac{27}{32} \\ 4\frac{15}{16} \\ 5\frac{1}{32} \end{array}$	13 32 7 16 66	6,16	18	55.0 60.0 65.0 70.0	31/4	431 516 518 5732	11 16 23 36	153
9	21.0 25.0 30.0 35.0	2½ "	$\begin{array}{c} 4_{\frac{25}{322}} \\ 4_{\frac{29}{322}} \\ 5_{\frac{16}{32}} \\ 5_{\frac{7}{32}} \end{array}$	7 16 15 32	7,16	20	65.0 70.0 75.0	31/2	5 5 5 32 5 5 5 32 5 5	250	1615
10	25.0 30.0 35.0 40.0	25/8	$\begin{array}{c} 4_{16}^{13} \\ 4_{16}^{15} \\ 5_{32}^{32} \\ 5_{14}^{1} \end{array}$	$\frac{15}{32}$ $\frac{1}{2}$ $\frac{17}{32}$	7,15	20	80.0 85.0 90.0	4	5 <sup>3</sup> / <sub>32</sub> 5 <sup>5</sup> / <sub>32</sub> 5 <sup>1</sup> / <sub>4</sub> 5 <sup>1</sup> / <sub>6</sub> 5 <sup>3</sup> / <sub>8</sub>	29 32 66	16716
12	31.5	23/4	$\frac{4\frac{27}{32}}{4\frac{15}{16}}$ $5\frac{1}{16}$	1732	93/4		100.0	4		15	9011
12	40.0 40.0 45.0 50.0	3	$egin{array}{c} f{5}_{16}^{\frac{1}{16}} \\ f{4}_{312}^{\frac{31}{32}} \\ f{5}_{32}^{\frac{3}{32}} \\ f{5}_{16}^{\frac{3}{16}} \\ \end{array}$	9 16 21 32 66	9,5	24	85.0 90.0 95.0	4	5 16 5 1/8 5 36 5 1/4	7/8	2011

### STANDARD SPACING OF RIVET AND BOLT HOLES IN FLANGES AND CONNECTION ANGLES OF CHANNELS, AND TANGENT DISTANCES BETWEEN FILLETS MEASURED ALONG THE WEB.





											-
Depth of Channel	Weight.	m	е	q	T	Depth of Channel	Weight.	m	е	q	T
Inches.	Lbs.perFt.	Inches.	Inches.	In.	Inches.	Inches.	Lbs.per Ft.	Inches.	Inches.	In.	Inches.
3 "	4.0 5.0 6.0	15	4 <sup>21</sup> / <sub>3</sub> 2 4 <sup>3</sup> / <sub>4</sub> 4 <sup>7</sup> / <sub>8</sub>	1/4	1,136	8	21.25 13.25	1 ½ 13%	532 43/4	132	6 <sup>5</sup> <sub>16</sub>
4.66	5.25 6.25 7.25	1	4 <sup>11</sup> / <sub>16</sub> 4 <sup>3</sup> / <sub>4</sub> 4 <sup>27</sup> / <sub>32</sub>	9 32 9 32 5	211	"	15.00 20.00 25.00	$\begin{array}{c} 1\frac{3}{8} \\ 1\frac{7}{16} \\ 1\frac{9}{16} \\ 1\frac{3}{4} \end{array}$	43/4 425/245 411/8 51/8	3/8/3/3/3/3/3/3/3/3/3/3/3/3/3/3/3/3/3/3	66
5	6.5 9.0 11.5	1 11/4	$\begin{array}{c} 4_{\overline{3}\overline{2}} \\ 4_{\overline{1}\overline{1}6} \\ 4_{\overline{3}\overline{2}} \\ 4_{\overline{3}\overline{2}} \\ 4_{\overline{3}\overline{2}} \end{array}$	5 16 9 32 5 16	35/8	10	15.0 20.0 25.0	11/2 15/8 13/4 11/5 16	4 <sup>3</sup> / <sub>4</sub> 4 <sup>27</sup> / <sub>5</sub> 5 <sup>1</sup> / <sub>2</sub>	7 16 3/8	8 <sub>16</sub>
8 "	8.0 10.5 13.0	$egin{array}{c} {f 1} rac{1}{16} \ {f 1} rac{3}{16} \ {f 1} rac{5}{16} \ {f 1} rac{7}{16} \end{array}$	4 1 1 6 4 1 1 6 4 1 1 6 6 6 6 6 6 6 6 6	16	41/2	"	30.0 35.0 20.5	$\mathcal{Z}_{\overline{16}}$	5 3 2 5 3 5 1 6 5 1 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	3/8 13/3/2 7 16	66
7	15.5 9.75	$1\frac{16}{16}$ $1\frac{3}{16}$	5 1 6 4 2 3 4 2 3	66	5,7 1,16	12	25.0 30.0	13/4 17/8 2 21/8 21/4	4 <sup>25</sup> / <sub>3</sub> 2 4 <sup>7</sup> / <sub>8</sub> 5	150 250 250 250 270 131 270	915
66	12.25 14.75 17.25	$1\frac{3}{16}$ $1\frac{5}{16}$ $1\frac{7}{16}$ $1\frac{7}{8}$	42324 41169 4231 518 518	11/2/20	66	15	35.0 40.0 33.0		51/8 51/4		66
" 8	19.75 11.25	15/8	5½ 423	3/	6.5	15	35.0 40.0	17/8 115 2 21/8	$\begin{array}{c} 4_{\frac{29}{32}} \\ 4_{\frac{16}{16}} \\ 5_{\frac{1}{32}} \end{array}$	21 32 11	123/8
8 "	13.75 16.25	$1\frac{1}{4}$ $1\frac{5}{16}$ $1\frac{3}{8}$ $1\frac{1}{2}$	4 <sup>23</sup> / <sub>3</sub> 2 4 <sup>13</sup> / <sub>16</sub> 4 <sup>29</sup> / <sub>32</sub> 5	3/00/30/00/0	6,5	66	45.0 50.0	21/8 21/4	5 \frac{1}{32} \ 5 \frac{7}{32} \ 5 \frac{5}{16} \]	11/6/81/2 5/81/2	66
66	18.75	11/2	5°2	13/32	66	"	55.0	$2^{1/4}_{2^{5}_{16}}$	5 5 5	22	66

# MAXIMUM SIZE OF RIVETS IN BEAMS AND CHANNELS.

		Channels.						
Depth of Beam.	Weight.	Diameter of Rivets.	Depth of Beam.	Weight.	Diameter of Rivets.	Depth of Channel.	Weight.	Diameter of Rivets.
Inches.	Lbs. per Ft.	Inches.	Inches.	Lbs. per Ft.	Inches.	Inches.	Lbs. per Ft.	Inches.
3 4 5 6 7 8 9 10 12 12	5.50 750 9.75 12.25 15.00 18.00 21.00 25.00 31.50 40.00	3/0/24 5/04 3/4	15 15 15 18 20 20 24	42.0 60.0 80.0 55.0 65.0 80.0 80.0	3/4 7/8 1 	34 56 78 9 10 12 15	4.00 5.25 6.50 8.00 9.75 11.25 13.25 15.00 20.50 33.00	3/8 1/2 5/8 68 3/4 64 66

### STANDARD SPACING OF RIVET AND BOLT HOLES IN ANGLES, T-BARS AND Z-BARS, WITH MAXIMUM SIZE OF RIVETS TO BE USED.







### ANGLES.

Length of Leg.	m	Diameter of Rivet.	Length of Leg.	m	Diameter of Rivet.	Length of Leg.	m	Diameter of Rivet.
Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
3/4 1 11/4 11/6 13/8 11/3/4	7 19 15 16 4 3 3 5 5 6 5 6 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1/4 3/8 1/2   5/8	21/44 22/5/6/22/23/4 22/33/4	1½ 1¼ 1¼ 1½ 1¾	5/8 3/4 66 66 66 7/8	3½ 4 4½ 5 6 7	Variable, depending on diameter of rivet, thickness of metal and length of leg.	1 66 66 66 66

### T-BARS.

I-DARS.									
Section Number.	Width of Flange.	Depth of Bar.	Weight.	m	Max. Diam. of Rivets in Stem.	n	Max. Diam. of Rivets in Flange.		
	Inches.	Inches.	Lbs. per Ft.	Inches.	Inches.	Inches.	Inches.		
T "181 "183 "187 "189 " 39 " 41 " 42 " 467 " 69 " 73 " 182 " 654 " 140 " 169	1 1 1 8 5 6 1 1 1 1 8 8 8 8 1 1 1 1 1 1 1 1 1 1 1	1 1 1/8 5 6 1 1/4 1/2 2 1 1/4 1/2 3 1 1/4 2 1/2 4 4 1/2 3 3 1/4 2 1/2 4 4 1/2 4 4 1/2 4 4 1/2 3 3 1/4 1/4 1/2 4 1/2 4 4 1/2 4	1.0 1.4 1.7 1.9 2.7 4.2 5.6 6.8 10.1 2.3 1.5 9.0 10.9 13.6	9 15 \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	37 1/6 5% 3/4 1% 1 3/1/3/4 1 1 1/8	5/8	1/4 		

### Z-BARS.

Section	Depth of Bar.	Weight.	m	Max. Diam. of Rivets.  Inches.	
Number.	Inches.	Lbs. per Foot.	Inches.		
Z 5-Z 9-Z13 "21-"25-"29 "37-"41-"45 "53-"57-"61	3 to 316 4 " 418 5 " 518 6 " 618	6.7 to 14.2 8.2 " 23.0 11.6 " 28.3 15.6 " 34.6	15/8 13/4 17/8 2	3/4 7/8 1	

### FIREPROOF CONSTRUCTION.

Buildings of fireproof construction consist essentially of a steel frame or skeleton to support the floors, and in the case of high buildings, the outside walls are also carried by the steel framing. All parts of the steel work are enclosed and protected by some fire-resisting material which should be of such quality and arrangement as not to disintegrate or fall away when heated to high temperatures and at the same time exposed to a stream of cold water. The fireproofing for the floors, in addition to its ability to afford a fireproof protection to the steel beams, must be capable of supporting the load and distributing it to the floor beams, which in turn transmit it to the columns and thence to the foundations.

One of the earlier forms of floors consists of brick arches built between and supported by the bottom flanges and lower portions of the web of iron or steel I-Beams, but this style has considerable dead weight and as ordinarily constructed does not provide fireproof protection for the bottom flanges of the beams. Another of the earlier forms of floor is composed of sheets of corrugated iron arched between the beams, on which a concrete filling is placed, and this also, as ordinarily constructed, does not provide protection for the bottom flanges of the beams, besides which, it is quite heavy.

A later style of floor is the hollow tile system, which is composed of flat or segmental arches constructed of moulded blocks of hard burned clay, specially shaped, and of various depths to suit different loads and the sizes of the I-beams supporting them. In the hollow tile system, the blocks may also be of porous terra-cotta which is lighter than hard clay.

Various other systems of fireproofing are now in use, the most usual forms of which consist of cement, concrete or other material used alone or deposited or arranged about a strengthening or supporting framework of steel shapes, bars, rods, wire, wire-cloth, etc.

Column or girder fireproofing may be accomplished by the use of hard clay or porous terra-cotta blocks shaped to fit and enclose the steel work, or the steel may be wrapped with wire, wire-cloth, metal lath, etc., and a concrete or plastered coating applied to it.

Fireproof partitions may be constructed of hollow tiles composed of hard clay or porous terra-cotta to which the plaster finish may be directly applied, or they may be composed of suitable metal studding on which is secured the wire-cloth or metal lath that serves to support the concrete or other fireproofing, the surface then being plastered in the usual manner.

The dead weights of fireproof floors vary between wide limits dependent upon the system employed, the load to be carried and the distance between the supporting beams.

### TESTS OF FLOOR ARCHES.

Reports of tests of various forms of floor arches may be found in the American Architect, March, 1891, and in the Engineering Record

for September and October, 1897.

A paper on this subject, entitled "Tests of Fire-proof Flooring Material," was published in the *Transactions of the American Society of Civil Engineers*, with discussions, in Vols. xxxiv and xxxv, dated 1895 and 1896.

A summary of the principal data and results of the tests which were the subject of the latter paper is given in the following table:

### BREAKING LOAD OF HOLLOW TILE ARCHES.

						Total	Hori-	B	LOCKS.		
Depth	Rise,	Cnon	Langth	Total	Load	Hori-	zontal			Character	Manner
Arch.	Alse.	opan.	Length.	Load.	per Sq.Foot.	zontal	Thrust		31.	of	of
22.02.					Dq.1 000.	Thrust.	per Ft.	19	Material,	Load.	Laying Joints.
Ins.	Ins.	Ins.	Ins.	Lbs.	Lbs.	Lbs.	Arch.	Style.	Ma		aotnes.
6.	3.5	60	48.	13750	688	29474	7369	E	Hard	Dis.	Port.
7.5	5.	46	11.5	9000	2452		10818	66	66	66	N. M.
7.5	5.	60	35.2	11250	10 2010		11505	66	66	Cen.	Port.
7.5	5.	60	36.5	13000		39000	12822	66	Porous	66	66
8.	7.	60		14500		31071	9747	66	66	66	66
8.	7.	60		15750		33750	10588	66	Hard	66	66
12.	10.	60	41.	16400		24600	7200	66	66	66	66
12.	8.75	60	10.	3100		5314	6377	66	66	66	N. M.
12.	9.	60	10.	5000			10000	66	66	66	66
12.	9.	60	10.	15100	3630	12583	15100	66	66	Dis.	66
12.	9.5	60	10.	2500		3947	4736	66	66	Cen.	
8.	5.5	46	11.5	2500		2614	2727	S	66	Dis.	N. M.
8.	5.	45	11.5	1300	362	1463		66	66	66	66
8.	6.	60	36.	10000		25000		66	66	Cen.	Port.
8.	5.	60	36.	5700				66	66	Dis.	66
8.	5.	60	12.	3500	700	5250		66	66	. 66	N. M.
8.	5.5	60	12.	10000	2000	13636		66	66	66	66
8.	5.5	60	12.	2500		6818		66	66	Cen.	66
8.	5.5	60	24.	9950		13568		66	"	Dis.	66
8.	5.5	60	24.	2500		6818		66	66	Cen.	66
10.	7.5	60	36.	13500		13500		66	66	Dis.	Port.
10.	8.	60	37.	14500		13594		66	66	66	
-											

NOTE.—In the above table the following abbreviations are used: "E," End Construction; "S," Side Construction; "Hard," Hard Clay; "Porous," Porous Terra-Cotta; "Dis.," Distributed Load; "Cen.," Concentrated Load at Centre; "Port," Portland Cement, and "N. M.," No Mortar.

The Loads per Sq. Foot in the above table were obtained in all cases by dividing the Total Load by the superficial area of the arch in square feet. The Horizontal Thrust for distributed and Central Loads was obtained by formulæ similar to those given therefor on one of the preceding pages, and for Central Loads this is double that for a distributed load of the same weight.

### THRUST OF ARCHES.

The horizontal thrust of segmental floor arches, on the assumption of uniform loading, may be found by the following formula:

$$T = \frac{3WL^2}{2R}$$

in which

T = pressure or thrust in pounds per lineal foot of arch.

W= load on arch in pounds per square foot, uniformly distributed.

L = span of arch in feet.

R = rise of segmental arch in inches.

For a concentrated load at the centre, of weight P, the thrust

$$T = \frac{3PL}{R}$$

For arches with flat tops and bottoms, such as are used in floors, the voussoir joints on each side of the central key are usually laid out on parallel lines, and in these cases the thrust may be determined approximately by using for R, in the above formula, the effective depth of the arch.

For segmental arches the rise R is the vertical distance from the highest part of the intrados to the plane of the springing line. If the radius of the intrados for segmental arches is r, the rise may be obtained from the following formula:

$$R=r{-}\sqrt{r^2{-}\frac{L^2}{4}}$$
 conversely,  $r=\frac{R}{2}+\frac{L^2}{8R}$ 

## TIE RODS.

Although in the completed structure the horizontal thrusts of adjoining arches may counterbalance each other, the tie rods should be so proportioned and spaced as to withstand the entire thrust of the arches, thus tying the structure together and facilitating the construction.

## SPACING OF TIE RODS FOR TILE ARCHES.

The table on the next page was computed from the following formula, which was obtained from that giving the thrust of arches on page 53.

$$B = \frac{A \times R \times 10000}{WL^2}$$

in which

B = spacing of tie rods in feet.

A = net area of rod in square inches.

R = rise of arch in inches.

W = load in pounds per square foot of the arch.

L = span of arch in feet.

The above formula gives the spacing of tie rods corresponding to a tensile stress in the rods of 15 000 pounds per square inch, without considering the flexure of the beams.

In spacing tie rods, the lateral strength of beams, for flexure due to the thrust of the arches should be taken into consideration, explanations for which are given on pages 58 to 61 herein.

Spacings for other loads than that of the table may be found by proportion, thus:

Required spacing =

New load in lbs. per sq. ft. + weight of arch in lbs. per sq. ft. × spacing from table.

Weights of tile arches per square foot are given on page 57.

As noted under the heading "Lateral Strength of Beams," on pages 62 and 63, care should be taken that the spacing of tie rods is not greater than twenty times the least flange width, otherwise the safe loads should be reduced to compensate for the strains produced by flexure of the upper flange considered as a column in compression.

## SPACING OF TIE RODS FOR TILE ARCHES.

For a uniform load of 100 lbs. per square foot in addition to the weight of the arch.

		Nominal Depth of Arch. Inches.							
Span of Arch.	Diameter of	6	7	8	9	10	12		
Feet,	Tie Rods. Inches.	Eff	ective		or Riches.	ise of	Arch.		
		3.6	4.6	5.6	6.6	7.6	9.6		
3 "	5)@0341~ 00	6.4 9.5 13.2	8.0 12.0 16.6	9.5 14.2 19.8	10.9 16.3 22.6	12.3 18.3 25.5	15.0 22.4 31.1		
4 "	5/000/41-100	3.6 5.4 7.4	4.5 6.7 9.4	5.4 8.0 11.1	6.1 9.2 12.7	6.9 10.3 14.3	8.4 12.6 17.5		
5 "	5 000 47 00	2.3 3.4 4.8	2.9 4.3 6.0	3.4 5.1 7.1	3.9 5.9 8.1	4.4 6.6 9.2	5.4 8.0 11.2		
6	5,00 to) 417- 00	• •	2.0 3.0 4.2	2.4 3.6 4.9	2.7 4.1 5.7	3.1 4.6 6.4	3.7 5.6 7.8		
7 	00 -1 <del>01 00</del>			• •	2.0 3.0 4.2	2.3 3.4 4.7	2.8 4.1 5.7		
8	15/00 <b>15/41/0</b> 0		• •		• •	1.7 2.6 3.6	2.1 3.1 4.4		

### BEAM TABLES.

Tables of safe loads for beams and channels and spacings of I-Beams for floors are given with explanatory notes on pages 70 to 103 inclusive.

### BEAMS AS GIRDERS.

In some cases two or more beams may be bolted together side by side to form a girder, in which case cast iron separators with bolts should be used to hold the various members together. Separators should be placed at each end of the girder, at points of concentrated loading, and for uniform loading should be located at distances apart not greater than twenty times the width of the smallest beam flange, in order to laterally support the upper flanges which are in compression and prevent their failure by buckling. The separators should fit closely between the beam flanges so as to unite the beams forming the girder and thereby cause them to act together in resisting the load. A table of separators is given on page 42.

## CONNECTION ANGLES.

When beams are coped or fitted together at right angles, connection angles are generally used, standards for which, covering usual cases, are shown on pages 43, 44 and 45. Explanations and tables of limiting spans for which these standards may be used are given on pages 40 and 41. Beams may be fitted together thus with flush tops or bottoms or in intermediate positions, as required in cases where the girder or trimmer beam is the larger. In cases where the girder or trimmer beam is the smaller, special stirrups or other connections are required.

## LIVE LOADS FOR FLOORS.

The following loads per square foot, exclusive of weight of floor materials, show the range assumed in usual practice:

Buildings for public assembly. .120 to 150 lbs. per sq. ft.

Stores, warehouses, etc........150 to 250 lbs. and upwards per sq. ft.

On page 301 are given in detail the safe loads for which floors should be designed in accordance with the building laws of various cities.

# WEIGHTS OF HOLLOW TILE FLOOR ARCHES AND FIREPROOF MATERIALS.

## END CONSTRUCTION, FLAT ARCH.

Width of Span Between Beams.	Depth of Arch.	Weight per Square Foot.		
5 feet to 6 feet.	8 inches.	27 pounds.		
6 " 7 "	9 "	29 "		
7 " 8 "	10 "	33 "		
8 " 9 "	12 "	38 "		

### HOLLOW BRICK FOR FLAT ARCHES

(SIDE CONSTRUCTION).

-	Width of Span Between Beams.							Depth	of Arch.	Weight per Square Foot.
3	feet	6	inches	to 4	feet	0	inches.	6 ii	nches.	27 pounds.
4	66	0	66	4	66	6	66	7	66	29 "
4	66	6	66	5	66	0	6.6	8	66	32 "
5	66	6	66	6	66	0	66	9	66	36 "
6	66	0	66	6	66	6	66	10	66	39 "
6	66	6	"	7	66	0	66	12	66	44 "

#### PARTITIONS.

				Thickness.	Weight per Square Foot.
Hollow	Brick	(Clay)	Partitions	2 inches.	11 pounds.
66	66	. "	"	3 "	14 "
66	66	66	66	4 "	15 "
66	66	66	44	5 "	19 "
66	66	66	66	6 "	20 "
66	66	66	"	8 "	27 "
Porous '	Terra-	Cotta P	artitions	3 "	16 "
66	66	46	66	4 "	19 "
66	66	"	"	5 "	22 "
66	66	66	66	6 "	23 "
66	66	66	66	8 "	33 "

## FURRING, ROOFING AND CEILING.

				Thi	ickness.	Weight pe	r Square Foot.
Porous	Terra-	Cotta	a Furring	2 i	nches.	8 pc	ounds.
66	66		Roofing	2	66	12	66
66	46	66	"	3	66	15	66
66	44	46	"	4	66	19	66
66	66	66	Ceiling	2	4.6	11	66
66	66	66	"	3	66	15	66
"	66	66	"	4	66	19	66

6-inch Segmental Arches, 27 pounds per square foot.

2-inch Porous Terra-Cotta Partition, 8 pounds per square foot.

## LATERAL STRENGTH OF BEAMS TO RESIST FLEXURE DUE TO THRUST OF ARCHES, ETC.

In special cases where the thrust of a floor arch is exerted against a beam, channel, angle or other shape without other lateral support than the tie rods, or braces, this will produce lateral flexure and stresses in addition to those caused by the vertical loading. Throughout the body of the floor the thrusts of the adjoining arches when completed will usually counterbalance each other, but in the outer beams around shafts or elsewhere if unsupported sideways the stresses due to the lateral forces should be considered.

The total allowable stress per square inch for the extreme fibres of beams has been placed at 16 000 pounds per square inch, and in order that this may not be exceeded owing to lateral stresses, the stress due to vertical loading should be correspondingly reduced so that the resultant intensity shall not exceed the allowable limit. This may be calculated by considering the beam as continuous and laterally supported at intervals by the tie rods, the spans being equal to the spacing of the rods.

In this case the fibre stress due to the lateral forces is:

$$p' = \frac{wx_1B^2}{I'} \qquad (1)$$

in which

p' = fibre stress in pounds per square inch due to lateral forces.

w = lateral load or thrust in pounds per lineal foot of section used as a beam.

 $x_1 =$ distance of the extreme fibre from the neutral axis in inches.

B = distance between tie rods or lateral supports in feet.

I' = moment of inertia about the vertical axis of the section or that one at right angles to the line of application of the lateral forces.

For I-Beams with the web placed vertically as usual  $x_1$  becomes equal to  $\frac{b}{2}$ , where b is the width of the flange in inches. In this case the above formula for intensity of unit stress due to lateral load becomes:

$$p' = \frac{wbB^2}{2I'}$$
 (2)

P

The resultant fibre stress from the horizontal or lateral and the vertical loads may be represented by the hypothenuse of a right angle triangle, the two sides of which represent the intensities of the horizontal and vertical stresses, thus:

In order that the total resultant stress shall not exceed the allowable limit of 16000 pounds per square inch, the stress due to vertical loading should therefore be reduced to equal the following:

$$p = \sqrt{16\ 000^3 - p'^2}$$
 (3)

Having thus obtained the reduced vertical stress p, the safe vertical load of the tables corresponding to this stress should accordingly be reduced by multiplying it by the ratio  $\frac{p}{16\,000}$  and similarly for other stresses and corresponding loads, thus making proper allowance for the additional stresses produced by the lateral forces.

If the reduction of the safe loads on this account is a considerable proportion of the original amount due to vertical loading only, it would be more economical to provide lateral braces or tie rods at shorter intervals, thus avoiding the use of an excessive amount of material in the beam.

As the stresses due to vertical forces for usual cases of loading are a maximum at the centre of the span it will ordinarily be sufficient to space the tie rods or braces at shorter intervals near the centre in order to allow for the combined stresses due to vertical loading and horizontal thrusts.

The above method of calculation is not exact when considering the lateral thrust of arches, or loads from similar materials which do not exert a uniform pressure throughout their surfaces of contact with the sustaining beam on account of the friction and bond of their component parts, but this analysis of the stresses may serve as a guide in designing.

The above formulæ should be used in connection with the tables and formula given on pages 62 and 63 relating to the lateral strength of beams, due to compression of the upper flange figured as a column between points of lateral support.

### EXAMPLE.

What is the proper size of I-Beam without other lateral support than the usual tie rods, corresponding to a total fibre stress of 16 000 pounds per square inch under the following conditions? The beam is 18 feet between end supports and carries a tile arch on one side having a nominal depth of 9 inches, effective depth of 6.6 inches, a span of 5 feet, designed to carry a superimposed load of 100 pounds per square foot in addition to the weight of the arch and other floor materials. The hollow tile arch weighs 36 pounds per square foot and the other materials, including plastering, weigh 14 pounds, making a total load, exclusive of the weight of the beam, equal to 150 pounds per square foot.

For tie rods of 3/11 diameter the spacing between them would be 5.9 feet, as shown by the table of Spacing of Tie Rods on page 55, in which the safe stresses in the rods only are considered.

Substituting the proper values in the formula for lateral thrust of arches, given on page 53, this will be

$$T = \frac{3 \times 150 \times 5^2}{2 \times 6.6} = 852$$
 lbs. per lineal foot.

Substituting this value for w in formula (2) page 58, we have

$$p' = \frac{852 \times 4.66 \times 5.9^2}{2 \times 6.89} = 10029$$
 lbs. per sq. in.

Therefore 
$$p = \sqrt{16000^2 - 10029^2} = 12466$$
 lbs. per sq. in.

Hence the safe load as determined by the consideration of vertical loads only, should be reduced to  $\frac{12\,466}{16\,000}$ , or approximately  $\frac{3}{4}$  of the amount given by the Tables of Safe Loads in case the spacing of the tie rods is not changed.

Assume a 10" beam 25 lbs. per foot, the moment of inertia of which is 6.89, as given in the Tables of Properties of I-Beams, page 156.

The safe vertical load for a 10" beam, weighing 25 lbs. per foot, 18 feet long between supports, for fibre stress of 16 000 lbs. per square inch, is 14 470 lbs. uniformly distributed, including the weight of the beam as given in the Tables of Safe Loads, on page 79, or 14 020 exclusive of the weight of the beam, and 34 of this is 10 515 lbs., which is the vertical load it can safely carry in order that the total stress due to it and the lateral thrust shall not exceed 16 000 lbs. per square inch.

The actual vertical load on the beam under consideration is as follows:

$$\frac{5}{2} \times 18 \times 150 = 6750$$
 lbs.,

which is less than the allowable amount, 10 515 lbs., as figured above, so that a smaller beam may suffice.

Therefore, assume a 9-inch beam, weighing 21 lbs. per foot, the moment of inertia of which about an axis coincident with centre line of web is found in the Table of Properties, on page 156, to be 5.16.

In this case

$$p' = \frac{852 \times 4.33 \times 5.9^2}{2 \times 5.16} = 12444$$
 lbs. per sq. in.

Substituting this in the formula for p we have

$$p = \sqrt{16\ 000^2 - 12\ 444^2} = 10\ 106\ lbs.$$
 per sq. in.

Therefore the safe vertical load will be  $\frac{10\,106}{16\,000}$ , or approximately  $\frac{5}{8}$  of the tabular safe load.

The safe vertical load for a 9" 21 lb. beam, 18 feet long, for a fibre stress of 16 000 lbs. per square inch is 11 180 lbs., as given in the Tables of Safe Loads, on page 79, and 5% of this is 6 987 lbs., which is slightly greater than the actual amount, 6 750 lbs., as calculated above, so that the 9" 21 lb. beam will suffice.

If the spacing of the tie rods at the centre be reduced from 5.9 feet to 4 feet it may be found in a manner similar to that used in the above calculations, that the safe vertical load for an 8" I-Beam, weighing 18.0 lbs. per foot, is reduced to % of its tabular value of 8 430 lbs., or 7 376 lbs., and as this amount is greater than the actual load as above, namely 6 750 lbs., the 8" beam would answer the purpose, under the changed conditions as to spacing of tie rods. As this beam might deflect beyond the limit for plastered ceilings, it should be examined in accordance with the rule or formula given for obtaining safe deflections in the explanation of the Tables of Safe Loads, and elsewhere herein.

Calculating this by the rule given on page 72, the safe load for the allowable limit of deflection is

$$W = \frac{9480 \times 16^2}{18^2} = 7491 \text{ lbs.,}$$

which is greater than the actual amount, 6750 lbs., so that the 8" beam is sufficient and proper if the spacing of central tie rods be changed to 4 feet, as assumed in the last case.

# LATERAL STRENGTH OF BEAMS, WITHOUT LATERAL SUPPORT.

The Tables of Safe Loads for Cambria I-Beams and Channels and Tables of Spacing of Cambria I-Beams, on pages 76 to 103, are calculated on the assumption that proper provision is made for preventing lateral deflection by means of tie rods or other braces. In order to prevent undue strains in the compression flange, considered as a column, the beams should be supported laterally at distances not exceeding twenty times the flange width, this ratio being determined by the following formula, which gives the safe load for solid columns of soft steel:

$$p = \frac{18000}{1 + \frac{1^2}{3000b^2}}$$

in which

p = allowable stress in pounds per square inch.

1 - length between lateral supports in inches.

b = width of flange in inches.

Substituting 16 000 for p in the above formula, which is the allowable unit stress of the safe load tables, it is found that the ratio  $\frac{1}{b} = 19.37$ , from which it may be seen that the compression flange should be supported laterally at distances not exceeding twenty times the flange width as stated above.

Beams which are not thus supported laterally should not be loaded to their full transverse capacity. The allowable fibre stresses and proportions of their full loads which they can safely carry when laterally supported at various distances is given in the following table:

## REDUCTION IN VALUES OF ALLOWABLE FIBRE STRESS AND SAFE LOADS FOR SHAPES USED AS BEAMS DUE TO LATERAL FLEXURE.

Ratio of Span or Distance between Lateral Supports to Flange Width.	Allowable Unit Stress for Direct Flexure in Extreme Fibre.	Proportion of Tabular Safe Load to be	Ratio of Span or Distance between Lateral Supports to Flange Width.	Allowable Unit Stress for Direct Flexure in Extreme Fibre.	Proportion of Tabular Safe Load to be
1 b	p	Used.	1 b	р	Used.
19.37 20 25 30 35	16000 15882 14897 13846 12781	1.0 .97 .93 .87 .80	65 70 75 80 85	7474 6835 6261 5745 5281	.47 .43 .39 .36 .33
40 45 50 55 60	11739 10746 9818 8963 8182	.73 .67 .61 .56	90 95 100 105 110	4865 4595 4154 3850 3576	.30 .29 .26 .24 .22

The above table should be used in connection with the Tables of Safe Loads Uniformly Distributed for Cambria I-Beams and Channels, on pages 76 to 92 inclusive, and limits the values found therein under the conditions given above.

#### EXAMPLE.

Required the safe load for a 15-inch standard I-Beam weighing 42 pounds per foot for a span of 30 feet without lateral supports:

From the data the ratio 
$$\frac{1}{b} = \frac{30 \times 12}{5.5} = 65$$

From the above table the proportion of the safe load which the beam can safely support under these conditions is .47. From the Table of Safe Loads for I-Beams, page 81, the safe load for this beam when properly supported laterally is 20 940 pounds, which multiplied by .47 gives 9 842 pounds as the safe load uniformly distributed under the conditions given, including the weight of the beam, or 8 582 pounds superimposed load.

# LIMITING SPANS AND MAXIMUM LOADS OF I-BEAMS AND CHANNELS DUE TO CRIP-PLING OF THE WEB.

I-Beams and Channels when used as beams for very short spans in which the ratio of length of span to depth of beam is small, should be examined for safe strength of the web considered as a column, subjected to crippling, due to the shearing strains.

The Tables of Safe Loads of Beams and Channels are computed with regard to the safe unit stresses due to flexure, and with one or two exceptions, as indicated by dotted lines and accompanying footnotes, the lengths of spans tabulated are such that the limitation due to web crippling does not appear. The shearing stresses acting in the web of a beam may be considered to consist of two stresses of equal intensity acting at right angles to each other, and at angles of 45 degrees with the neutral axis. The intensity of each of these stresses is equal to the intensity of the vertical shear, which is a maximum at the points of support for uniform loading, and uniform throughout from the point of loading to the supports for a superimposed concentrated load at the centre.

The vertical shears for different systems of loading may be obtained by the use of moments in the usual way, and these are given for various cases on pages 136 to 139 inclusive.

The shearing stresses which act at angles of 45 degrees with the neutral axis are equivalent to compressive and tensile forces, and the former will tend to buckle the web, which should therefore be figured as composed of a series of columns of a length equal to its diagonal depth.

If c is the vertical depth of the web in the clear between the fillets which connect it with the flanges, the square of the length of the column to be considered will be 2c<sup>2</sup>.

Substituting this value for l2 in the formula for long columns

$$p = \frac{12000}{1 + \frac{1^2}{3000 \, t^2}}$$

we have

$$p = \frac{12000}{1 + \frac{c^2}{1500 \, t^2}}$$

in which

p = intensity of vertical shear, in pounds per square inch =

Total shear in pounds

dt.

c = depth of web in clear between fillets, in inches.

t = thickness of web, in inches.

d = depth of beam, in inches.

This formula is also applicable for computing the safe shearing stress in the webs of plate girders, in which case the length 1 is the vertical distance between centres of upper and lower rows of rivet holes connecting the webs and flanges.

The webs of plate girders should be reinforced by stiffening angles at points of support and concentrated loading, and in cases where the intensity of shear exceeds that given by the above formula the web should be provided with stiffeners.

The following tables have been prepared based upon the above formula for safe unit shearing stress in the webs of beams and channels.

## MAXIMUM SAFE LOADS FOR I-BEAMS OF ANY LENGTH AND CORRESPONDING MINIMUM SAFE SPANS BASED UPON CRIPPLING OF THE WEB.

For loads in pounds uniformly distributed including weight of beam.

Section Number	Depth of Beam.	Weight per Foot.	Maximum Safe Load,	Mini- mum Span.	Section Number	Depth of Beam.	Weight per Foot.	Maximum Safe Load.	Mini- mum Span.
	Inches.	Pounds.	Pounds.	Feet.		Inches.	Pounds.	Pounds.	Feet.
В 5	3	5.5 6.5 7.5	10644 16983 23884	1.7 1.1 .9	B105	12	50 55	168991 203806	3.2 2.8
В 9	4	7.5 8.5 9.5 10.5	15045 21809 29349 35847	2.1 1.6 1.2 1.1	B 53	15	42 45 50 55 60	85591 104200 142044 179929 213732	7.3 6.2 4.8 4.0 3.6
B 13	5	9.75 12.25 14.75	19773 37984 54380	2.6 1.5 1.2	B109	15	60 65 70	157484 195147 228658	5.5 4.6 4.1
B 17	6	12.25 14.75 17.25	24826 42634 59857	3.1 2.0 1.6	B113	15	75 80 80	265452 301820 240024	3.7 3.4 4.6
B 21	7	15 17.5 20	30192 47720 66478	3.7 2.5 1.9	DITO	10	85 90 95 100	275411 308939 344691 380169	4.2 3.9 3.6 3.4
B 25	8	18. 20.25 22.75 25.25	35925 52072 69914 87403	4.2 3.1 2.4 2.1	B 65	18	55 60 65 70	107758 152031 188299 224737	8.8 6.6 5.5 4.9
В 29	9	21 25 30 35	41992 69224 104631 139074	4.8 3.1 2.3 1.9	В 73	20	65 70 75	127592 178434 201484	9.6 7.3 6.7
В 33	10	25 30 35 40	48406 83739 120792 156930	5.4 3.4 2.6 2.2	B121	20	80 85 90 95 100	179940 210096 250558 285966 321253	8.7 7.7 6.6 6.0 5.5
B 41	12	31.5 35 40	62193 89412 125695	6.2 4.5 3.5	B 89	24	80 85 90	126012 163791 197821	14.7 11.8 10.1
B105	12	40 45	97469 133560	4.9 3.8			95 100	232873 268596	8.8 7.9

## MAXIMUM SAFE LOAD FOR STANDARD CHAN-NELS OF ANY LENGTH AND CORRESPOND-ING MINIMUM SAFE SPANS BASED UPON CRIPPLING OF THE WEB.

For loads in pounds uniformly distributed including weight of Channel.

_										
	ection umber	Depth of Channel.	Weight per Foot.	Maximum Load.	Mini- mum Span.	Section Number	Depth of Channel.	Weight per Foot.	Maximum Load.	Mini- mum Span.
		Inches.	Pounds.	Pounds.	Feet.		Inches.	Pounds.	Pounds.	Feet.
	C5	3	4 5 6	10692 17016 23909	1.1 0.8 .6	025	8	18.75 21.25	79348 96698	1.5 1.3
	C9	4	5.25 6.25	14032 20868	1.4 1.1	C29	9	13.25 15 20	28044 41483 77711	4.0 2.9 1.8
			7.25	28424	.9			25	115740	1.4
(	013	5	6.5 9 11.5	19231 34382 52036	1.6 1.1 .9	C33	10	15 20 25	30461 65360 102947	4.7 2.6 1.9
(	017	6	8 10.5	20024 38027	2.3	0.44	40	30 35	139563 173036	1.6
			13 15.5	55414 72401	1.1 1.0	C41	12	20.5 25 30	41173 73588 109976	5.5 3.5 2.6
(	021	7	9.75 12.25 14.75	22865 42273 59506	2.8 1.7 1.4			35 40	148961 184279	2.1 1.9
			17.25 19.75	78006 94532	1.2 1.1	C53	15	33 35 40	82528 93615 114450	5.4 4.9 4.3
C	25	8	11.25 13.75 16.25	25494 43638 61676	3.4 2.2 1.7			45 50 55	165466 203148 245311	3.2 2.8 2.5

### COEFFICIENTS FOR DEFLECTION IN INCHES FOR CAMBRIA SHAPES, USED AS BEAMS SUB-JECTED TO SAFE LOADS UNIFORMLY DISTRIBUTED.

Distance between	Coefficient for Fibre Stress of	Coefficient for Fibre Stress of	Distance between	Coefficient for Fibre Stress of	Coefficient for Fibre Stress of
Supports in feet.	16 000 lbs. per Square Inch.	12 500 lbs. per Square Inch.	Supports in Feet.	16 000 lbs. per Square Inch.	12 500 lbs. per Square Inch.
L	Н	H'	L	H	<b>H</b> ′
4	.265	.207	23	8.756	6.841
5	.414	.323	24	9.534	7.448
6	.596	.466	25	10.345	8.082
7	.811	.634	26	11.189	8.741
8 9	1.059	.828	27	12.066	9.427
	1.341	1.047	28	12.977	10.138
10	1.655	1.293	29	13.920	10.875
11	2.003	1.565	30	14.897	11.638
12	2.383	1.862	31	15.906	12.427
13	2.797	2.185	32	16.949	13.241
14	3.244	2.534	33	18.025	14.082
15	3.724	2.909	34	19.134	14.948
16	4.237	3.310	35	20.276	15.841
17	4.783	3.737	36	21.451	16.759
18	5.363	4.190	37	22.659	17.703
19	5.975	4.668	38	23.901	18.672
20	6.621	5.172	39	25.175	19.668
21	7.299	5.703	40	26.483	20.690
22	8.011	6.259			

The above coefficients are for use in obtaining the deflection of steel shapes subjected to transverse strain, under their uniformly distributed safe loads for extreme fibre stresses of 16 000 pounds and 12 500 pounds per square inch; the modulus of elasticity being 29 000 000.

To find the deflection of any shape that is symmetrical about its neutral axis under the above conditions of loading when used as a beam, such as I-Beams, Channels, etc., divide the coefficient in the table corresponding to the given span and fibre stress, by the depth of the beam in inches. The result will be the deflection in inches.

To find the deflection of any shape that is unsymmetrical about its neutral axis when used as a beam, under the above conditions of loading such as T-Bars, Angles, etc., divide the coefficient in the table corresponding to the given span and fibre stress by twice the distance of the most remote fibre from the neutral axis, expressed in inches.

If in construction, the beam is placed in position in the usual manner upon its end supports without special scaffolding or falsework between them, it will deflect somewhat by reason of its own weight, and upon the addition of external loading a further deflection will occur.

The deflections obtained as above described are the total deflections due to the weight of the beam itself and the superimposed safe load uniformly distributed.

Thus to find from the preceding table the deflection in inches for Cambria shapes used as beams under their safe loads uniformly distributed including the weight of the beam:

Let D = deflection in inches.

L = length between supports in feet.

H = coefficient for deflection from table for fibre stress of 16 000 pounds per square inch.

H' = coefficient for deflection from table for fibre stress of 12 500 pounds per square inch.

d = depth of beam in inches for symmetrical sections.

x<sub>1</sub> = distances in inches from neutral axis to most remote fibre for unsymmetrical sections.

### FOR SYMMETRICAL SECTIONS.

For fibre stress of 16 000 pounds per square inch  $D = \frac{H}{d}$ 

For fibre stress of 12 500 pounds per square inch  $D = \frac{H'}{d}$ 

### FOR UNSYMMETRICAL SECTIONS.

For fibre stress of 16 000 pounds per square inch  $D = \frac{H}{2x_1}$ 

For fibre stress of 12 500 pounds per square inch D =  $\frac{H'}{2x_1}$ 

### EXAMPLES.

Case I.—To find the deflection of a 9" I-Beam weighing 30 pounds per foot, for a span of 15 feet and a maximum fibre stress of 16 000 pounds per square inch, under its safe load uniformly distributed.

From the above table the deflection coefficient for this case is found to be 3.724, which divided by 9, the depth of the beam in inches, gives

.414, which is the required deflection in inches.

The safe load for this beam under the conditions named is 16 100 pounds including the weight of the beam itself as stated in the Tables of Safe Loads for Cambria I-Beams on page 79.

Case II.—To find the deflection of a  $6'' \times 4'' \times \frac{1}{2}''$  angle, supported at the ends on its short leg as a horizontal base, for a span of 9 feet and a maximum fibre stress of 16 000 pounds per square inch under

its safe load uniformly distributed including its own weight.

From the table of "Properties of Angles" on page 173 the distance x' from the neutral axis to the back of the shorter leg is found to be 1.99 inches, which subtracted from the length of long leg, 6 inches, gives 4.01 as the distance  $x_1$  from the neutral axis to the most remote fibre. From the above table the deflection coefficient for this case is found to be 1.341, which divided by 8.02, twice  $x_1$ , gives .167, which is the required deflection in inches.

Note.—For deflections of Beams, Channels and Z-Bars due to any central or uniform load see coefficients of deflection N and N' in the Tables of Properties relating to these sections and the accompanying

explanations.

For deflections of any symmetrical beams due to various systems of loading, see general formulæ and diagrams on pages 134 to 139 inclusive.

# TABLES OF SAFE LOADS FOR CAMBRIA SEC-TIONS USED AS BEAMS, AND SPACING FOR CAMBRIA I-BEAMS.

Pages 76 to 133 inclusive.

TABLES OF SAFE LOADS AND SPACINGS.

The tables of safe loads for Cambria I-Beams, Channels, Angles, T-Bars and Z-Bars, give the safe loads in pounds uniformly distributed for all usual spans based upon extreme fibre stresses of 16 000 pounds per square inch.

These loads include the weight of the steel shape itself, which should be deducted in order to obtain the external load that it will safely carry. In case the shape is used to support a floor, the weight of the steel together with that of the other portions of the floor construction, must be deducted in order to obtain the net live load which can be safely sustained. Weights of hollow tile floor arches and fireproofing material are given on page 57, to which should be added the weight of plastering, filling on top of arches and the weight of the material forming the surface of the floor, in order to obtain the dead load of materials in figuring fireproof floors, in addition to the weight of the steel.

A table of superimposed loads per square foot, exclusive of the weights of materials, in accordance with the usual practice for different classes of buildings, is given on page 56.

The tables of safe loads for Cambria sections used as beams and the tables for spacing of Cambria I-Beams are calculated on the assumption that proper provision has been made for preventing lateral deflection by means of tie-rods or other braces spaced at suitable distances apart; which for beams and channels should not exceed twenty times the flange width. In cases where intermediate lateral

support is not provided, the safe loads shown in the tables must be reduced, and for beams and channels the amount of this reduction can be determined by reference to the explanations and tables therefor on pages 62 and 63.

The thrust of floor arches, which is considerable, particularly in the case of long spans or distances between tie-rods, should be taken into account where it tends to produce lateral flexure of the floor beams.

Explanations of this and a formula for reducing the unit stresses from vertical loading, on account of the additional stresses caused by horizontal forces, are given on pages 58 to 61 inclusive.

In some instances the allowable deflection will govern the design rather than the transverse strength, as in the case of beams carrying plastered ceilings, in which the deflection should be limited to  $\frac{1}{30}$  inch per foot of span, or  $\frac{1}{360}$  of the distance between supports in order to avoid cracking the plaster.

This limit of deflection is indicated in the tables by full horizontal lines, the figures below which correspond to loads or spacings for the given spans that will produce greater deflections than the allowable limit for plastered ceilings.

The deflection limits of the Tables of Safe Loads have been calculated for the total loads, including the weight of the section used as a beam. The superimposed live load will not produce all of this deflection, and therefore the deflection limit of the tables includes an element of safety for the reason that the beams will be deflected, after being put in place, by their own weight and that of the floor materials before the plastering is applied.

In cases where the deflection limits the use of the beam for the safe loads corresponding to the fibre stresses of the tables, the beam may be used with a less load such as to produce only the allowable deflection. The lesser load corresponding to the limit of deflection may be obtained for any span from the Table of Safe Loads as follows:

$$W = \frac{W_s \times L^2}{L_1^2}$$

in which

- W = safe load in pounds for the limit of deflection for plastered ceilings =  $\frac{1}{360}$  of the span.
- $W_s$  = safe load of tables next above the line giving the limit of deflection.
- L = length of span in feet corresponding to W, from the table.
- $L_1 =$  length of span for the case under consideration.

This may also be expressed by the following:

### RULE.

Multiply the safe load next above the heavy line of the tables by the square of the corresponding span in feet and divide the product by the square of the required span. The result will be the required load corresponding to the limit of allowable deflection for plastered ceilings.

A Table of Deflections for Cambria shapes used as beams, subjected to their safe loads uniformly distributed, and accompanying explanations with examples, is given on pages 68 and 69.

TABLES OF SAFE LOADS FOR I-BEAMS AND CHANNELS.

Tables of Safe Loads for all sizes and weights of Cambria I-Beams and channels for the usual spans, expressed in feet, are given on pages 76 to 92 inclusive.

TABLES FOR SPACING OF CAMBRIA I-BEAMS.

Tables for spacing of Cambria I-Beams for a total load of 100 pounds per square foot including the weight of the beam, corresponding to spans from 4 to 36 feet, are given on pages 93 to 103 inclusive.

For any given size of beam the spacing or distances from centers to centers for different intensities of loading varies inversely as the load, so that the spacing for any intensity of loading may be found from the tabular spacing by proportion as stated in the notes at the foot of the tables.

## TABLES OF SAFE LOADS FOR ANGLES, T-BARS AND Z-BARS.

Tables of uniformly distributed safe loads for the usual sizes of angles, all sections of T-Bars and all sections of standard Z-Bars are given on pages 106 to 133. In these tables the safe loads for equal leg angles are given on the assumption that one of the legs of the angle is horizontal and the other leg vertical. In the case of angles with unequal legs the safe loads are given for both positions, that is: with the long leg vertical and with the short leg vertical.

The safe loads for T-Bars are given on the assumption that the flange is horizontal and the stem vertical, and for Z-Bars with the web vertical.

# EXAMPLES OF APPLICATION OF TABLES OF SAFE LOADS AND TABLES OF SPACING.

### EXAMPLE I.

What is the proper size of beam with a clear span of 24 feet to carry a superimposed load of 30 000 pounds uniformly distributed, the deflection to be such as not to crack a plastered ceiling?

From the Tables of Safe Loads for Cambria I-Beams, page 81, it is found that a 15-inch standard beam of this length, weighing 60 pounds per foot, will carry a gross load of 31 910 pounds, and the weight of the beam itself is  $60 \times 24 = 1440$  pounds. Thus the net load may be 30 470 pounds, so that this is the proper size for the conditions named, as its deflection is within the allowable limit, which is shown to be at a span of 30 feet as indicated by the horizontal line on the table.

Similarly it may be found from page 82, that a 15-inch special beam, of 60 pounds per foot, will more than suffice, but as this section is not regularly kept in stock the standard 15-inch 60-pound beam should be ordered if prompt delivery is wanted.

It may also be found from page 84, that an 18-inch 55-pound beam will amply suffice, and as this is both stiffer and lighter than the 15-inch 60-pound beams, it could be used with economy if otherwise suitable for the location.

### EXAMPLE II.

What is the safe load for an 8-inch standard I-Beam weighing 18.0

pounds per foot for a span of 20 feet, the deflection to be such as not to crack a plastered ceiling?

From the Tables of Safe Loads, page 78, it is found that the safe load for the beam in question is 7 580 pounds, but this value is below the line which indicates the span corresponding to the allowable limit of deflection.

Substituting the proper values in the formula for obtaining the reduced load corresponding to the allowable deflection, as given on page 72 we have

$$W = \frac{W_s \times L^2}{L_1^2} = \frac{9480 \times 16^2}{20^2} = 6067$$
 pounds,

which is the safe load required.

### EXAMPLE III.

Required the best arrangement of beams for the floor system of a building 40 feet wide x 88 feet deep to safely support a live load of 100 pounds per square foot, using 10-inch tile arches resting on 12-inch I-Beams.

The weight of the floor materials will be about 50 pounds per square foot, allowing 39 pounds for the arch and 11 pounds for the other materials, or a total load of 150 pounds per square foot to be carried by the beams.

From the Table of Spacing for I-Beams for a uniform load of 100 pounds per square foot, page 97, it is seen that  $12^{\prime\prime}$  standard I-Beams weighing  $31\frac{1}{2}$  pounds per foot and spaced 9.6 feet apart from center to center can be used with a span of 20 feet, and for a load of 150 pounds per square foot the spacing will be

$$\frac{9.6 \times 100}{150}$$
 = 6.4 feet.

This will require one row of interior columns lengthwise of building.

To support the beams at the center of the building will require a line of girder beams resting on the columns. Assume the columns 22 feet apart, thus dividing the building into 8 bays, four on each side of the center.

The load on each girder will be

$$\frac{40}{2} \times 22 \times 150 = 66\,000$$
 pounds.

From the Table of Safe Loads, page 81, it is found that this will require two 15-inch standard I-Beams, each weighing 60 pounds per foot.

On account of the advisability of spacing the floor beams equally, the arrangement outlined above would reduce their distances to be  $\frac{22}{4} = 5.5$  feet center to center, so that 10-inch I-Beams, weighing 35 pounds per foot, might be used for the body of the floor, as may be determined by referring to the Table of Spacings of Cambria I-Beams, page 96, and calculating as before, with the result that the allowable spacing for these conditions is found to be 5.2 feet. The 10-inch 35-pound beams under these conditions, will, however, deflect to the allowable limit for plastered ceilings, besides which they are heavier than the 12-inch 31.5-pound beams first considered, so that the latter will be the stiffer and more economical.

Although the load on the girder is not uniformly distributed, but concentrated at three points between the supports, the bending moment in this case will be the same as if the load were figured to be distributed uniformly, and for similar cases with different spacings the moments would be very nearly identical.

## TABLES OF MAXIMUM BENDING MOMENTS.

The tables of maximum bending moments for beams and channels given on pages 104 and 105 are useful in determining the proper section required to support one or more irregularly located concentrated loads or various arrangements of loads to which the tables of safe loads uniformly distributed will not apply.

The method used consists in computing the maximum bending moment in foot pounds resulting from the specified loading, the proper section corresponding to a fibre stress of 16 000 or 12 500 lbs. per square inch, being taken directly from the tables without further computation.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of beam.

		STANDARD I-BEAMS.										
Distance between	3 In	nch No	. В 5.		4 Inch	No. B 9						
in feet.	5.5	6.5	7.5	7.5	8.5	9.5	10.5					
	1bs.	1bs.	1bs.	1bs.	1bs.	1bs.	1bs.					
4	4410	4780	5180	7950	8470	9000	9520					
5	3530	3830	4140	6360	6780	7200	7610					
6	2940	3190	3450	5300	5650	6000	6350					
7 8	2520	2730	2960	4540	4840	5140	5440					
	2210	2390	2590	3980	4240	4500	4760					
9	1960	2130	2300	3530	3770	4000	4230					
	1770	1910	2070	3180	3390	3600	3810					
11	1600	1740	1880	2890	3080	3270	3460					
12	1470	1590	1730	2650	2820	3000	3170					
13	1360	1470	1590	2450	2610	2770	2930					
14	1260	1370	1480	2270	2420	2570	2720					
15	1180	1280	1380	2120	2260	2400	2540					
16	1100	1200	1290	1990	2120	2250	2380					
17	1040	1130	1220	1870	1990	2120	2240					
18	980	1060	1150	1770	1880	2000	2120					
19	930	1010	1090	1670	1780	1890	2000					
20	880	960	1040	1590	1690	1800	1900					
21	840	910	990	1510	1610	1710	1810					

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of beam.

		STA	NDAR	D I-B	EAMS.	
Distance between	5 I1	nch No.	B 13.	6 I	nch No. B	17.
supports	9.75	12.25	14.75	12.25	14.75	17.25
in feet.	1bs.	1bs.	1bs.	1bs.	1bs.	1bs.
4 5	12900	14520	16160	19370	21320	23280
	10320	11620	12930	15490	17050	18620
6 7 8 9	8600 7370 6450 5730 5160	9680 8300 7260 6460 5810	10770 9230 8080 7180 6460	12910 11070 9680 8610 7750	14210 12180 10660 9470 8530	15520 13300 11640 10350 9310
11	4690	5280	5880	7040	7750	8460
12	4300	4840	5390	6460	7110	7760
13	3970	4470	4970	5960	6560	7160
14	3680	4150	4620	5530	6090	6650
15	3440	3870	4310	5160	5680	6210
16	3220	3630	4040	4840	5330	5820
17	3030	3420	3800	4560	5020	5480
18	2870	3230	3590	4300	4740	5170
19	2720	3060	3400	4080	4490	4900
20	2580	2900	3230	3870	4260	4660
21	2460	2770	3080	3690	4060	4430
22	2340	2640	2940	3520	3880	4230
23	2240	2530	2810	3370	3710	4050
24	2150	2420	2690	3230	3550	3880
25	2060	2320	2590	3100	3410	3720
26 27 28 29	1980 1910	2230 2150	2490 2390	2980 2870 2770 2670	3280 3160 3050 2940	3580 3450 3330 3210

Safe loads below are figured for fibre stress of 16000 pounds per square inch and include weight of beam.

		STANDARD I-BEAMS.										
Distance between	7 In	ch No.	В 21.		8 Inch No. B 25.							
in feet.	15 1bs.	17.5 1bs.	20 1bs.	18.00 1bs.	20.25 1bs.	22.75 1bs.	25.25 1bs.					
<u>4</u> 5	27600 22080	29850 23880	32140 25710	37920 30330	40130 32100	42740 34190	45360 36290					
6 7 8 9	18400 15770 13800 12270 11040	19900 17060 14930 13270 11940	21430 18370 16070 14280 12860	25280 21670 18960 16850 15170	26750 22930 20060 17830 16050	28500 24420 21370 19000 17100	30240 25920 22680 20160 18140					
11 12 13 14 15	10040 9200 8490 7890	10860 9950 9190 8530 7960	11690 10710 9890 9180 8570	13790 12640 11670 10830 10110	14590 13380 12350 11470 10700	15540 14250 13150 12210 11400	16490 15120 13960 12960 12100					
16 17 18 19 20	7360 6900 6490 6130 5810 5520	7460 7020 6630 6280 5970	8030 7560 7140 6770 6430	9480 8920 8430 7980 7580	10030 9440 8920 8450 8030	10690 10060 9500 9000 8550	11340 10670 10080 9550 9070					
21 22 23 24 25	5260 5020 4800 4600 4420	5690 5430 5190 4980 4780	6120 5840 5590 5360 5140	7220 6890 6590 6320 6070	7640 7300 6980 6690 6420	8140 7770 7430 7120 6840	8640 8250 7890 7560 7260					
26 27 28 29	4250 4090 3940 3810	4590 4420 4260 4120	4940 4760 4590 4430	5830 5620 5420 5230	6170 5940 5730 5530	6580 6330 6110 5900	6980 6720 6480 6260					

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings  $=\frac{1}{360}$  span. Safe loads above dotted line are greater than safe loads for web crip-

pling as shown on pages 64 to 66 inclusive.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of beam.

Distance	STANDARD I-BEAMS.										
between	9	Inch l	No. B	29.	10 Inch No. B 33.						
supports in feet.	21	25	30	35	25	30	35	40			
	1bs.	1bs.	1bs.	1bs.	1bs.	1bs.	1bs.	1bs.			
8	25160	27240	30180	33120							
9	22370	24210	26830	29440							
10	20130	21790	24150	26500	26050	28620	31240	33850			
11	18300	19810	21950	24090	23680	26020	28400	30780			
12	16770	18160	20120	22080	21710	23850	26030	28210			
13	15480	16760	18570	20380	20040	22020	24030	26040			
14 15	14380	15570	17250	18930	18610	20450	22310	24180			
19	13420	14530	16100	17670	17360	19080	20830	22570			
16	12580	13620	15090	16560	16280	17890	19520	21160			
17	11840	12820	14200	15590	15320	16840	18380	19910			
18	11180	12110	13410	14720	14470	15900	17350	18810			
19	10590	11470	12710	13950	13710	15070	16440	17820			
20	10064	10900	12070	13250	13020	14310	15620	16930			
21	9590	10380	11500	12620	12400	13630	14880	16120			
22	9150	9910	10980	12050	11840	13010	14200	15390			
23	8750	9480	10500	11520	11320	12450	13580	14720			
24	8390	9080	10060	11040	10850	11930	13020	14110			
25	8050	8720	9660	10600	10420	11450	12500	13540			
26	7740	8380	9290	10190	10020	11010	12020	13020			
27	7460	8070	8940	9810	9650	10600	11570	12540			
28	7190	7780	8620	9460	9300	10220	11160	12090			
29	6940	7510	8330	9140	8980	9870	10770	11670			
30	6710	7260	8050	8830	8680	9540	10410	11280			
31	6490	7030	7790	8550	8400	9230	10080	10920			
32		• • • •			8140	8950	9760	10580			
33	• • • •	• • • • •	• • • •		7890	8670	9470	10260			

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of beam.

Distance		AND. SEA	ARD MS.	STA	RD-S BEAL				
between	12 I:	nch No	. В 41.	1	12 Inch No. B 105.				
supports in feet.	31.5	35	40	40	45	50	55		
111 1660,	1bs.	1bs.	1bs.	1bs.	1bs.	1bs.	1bs.		
10	38370	40580	43720	47810	50790	53930	57070		
11 12	34880 31970	36890 33820	39740 36430	43470 39840	46180 42330	49030	51880 47560		
13	29510	31220	33630	36780	39070	44940 41480	43900		
14	27400	28990	31230	34150	36280	38520	40760		
15	25580	27050	29140	31880	33860	35950	38040		
16	23980	25360	27320	29880	31750	33710	35670		
17	22570	23870	25720	28130	29880	31720	33570		
18	21310	22540	24290	26560	28220	29960	31700		
19	20190	21360	23010	25160	26730	28380	30040		
20	19180	20290	21860	23910	25400	26960	28530		
21	18270	19320	20820	22770	24190	25680	27170		
22	17440	18450	19870	21730	23090	24510	25940		
23	16680	17640	19010	20790	22080	23450	24810		
24	15990	16910	18220	19920	21160	22470	23780		
25	15350	16230	17490	19130	20320	21570	22830		
26	14760	15610	16810	18390	19540	20740	21950		
27	14210	15030	16190	17710	18810	19970	21140		
28	13700	14490	15610	17080	18140	19260	20380		
29 30	13230 12790	13990 13530	15070	16490 15940	17510 16930	18600 17980	19680 19020		
50	12/90	15550	14570	19940	10950	17900	19020		
31	12380	13090	14100	15420	16380	17400	18410		
32	11990	12680	13660	14940	15870	16850	17830		
33	11630	12300	13250	14490	15390	16340	17290		
34 35	11280 10960	11940 11590	$12860 \\ 12490$	14060 13660	14940 14510	15860 15410	16780 16300		
00	10300	11000	12400	19000	14010	10410	10000		
36	10660	11270	12140	13280	14110	14980	15850		

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of beam.

	STANDARD I-BEAM.											
Distance		15	Inch No. 1	B 53.								
between												
supports in feet.	42	45	50	55	60							
III 1660.	1bs.	1bs.	1bs.	1bs.	1bs.							
10	62830	64830	68750	72670	76600							
11	57120	58940	62500	66070	69630							
12	52360	54030	57290	60560	63830							
13 14	48330 44880	49870 46310	52890 49110	55900 51910	58920 54710							
15	41880	43220	45840	48450	51060							
10	41000	10000	40010	40100	01000							
16	39270	40520	42970	45420	47870							
17	36960	38140	40440	42750	45060							
18	34900	36020	38200	40370	42550							
19 20	33070 31410	34120 32420	36190 34380	38250 36340	40310 38300							
20	01410	0242U	94900	90940	90900							
21	29920	30870	32740	34610	36470							
22	28560	29470	31250	33030	34820							
23	27320	28190	29890	31600	33300							
24	26180	27010	28650	30280	31910							
25	25130	25930	27500	29070	30640							
26	24160	24940	26440	27950	29460							
27	23270	24010	25460	26920	28370							
28	22440	23150	24550	25960	27360							
29	21660	22360	23710	25060	26410							
30	20940	21610	22920	24220	25530							
31	20270	20910	22180	23440	24710							
32	19630	20260	21490	22710	23940							
33	19040	19650	20830	22020	23210							
34	18480	19070	20220	21370	22530							
35	17950	18520	19640	20760	21880							
36	17450	18010	19100	20190	21280							

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of beam.

	STANDARD-SPECIAL I-BEAM.								
Distance between		15	15 Inch No. B 109.						
supports	60	65	70	75	80				
in feet.	1bs.	1bs.	1bs.	1bs.	1bs.				
10	86610	90470	94390	98310	102230				
11	78740	82240	85810	89370	92940				
12	72180	75390	78660	81920	85190				
13	66630	69590	72610	75620	78640				
14	61870	64620	67420	70220	73020				
15	57740	60310	62920	65540	68150				
16	54130	56540	58990	61440	63890				
17	50950	53220	55520	57830	60140				
18	48120	50260	52440	54620	56790				
19	45590	47610	49680	51740	53810				
20	43310	45230	47190	49150	51120				
21	41240	43080	44950	46810	48680				
22	39370	41120	42900	44690	46470				
23	37660	39330	41040	42740	44450				
24	36090	37690	39330	40960	42600				
25	34650	36190	37750	39320	40890				
26	33310	34790	36300	37810	39320				
27	32080	33510	34960	36410	37860				
28	30930	32310	33710	35110	36510				
29	29870	31200	32550	33900	35250				
30	28870	30160	31460	32770	34080				
31	27940	29180	30450	31710	32980				
32	27070	28270	29500	30720	31950				
33	26250	27410	28600	29790	30980				
34	25470	26610	27760	28910	30070				
35	24750	25850	26970	28090	29210				
36	24060	25130	26220	27310	28400				

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of beam.

	STA	NDARI	)-SPEC	IAL I-E	BEAM.
Distance between		15	Inch No. 1	B 113.	
supports	80	85	90	95	100
in feet.	1bs.	1bs.	1bs.	1bs.	1bs.
	105.	ibs.	108.	ibs.	10S.
10	112230	116030	119960	123880	127800
11	102030	105490	109050	112620	116180
12	93520	96700	99960	103230	106500
13	86330	89260	92270	95290	98310
14	80160	82880	85680	88480	91280
15	74820	77360	79970	82580	85200
16	70140	72520	74970	77420	79870
17	66020	68260	70560	72870	75180
18	62350	64460	66640	68820	71000
19	59070	61070	63130	65200	67260
20	56110	58020	59980	61940	63900
21	53440	55250	57120	58990	60860
22	51010	52740	54530	56310	58090
23	48800	50450	52150	53860	55560
24	46760	48350	49980	51620	53250
25	44890	46410	47980	49550	51120
26	43170	44630	46140	47650	49150
27	41570	42980	44430	45880	47330
28	40080	41440	42840	44240	45640
29	38700	40010	41360	42720	44070
30	37410	38680	39990	41290	42600
31	36200	37430	38700	39960	41230
32	35070	36260	37490	38710	39940
33	34010	35160	36350	37540	38730
34	33010	34130	35280	36430	37590
35	32070	33150	34270	35390	36510
36	31170	32230	33320	34410	35500

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of beam.

	STANDARD I-BEAMS.										
Distance between	1	8 Inch	No. B	65.	20 I	20 Inch No. B 73.					
supports	55	60	65	70	65	70	75				
in feet.	1bs.	1bs.	1bs.	1bs.	1bs.	1bs.	1bs.				
10	94290	99770	104470	109180	124750	130110	135340				
11	85720	90700	94980	99250	113410	118280	123040				
12	78570	83140	87060	90980	103960	108430	112780				
13	72530	76740	80360	83980	95960	100090	104110				
14	67350	71260	74620	77990	89110	92940	96670				
15	62860	66510	69650	72790	83170	86740	90230				
16	58930	62360	65300	68240	77970	81320	84590				
17	55460	58650	61460	64220	73380	76540	79610				
18	52380	55430	58040	60660	69310	72280	75190				
19	49630	52510	54990	57460	65660	68480	71230				
20	47140	49880	52240	54590	62370	65060	67670				
21	44900	47510	49750	51990	59400	61960	64450				
22	42860	45350	47490	49630	56700	59140	61520				
23	40990	43380	45420	47470	54240	56570	58840				
24	39290	41570	43530	45490	51980	54210	56390				
25	37720	39910	41790	43670	49900	52040	54140				
26	36260	38370	40180	41990	47980	50040	52050				
27	34920	36950	38690	40440	46200	48190	50130				
28	33670	35630	37310	38990	44550	46470	48340				
29	32510	34400	36030	37650	43020	44870	46670				
30	31430	33260	34820	36390	41580	43370	45110				
31	30420	32180	33700	35220	40240	41970	43660				
32	29460	31200	32650	34120	38980	40660	42290				
33	28570	30230	31660	33080	37800	39430	41010				
34	27730	29340	30730	32110	36690	38270	39810				
35	26940	28510	29850	31190	35640	37170	38670				
36	26190	27710	29020	30330	34650	36140	37590				

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of beam.

	STANDARD-SPECIAL I-BEAM.									
Distance between	20 Inch No. B 121.									
supports in feet,	80	85	90	95	100					
	1bs.	1bs.	1bs.	1bs.	1bs.					
10	156410	160910	166140	171370	176600					
11	142190	146280	151040	155790	160540					
12 13	130340 120310	134090 123780	138450 127800	142810 131820	147160					
14	111720	114940	118670	122410	135840 126140					
15	104270	107270	110760	114250	117730					
16	97750	100570	103840	107100	110370					
17 18	92000 86890	94650 89390	97730 92300	100800 95200	103880 98110					
19	82320	84690	87440	90190	92950					
20	78200	80460	83070	85680	88300					
21	74480	76620	79110	81600	84090					
22 23	71090 68000	73140 69960	75520 72230	77890 74510	80270 76780					
24	65170	67050	69220	71400	73580					
25	62560	64360	66460	68550	70640					
	221.22	1								
26	60160	61890	63900	65910	67920					
27 28	57930 55860	59600 57470	61530 59340	63470 61200	65410 63070					
29	53930	55490	57290	59090	60900					
30	52140	53640	55380	57120	58870					
0.4	20120	F4040	F0F00	*****	N. COTTO					
31 32	50450 48880	51910 50280	53590	55280	56970					
32 33	47400	48760	51920 50350	53550 51930	55190 53510					
34	46000	47330	48860	50400	51940					
35	44690	45970	47470	48960	50460					
36	43450	44700	46150	47600	49050					

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of beam.

	STANDARD I-BEAM.										
Distance											
between		24	Inch No.	B 89.							
supports											
in feet.	80	85	90	95	95 100						
	1bs.	1bs.	1bs.	1bs.	1bs.						
10	185530	192700	198970	205240	211520						
11	168660	175180	180880	186590	192290						
12	154610	160580	165810	171040	176270						
13	142720	148230	153050	157880	162710						
14	132520	137640	142120	146600	151080						
15	123690	128460	132650	136830	141010						
16	115960	120430	124360	128280	132200						
17	109140	113350	117040	120730	124420						
18	103070	107050	110540	114020	117510						
19	97650	101420	104720	108020	111330						
20	92770	96350	99480	102620	105760						
21	88350	91760	94750	97740	100720						
22	84330	87590	90440	93290	96140						
23	80670	83780	86510	89240	91960						
24	77300	80290	82900	85520	88130						
25	74210	77080	79590	82100	84610						
26	71360	74110	76530	78940	81350						
27	68720	71370	73690	76020	78340						
28	66260	68820	71060	73300	75540						
29	63980	66450	68610	70770	72940						
30	61840	64230	66320	68410	70510						
31	59850	62160	64180	66210	68230						
32	57980	60220	62180	64140	66100						
33	56220	58390	60290	62200	64100						
34	54570	56680	58520	60370	62210						
35	53010	55060	56850	58640	60430						
36	51540	53530	55270	57010	58760						

Safe loads above dotted line are greater than safe loads for web crippling, as shown on pages 64 to 66 inclusive.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of channel.

		STANDARD CHANNELS.									
Distance between	3 In	ch N	o. C 5.	4 In	ch No.	C 9.	5 In	5 Inch No. C 13.			
supports	4	5	6	5.25	6.25	7.25	6.5	9	11.5		
in feet.	1bs.	1bs.	1bs.	1bs.	1bs.	1bs.	1bs.	1bs.	1bs.		
4 5	2910	3290	3680	5060	5570	6090	7910	9460	11100		
	2330	2630	2940	4050	4450	4870	6330	7570	8880		
6	$\frac{1940}{1660}$ $1450$	2190	2450	3370	3710	4060	5270	6310	7400		
7		1880	2100	2890	3180	3480	4520	5410	6340		
8		1640	1840	2530	2780	3050	3960	4730	5550		
9	1290	1460	1630	2250	2470	2510	3520	4210	4930		
	1160	1310	1470	2020	2230	2440	3160	3790	4440		
11	1060	1190	1340	1840	2020	2210	2880	3440	4040		
12	970	1100	1230	1690	1860	2030	2640	3150	3700		
13	890	1010	1130	1560	1710	1870	2430	2910	3410		
14	830	940	1050	1440	1590	1740	2260	2700	3170		
15	780	880	980	1350	1480	1620	2110	2520	2960		
16	730	820	920	1260	1390	1520	1980	2370	2770		
17	680	770	870	1190	1310	1430	1860	2230	2610		
18	650	730	820	1120	1240	1350	1760	2100	2470		
19	610	690	770	1060	1170	1280	1670	1990	2340		
20	580	660	740	1010	1110	1220	1580	1890	2220		
21	550	630	700	960	1060	1160	1510	1800	2110		
22	530	600	670	920	1010	1110	1440	1720	2020		
23	510	570	640	880	970	1060	1380	1650	1930		
24	480	550	610	840	930	1020	1320	1580	1850		
25	470	530	590	810	890	970	1270	1510	1780		

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of channel.

7.	STANDARD CHANNELS.											
Distance between	6	Inch	No. C	17.	7 Inch No. C 21.							
supports	8	10.5	13	15.5	9.75	12.25	14.75	17.25	19.75			
in feet.	1bs.	1bs.	1bs.	1bs.	1bs.	1bs.	1bs.	1bs.	1bs.			
4		13440	15400	17360	16070	18410	20700	22990	25280			
5		10750	12320	13890	12850	14730	16560	18390	20220			
6	7700	8960	10270	11570	10710	12280	13800	15330	16850			
7	6600	7680	8800	9920	9180	10520	11830	13140	14440			
8	5780	6720	7700	8680	8030	9210	10350	11490	12640			
9	5130	5970	6840	7720	7140	8180	9200	10220	11230			
10	4620	5380	6160	6940	6430	7370	8280	9200	10110			
11	4200	4890	5600	6310	5840	6700	7530	8360	9190			
12	3850	4480	5130	5790	5360	6140	6900	7660	8430			
13	3550	4130	4740	5340	4940	5670	6370	7070	7780			
14	3300	3840	4400	4960	4590	5260	5910	6570	7220			
15	3080	3580	4110	4630	4280	4910	5529	6130	6740			
16	2890	3360	3850	4340	4020	4600	5180	5750	6320			
17	2720	3160	3620	4080	3780	4330	4870	5410	5950			
18	2570	2990	3420	3860	3570	4090	4600	5110	5620			
19	2430	2830	3240	3650	3380	3880	4360	4840	5320			
20	2310	2690 2560	3080 2930	3470 3310	3210	3680 3510	3940	4380	5060 4810			
22	2100	2440	2800	3160	2920	3350	3760	4180	4600			
23	2010	2340	2680	3020	2790	3200	3600	4000	4400			
24	1930	2240	2570	2890	2680	3070	3450	3830	4210			
25	1850	2150	2460	2780	2570	2950	3310	3680	4040			

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of channel.

Distance	٠.	STA	MD.	ARI	CH	ANI	TEL:	5.	STANDARD CHANNELS.										
Distance between		8 Inc	h No.	C 25.		9 1	nch No	o. C 2	9,										
supports	11.25	13.75	16.25	18.75	21.25	13.25	15	20	25										
in feet.	1bs.	1bs.	1bs.	1bs.	1bs.	1bs.	1bs.	1bs.	1bs.										
4	21530	24000	26610	29230	31840	28040	30130	36020	41900										
. 5	17230	19200	21290	23380	25470	22430	24110		33520										
6	14360	16000	17740	19480	21230	18690	20090		27930										
7	12310	13710	15210	16700	18200	16020	17220		23940										
8 9	10770 9570	12000 10670	13310 11830	14610 12990	15920 14150	14020 12460	15070 13390		20950 18620										
10	8610	9600	10650	11690	12740	11220	12050		16760										
11	7830	8730	9680	10630	11580	10200	10960	13100	15240										
12	7180	8000	8870	9740	10610	9350	10040	12010	13970										
13	6630	7380	8190	8990	9800	8630	9270	11080											
14 15	6150 5740	6860 6400	7600 7100	8350 7790	9100 8490	8010 7480	8610 8040	10290	11970 11170										
10	0140	0400	1100	1100	0400	1400	0040	0000	11110										
16	5380	6000	6650	7310	7960	7010	7530	1	10470										
17	5070	5650	6260	6880	7490	6600	7090	8470	9860										
18	4790	5330	5910	6490	7080	6230	6700	8000	9310										
19 20	4530 4310	5050 4800	5600 5320	6150 5850	6700 6370	5900 5610	6340 6030	7580 7200	8820 8380										
21 22	4100	4570	5070	5570	6070	5340	5740	6860	7980										
23	3920 3750	4360 4170	4840 4630	5310 5080	5790 5540	5100 4880	5480 5240	6550 6260	7620 7290										
24	3590	4000	4440	4870	5310	4670	5020	6000	6980										
25	3450	3840	4260	4680	5090 l	4490	4820	5760	6700										

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of channel.

	s	STANDARD CHANNEL.								
Distance between		10 Inch No. C 33.								
in feet.	15	20	25	30	35					
	1bs.	1bs.	1bs.	1bs.	1bs.					
10	14270	16790	19410	22020	24640					
11	12970	15270	17640	20020	22400					
12	11890	14000	16170	18350	20530					
13	10980	12920	14930	16940	18950					
14	10190	12000	13860	15730	17600					
15	9510	11200	12940	14680	16430					
16	8920	10500	12130	13760	15400					
17	8390	9880	11420	12950	14490					
18	7930	9330	10780	12240	13690					
19	7510	8840	10220	11590	12970					
20	7130	8400	9700	11010	12320					
21	6790	8000	9240	10490	11730					
22	6490	7630	8820	10010	11200					
23	6200	7300	8440	9580	10710					
24	5940	7000	8090	9180	10270					
25	5710	6720	7760	8810	9860					
26	5490	6460	7460	8470	9480					
27	5280	6220	7190	8160	9130					
28	5100	6000	6930	7870	8800					
29	4920	5790	6690	7590	8500					
30	4760	5600	6470	7340	8210					

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of channel.

	STANDARD CHANNEL.								
Distance between	12 Inch No. C 41.								
supports in feet.	20.5	25	30	35	40				
	1bs.	1bs.	1bs.	1bs.	1bs.				
10	22780	25600	28740	31870	35010				
11	20700	23270	26120	28980	31830				
12	18980	21330	23950	26560	29180				
13	17520	19690	22110	24520	26930				
14 15	16270 15180	18290 17070	20530 19160	22770 21250	25010 23340				
19	19100	17070	19100	21200	20040				
16	14230	16000	17960	19920	21880				
17	13400	15060	16900	18750	20600				
18	12650	14220	15970	17710	19450				
19	11990	13470	15120	16780	18430				
20	11390	12800	14370	15940	17510				
21	10850	12190	13680	15180	16670				
22	10350	11640	13060	14490	15910				
23	9900	11130	12490	13860	15220				
24	9490	10670	11970	13280	14590				
25	9110	10240	11490	12750	14000				
26	8760	9850	11050	12260	13470				
27	8440	9480	10640	11810	12970				
28	8130	9140	10260	11380	12500				
29	7850	8830	9910	10990	12070				
30	7590	8530	9580	10620	11670				

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of channel.

P. 1		STANDARD CHANNEL.								
Distance between			15 Inch	No. C 53	3.					
supports in feet.	33	35	40	45	50	55				
	1bs.	1bs.	1bs.	1bs.	1bs.	1bs.				
10	44450	45500	49420	53350	57270	61190				
11	40410	41370	44930	48500	52060	55630				
12	37040	37920	41190	44460	47720	50990				
13	34190	35000	38020	41040	44050	47070				
14	31750	32500	35300	38100	40910	43710				
15	29630	30340	32950	35560	38180	40790				
16	27780	28440	30890	33340	35790	38240				
17	26150	26770	29070	31380	33690	35990				
18	24700	25280	27460	29640	31820	33990				
19	23400	23950	26010	28080	30140	32210				
20	22230	22750	24710	26670	28630	30590				
21	21170	21670	23540	25400	27270	29140				
22	20210	20680	22470	24250	26030	27810				
23	19330	19780	21490	23190	24900	26600				
24	18520	18960	20590	22230	23860	25500				
25	17780	18200	19770	21340	22910	24480				
26	17100	17500	19010	20520	22030	23530				
27	16460	16850	18310	19760	21210	22660				
28	15880	16250	17650	19050	20450	21850				
29	15330	15690	17040	18400	19750	21100				
30	14820	15170	16470	17780	19090	20400				

Proper distance in feet, center to center of Beams.

Maximum fibre stress 16 000 pounds per square inch.

Distance		STA	NDAI	RD I-	BEAR	MS.	
be ween supports in	3 In	nch No.	B 5.	4			
feet.	5.5 1bs.	6.5 1bs.	7.5 1bs.	7.5 1bs.	8.5 1bs.	9.5 1bs.	10.5 1bs.
4 5	11.0 7.1	12.0 7.7	12.9 8.3	19.9 12.7	21.2 13.6	22.5 14.4	23.8 15.2
6	4.9	5.3	5.8	8.8	9.4	10.0	10.6
7 8	3.6 2.8	3.9 3.0	4.2 3.2	6.5 5.0	6.9 5.3	7.3 5.6	7.8 5.9
9	2.2 1.8	2.4 1.9	$\frac{2.6}{2.1}$	3.9 3.2	4.2 3.4	4.4 3.6	4.7 3.8
11 12 13 14	1.5 1.2 1.0	1.6 1.3 1.1 1.0	1.7 1.4 1.2 1.1	2.6 2.2 1.9 1.6	2.8 2.4 2.0 1.7	3.0 2.5 2.1 1.8	3.1 2.6 2.3 1.9
15 16 17 18				1.4 1.2 1.1 1.0	1.5 1.3 1.2 1.0	1.6 1.4 1.2 1.1	1.7 1.5 1.3 1.2
19 20				• • • •	• • • •	1.0	1.1

For spacings below the heavy lines the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{360}$  span.

Spacings for other intensities of loading may be obtained from those in tables as follows:

 $\frac{\text{Required spacing} = \frac{\text{Intensity of loading from table}}{\text{New intensity of loading}} \times \text{Computed spacing from table}.$ 

Proper distance in feet, center to center of Beams. Maximum fibre stress 16 000 pounds per square inch.

Distance		STANI	DARD	I-BEA	MS.	
between supports	5 In	ich No. E	3 13.	6 Inc	h No. B	17.
in	9.75	12.25	14.75	12.25	14.75	17.25
feet.	1bs.	1bs.	1bs.	1bs.	1bs.	1bs.
4	32.2	36.3	40.4	48.4	53.3	58.2
5	20.6	23.2	25.9	31.0	34.1	37.2
6	14.3	16.1	18.0	21.5	23.7	25.9
7	10.5	11.9	13.2	15.8	17.4	19.0
8	8.1	9.1	10.1	12.1	13.3	14.5
9	6.4	7.2	8.0	9.6	10.5	11.5
10	5.2	5.8	6.5	7.7	8.5	9.3
11	4.3	4.8	5.3	6.4	7.0	7.7
12	3.6	4.0	4.5	5.4	5.9	6.5
13	3.1	3.4	3.8	4.6	5.0	5.5
14	2.6	3.0	3.3	4.0	4.4	4.8
15	2.3	2.6	2.9	3.4	3.8	4.1
16	2.0	2.3	2.5	3.0	3.3	3.6
17	1.8	2.0	2.2	2.7	3.0	3.2
18	1.6	1.8	2.0	2.4	2.6	2.9
19	1.4	1.6	1.8	2.1	2.4	2.6
20	1.3	1.5	1.6	1.9	2.1	2.3
21 22 23 24 25	1.2 1.1 1.0	1.3 1.2 1.1 1.0	1.5 1.3 1.2 1.1 1.0	1.8 1.6 1.5 1.3 1.2	1.9 1.8 1.6 1.5	2.1 1.9 1.8 1.6 1.5
26 27 28 29	• • • •	* * * * * * * * * * * * * * * * * * *	1.0	1.1 1.1 1.0	1.3 1.2 1.1 1.0	1.4 1.3 1.2 1.1

For spacings below the heavy lines the deflections will be greater than the allowable limit for plastered ceilings  $=\frac{1}{360}$  span. Spacings for other intensities of loading may be obtained from those in tables as

follows:

Required spacing =  $\frac{\text{Intensity of loading from table}}{\text{New intensity of loading}} \times \text{Computed spacing from table.}$ 

Proper distance in feet, center to center of Beams. Maximum fibre stress 16 000 pounds per square inch.

Distance		STA	NDA	RD I-	BEA	MS.	
between supports	7 In	ch No.	B 21.	8	Inch N	o. B 25	•
in feet.	15 1bs.	17.5 1bs.	20 1bs.	18.00 1bs.	20.25 1bs.	22.75 1bs.	25.25 1bs.
4	69.0	74.6	80.3	94.8	100.3	106.9	113.4
5	44.2	47.8	51.4	60.7	64.2	68.4	72.6
6	30.7	33.2	35.7	42.1	44.6	47.5	50.4
7	22.5	24.4	26.2	31.0	32.8	34.9	37.0
8	17.3	18.7	20.1	23.7	25.1	26.7	28.3
9 10	13.6	14.7	15.9	18.7	19.8	21.1	22.4
10	11.0	11.9	12.9	15.2	16.1	17.1	18.1
11	9.1	9.9	10.6	12.5	13.3	14.1	15.0
$\tilde{1}\tilde{2}$	7.7	8.3	8.9	10.5	11.1	11.9	12.6
13	6.5	7.1	7.6	9.0	9.5	10.1	10.7
14	5.6	6.1	6.6	7.7	8.2	8.7	9.3
15	4.9	5.3	5.7	6.7	7.1	7.6	8.1
16	4.3	4.7	5.0	5.9	6.3	6.7	7.1
17	3.8	4.1	4.4	5.2	5.6	5.9	6.3
18	3.4	3.7	4.0	4.7	5.0	5.3	5.6
19	3.1	3.3	3.6	4.2	4.4	4.7	5.0
20	2.8	3.0	3.2	3.8	4.0	4.3	4.5
21	2.5	2.7	2.9	3.4	3.6	3.9	4.1
22	2.3	2.5	2.7	3.1	3.3	3.5	3.7
23	2.1	2.3	2.4	2.9	3.0	3.2	3.4
24	1.9	2.1	2.2	2.6	2.8	3.0	3.1
25	1.8	1.9	2.1	2.4	2.6	2.7	2.9
26	1.6	1.8	1.9	2.2	2.4	2.5	2.7
27	1.5	1.6	1.8	2.1	2.2	2.3	2.5
28	1.4	1.5	1.6	1.9	2.0	2.2	2.3
29	1.3	1.4	1.5	1.8	1.9	2.0	2.2

For spacings above the dotted lines the safe loads for bending are greater than the safe loads for web crippling, as explained on pages 64 to 66 inclusive.

For spacings below the heavy lines the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{360}$  span.

Spacings for other intensities of loading may be obtained from those in tables as

follows:

Required spacing = Intensity of loading from table

New intensity of loading. × Computed spacing from table. New intensity of loading

Proper distance in feet, center to center of Beams. Maximum fibre stress 16 000 pounds per square inch.

Distance		ST	ANI	DAR	D I-F	BEA	MS.	
between supports	9	Inch I	No. B	29.	10	Inch :	No. B	33.
in feet,	21 lbs.	25 1bs.	30 1bs.	35 1bs.	25 1bs.	30 1bs.	35 1bs.	40 1bs.
8 9 10	31.5 24.9 20.1	34.1 26.9 21.8	37.7 29.8 24.1	41.4 32.7 26.5	26,0	28.6	31.2	33.9
11 12 13 14	16.6 14.0 11.9 10.3	18.0 15.1 12.9 11.1	20.0 16.8 14.3 12.3	21.9 18.4 15.7 13.5	21.5 18.1 15.4 13.3	23.7 19.9 16.9 14.6	25.8 21.7 18.5 15.9	28.0 23.5 20.0 17.3
16 17	7.9 7.0	9.7 8.5 7.5	9.4 8.4	11.8 10.4 9.2	11.6 10.2 9.0	12.7 11.2 9.9	13.9 12.2 10.8	15.0 13.2 11.7
18 19 20	6.2 5.6 5.0	6.7 6.0 5.4	7.5 6.7 6.0	7.3 6.6	8.0 7.2 6.5	8.8 7.9 7.2	9.6 8.7 7.8	9.4 8.5
21 22 23 24 25	4.6 4.2 3.8 3.5 3.2	4.9 4.5 4.1 3.8 3.5	5.5 5.0 4.6 4.2 3.9	6.0 5.5 5.0 4.6 4.2	5.9 5.4 4.9 4.5 4.2	6.5 5.9 5.4 5.0 4.6	7.1 6.5 5.9 5.4 5.0	7.7 7.0 6.4 5.9 5.4
26 27 28 29 30	3.0 2.8 2.6 2.4 2.2	3.2 3.0 2.8 2.6 2.4	3.6 3.3 3.1 2.9 2.7	3.9 3.6 3.4 3.2 2.9	3.9 3.6 3.3 3.1 2.9	4.2 3.9 3.7 3.4 3.2	4.6 4.3 4.0 3.7 3.5	5.0 4.6 4.3 4.0 3.8
31 32 33	2.1	<b>2.</b> 3	2.5	2.8	2.7 2.5 2.4	3.0 2.8 2.6	3.3 3.1 2.9	3.5 3.3 3.1

For spacings below the heavy lines the deflections will be greater than the allowable limit for plastered ceilings  $=\frac{1}{360}$  span. Spacings for other intensities of loading may be obtained from those in tables as

follows:

Required spacing =  $\frac{\text{Intensity of loading from table}}{\text{New intensity of loading}} \times \text{Computed spacing from table}.$ 

Proper distance in feet, center to center of Beams. Maximum fibre stress 16 000 pounds per square inch.

Distance between		ANDA BEAI		SPECIAL I-BEAM.				
supports	12 Iı	nch No.	B 41.	12 Inch No. B 105.				
in	31.5	35	40	40	45	50	55	
feet.	1bs.	1bs.	1bs.	1bs.	1bs.	1bs.	1bs.	
10	38.4	40.6	43.7	47.8	50.8	53.9	57.1	
11	31.7	33.5	36.1	39.5	42.0	44.6	47.2	
12	26.6	28.2	30.4	33.2	35.3	37.5	39.6	
13	22.7	24.0	25.9	28.3	30.1	31.9	33.8	
14	19.6	20.7	22.3	24.4	25.9	27.5	29.1	
15	17.1	18.0	19.4	21.3	22.6	24.0	25.4	
16	15.0	15.9	17.1	18.7	19.8	21.1	22.3	
17	13.3	14.0	15.1	16.5	17.6	18.7	19.7	
18	11.8	12.5	13.5	14.8	15.7	16.6	17.6	
19	10.6	11.2	12.1	13.2	14.1	14.9	15.8	
20	9.6	10.1	10.9	12.0	12.7	13.5	14.3	
21	8.7	9.2	9.9	10.8	11.5	12.2	12.9	
22	7.9	8.4	9.0	9.9	10.5	11.1	11.8	
23	7.3	7.7	8.3	9.0	9.6	10.2	10.8	
24	6.7	7.0	7.6	8.3	8.8	9.4	9.9	
25	6.1	6.5	7.0	7.7	8.1	8.6	9.1	
26	5.7	6.0	6.5	7.1	7.5	8.0	8.4	
27	5.3	5.6	6.0	6.6	7.0	7.4	7.8	
28	4.9	5.2	5.6	6.1	6.5	6.9	7.3	
29	4.6	4.8	5.2	5.7	6.0	6.4	6.8	
30	4.3	4.5	4.9	5.3	5.6	6.0	6.3	
31	4.0	4.2	4.5	5.0	5.3	5.6	5.9	
32	3.7	4.0	4.3	4.7	5.0	5.3	5.6	
33	3.5	3.7	4.0	4.4	4.7	5.0	5.2	
34	3.3	3.5	3.8	4.1	4.4	4.7	4.9	
35	3.1	3.3	3.6	3.9	4.1	4.4	4.7	
36	3.0	3.1	3.4	3.7	3.9	4.2	4.4	

For spacings below the heavy lines the deflections will be greater than the

allowable limit for plastered ceilings  $=\frac{1}{380}$  span. Spacings for other intensities of loading may be obtained from those in tables as

Required spacing =  $\frac{\text{Intensity of loading from table}}{\text{New intensity of loading}} \times \text{Computed spacing from table.}$ 

Proper distance in feet, center to center of Beams. Maximum fibre stress 16 000 pounds per square inch.

Distance	5	STAND	ARD I-	BEAM.	
between supports		15 I	nch No. B	53.	
in feet.	42	45	50	55	60
	1bs.	1bs.	1bs.	1bs.	1bs.
10	62.8	64.8	68.8	72.7	76.6
11	51.9	53.6	56.8	60.1	63.3
12	43.6	45.0	47.7	50.5	53.2
13	37.2	38.4	40.7	43.0	45.3
14	32.0	33.1	35.1	37.1	39.1
15	27.9	28.8	30.6	32.3	34.0
16	24.5	25.3	26.9	28.4	29.9
17	21.7	22.4	23.8	25.1	26.5
18	19.4	20.0	21.2	22.4	23.6
19	17.4	18.0	19.0	20.1	21.2
20	15.7	16.2	17.2	18.2	19.1
21	14.2	14.7	15.6	16.5	17.4
22	13.0	13.4	14.2	15.0	15.8
23	11.9	12.3	13.0	13.7	14.5
24	10.9	11.3	11.9	12.6	13.3
25	10.1	10.4	11.0	11.6	12.3
26	9.3	9.6	10.2	10.8	11.3
27	8.6	8.9	9.4	10.0	10.5
28	8.0	8.3	8.8	9.3	9.8
29	7.5	7.7	8.2	8.6	9.1
30	7.0	7.2	7.6	8.1	8.5
31	6.5	6.7	7.2	7.6	8.0
32	6.1	6.3	6.7	7.1	7.5
33	5.8	6.0	6.3	6.7	7.0
34	5.4	5.6	5.9	6.3	6.6
35	5.1	5.3	5.6	5.9	6.3
36	4.8	5.0	5.3	5.6	5.9

For spacings below the heavy lines the deflections will be greater than the allowable limit for plastered ceilings  $= \frac{1}{360}$  span. Spacings for other intensities of loading may be obtained from those in tables as

follows:

Required spacing =  $\frac{\text{Intensity of loading from table}}{\text{New intensity of loading}} \times \text{Computed spacing from table}.$ 

Proper distance in feet, center to center of Beams. Maximum fibre stress 16000 pounds per square inch.

Distance		SPEC	AL I-B	EAM.	
between supports		15 Iı	nch No. B	109.	
in	60	65	70	75	80
feet.	1bs.	1bs.	1bs.	1bs.	1bs.
10	86.6	90.5	94.4	98.3	102.2
11	71.6	74.8	78.0	81.2	84.5
12	60.1	62.8	65.5	68.3	71.0
13	51.3	53.5	55.9	58.2	60.5
14	44.2	46.2	48.2	50.2	52.2
15	38.5	40.2	41.9	43.7	45.4
16	33.8	35.3	36.9	38.4	39.9
17	30.0	31.3	32.7	34.0	35.4
18	26.7	27.9	29.1	30.3	31.6
19	24.0	25.1	26.1	27.2	28.3
20	21.7	22.6	23.6	24.6	25.6
21	19.6	20.5	21.4	22.3	23.2
22	17.9	18.7	19.5	20.3	21.1
23	16.4	17.1	17.8	18.6	19.3
24	15.0	15.7	16.4	17.1	17.7
25	13.9	14.5	15.1	15.7	16.4
26	12.8	13.4	14.0	14.5	15.1
27	11.9	12.4	12.9	13.5	14.0
28	11.0	11.5	12.0	12.5	13.0
29	10.3	10.8	11.2	11.7	12.2
30	9.6	10.1	10.5	10.9	11.4
31	9.0	9.4	9.8	10.2	10.6
32	8.5	8.8	9.2	9.6	10.0
33	8.0	8.3	8.7	9.0	9.4
34	7.5	7.8	8.2	8.5	8.8
35	7.1	7.4	7.7	8.0	8.3
36	6.7	7.0	7.3	7.6	7.9

For spacings below the heavy lines the deflections will be greater than the allowable limit for plastered ceilings  $=\frac{1}{360}$  span. Spacings for other intensities of loading may be obtained from those in tables as

follows:

Intensity of loading from table Computed spacing from table. Required spacing = New intensity of loading

Proper distance in feet, center to center of Beams. Maximum fibre stress 16 000 pounds per square inch.

Distance										
between supports		15 In	nch No. B	113.						
in	80	85	90	95	100					
feet.	1bs.	1bs.	1bs.	1bs.	1bs.					
10	112.2	116.0	120.0	123.9	127.8					
11	92.8	95.9	99.1	102.4	105.6					
12	77.9	80.6	83.3	86.0	88.7					
13	66.4	68.7	71.0	73.3	75.6					
14	57.3	59.2	61.2	63.2	65.2					
15	49.9	51.6	53.3	55.1	56.8					
16	43.8	45.3	46.9	48.4	49.9					
17	38.8	40.2	41.5	42.9	44.2					
18	34.6	35.8	37.0	38.2	39.4					
19	31.1	32.1	33.2	34.3	35.4					
20	28.1	29.0	30.0	31.0	31.9					
21	25.4	26.3	27.2	28.1	29.0					
22	23.2	24.0	24.8	25.6	26.4					
23	21.2	21.9	22.7	23.4	24.2					
24	19.5	20.1	20.8	21.5	22.2					
25	18.0	18.6	19.2	19.8	20.4					
26	16.6	17.2	17.7	18.3	18.9					
27	15.4	15.9	16.5	17.0	17.5					
28	14.3	14.8	15.3	15.8	16.3					
29	13.3	13.8	14.3	14.7	15.2					
30	12.5	12.9	13.3	13.8	14.2					
31	11.7	12.1	12.5	12.9	13.3					
32	11.0	11.3	11.7	12.1	12.5					
33	10.3	10.7	11.0	11.4	11.7					
34	9.7	10.0	10.4	10.7	11.1					
35	9.2	9.5	9.8	10.1	10.4					
36	8.7	9.0	9.3	9.6	9.9					

For spacings below the heavy lines the deflections will be greater than the allowable limit for plastered ceilings  $=\frac{1}{360}$  span. Spacings for other intensities of loading may be obtained from those in tables as

follows:

Intensity of loading from table.

New intensity of loading 

Computed spacing from table. Required spacing =

Proper distance in feet, center to center of Beams. Maximum fibre stress 16 000 pounds per square inch.

Distance	STANDARD I-BEAMS.											
between supports	1	8 Inch	No. B 6	5.	20 In	ch No.	B 73.					
in	55	60	65	70	65	70	75					
feet.	1bs.	1bs.	1bs.	1bs.	1bs.	1bs.	1bs.					
10	94.3	99.8	104.5	109.2	124.7	130.1	135.3					
11	77.9	82.5	86.3	90.2	103.1	107.5	111.9					
12	65.5	69.3	72.6	75.8	86.6	90.4	94.0					
13	55.8	59.0	61.8	64.6	73.8	77.0	80.1					
14	48.1	50.9	53.3	55.7	63.6	66.4	69.1					
15	41.9	44.3	46.4	48.5	55.4	57.8	60.2					
16	36.8	39.0	40.8	42.6	48.7	50.8	52.9					
17	32.6	34.5	36.2	37.8	43.2	45.0	46.8					
18	29.1	30.8	32.2	33.7	38.5	40.2	41.8					
19	26.1	27.6	28.9	30.2	34.6	36.0	37.5					
20	23.6	24.9	26.1	27.3	31.2	32.5	33.8					
21	21.4	22.6	23.7	24.8	28.3	29.5	30.7					
22	19.5	20.6	21.6	22.6	25.8	26.9	28.0					
23	17.8	18.9	19.7	20.6	23.6	24.6	25.6					
24	16.4	17.3	18.1	19.0	21.7	22.6	23.5					
25	15.1	16.0	16.7	17.5	20.0	20.8	21.7					
26	13.9	14.8	15.5	16.2	18.5	19.2	20.0					
27	12.9	13.7	14.3	15.0	17.1	17.8	18.6					
28	12.0	12.7	13.3	13.9	15.9	16.6	17.3					
29	11.2	11.9	12.4	13.0	14.8	15.5	16.1					
30	10.5	11.1	11.6	12.1	13.9	14.5	15.0					
31	9.8	10.4	10.9	11.4	13.0	13.5	14.1					
32	9.2	9.7	10.2	10.7	12.2	12.7	13.2					
33	8.7	9.2	9.6	10.0	11.5	11.9	12.4					
34	8.2	8.6	9.0	9.4	10.8	11.3	11.7					
35	7.7	8.1	8.5	8.9	10.2	10.6	11.0					
36	7.3	7.7	8.1	8.4	9.6	10.0	10.4					

Spacings for other intensities of loading may be obtained from those in tables as follows:

Required spacing = Intensity of loading from table.

New intensity of loading × Computed spacing from table.

Proper distance in feet, center to center of Beams. Maximum fibre stress 16 000 pounds per square inch.

Distance		SPECI	AL I-BEAM.					
between supports		20 I	nch No. B	121.				
in	80	85	90	95	100			
feet.	1bs.	1bs.	1bs.	1bs.	1bs.			
10	156.4	160.9	166.1	171.4	176.6			
11	129.3	133.0	137.3	141.6	145.9			
12	108.6	111.7	115.4	119.0	122.6			
13	92.5	95.2	98.3	101.4	104.5			
14	79.8	82.1	84.8	87.4	90.1			
15	69.5	71.5	73.8	76.2	78.5			
16	61.1	62.9	64.9	66.9	69.0			
17	54.1	55.7	57.5	59.3	61.1			
18	48.3	49.7	51.3	52.9	54.5			
19	43.3	44.6	46.0	47.5	48.9			
20	39.1	40.2	41.5	42.8	44.1			
21	35.5	36.5	37.7	38.9	40.0			
22	32,3	33.2	34.3	35.4	36.5			
23	29.6	30.4	31.4	32.4	33.4			
24	27.2	27.9	28.8	29.8	30.7			
25	25.0	25.7	26.6	27.4	28.3			
26	23.1	23.8	24.6	25.4	26.1			
27	21.5	22.1	22.8	23.5	24.2			
28	19.9	20.5	21.2	21.9	22.5			
29	18.6	19.1	19.8	20.4	21.0			
30	17.4	17.9	18.5	19.0	19.6			
31	16.3	16.7	17.3	17.8	18.4			
32	15.3	15.7	16.2	16.7	17.2			
33	14.4	14.8	15.3	15.7	16.2			
34	13.5	13.9	14.4	14.8	15.3			
35	12.8	13.1	13.6	14.0	14.4			
36	12.1	12.4	12.8	13.2	13.6			

Spacings for other intensities of loading may be obtained from those in tables as follows:

Required spacing = Intensity of loading from table.

New intensity of loading 

Computed spacing from table.

Proper distance in feet, center to center of Beams. Maximum fibre stress 16 000 pounds per square inch.

Distance	STANDARD I-BEAM.											
between supports		24 I	nch No. B	89.								
in	80	85	90	95	100							
feet.	1bs.	1bs.	1bs.	1bs.	1bs.							
10	185.5	192.7	199.0	205.2	211.5							
11	153.3	159.3	164.4	169.6	174.8							
12	128.8	133.8	138.2	142.5 $121.4$ $104.7$	146.9							
13	109.8	114.0	117.7		125.2							
14	94.7	98.3	101.5		107.9							
15	82.5	85.6	88.4	91.2	94.0							
16	72.5	75.3	77.7	80.2	82.6							
17	64.2	66.7	68.8	71.0	73.2							
18	57.3	59.5	61.4	63.3	65.3							
19	51.4	53.4	55.1	56.9	58.6							
20	46.4	48.2	49.7	51.3	52.9							
21	42.1	43.7	45.1	46.5	48.0							
22	38.3	39.8	41.1	42.4	43.7							
23	35.1	36.4	37.6	38.8	40.0							
24	32.2	33.5	34.5	35.6	36.7							
25	29.7	30.8	31.8	32.8	33.8							
26	27.4	28.5	29.4	30.4	31.3							
27	25.5	26.4	27.3	28.2	29.0							
28	23.7	24.6	25.4	26.2	27.0							
29	22.1	22.9	23.7	24.4	25.2							
30	20.6	21.4	22.1	22.8	23.5							
31	19.3	20.1	20.7	21.4	22.0							
32	18.1	18.8	19.4	20.0	20.7							
33	17.0	17.7	18.3	18.8	19.4							
34	16.0	16.7	17.2	17.8	18.3							
35	15.1	15.7	16.2	16.8	17.3							
36	14.3	14.9	15.4	15.8	16.3							

For spacings above the dotted lines the safe loads for bending are greater than the safe loads for web crippling, as explained on pages 64 to 66 inclusive.

Spacings for other intensities of loading may be obtained from those in tables as

follows:

Required spacing = Intensity of loading from table New intensity of loading × Computed spacing from table.

# MAXIMUM BENDING MOMENTS IN FOOT POUNDS FOR CAMBRIA I-BEAMS.

Sec	tion	Depth	Weight	Maximum Mom		Section	Depth	Weight	Maximum Mom	Bending ents.
	m-	of	per	Foot P	ounds.	Num-	of	per	Foot P	ounds.
	er.	Beam,	Foot.	Fibre	Fibre	ber,	Beam.	Foot.	Fibre	Fibre
		Dough,	1000,	Stress	Stress	501,	Doulli,	1000,	Stress	Stress
		Inches,	Dounds	16 000 lbs. per Sq. In.			Inches.	Pounds.	per Sq. In.	12 500 lbs.
	[	THURES.	Pounds.	per 64. III.	per sq. III.		11101168,	rounus.	per oq. III.	per Sq. In.
В	5	3	5.5	2270	1770	B105	12	50	67470	52710
Ъ	65		6.5	2400	1880	D100	12	55	71330	
	66	66						99	(1990	55730
	**		7.5	2530	1980	B 53	15	42	78530	61350
В	9	4	7.5	4000	3130	D 00	66	45	81070	63330
ע	"	"	8.5	4270	3330	66	66	50	86000	67190
	66	66				66	66			
	66	66	9.5	4530	3540	66	66	55	90800	70940
	**	**	10.5	4800	3750	"	"	60	95730	74790
В	13	E	9.75	6400	5000	D100	15	60	108270	84580
D	10	5 "				B109	10	65		
	66	66	12.25	7200	5630	"	66	60	113070	88330
		**	14.75	8130	6350		66	70	118000	92190
D	17	6	12.25	9730	7600	66	66	75	122930	96040
D	16	0 "				66	6.6	80	127730	99790
	66	66	14.75	10670	8330	DATE	4 P	00	440070	400500
	••	**	17.25	11600	9060	B113	15	80	140270	109580
В	21	7	15	13870	10830	66	1	85	145070	113330
D	κ1 ((	66	15			66	66	90	150000	117190
	66	66	17.5	14930	11670	66	66	95	154800	120940
	**	**	20	16130	12600	66	66	100	159730	124790
В	25	8	18	18930	14790	D 05	4.0	P P	1.48080	00000
ъ	11	0	20.25		15630	B 65	18	55	117870	92080
	66	66		20000		66	66	60	124670	97400
	66	66	22.75	21330	16670	66 1	66	65	130530	101980
		**	25.25	22670	17710	66	66	70	136530	106670
В	29	9	21	25200	19690	70 M/O	00	ar	4 = 2000	404000
D	11	9	25	27200	21250	B 73	20	65	156000	121880
	66	- 66				66	66	70	162670	127080
	66	66	30	30130	23540	66	66	75	169200	132190
	1	.,	35	33070	25830	j				
В	33	10	25	32530	25420	B121	20	80	195470	152710
Д	00	10	$\frac{20}{30}$	35730	27920	6.6	66	85	201200	157190
	66	66				66	66	90	207730	162290
	66	- 66	35	39070	30520	66	66	95	214270	167400
	**	- "	40	42270	33020	66	66	100	220800	172500
D	41	12	31.5	48000	37500					
Б	41	12	35	50670	39580	B 89	24	80	231870	181150
	66	- 66				D 00	"	85	240930	188230
		•	40	54670	42710	66	66	90	248670	194270
D1	05	12	40	59730	46670	66	66	95	256530	200420
ום	.00	12	45	63470	49580	66	6.	100	264400	
			40	00470	40000 1		1	100	×01100	200000

# MAXIMUM BENDING MOMENTS IN FOOT POUNDS FOR CAMBRIA CHANNELS.

0 1	Depth	epth Weight Maximum Bending		9.4	Depth	377.:.1.4	Maximum	Bending nents.	
Section Num-	of	Weight		Pounds.	Section Num-	of	Weight		ounds.
ber	Chan-	per Foot.	Fibre	Fibre	ber.	Chan-	per Foot.	Fibre	Fibre
DOL	nel.	1000.	Stress	Stress	DO1.	nel.	F 000,	Stress	Stress
	Inches.	Pounds.	per Sq. In.	12 500 lbs. per Sq. In.		Inches.	Pounds.		12 500 lbs. per Sq. In.
		- Journal	por bq. III,	por eq. m.			- TOWNER,	por oq. 11.	por bq. III,
C 5	3	4	1470	1150	C25	8	18.75	14670	11460
"	"	5	1600	1250	"	"	21.25	15870	12400
66	66	6	1870	1460			1021100	20010	12100
					029	9	13.25	14000	10940
C 9	4	5.25	2530	1980	46	66	15	15070	11770
66	66	6.25	2800	2190	66	66	20	18000	14060
66	66	7.25	3070	2400	66	66	25	20930	16350
İ									
C13	5	6.5	4000	3130	C33	10	15	17870	13960
66	66	9	4670	3650	66	66	20	20930	16350
66	"	11.5	5600	4380	66	66	25	24270	18960
					66	66	30	27470	21460
C17	6	8	5730	4480	66	66	35	30800	24060
66	66	10.5	6670	5210					
66	66	13	7730	6040	C41	12	20.5	28530	22290
44	66	15.5	8670	6770	66	66	25	32000	25000
004	-	0 1011	0000	2010	66	66	30	35870	28020
021	7	9.75	8000	6250	66	66	35	39870	31150
66	"	12.25	9200	7190	66		40	43730	34170
66	66	14.75	10400	8130	ara	45	00	FF600	10110
66	66	17.25	11470	8960	C53	15	33	55600	43440
	•••	19.75	12670	9900	66	66	35	56930	44480
025	8	11.25	10800	8440	66	66	40 45	61730 66670	48230 52080
11	"	13.75	12000	9380	66	66	50	71600	55940
66	66	16.25	13330	10420	66	66	55	76530	59790
1	- 1	10.20	10000	10450			00	10000	00100

### EQUAL LEGS.

### NEUTRAL AXIS PARALLEL TO EITHER LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



-1.	Section No. A 11.										
Distance between		$1\frac{1}{2}'' \times 1\frac{1}{2}''$									
supports in	½'/	$\frac{1}{8}''$   $\frac{3}{16}''$   $\frac{1}{4}''$   $\frac{5}{16}''$   $\frac{3}{8}''$   $\frac{7}{16}''$									
feet.	1.3 lbs. per ft.	1.8 lbs. per ft.	2.4 lbs. per ft.	2.9 lbs. per ft.	3.4 lbs. per ft.	3.9 lbs. per ft.					
2 3	390 260	560 370	720 480	860 580	1010 670	1140 760					
4	190	280	360	430	500	570					
5	150	220	290	350	400	460					
6 7 8 9	130 110 100 90	190 160 140 120	240 200 180 160	290 250 220 190	340 290 250 220	380 330 290 250					

	Section No. A 13.									
Distance between		$1\frac{3}{4}$ x $1\frac{3}{4}$								
supports in	3// 16	1//	5// 16	3//	$\frac{7}{16}$	$\frac{1}{2}$				
feet.	2.2 lbs.	2.8 lbs.	3.4 lbs.	4.0 lbs.	4.6 lbs.	5.1 lbs.				
	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.				
2	770	990	1200	1400	1600	1780				
3	510	660	800	940	1060	1190				
4	380	500	600	700	800	890				
5	310	400	480	560	640	710				
6	260	330	400	470	530	590				
7	220	280	340	400	460	510				
8	190	250	300	350	400	450				
9	170	220	270	310	350	400				
10	150	200	240	280	320	360				

D:-1	Section No. A 15.									
Distance between		2'' x 2''								
supports in	3// 16//	$\frac{3}{16}''$   $\frac{1}{4}''$   $\frac{5}{16}''$   $\frac{3}{8}''$   $\frac{7}{16}''$   $\frac{1}{2}''$								
feet.	2.5 lbs. per ft.	3.2 lbs. per ft.	4.0 lbs. per ft.	4.7 lbs. per ft.	5.3 lbs. per ft.	6.0 lbs. per ft.				
2 3 4 5	1020 680 510 410	1320 880 660 530	1600 1070 800 640	1870 1250 940 750	2130 1420 1070 850	2380 1590 1190 950				
6 7 8 9	340 290 250 230 200	440 380 330 290 260	530 460 400 360 320	620 540 470 420 370	710 610 530 470 430	790 680 600 530 480				

#### EQUAL LEGS.

### NEUTRAL AXIS PARALLEL TO EITHER LEG.



Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.

	Section No. A 41.							
Distance between supports in	$2\frac{1}{4}'' \times 2\frac{1}{4}''$							
feet.	3//	1//	5/1/ 16	3//	<u>7</u> //			
	2.8 lbs.	3.7 lbs.	4.5 lbs.	5.3 lbs.	6.1 lbs.			
	per ft.	per ft.	per ft.	per ft.	per ft.			
2	1300	1690	2060	2410	2750			
3	870	1120	1370	1610	1830			
4	650	840	1030	1210	1380			
5	520	670	820	960	1100			
6	430	560	690	800	920			
7	370	480	590	690	790			
8	320	420	510	600	690			
9	290	380	460	540	610			
10	260	340	410	480	550			
11	240	310	370	440	500			
12	220	280	340	400	460			

Distance		\$	Section	No. A	17.		
between		i de-	$2\frac{1}{2}''$	$x 2\frac{1}{2}''$			
supports	3//	1//	$\frac{5}{16}$ //	3//	$\frac{7}{16}$	$\frac{1}{2}''$	9//
in feet.	3.1 lbs. per ft.	4.1 lbs. per ft.	5.0 lbs. per ft.	5.9 lbs. per ft.	6.8 lbs. per ft.	7.7 lbs. per ft.	8.5 lbs. per ft.
2 3 4 5	1610 1080 810 650	2100 1400 1050 840	2570 1710 1290 1030	3020 2010 1510 1210	3450 2300 1720 1380	3860 2580 1930 1550	4260 2840 2130 1710
6 7 8	540 460 400	700 600 530	860 730 640	1010 860 760	1150 990 860	1290 1100 970	$\begin{array}{r} 1420 \\ 1220 \\ \hline 1070 \end{array}$
8 9 10	360 320	470 420	570 510	670 600	770 690	860 770	950 850
11 12	290 270	380 350	470 430	550 500	630 580	. 700 640	780 710

### EQUAL LEGS.

### NEUTRAL AXIS PARALLEL TO EITHER LEG.

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Safe loads below are figured for fibre stress of  $16\,000$  pounds per square inch and include weight of angle.

	Section No. A 43.								
Distance between supports in	2 <sup>3</sup> / <sub>4</sub> // x 2 <sup>3</sup> / <sub>4</sub> //								
feet.	3//	$\frac{1}{4}$ //	5 // 16	3//	7/16	1//			
10000	3.4 lbs.	4.5 lbs.	5.6 lbs.	6.6 lbs.	7.6 lbs.	8.5 lbs.			
	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.			
2	1970	2570	3140	3700	4230	4740			
3	1310	1710	2090	2460	2820	3160			
4	980	1280	1570	1850	2110	2370			
5	790	1030	1260	1480	1690	1900			
67	660	860	1050	1230	1410	1580			
	560	730	900	1060	1210	1360			
8 9 10	490 440 390	570 510	790 700 630	920 820 740	1060 940 850	1190 1050 950			
11	360	470	570	670	770	860			
12	330	430	520	620	710	790			

Distance	Section No. A 19.										
between		3'' x 3''									
supports	1//	$\frac{5}{16}$	3//	$\frac{7}{16}$	$\frac{1}{2}''$	$\frac{9}{16}''$	5//	$\frac{116}{16}$			
in feet.	4.9 lbs. per ft.	6.1 lbs. per ft.	7.2 lbs. per ft.	8.3 lbs. per ft.	9.4 lbs. per ft.	lbs. per ft.	lbs. per ft.	12.5 lbs. per ft.			
2	3080	3770	4440	5090	5720	6320	6910	7480			
3	2050	2510	2960	3390	3810	4210	4610	4990			
4	1540	1890	2220	2540	2860	3160	3450	3740			
5	1230	1510	1780	2040	2290	2530	2760	2990			
6	1030	1260	1480	1700	1910	2110	2300	2490			
7	880	1080	1270	1450	1 <b>6</b> 30	1810	1970	2140			
8	770	940	1110	1270	1430	1580	1730	1870			
9	680	840	990	1130	1270	1410	1540	1660			
10	620	750	890	1020	1140	1260	1380	1500			
11	560	690	810	930	1040	1150	1260	1360			
12	510	630	740	850	950	1050	1150	1250			

EQUAL LEGS.

Section No. A 21.

NEUTRAL AXIS PARALLEL TO EITHER LEG. Safe loads below are figured for fibre stress of 16 000 pounds per

Safe loads below are ngured for fibre stress of 10000 pounds p square inch and include weight of angle.

I	

Distance					$3\frac{1}{2}$ ''	$x \ 3\frac{1}{2}$	11				
between	$\frac{5}{16}$	3//	$\frac{7}{16}$	$\frac{1}{2}''$	$\frac{9}{16}''$	<u>5</u> //	$\frac{11}{16}$	3//	$\frac{13}{16}$	7//	
supports in feet.	7.2 lbs. per ft.	8.5 lbs. per ft.	9.8 lbs. per ft.	lbs. per ft.	12.4 lbs. per ft.	13.6 lbs. per ft.	14.8 lbs. per ft.	16.0 lbs. per ft.	17.1 lbs. per ft.	18.3 lbs. per ft.	
2 3 4 5	5200 3470 2600 2080	6140 4100 3070 2460	7050 4700 3530 2820	7940 5290 3970 3180	8800 5860 4400 3520	9630 6420 4810 3850	10440 6960 5220 4180	11230 7490 5620 4490	12010 8000 6000 4800	12760 8510 6380 5110	
6 7 8 9 10	1730 1490 1300 1160 1040	2050 1760 1540 1370 1230	2350 2020 1760 1570 1410	2650 2270 1980 1760 1590	2930 2510 2200 1950 1760	3210 2750 2410 2140 1930	3480 2980 2610 2320 2090	3740 3210 2810 2500 2250	4000 3430 3000 2670 2400	4250 3650 3190 2840 2550	
11 12 13 14 15	950 870 800 740 690	1120 1020 950 880 820	1280 1180 1090 1010 940	1440 1320 1220 1130 1060	1600 1470 1350 1260 1170	1750 1600 1480 1380 1280	1900 1740 1610 1490 1390	2040 1870 1730 1610 1500	2180 2000 1850 1720 1600	2320 2130 1960 1820 1700	
16	650	770	880	990	1100	1200	1310	1400	1500	1600	
				Sec	ction	No.	A 23	3,			
Distance					4''	x 4'	/				
between supports	$\frac{5}{16}$	3//	$\frac{7}{16}$	$\frac{1}{2}''$	$\frac{9}{16}$ //	$\frac{5}{8}$ //	$\frac{1}{1}\frac{1}{6}$	3//	$\frac{1}{1}\frac{3}{6}''$	7//	
in feet.	8.2 lbs. per ft.	9.8 lbs. per ft.	lbs. per ft.	12.8 lbs. per ft.	14.3 lbs. per ft.	15.7 lbs. per ft.	17.1 lbs. per ft.	18.5 lbs. per ft.	19.9 lbs. per ft.	21.2 lbs. per ft.	
2	6870	8120	9340	10530	11690	12810	13910	14980	16030	17060	

Distance													
between supports	5//	$\frac{3}{8}$ //	$\frac{7}{16}$	1//	$\frac{9}{16}''$	$\frac{5}{8}$ //	$\frac{11}{16}$	$\frac{3}{4}''$	$\frac{13}{16}''$	7//			
in feet.	8.2 lbs. per ft.	9.8 lbs. per ft.	11.3 lbs. per ft.	12.8 lbs. per ft.	14.3 lbs. per ft.	15.7 lbs. per ft.	17.1 lbs. per ft.	18.5 lbs. per ft.	19.9 lbs. per ft.	21.2 lbs. per ft.			
2 3 4 5	6870	8120	9340	10530	11690	12810	13910	14980	16030	17060			
3	$\frac{4580}{3430}$	5420 4060	6230 4670	7020 5270	7790 5840	8540 6410	9270 6960	9990 7490	10690 8020	11370 8530			
5	2750	3250	3740	4210	4670	5130	5560	5990	6410	6820			
6 7 8 9 10	2290 1960 1720 1530 1370	2710 2320 2030 1810 1620	3120 2670 2340 2080 1870	3510 3010 2630 2340 2110	3900 3340 2920 2600 2340	4270 3660 3200 2850 2560	4640 3970 3480 3090 2780	4990 4280 3740 3330 3000	5340 4580 4010 3560 3210	5690 4870 4260 3790 3410			
11	1250	1480	1700	1910	2130	2330	2530	2720	2910	3100			
12	1140	1350	1560	1760	1950	2140	2320	2500	2670	2840			
13	1060	1250	1440	1620	1800	1970	2140	2300	2470	2620			
14 15	980 920	1160 1080	1340 1250	1500 1400	1670 1560	1830 1710	1990 1860	$\frac{2140}{2000}$	$\frac{2290}{2140}$	$\frac{2440}{2270}$			
16	860	1020	1170	1320	1460	1600	1740	1870	2000	2130			

17 18

### SAFE LOADS IN POUNDS UNIFORMLY DIS-TRIBUTED FOR CAMBRIA ANGLES.

#### EQUAL LEGS.

#### NEUTRAL AXIS PARALLEL TO EITHER LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.

Distance	Section No. A 45.													
between				$4\frac{1}{2}$ // x $4\frac{1}{2}$	2//									
supports	$\frac{5}{16}$ //	$\frac{3}{8}$ / /	$\frac{7}{16}$ "	$\frac{1}{2}''$	$\frac{9}{16}$ "	<u>5</u> //	$\frac{11}{16}$							
in feet.	9.3 lbs.	11.0 lbs.	12.8 lbs.	14.5 lbs.	16.2 lbs.	17.8 lbs.	19.5 lbs.							
	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.							
2	8760	10380	11960	13490	14990	16460	17890							
2345	5840	6920	7970	9000	10000	10970	11930							
4	4380	5190	5980	6750	7500	8230	8950							
5	3510	4150	4780	5400	6000	6580	7160							
6	2920	3460	3990	4500	5000	5490	5960							
6 7 8 9	2500	2970	3420	3860	4280	4700	5110							
8	2190	2600	2990	3370	3750	4120	4470							
9	1950	2310	2660	3000	3330	3660	3980							
10	1750	2080	2390	2700	3000	3290	3580							
11	1590	1890	2170	2450	2730	2990	3250							
12	1460	1730	1990	2250	2500	2740	2980							

	Section No. A 47.											
Distance between			5" >	5"								
supports in	3//	7//	$\frac{1}{2}''$	9 // 16	5//	11/1/ 16						
feet.	12.3 lbs.	14.3 lbs.	16.2 lbs.	18.1 lbs.	20.0 lbs.	21.8 lbs.						
	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.						
2	12910	14900	16830	18720	20570	22380						
3	8610	9930	11220	12480	13710	14920						
4	6460	7450	8410	9360	10280	11190						
5	5170	5960	6730	7490	8230	8950						
6	4310	4960	5610	6240	6860	7460						
7	3690	4260	4810	5350	5880	6390						
8	3230	3720	4210	4680	5140	5600						
9	2870	3310	3740	4160	4570	4970						
10	2580	2980	3370	3740	4110	4480						
11	2350	2710	3060	3400	3740	4070						
12	2150	2480	2800	3120	3430	3730						
13	1990	2290	2590	2880	3160	3440						
14	1850	2130	2400	2670	2940	3200						
15	1720	1990	2240	2500	2740	2980						
16	1610	1860	2100	2340	2570	2800						
17	1520	1750	1980	2200	2420	2630						
18	1440	1660	1870	2080	2290	2490						

### EQUAL LEGS.

### NEUTRAL AXIS PARALLEL TO EITHER LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



	Section No. A 27.													
Distance					6/	'' x 6	,,							
between														
sup-	3/1	$\frac{7}{16}$	$\frac{1}{2}$	$\frac{9}{16}$ //	<u>5</u> //	$\frac{1}{1}\frac{1}{6}''$	3//	$\frac{13}{16}$ //	7//	$\frac{15}{16}$	1′′			
ports														
in feet.	14.9 lbs. per ft.	17.2 lbs. per ft.	19.6 lbs. per ft.	21.9 lbs. per ft.	24.2 lbs. per ft.	26.5 lbs. per ft.	28.7 lbs. per ft.	31.0 lbs. per ft.	33.1 lbs. per ft.	35.3 lbs. per ft.	37.4 lbs. per ft.			
2	18820 12550	21720 14480	24610 16400	27420 18280	30170 20120	32880 21920	35540 23690	38150 25430	40720 27150	43240 28830	45720 30480			
2345	9410 7530	10860 8690	12300 9840	13710 10970	15090 12070	16440 13150	17770 14220	19080 15260	20360 16290	21620 17300	22860 18290			
6 7 8 9 10	6270 5380 4700 4180 3760	7240 6210 5430 4830 4340	8200 7030 6150 5470 4920	9140 7830 6850 6090 5480	10060 8620 7540 6710 6030	10960 9390 8220 7310 6580	11850 10150 8890 7900 7110	12720 10900 9540 8480 7630	13570 11630 10180 9050 8140	14410 12360 10810 9610 8650	15240 13060 11430 10160 9140			
11 12 13 14 15	3420 3140 2900 2690 2510	3950 3620 3340 3100 2900	4470 4100 3790 3520 3280	4990 4570 4220 3920 3660	5490 5030 4640 4310 4020	5980 5480 5060 4700 4380	6460 5920 5470 5080 4740	6940 6360 5870 5450 5090	7400 6790 6260 5820 5430	7860 7210 6650 6180 5770	8310 7620 7030 6530 6100			
16	2350	2720	3080	3430	3770	4110	4440	4770	5090	5410	5720			
17 18	$\frac{2210}{2090}$	$\frac{2560}{2410}$	$\frac{2900}{2730}$	3230 3050	3550 3350	$\frac{3870}{3650}$	$\frac{4180}{3950}$	4490 4240	4790 4520	5090 4810	5380 5080			
19 20	1980 1880	$\frac{2290}{2170}$	2590 2460	$2890 \\ 2740$	3180 3020	3460 3290	3740 3550	4020 3820	4290 4070	4550 4320	4810 4570			
21 22	1790 1710	2070 1970	2340 2240	2610 2490	2870 2740	3130 2990	3390 3230	3630 3470	3880 3700	4120 3930	4350 4160			

### EQUAL LEGS.

#### NEUTRAL AXIS PARALLEL TO EITHER LEG.

Safe loads below are figured for fibre stress of  $16\,000$  pounds per square inch and include weight of angle.



Section No. A 35.													
				//	′′ x 8	8					Distance between		
1\frac{1}{8}''	116"	1''	15/1	7/1/8	13//	3//	$\frac{1}{1}\frac{1}{6}$	5//	9/16	1// 2//	sup-		
lbs.	<b>54.0</b> lbs. per ft.	51.0 lbs. per ft.	48.1 lbs. per ft.	45.0 lbs. per ft.	42.0 lbs. per ft.	38.9 lbs. per ft.	35.8 lbs. per ft.	32.7 lbs. per ft.	29.6 lbs. per ft.	26.4 lbs. per ft.	in feet.		
	44450 35560	42120 33700	39760 31810	37370 29900	34950 27960	32490 25990	30000 24000	27470 21980	24910 19920	22310 17850	4 5		
0 26710 0 23370 0 20780	29630 25400 22220 19760 17780	28080 24070 21060 18720 16850	26510 22720 19880 17670 15910	24920 21360 18690 16610 14950	23300 19970 17480 15530 13980	21660 18570 16250 14440 13000	20000 17140 15000 13330 12000	18310 15700 13740 12210 10990	16600 14230 12450 11070 9960	14880 12750 11160 9920 8930	6 7 8 9 10		
0 15580 0 14380 0 13360	16160 14820 13680 12700 11850	15320 14040 12960 12030 11230	14460 13250 12240 11360 10600	13590 12460 11500 10680 9970	12710 11650 10750 9990 9320	11820 10830 10000 9280 8660	10910 10000 9230 8570 8000	9990 9160 8450 7850 7330	9060 8300 7660 7120 6640	8110 7440 6870 6380 5950	11 12 13 14 15		
11000 10390 9840	11110 10460 9880 9360 8890	10530 9910 9360 8870 8420	9940 9360 8840 8370 7950	9340 8790 8310 7870 7470	8740 8220 7770 7360 6990	8120 7650 7220 6840 6500	7500 7060 6670 6320 6000	6870 6460 6100 5780 5490	6230 5860 5530 5240 4980	5580 5250 4960 4700 4460	16 17 18 19 20		
8500	8470 8080 7730	8020 7660 7330	7570 7230 6920	7120 6800 6500	6660 6350 6080	6190 5910 5650	5710 5450 5220	5230 4990 4780	4740 4530 4330	4250 4060 3880	21 22 23		
7480	7410 7110	7020 6740	6630 6360	6230 5980	5830 5590	5420 5200	5000 4800	4580 4400	4150 3980	3720 3570	24 25		
6930 6680 6450	6840 6590 6350 6130 5930	6480 6240 6020 5810 5620	5890 5680 5480 5300	5750 5540 5340 5160 4980	5380 5180 4990 4820 4660	5000 4810 4640 4480 4330	4620 4440 4290 4140 4000	4230 4070 3920 3790 3660	3830 3690 3560 3440 3320	3430 3310 3190 3080 2980	26 27 28 29 30		
600 600 600 600 600 600 600 600 600 600	296 254 222 197 177 161 148 136 127 118 111 104 98 93 88 77; 74 71: 684 659 633 613	28080 24070 21060 18720 16850 15320 14040 12960 12030 11230 10530 9910 9360 8870 8420 8020 7660 7330 7020 6740 6480 6240 6020 5810	26510 22720 19880 17670 15910 14460 13250 12240 11360 10600 9940 9360 8840 8370 7950 7570 7230 6920 6630 6360 6120 5890 5680 5480	24920 21360 18690 16610 14950 13590 12460 11500 10680 9970 9340 8790 8310 7870 7470 7120 6800 6230 5980 5750 5340 5340 5160	23300 19970 17480 15530 13980 12710 11650 10750 9990 9320 8740 8220 7770 7360 6990 6660 6350 5830 5590 5380 4990 4820	21660 18570 16250 14440 13000 11820 10830 10000 9280 8660 8120 7650 7220 6840 6500 5910 5650 5200 5000 4810 4640 4480	20000 17140 15000 13330 12000 10910 10000 9230 8570 8000 7500 7660 6670 6320 6000 5710 5450 5220 5000 4800 4620 4440 4290 4140	18310 15700 13740 12210 10990 9990 9160 8450 7850 7330 6870 6460 6100 5780 4990 4780 4580 4400 4230 4070 3920 3790	16600 14230 12450 11070 9960 9060 8300 7660 7120 6640 6230 5860 5530 5240 4980 4740 4530 4330 4150 3980 3869 3560 3560 3440	14880 12750 11160 9920 8930 8110 7440 6870 6380 5950 5250 4960 4700 4460 4250 4060 3880 3720 3570 3430 3190 3080	67890 10 1123145 1671890 212 223 245 26789		

### UNEQUAL LEGS. NEUTRAL AXIS PARALLEL TO LONG LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.

Distance	Se	ction	No.	A 1	21.	Section No. A 123.						
between		2/	$^{\prime}$ x $1\frac{3}{8}$	3//		$2'' \times 1\frac{1}{2}''$						
sup-	$\frac{3}{16}$ //	$\frac{1}{4}$	$1\frac{5}{6}$	$\frac{3}{8}$ / /	T6''	1// 8	$\frac{3}{16}$	$\frac{1}{4}$	$\frac{5}{16}$	$\frac{3}{8}$ //	T6"	
ports	2.1	2.7	3.3	3.9	4.4	1.5	2.2	2.8	3.4	4.0	4.6	
in feet.	lbs. per ft.	lbs. per ft.	lbs. per ft.	lbs. per ft.	lbs. per ft.	lbs. per ft.	lbs. per ft.	lbs. per ft.	lbs. per ft.	lbs. per ft.	lbs. per ft.	
0		600	760	880	1000	400	580	740	000	1050	1190	
23	$\frac{510}{340}$	620 420	500	590	670	270	380	740 500	900 600	700	800	
4	260	310	380	440	500	200	290	370	450	520	600	
5	200	250	300	350	400	160	230	300	360	420	480	
6	170	210	250	290	330	130	190	250	300	350	400	
6 7 8	150	180	220	250	290	110	160	210	260	300	340	
8	130	160	190	220	250	100	140	190	230	260	300	

	Se	ction	No.	A 19	Section No. A 127.						
Distance		$2\frac{1}{2}$	′′ x 1	$\frac{1}{4}$ //		$2\frac{1}{2}$ // x $1\frac{1}{2}$ //					
between	$\frac{3}{16}$ / /	$\frac{1}{4}$	$\frac{5}{16}$ //	3//	$\frac{7}{16}$	3// 16	$\frac{1}{4}$	$\frac{5}{16}$	3//	7/1	
supports in feet.	2.3 lbs. per ft.	3.0 lbs. per ft.	3.7 lbs. per ft.	4.4 lbs. per ft.	5.0 lbs. per ft.	2.5 lbs. per ft.	3.2 lbs. per ft.	4.0 lbs. per ft.	4.7 lbs. per ft.	5.3 lbs. per ft.	
2 3	440 290	530 <b>3</b> 50	640 430	750 500	860 570	590 390	760 510	930 620	1080 720	1230 820	
4	220	260	320	380	430	300	380	460	540	620	
5	170	210	260	300	340	240	300	370	430	490	
6 7 8	150 120 110	180 150 130	210 180 160	250 210 190	290 250 210	200 170 150	250 220 190	310 260 230	360 310 270	410 350 310	

	No. A	161.	Section No. A 91.								
Distance	$2\frac{1}{2}$ "	$1\frac{3}{4}$			$2\frac{1}{2}''$	x 2''					
between	3//	$\frac{1}{4}$ //	3//	$\frac{1}{4}$ //	$\frac{5}{16}$ //	3// 8	$\frac{7}{16}$	$\frac{1}{2}''$	19/1		
in feet.	2.6	3.4	2.8	3.7	4.5	5.3	6.1	6.8	7.6		
	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.		
	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.		
2	800	1040	1050	1360	1650	1930	2200	2460	2720		
3	540	690	700	900	1100	1290	1470	1640	1810		
4	400	520	520	680	830	970	1100	1230	1360		
5	320	420	420	540	660	770	880	990	1090		
6	270	350	350	450	550	640	730	820	910		
7	230	300	300	390	470	550	630	700	780		
8	200	260	260	340	410	480	550	620	680		

### UNEQUAL LEGS.

### NEUTRAL AXIS PARALLEL TO LONG LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



	Se	ction	No.	A 19	28.	Section No. A 129.					
Distance between		$2\frac{3}{4}$	′′ x 1	$\frac{1}{2}$				3′′ 2	x 2"		
sup-	3//	1//	$\frac{5}{16}$	3//	$\frac{7}{16}$ "	3 // 16	1//	5/1/ 16	3//	$\frac{7}{16}$	$\frac{1}{2}$
ports in feet.	2.6 lbs. per ft.	3.4 lbs. per ft.	4.2 lbs. per ft.	5.0 lbs, per ft.	5.7 lbs. per ft.	3.1 lbs. per ft.	4.1 lbs. per ft.	5.0 lbs. per ft.	5.9 lbs. per ft.	6.8 lbs. per ft.	7.7 lbs. per ft.
2 3 4	600 400 300	770 520 390	940 620 470	1100 730 550	1250 830 630	1070 710 530	1390 920 690	1690 1120 840	1980 1320 990	2260 1510 1130	2530 1690 1260
5 6	240	310 260	370 310	370	500 420	430 360	550 460	670 560	790 660	900 750	840
7 8 9 10	170 150 130 120	220 190 170 150	270 230 210 190	310 270 240 220	360 310 280 250	310 270 240 210	400 350 310 280	480 420 370 340	570 500 440 400	650 560 500 450	720 630 560 510
11 12	110 100	140 130	170 160	200 180	230 210	190 180	250 230	310 280	360 330	410 380	460 420

D: 1	Section No. A 93.												
Distance between				3'' x 2½	"								
supports in feet.	1//	$\frac{5}{16}$	3//	7 17	1//	9//	5//						
III 1000.	4.5 lbs. per ft.	5.6 lbs. per ft.	6.6 lbs. per ft.	7.6 lbs. per ft.	8.5 lbs. per ft.	9.5 lbs. per ft.	10.4 lbs. per ft.						
2 3 4 5	2160 1440 1080 860	2640 1760 1320 1050	3100 2060 1550 1240	3540 2360 1770 1420	3970 2650 1980 1590	4380 2920 2190 1750	4780 3190 2390 1910						
6	720	880	1030	1180	1320	1460	1590						
7	620	750	880	1010	1130	1250	1370						
8 9 10	540 480 430	660 590 530	770 690 620	890 790 710	990 880 790	1100 970 880	1200 1060 960						
11 12	390 360	480 440	560 520	640 590	720 660	800 730	870 800						

### UNEQUAL LEGS.

### NEUTRAL AXIS PARALLEL TO LONG LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



n' .	Section No. A 151.												
Distance between		3½'' x 2''											
supports	1//	$\frac{5}{16}$	3//	$\frac{7}{16}$	$\frac{1}{2}''$	196''	5//						
in feet.	4.5 lbs. per ft.	5.6 lbs. per ft.	6.6 lbs. per ft.	7.6 lbs. per ft.	8.5 lbs. per ft.	9.5 lbs. per ft.	10.4 lbs. per ft.						
2 3 4 5	1410 940 710 560	1720 1150 860 690	2020 1340 1010 810	2300 1540 1150 920	2580 1720 1290 1030	2860 1900 1430 1140	3130 2080 1560 1250						
6 7 8 9	470 400 350 310 280	570 490 430 380 340	580 500 450 400	770 660 580 510 460	860 740 650 570 520	950 820 710 630 570	1040 890 780 690 630						
11 12	260 240	310 290	370 340	420 380	470 430	520 480	570 520						

Distance				Sec	tion N	o. A 9	95.		
between sup-					$3\frac{1}{2}$ '' x	$2\frac{1}{2}''$			
ports	1//	$\frac{5}{16}$	3//	$\frac{7}{16}$	$\frac{1}{2}$	<u>9</u> //	<u>5</u> //	$\frac{1}{16}''$	3//
in feet.	4.9 lbs. per ft.	6.1 lbs. per ft.	7.2 lbs. per ft.	8.3 lbs. per ft.	9.4 lbs. per ft.	10.4 lbs. per ft.	11.5 lbs. per ft.	12.5 lbs. per ft.	13.4 lbs. per ft.
2 3 4 5	2200 1460 1100 880	2690 1790 1340 1080	3160 2110 1580 1260	3610 2410 1810 1450	4050 2700 2030 1620	4480 2990 2240 1790	4890 3260 2450 1960	5300 3530 2650 2120	5700 3800 2850 2280
6 7 8 9	730 630 550 490 440	900 770 670 600 540	1050 900 790 700 630	1200 1030 900 800 720	1350 1160 1010 900 810	1490 1280 1120 1000 900	1630 1400 1220 1090 980	1770 1510 1320 1180 1060	1900 1630 1420 1270 1140
11 12	400 370	490 450	570 530	660 600	740 680	810 750	890 820	960 880	1040 950

### UNEQUAL LEGS.

### NEUTRAL AXIS PARALLEL TO LONG LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



				Se	ction	No.	A 9	7.		
Distance					$3\frac{1}{2}$	′′ x 3	//			
between	5 // 16	3//	7 1 6	$\frac{1}{2}$	$\frac{9}{16}$	<u>5</u> //	$\frac{11}{16}$	3//	13// 16	7/1
in feet.	6.6	7.9	9.1	10.2	11.4	12.5	13.6	14.7	15.8	16.8
	lbs.	lbs.	lbs.	lbs,	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.
	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.
2	3850	4540	5200	5840	6460	7070	7660	8230	8790	9350
3	2570	3030	3470	3900	4310	4710	5110	5490	5860	6230
4	1930	2270	2600	2920	3230	3530	3830	4120	4400	4670
5	1540	1820	2080	2340	2590	2830	3060	3290	3520	3740
6	1280	1510	1730	1950	2150	2360	2550	2740	2930	3120
7	1100	1300	1490	1670	1850	2020	2190	2350	2510	2670
8	960	1130	1300	1460	1620	1770	1910	2060	2200	2340
10	860	1010	1160	1300	1440	1570	1700	1830	1950	2080
	770	910	1040	1170	1290	1410	1530	1650	1760	1870
11	700	830	950	1060	1180	1290	1390	1500	1600	1700
12	640	760	870	970	1080	1180	1280	1370	1470	1560
13	590	700	800	900	990	1090	1180	1270	1350	1440
14	550	650	740	830	920	1010	1090	1180	1260	1340

				Se	ction	No.	A 9	9.		
Distance				,						
between	5 // 16	3//	7/1	$\frac{1}{2}$	$\frac{9}{16}$	<u>5</u> //	$\frac{1}{1}\frac{1}{6}^{\prime\prime}$	3//	13//	7//8
in feet.	7.2	8.5	9.8	11.1	12.4	13.6	14.8	16.0	17.1	18.3
	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.
	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.
2	3920	4620	5290	5950	6580	7200	7810	8400	8980	9550
3	2610	3080	3530	3960	4390	4800	5200	5600	5980	6360
4	1960	2310	2650	2970	3290	3600	3900	4200	4490	4770
5	1570	1850	2120	2380	2630	2880	3120	3360	3590	3820
6	1310	1540	1760	1980	2190	2400	2600	2800	2990	3180
7	1120	1320	1510	1700	1880	2060	2230	2400	2560	2730
8	980	1150	1320	1490	1650	1800	1950	2100	2240	2390
9	870	1030	1180	1320	1460	1600	1730	1870	1990	2120
	780	920	1060	1190	1320	1440	1560	1680	1800	1910
11	710	840	960	1080	1200	1310	1420	1530	1630	1740
12	650	770	880	990	1100	1200	1300	1400	1500	1590
13	600	710	810	910	1010	1110	1200	1290	1380	1470
14	560	660	760	850	940	1030	1120	1200	1280	1360

#### UNEQUAL LEGS.

#### NEUTRAL AXIS PARALLEL TO LONG LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



D:-t			Sect	ion No.	A 131.								
Distance between	$\frac{4'' \times 3\frac{1}{2}''}{\frac{5}{2}'' \mid \frac{3}{2}'' \mid \frac{7}{2}'' \mid \frac{1}{2}'' \mid \frac{9}{2}'' \mid \frac{5}{2}'' \mid \frac{1}{2}\frac{1}{2}''}$												
supports	$\frac{5}{16}$ / /	3//	$\frac{7}{16}$	$\frac{1}{2}''$	9//	<u>5</u> //	$\frac{116}{16}$						
in feet.	7.7 lbs. per ft.	9.1 lbs. per ft.	10.6 lbs. per ft.	11.9 lbs. per ft.	13.3 lbs. per ft.	14.7 lbs. per ft.	16.0 lbs. per ft.						
2 3 4 5	5300 3530 2650	6260 4170 3130	7190 4790 3590	8090 5390 4040	8970 5980 4480	9760 6510 4880	10650 7100 5320						
5 6 7 8 9	2120 1770 1510 1320 1180	2500 2090 1790 1560 1390	2870 2400 2050 1800 1600	3240 2700 2310 2020 1800	3590 2990 2560 2240 1990	3900 3250 2790 2440 2170	4260 3550 3040 2660 2370						
10	960	1250	1310	1470	1790 1630	1950 1770	2130 1940						
12 13 14	880 820 760	1040 960 890	1200 1110 1030	1350 1240 1160	1490 1380 1280	1630 1500 1390	1770 1640 1520						

#### Section No. A 133. Distance $4\frac{1}{2}$ // x 3 // between 1// $\frac{3}{8}$ / / $\frac{7}{16}''$ $\frac{9}{16}$ / / <u>5</u>// $\frac{11}{6}$ supports in feet. 9.1 lbs. 10.6 lbs. 11.9 lbs. 13.3 lbs. 14.7 lbs. 16.0 lbs. per ft. per ft. per ft. per ft. per ft. per ft. 13

#### UNEQUAL LEGS.

### NEUTRAL AXIS PARALLEL TO LONG LEG.

Safe loads below are figured for fibre stress of  $16\,000\,$  pounds per square inch and include weight of angle.



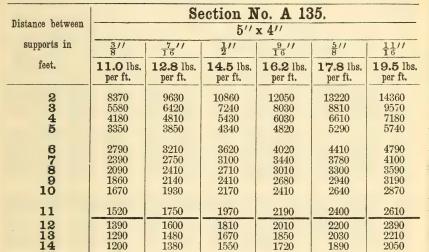
	Section No. A 101.												
Distance		5'' x 3''											
between	5// 16	3//	$\frac{7}{16}$	$\frac{1}{2}''$	$\frac{9}{16}$	5//	$\frac{11}{6}$	3//	13// 16	7//8			
in feet.	8.2	9.8	11.3	12.8	14.3	15.7	17.1	18.5	19.9	21.2			
	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs,	lbs.	lbs.			
	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.			
2	4020	4740	5430	6110	6770	7410	8040	8660	9270	9870			
3	2680	3160	3620	4070	4510	4940	5360	5770	6180	6580			
4	2010	2370	2720	3060	3380	3710	4020	4330	4630	4940			
5	1610	1900	2170	2440	2710	2960	3220	3460	3710	3950			
6	1340	1580	1810	2040	2260	2470	2680	2890	3090	3290			
7	1150	1350	1550	1750	1930	2120	2300	2470	2650	2820			
8	1000	1180	1360	1530	1690	1850	2010	2160	2320	2470			
9 10	890	1050 950	1210	1360 1220	1500 1350	1650 1480	1790 1610	1920 1730	2060 1850	2190 1970			
11	730	860	990	1110	1230	1350	1460	1570	1690	1790			
12	670	790	910	1020	1130	1240	1340	1440	1540	1650			
13	620	730	840	940	1040	1140	1240	1330	1430	1520			
14	570	680	780	870	970	1060	1150	1240	1320	1410			

Distance	Section No. A 103.											
between		5'' x 3½''										
sup-	<u>5</u> //	3//	$\frac{7}{16}$	$\frac{1}{2}''$	9//	<u>5</u> //	11//	3//	13//	7//8	$\frac{15}{16}$	
ports in feet.	8.7 lbs. per ft.	10.4 lbs, per ft.	12.0 lbs. per ft.	13.6 lbs. per ft.	15.2 lbs. per ft.	16.8 lbs. per ft.	18.3 lbs. per ft.	19.8 lbs. per ft.	21.3 lbs. per ft.	22.7 lbs. per ft.	24.2 lbs. per ft.	
2345	5450 3630 2720 2180	6430 4290 2220 2570	7400 4930 3700 2960	8320 5550 4160 3330	9230 6150 4610 3690	10110 6740 5060 4050	10980 7320 5490 4390	11820 7880 5910 4730	12650 8430 6330 5060	13460 8970 6730 5380	14270 9510 7130 5710	
6 7 8 9	1820 1560 1360 1210 1090	2140 1840 1610 1430 1290	2470 2110 1850 1640 1480	2770 2380 2080 1850 1660	3080 2640 2310 2050 1850	3370 2890 2530 2250 2020	3660 3140 2740 2440 2200	3940 3380 2960 2630 2360	4220 3610 3160 2810 2530	4490 3850 3370 2990 2690	4760 4080 3570 3170 2850	
11 12 13 14	990 910 840 780	1170 1070 990 920	1340 1230 1140 1060	1510 1390 1280 1190	1680 1540 1420 1320	1840 1690 1560 1440	2000 1830 1690 1570	2150 1970 1820 1690	2300 2110 1950 1810	2450 2240 2070 1920	2590 2380 2190 2040	

#### UNEQUAL LEGS.

#### NEUTRAL AXIS PARALLEL TO LONG LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



				Se	ction	No.	A 10	5.				
Distance between		$6^{\prime\prime} \times 3^{12}_{2}^{\prime\prime}$										
sup-	3//	7/16	$\frac{1}{2}''$	$\frac{9}{16}$	<u>5</u> //	11/1	3//	13//	7//	$\frac{15}{16}$	1′′	
ports in feet.	11.7 lbs. per ft.	13.5 lbs. per ft.	15.3 lbs. per ft.	17.1 lbs. per ft.	18.9 lbs. per ft.	20.6 lbs, per ft.	22.4 lbs. per ft.	24.0 lbs. per ft.	25.7 lbs. per ft.	27.3 lbs. per ft.	28.9 lbs. per ft.	
2 3 4 5	6570 4380 3280 2630	7550 5030 3770 3020	8500 5670 4250 3400	9430 6290 4720 3770	10340 6890 5170 4140	11230 7480 5610 4490	12100 8070 6050 4840	12960 8640 6480 5180	13800 9200 6900 5520	14640 9760 7320 5850	15470 10310 7730 6190	
6 7 8 9	2190 1880 1640 1460 1310	2520 2160 1890 1680 1510	2830 2430 2120 1890 1700	3140 2690 2360 2100 1890	3450 2950 2580 2300 2070	3740 3210 2810 2490 2250	4030 3460 3020 2690 2420	4320 3700 3240 2880 2590	4600 3940 3450 3070 2760	4880 4180 3660 3250 2930	5160 4420 3870 3440 3090	
11 12 13 14	1190 1090 1010 940	1370 1260 1160 1080	1550 1420 1310 1210	1710 1570 1450 1350	1880 1720 1590 1480	2040 1870 1730 1600	2200 2020 1860 1730	2360 2160 1990 1850	2510 2300 2120 1970	2660 2440 2250 2090	2810 2580 2380 2210	

### UNEQUAL LEGS.

NEUTRAL AXIS PARALLEL TO LONG LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.

Distance	Section No. A 107.										
between					6	" x 4	//				
sup-	3//	$\frac{7}{16}$	$\frac{1}{2}''$	9//	<u>5</u> //	$\frac{11}{16}$	3//	13/1 16	7/1/8	15//	1''
ports in feet,	12.3 lbs. per ft.	14.3 lbs. per ft.	16.2 lbs, per ft.	18.1 lbs, per ft.	20.0 lbs. per ft.	21.8 lbs, per ft,	23.6 lbs, per ft,	25.4 lbs, per ft.	27.2 lbs. per ft.	28.9 lbs, per ft,	30.6 lbs. per ft.
2 3 4 5	8550 5700 4280 3420	9840 6560 4920 3940	11100 7400 5550 4440	12320 8220 6160 4930	13520 9020 6760 5410	14690 9800 7350 5880	15840 10560 7920 6340	16970 11310 8480 6790	18070 12050 9040 7230	19160 12770 9580 7660	20230 13490 10120 8090
6 7 8 9	2850 2440 2140 1900 1710	3280 2810 2460 2190 1970	3700 3170 2770 2470 2220	4110 3520 3080 2740 2460	4510 3860 3380 3010 2700	4900 4200 3670 3270 2940	5280 4530 3960 3520 3170	5660 4850 4240 3770 3390	6020 5760 4520 4020 3610	6390 5470 4790 4260 3830	6740 5780 5060 4500 4050
11 12 13 14 15	1550 1430 1320 1220 1140	1790 1640 1510 1410 1310	2020 1850 1710 1590 1480	2240 2050 1900 1760 1640	2460 2250 2080 1930 1800	2670 2450 2260 2100 1960	2880 2640 2440 2260 2110	3080 2830 2610 2420 2260	3290 3010 2780 2580 2410	3480 3190 2950 2740 2550	3680 3370 3110 2890 2700
16	1070	1230	1390	1540	1690	1840	1980	2120	2260	2400	2530

		Section No. A 109.										
Distance	$7'' \times 3\frac{1}{2}''$											
between	7/1	$\frac{1}{2}$ '	9/1	5/1	$\frac{11}{16}$	3//	13//	7/1	15//	1′′		
supports in feet.	15.0 lbs. per ft.	17.0 lbs. per ft.	19.1 lbs. per ft.	21.0 lbs, per ft.	23.0 lbs, per ft,	24.9 lbs. per ft.	26.8 lbs. per ft.	28.7 lbs. per ft.	30.5 lbs. per ft.	32.3 lbs, per ft,		
2 3 4 5	7670 5110 2830 3070	8640 5760 4320 3460	9590 6390 4790 3840	10520 7010 5260 4210	11430 7620 5710 4570	12320 8220 6160 4930	13210 8810 6600 5280	14090 9390 7040 5630	14950 9960 7470 5980	15810 10540 7900 6320		
6 7 8 9 10	2560 2190 1920 1700 1530	2880 2470 2160 1920 1730	3200 2740 2400 2130 1920	3510 3010 2630 2340 2100	3810 3270 2860 2540 2290	4110 3520 3080 2740 2460	4400 3770 3300 2940 2640	4700 4020 3520 3130 2820	4980 4270 3740 3320 2990	5270 4520 3950 3510 3160		
11 12 13 14 15	1390 1280 1180 1100 1020	1570 1440 1330 1230 1150	1740 1600 1480 1370 1280	1910 1750 1620 1500 1400	2080 1900 1760 1630 1520	2240 2050 1900 1760 1640	2400 2200 2030 1890 1760	2560 2350 2170 2010 1880	2720 2490 2300 2140 1990	2870 2630 2430 2260 2110		
16	960	1080	1200	1320	1430	1540	1650	1760	1870	1980		

### UNEQUAL LEGS.

#### NEUTRAL AXIS PARALLEL TO SHORT LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



	No. A	161.	Section No. A 91.								
Distance between	$2\frac{1}{2}''$	13//				$2\frac{1}{2}$ " x	2"				
supports	3// 16	$\frac{1}{4}$	$\frac{3}{16}$	$\frac{1}{4}$	$\frac{5}{16}$	3//	$\frac{7}{16}$	$\frac{1}{2}$	$\frac{9}{16}$		
in feet.	2.6 lbs. per ft.	3.4 lbs. per ft.	2.8 lbs. per ft.	3.7 lbs. per ft.	d.5 lbs. per ft.	5.3 lbs. per ft.	6.1 lbs. per ft.	6.8 lbs. per ft.	7.6 lbs. per ft.		
2 3 4 5	1530 1020 760 610	1990 1330 1000 800	1560 1040 780 620	2030 1360 1020 810	2490 1660 1240 990	2920 1940 1460 1170	3330 2220 1660 1330	3730 2480 1860 1490	4110 2740 2050 1640		
6	510	660	520	680	_830	970	1110	1240	1370		
7	440	570	450	580	710	830	950	1070	1170		
8 9 10	380 340 310	500 440 400	390 350 310	510 450 410	620 550 500	730 650 580	830 740 670	930 830 <b>7</b> 50	1030 910 820		
11 12	280 260	360 330	280 260	370 340	450 410	530 490	610 560	680 620	750 690		

701	Se	ction	No.	A 12	28.	Section No. A 129.						
Distance between		$2\frac{3}{4}$	′′ x 1	$\frac{1}{2}''$		3'' x 2''						
sup-	3//	$\frac{1}{4}$	$\frac{5}{16}$	3//	$\frac{7}{16}$	$\frac{3}{16}$ "	$\frac{1}{4}$	$\frac{5}{16}$	<u>3</u> //	$\frac{7}{16}$ "	1//	
ports in feet.	2.6 lbs. per ft.	3.4 lbs. per ft.	4.2 lbs. per ft.	5.0 lbs. per ft.	5.7 lbs. per ft.	3.1 lbs. per ft.	4.1 lbs. per ft.	5.0 lbs. per ft.	5.9 lbs. per ft.	6.8 lbs. per ft.	7.7 lbs. per ft.	
2 3 4 5	1790 1190 890 710	2330 1550 1160 930	2850 1900 1420 1140	3340 2230 1670 1340	3810 2540 1910 1530	2210 1470 1110 880	2890 1930 1440 1160	3540 2360 1770 1420	4170 2780 2080 1670	4770 3180 2380 1910	5350 3570 2670 2140	
6	600 510	780 670	950 810	1110 950	1270 1090	740 630	960 830	1180 1010	1390 1190	1590 1360	1780 1530	
8	450	580	710	840	950	550	720	890	1040	1190	1340	
10	400 360	$\frac{520}{470}$	630 570	740 670	850 760	490 440	640 580	790 710	930 830	1060 950	1190 1070	
11 12	320 300	420 390	520 470	610 560	690 640	400 370	530 480	640 590	760 690	870 800	970 890	

### UNEQUAL LEGS.

### NEUTRAL AXIS PARALLEL TO SHORT LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle,



	Se	ction	No.	A 1	21.	Section No. A 123.							
Distance between		2'	/ x 1	3//			2" x 1½"						
sup-	3//	1//	5 // 16	3//	7/1	<u>1</u> //	16	$\frac{1}{4}$	<u>5</u> //	3// 8	16//		
ports in feet,	2.1 lbs. per ft.	2.7 lbs. per ft.	3.3 lbs. per ft.	3.9 lbs. per ft.	d.4 lbs. per ft.	1.5 lbs. per ft.	2.2 lbs. per ft.	2.8 lbs. per ft.	3.4 lbs. per ft.	4.0 lbs. per ft.	4.6 lbs. per ft.		
2 3 4 5	960 640 480 380	1240 830 620 500	1510 1010 750 600	1760 1170 880 700	2000 1330 1000 800	670 440 330 270	970 650 490 390	1260 840 630 500	1530 1020 770 610	1790 1190 890 720	2030 1350 1020 810		
6 7 8 9	320 270 240 210 190	410 350 310 280 250	500 430 380 340 300	590 500 440 390 350	670 570 500 450 400	220 190 170 150 130	320 280 240 220 190	420 360 320 280 250	510 440 380 340 310	600 510 450 400 360	680 580 510 450 410		
11 12	170 160	230 210	270 250	320 290	360 330	120 110	180 160	230 210	280 260	330 300	370 340		

	Se	ction	No.	A 12	25.	Section No. A 127.						
Distance		$2\frac{1}{2}$	" x 1	$\frac{1}{4}$ / /		$2\frac{1}{2}'' \times 1\frac{1}{2}''$						
between supports	3//	1//	5 // 16	3//	17/1/	3//	$\frac{1}{4}$	5// 16	3//	16"		
in feet.	2.3 lbs. per ft.	3.0 lbs. per ft.	3.7 lbs. per ft.	d.4 lbs. per ft.	bs. per ft.	2.5 lbs. per ft.	3.2 lbs. per ft.	4.0 lbs. per ft.	4.7 lbs. per ft.	5.3 lbs. per ft.		
2345	1440 960 720 580	1880 1250 940 750	2290 1530 1140 920	2680 1790 1340 1070	3050 2040 1530 1220	1490 990 750 600	1940 1290 970 780	2370 1580 1180 950	2770 1850 1390 1110	3160 2110 1580 1270		
в	480	630	760	890	1020	500	650	790	920	1050		
7 8 9 10	410 360 320 290	540 470 420 380	650 570 510 460	770 670 600 540	870 760 680 610	430 370 330 300	550 490 430 390	680 590 530 470	790 690 620 550	900 790 700 630		
11 12	260 240	340 310	420 380	490 450	560 510	270 250	350 320	430 390	500 460	580 530		

### UNEQUAL LEGS.

NEUTRAL AXIS PARALLEL TO SHORT LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.

П	
П	
Н	_
'	

	Section No. A 151.									
Distance between	$3\frac{1}{2}'' \times 2''$									
supports in	1//	5// 16	3//	$\frac{7}{16}$	$\frac{1}{2}''$	1 6 ''	<u>5</u> //			
feet.	d.5 lbs. per ft.	5.6 lbs. per ft.	6.6 lbs. per ft.	7.6 lbs. per ft.	8.5 lbs. per ft.	9.5 lbs. per ft.	lbs. per ft.			
2	3880	4760	5610	6440	7230	8000	8750			
3	2580	3170	3740	4290	4820	5340	5830			
4	1940	2380	2810	3220	3620	4000	4370			
5	1550	1900	2250	2570	2890	3200	3500			
6	1290	1590	1870	2150	2410	2670	2920			
7	1110	1360	1600	1840	2070	2290	2500			
8	970	1190	1400	1610	1810	2000	2190			
9	860	1060	1250	1430	1610	1780	1940			
10	780	950	1120	1290	1450	1600	1750			
11	710	870	1020	1170	1310	1460	1590			
12	650	790	940	1070	1210	1330	1460			
13	600	730	860	990	1110	1230	1350			
14	550	680	800	920	1030	1140	1250			

		Section No. A 93.									
Dis	tance between	3'' x 2½''									
. 8	supports in	1//	$\frac{5}{16}''$	<u>3</u> //	76//	$\frac{1}{2}$	9//	5//			
	feet.	4.5 lbs. per ft.	5.6 lbs. per ft.	6.6 lbs. per ft.	7.6 lbs. per ft.	8.5 lbs. per ft.	9.5 lbs. per ft.	lbs. per ft.			
	2 3 4 5	2990 2000 1500 1200	3670 2450 1840 1470	4320 2880 2160 1730	4950 3300 2470 1980	5560 3700 2780 2220	6140 4090 3070 2460	6710 4470 3350 2680			
	6 7 8 9	1000 860 750 670	1220 1050 920 820	1440 1230 1080	1650 1410 1240 1100	1850 1590 1390 1230	2050 1760 1540 1360	2240 1920 1680 1490			
	10	600	730	860	990	1110	1230	1340			
	11 12 13 14	540 500 460 430	670 610 560 520	790 720 660 620	900 820 760 710	1010 930 850 790	1120 1020 940 880	1220 1120 1030 960			

### UNEQUAL LEGS. NEUTRAL AXIS PARALLEL TO SHORT LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.

	Section No. A 95.									
Distance between	$3\frac{1}{2}'' \times 2\frac{1}{2}''$									
supports in	1//	5// 16	3//	$\frac{7}{16}''$	$\frac{1}{2}$ / /	$\frac{9}{16}$	5//	11/1 16	3//	
feet.	4.9 lbs. per ft.	6.1 lbs. per ft.	7.2 lbs. per ft.	8.3 lbs. per ft.	9.4 lbs. per ft.	10.4 lbs. per ft.	11.5 lbs. per ft.	12.5 lbs. per ft.	13.4 lbs. per ft.	
2 3 4 5	4020 2680 2010 1610	4940 3300 2470 1980	5830 3890 2920 2330	6690 4460 3350 2680	7530 5020 3760 3010	8330 5560 4170 3330	9120 6080 4560 3650	9880 6580 4940 3950	10620 7080 5310 4250	
6 7 8	1340 1150 1010	1650 1410 1240	1940 1670 1460	2230 1910 1670	2510 2150 1880	2780 2380 2080	3040 2600 2280	3290 2820 2470	3540 3030 2650	
10	890	990	1300	1490 1340	1670 1510	1850 1670	2030 1820	2190 1980	2360 2120	
11 12 13 14 15	730 670 620 570 540	900 820 760 710 660	1060 970 900 830 780	1220 1120 1030 960 890	1370 1250 1160 1080 1000	1520 1390 1280 1190 1110	1660 1520 1400 1300 1220	1800 1650 1520 1410 1320	1930 1770 1630 1520 1420	
16	500	620	730	840	940	1040	1140	1230	1330	

7.	Section No. A 97.											
Distance between		$3\frac{1}{2}$ / x $3$ / /										
supports	5//	3//	$\frac{7}{16}$ //	$\frac{1}{2}''$	$\frac{9}{16}$	<u>5</u> //	$\frac{116}{16}$	3//	$\frac{13}{16}$	7/1/8		
in feet.	6.6 lbs. per ft.	7.9 lbs. per ft.	9.1 lbs. per ft.	lbs. per ft.	11.4 lbs. per ft.	12.5 lbs. per ft.	13.6 lbs. per ft.	14.7 lbs. per ft.	15.8 lbs. per ft.	16.8 lbs. per ft.		
2 3 4 5	5090 3390 2540 2040	6010 4000 3000 2400	6890 4600 3450 2760	7750 5170 3880 3100	8590 5730 4290 3440	9400 6270 4700 3760	10190 6790 5090 4080	10960 7300 5480 4380	11710 7800 5850 4680	12440 8290 6220 4980		
6 7 8 9	1700 1450 1270 1130	2000 1720 1500 1330	2300 1970 1720 1530 1380	2580 2220 1940 1720	2860 2450 2150 1910	3130 2690 2350 2090	3400 2910 2550 2260 2040	3650 3130 2740 2430 2190	3900 3340 2930 2600 2340	4150 3550 3110 2760		
11 12 13 14 15	930 850 780 730 680	1090 1000 920 860 800	1250 1150 1060 980 920	1410 1290 1190 1110 1030	1560 1430 1320 1230 1150	1710 1570 1450 1340 1250	1850 1700 1570 1460 1360	1990 1830 1690 1570 1460	2130 1950 1800 1670 1560	2260 2070 1910 1780 1660		
16	640	750	860	970	1070	1180	1270	1370	1460	1550		

# UNEQUAL LEGS. NEUTRAL AXIS PARALLEL TO SHORT LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.

				Sect	tion 1	No. A	99.			
Distance					4''	x 3′′				
between	5// 16	3//	$\frac{7}{16}$	$\frac{1}{2}''$	$\frac{9}{16}$ "	<u>5</u> //	$\frac{1}{1}\frac{1}{6}''$	3//	$\frac{13}{16}''$	$\frac{7}{8}$ //
supports in feet.	7.2 lbs, per ft.	8.5 lbs. per ft.	9.8 lbs. per ft.	11.1 lbs. per ft.	12.4 lbs. per ft.	13.6 lbs. per ft.	14.8 lbs. per ft.	16.0 lbs. per ft.	17.1 lbs. per ft.	18.3 lbs. per ft.
2 3 4 5	6580 4390 3290 2630	7780 5180 3890 3110	8940 5960 4470 3580	10070 6710 5040 4030	11170 7450 5590 4470	12240 8160 6120 4900	13280 8860 6640 5310	14300 9530 7150 5720	15290 10190 7650 6120	16260 10840 8130 6500
6 7 8 9	2190 1880 1640 1460 1320	2590 2220 1940 1730 1560	2980 2550 2240 1990 1790	3360 2880 2520 2240 2010	3720 3190 2790 2480 2230	4080 3500 3060 2720 2450	4430 3800 3320 2950 2660	4770 4090 3580 3180 2860	5100 4370 3820 3400 3060	5420 4650 4060 3610 3250
11 12 13 14 15	1200 1100 1010 940 880	1410 1300 1200 1110 1040	1630 1490 1380 1280 1190	1830 1680 1550 1440 1340	2030 1860 1720 1600 1490	2230 2040 1880 1750 1630	2420 2210 2040 1900 1770	2600 2380 2200 2040 1910	2780 2550 2350 2180 2040	2960 2710 2500 2320 2170
16	820	970	1120	1260	1400	1530	1660	1790	1910	2030

		\$	Section	No.	A 131.		
Distance between			4	$'' \times 3\frac{1}{2}$	11		
supports in	5 // 16	3//	$\frac{7}{16}''$	$\frac{1}{2}$	$\frac{9}{16}$ "	5//	$\frac{11}{6}''$
feet.	7.7 lbs. per ft.	9.1 lbs. per ft.	10.6 lbs. per ft.	11.9 lbs. per ft.	13.3 lbs. per ft.	14.7 lbs. per ft.	16.0 lbs. per ft.
2 3 4 5	6740 4490 3370 2690	7970 5310 3980 3190	9160 6110 4580 3660	10320 6880 5160 4130	11450 7640 5730 4580	12550 8370 6280 5020	13630 9080 6810 5450
6 7 8 9	2250 1920 1680 1500 1350	2660 2280 1990 1770 1590	3050 2620 2290 2040 1830	3440 2950 2580 2290 2060	3820 3270 2860 2550 2290	4180 3590 3140 2790 2510	4540 3890 3410 3030 2730
11 12 13 14 15	1220 1120 1040 960 900	1450 1330 1230 1140 1060	1670 1530 1410 1310 1220	1880 1720 1590 1470 1380	2080 1910 1760 1640 1530	2280 2090 1930 1790 1670	2480 2270 2100 1950 1820
16	840	1000	1150	1290	1430	1570	1700

# UNEQUAL LEGS. NEUTRAL AXIS PARALLEL TO SHORT LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.

Distance between		Section No. A 133.											
			$4\frac{1}{2}''$	x 3′′									
supports in	3//	$\frac{7}{16}$	$\frac{1}{2}''$	9//	5//	$\frac{11}{16}$							
feet.	9.1 lbs. per ft.	10.6 lbs. per ft.	11.9 lbs. per ft.	13.3 lbs. per ft.	14.7 lbs. per ft.	16.0 lbs. per ft.							
2345	9750 6500 4880	11230 7480 5610	12660 8440 6330	14060 9370 7030	15420 10280 7710	16750 11170 8380							
	3900	4490	5060	5620	6170	6700							
6 7 8 9 10	3250 2790 2440 2170 1950	3740 3210 2810 2490 2250	4220 3620 3170 2810 2530	4690 4020 3510 3120 2810	5140 4410 3860 3430 3080	5580 4790 4190 3720 3350							
11	1770	2040	2300	2560	2800	3050							
12	1630	1870	2110	2340	2570	2790							
13 14 15	1500 1390 1300	1730 1600 1500	1950 1810 1690	2160 2010 1870	2370 2200 2060	2580 2390 2230							
16 17 18	1220 1150 1080	1400 1320 1250	1580 1490 1410	1760 1650 1560	1930 1810 1710	2090 1970 1860							

				Sect	ion 1	No. A	101			
Distance between					5" x	3//				
supports	5/1 16	3//	7//	$\frac{1}{2}''$	$\frac{9}{16}$	5//	$\frac{11}{16}$	3//	13//	7/1
in feet.	8.2 lbs.	9.8 lbs.	11.3 lbs.	12.8 lbs.	14.3 lbs.	15.7 lbs.	17.1 lbs.	18.5 lbs.	19.9 lbs.	21.2 lbs.
	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.
2	10060	11920	13740	15510	17240	18930	20580	22190	23770	25310
2 3 4 5	6710 5030	7950 5960	9160 6870	10340 7760	11490 8620	12620 9470	13720 10290	14790 11100	15850 11880	16870 12660
5	4020	4770	5500	6210	6900	7570	8230	8880	9510	10120
6	3350	3970	4580	5170	5750	6310	6860	7400	7920	8440
7 8 9 10	2870 2520	3410 2980	3930 3440	4430 3880	4930 4310	5410 4730	5880 5140	6340 5550	6790 5940	7230 6330
9	2240	2650	3050	3450	3830	4210	4570	4930	5280	5620
10	2010	2380	2750	3100	3450	3790	4120	4440	4750	5060
11	1830	2170	2500	2820	3130	3440	3740	4030	4320	4600
12	1680	1990	2290	2590	2870	3160	3430	3700	3960	4220
13	1550	1830	2110	2390	2650	2910	3170	3410	3660	3890
14 15	1440 1340	1700 1590	1960 1830	$\frac{2220}{2070}$	2460 2300	2700 2520	2940 2740	3170 2960	3400 3170	3620 3370
									1	
16	1260	1490	1720	1940	2160	2370	2570	2770	2970	3160
17 18	1180 1120	1400 1330	1620 1530	1830 1720	2030 1920	2230 2100	2420 2290	$2610 \\ 2470$	2800 2640	2980 2810
10	1120	T990	1000	1/20	1320	2100:	2230	24101	2010	2010

# UNEQUAL LEGS. NEUTRAL AXIS PARALLEL TO SHORT LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.

Distance				Se	ction	No.	A 10	03.			COLUMN ALAN
Distance	-				5//	$\times 3\frac{1}{2}$	.//	The state of the s	-		
between					<u></u>		·				
sup-	$\frac{5}{16}$	3//	$\frac{7}{16}$	$\frac{1}{2}''$	$\frac{9}{16}$ / /	<u>5</u> //	$\frac{11}{16}$	3//	$\frac{13}{16}$	$\frac{7}{8}$ //	$\frac{15}{16}$
ports	8.7	10.4	12.0	13.6	15.2	16.8	18.3	19.8	21.3	22.7	24.2
in feet.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.
132 20001	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft,	per ft.	per ft.	per ft.	per ft.
2	10320	12240	14100	15930	17710	19450	21150	22810	24440	26030	27590
3 4	6880	8160	9400	10620	11810	12970	14100	15210	16290	17350	18400
4	5160	6120	7050	7960	8850	9720	10570	11410	12220	13020	13800
5	4130	4890	5640	6370	7080	7780	8460	9120	9780	10410	11040
6	3440	4080	4700	5310	5900	6480	7050	7600	8150	8680	9200
7	2950	3500	4030	4550	5060	5560	6040	6520	6980	7440	7880
8	2580		3530	3980	4430	4860	5290	5700	6110		6900
9	2290	<b>27</b> 20	3130	3540	3940	4320	4700	5070	5430		
10	2060	2450	2820	3190	3540	3890	4230	4560	4890	5210	5520
11	1880	2220	2560	2900	3220	3540	3850	4150	4440	4730	5020
12	1720	2040	2350	2650	2950	.3240	3520	3800	4070	4340	4600
13	1590	1880	2170	2450	2720	2990	3250	3510	3760	4000	4240
14	1470	1750	2010	2280	2530	2780	3020	3260	3490	3720	3940
15	1380	1630	1880	2120	2360	2590	2820	3040		3470	3680

		Se	ection N	o. A 13	5.	
Distance between	, ,		5′′ ≥	4//		
supports in	3//	7/16	$\frac{1}{2}$	9 // 16	<u>5</u> //	$\frac{1}{16}$ ''
feet.	11.0 lbs. per ft.	12.8 lbs. per ft.	<b>14.5</b> lbs. per ft.	16.2 lbs. per ft.	17.8 lbs. per ft.	19.5 lbs. per ft.
2 3 4 5	12500 8330 6250 5000	14410 9610 7200 5760	16280 10850 8140 6510	18100 12070 9050 7240	19880 13250 9940 7950	21620 14420 10810 8650
6 7 8 9	4170 3570 3120 2780 2500	4800 4120 3600 3200 2880	5430 4650 4070 3620 3260	6030 5170 4520 4020 3620	6630 5680 4970 4420 3980	7210 6180 5410 4810 4320
11 12 13	2270 2080 1920	2620 2400 2220	2960 2710 2500	3290 3020 2780	3610 3310 3060	3930 3600 3330
14 15	1790 1670	2060 1920	2330 2170	2590 2410	2840 2650	3090 2880
16 17 18	1560 1470 1390	1800 1700 1600	2030 1910 1810	2260 2130 2010	2490 2340 2210	2700 2540 2400

### UNEQUAL LEGS.

#### NEUTRAL AXIS PARALLEL TO SHORT LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



					Se	ction	No.	A 10	)5.			
	stance					6'	$^{\prime}$ x $3\frac{1}{2}$	//				
	sup-	3//	7/16	1//	9 // 16	5//	11//	3//	13//	7//	15//	1′′
	ports	-	10									
il	1 feet.	11.7 lbs.	13.5 lbs.	15.3 lbs.	17.1 lbs.	18.9 lbs.	20.6 lbs.	22.4 lbs.	24.0 lbs.	25.7 lbs.	27.3 lbs.	28.9 lbs.
_		per ft.	per ft.	per ft.	per ît.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.
	2 3 4 5	17390 11540 8650 6920	19980 13320 9990 7990	22600 15060 11300 9040	25160 16770 12580 10060	27670 18450 13840 11070	30130 20090 15070 12050	32550 21700 16270 13020	34910 23270 17460 13960	37230 24820 18620 14890	39510 26340 19760 15800	41630 27750 20810 16650
	6 7 8 9 10	5770 4940 4330 3850 3460	6660 5710 4990 4440 4000	7530 6460 5650 5020 4520	8390 7190 6290 5590 5030	9220 7910 6920 6150 5530	10040 8610 7530 6700 6030	10850 9300 8140 7230 6510	11640 9970 8730 7760 6980	12410 10640 9310 8270 7450	13170 11290 9880 8780 7900	13880 11890 10410 9250 8330
	11 12 13 14 15	3150 2880 2660 2470 2310	3630 3330 3070 2850 2660	4110 3770 3480 3230 3010	4570 4190 3870 3590 3350	5030 4610 4260 3950 3690	5480 5020 4640 4300 4020	5920 5420 5010 4650 4340	6350 5820 5370 4990 4650	6770 6210 5730 5320 4960	7180 6590 6080 5640 5270	7570 6940 6400 5950 5550
	16 17 18 19 20	2160 2040 1920 1820 1730	2500 2350 2220 2100 2000	2820 2660 2510 2380 2260	3150 2960 2800 2650 2520	3460 3260 3070 2910 2770	3770 3550 3350 3170 3010	4070 3830 3620 3430 3250	4360 4110 3880 3680 3490	4650 4380 4140 3920 3720	4940 4650 4390 4160 3950	5200 4900 4630 4380 4160
	21 22	1650 1570	1900 1810	2150 2050	2400 2290	2640 2520	2870 2740	3100 2960	3320 3170	3550 3380	3760 3590	3960 3780

### UNEQUAL LEGS.

#### NEUTRAL AXIS PARALLEL TO SHORT LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



				Sec	ction	No.	A 10	7.			
Distance between					6	′′ x 4	//				
sup-	3//	7//	$\frac{1}{2}$	9//	<u>5</u> //	11/1 16	3//	13// 16	7//8	15/1 16	1′′
in feet.	12.3 lbs. per ft.	14.3 lbs. per ft.	16.2 lbs. per ft.	18.1 lbs. per ft.	20.0 lbs. per ft.	21.8 lbs.	23.6 lbs. per ft.	25.4 lbs.	27.2 lbs.	28.9 lbs. per ft.	30.6 lbs.
	per 1t.	рег 16.	per 1t.	por 10.	per 16.	por 16,	por 10.	per 16.	per 10.	per 10.	her 10°
2 3 4 5	17700 11800 8850 7080	20430 13620 10230 8170	23120 15410 11560 9250	25750 17160 12870 10300	28320 18880 14160 11330	30850 20570 15420 12340	33330 22220 16660 13330	35760 23840 17880 14300	38140 25430 19070 15260	40480 26990 20240 16190	42780 28520 21390 17110
6 7 8 9 10	5900 5060 4420 3930 3540	6810 5840 5110 4540 4090	7710 6600 5780 5140 4620	8580 7360 6440 5720 5150	9440 8090 7080 6290 5660	10280 8810 7710 6860 6170	11110 9520 8330 7410 6670	11920 10220 8940 7950 7150	12710 10900 9540 8480 7630	13490 11570 10120 9000 8100	14260 12220 10700 9510 8560
11 12 13 14 15	3220 2950 2720 2530 2360	3720 3410 3140 2920 2720	4200 3850 3560 3300 3080	4680 4290 3960 3680 3430	5150 4720 4360 4050 3780	5610 5140 4750 4410 4110	6060 5550 5130 4760 4440	6500 5960 5500 5110 4770	6930 6360 5870 5450 5090	7360 6750 6230 5780 5400	7780 7130 6580 6110 5700
16	2210	2550	2890	3220	3540	3860	4170	4470	4770	5060	5350
17 18 19 20	2080 1970 1860 1770	2400 2270 2150 2040	2720 2570 2430 2310	3030 2860 2710 2570	3330 3150 2980 2830	3630 3430 3250 3080	3920 3700 3510 3330	4210 3970 3760 3580	4490 4240 4020 3810	4760 4500 4260 4050	5030 4750 4500 4280
21 22	1690 1610	1950 1860	2200 2100	2450 2340	2700 2570	2940 2800	3170 3030	3400 3250	3630 3470	3860 3680	4070 3890

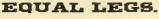
## UNEQUAL LEGS.

#### NEUTRAL AXIS PARALLEL TO SHORT LEG.

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of angle.



			S	ectio	n No	. A 1	.09.			
Distance between				7	''' x 8	} <u>1</u> ''				
sup-	716//	$\frac{1}{2}$ //	9/1	<u>5</u> //	11/1	3//	13/1 16	7//8	$\frac{15}{16}$	1′′
in feet.	15.0	17.0	19.1	21.0	23.0	24.9	26.8	28.7	30.5	32.3
	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.
	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.
4 5	13360	15140	16900	18570	20260	21910	23530	25110	26670	28210
	10690	12120	13520	14850	16210	17530	18830	20090	21340	22560
6	8910	10100	11270	12380	13510	14600	15690	16740	17780	18800
7	7640	8650	9660	10610	11580	12520	13450	14350	15240	16120
8	6680	7570	8450	9280	10130	10950	11770	12560	13340	14100
9	5940	6730	7510	8250	9010	9740	10460	11160	11850	12540
10	5340	6060	6760	7430	8100	8760	9410	10050	10670	11280
11	4860	5510	6150	6750	7370	7970	8560	9130	9700	10260
12	4450	5050	5630	6190	6750	7300	7840	8370	8890	9400
13	4110	4660	5200	5710	6230	6740	7240	7730	8210	8680
14	3820	4330	4830	5310	5790	6260	6720	7180	7620	8060
15	3560	4040	4510	4950	5400	5840	6280	6700	7110	7520
16	3340	3790	4230	4640	5070	5480	5880	6280	6670	7050
17	3140	3560	3980	4370	4770	5150	5540	5910	6280	6640
18	2970	3370	3760	4130	4500	4870	5230	5580	5930	6270
19	2810	3190	3560	3910	4270	4610	4950	5290	5620	5940
20	2670	3030	3380	3710	4050	4380	4710	5020	5330	5640
21	2550	2880	3220	3540	3860	4170	4480	4780	5080	5370
22	2430	2750	3070	3380	3680	3980	4280	4570	4850	5130
23	2320	2630	2940	3230	3520	3810	4090	4370	4640	4910
24	2230	2520	2820	3090	3380	3650	3920	4190	4450	4700





Safe loads below are figured for fibre stress of 16000 pounds per square inch and include weight of T-Bar.

Width of Number   Flange   Bar.   Foot   Center to Center of Bearings   Inches   I	include	weight	or 1-B	аг.										-	-
T 5 1 1 1 1.0 180 120 90 70 60 50 40		of	of	per	C	ent	er	to (				Ве	ari	ngs	3
T181 $1\frac{1}{8}$ $1\frac{1}{8}$ $1\frac{1}{8}$ $1.6$ $280$ $190$ $140$ $110$ $90$ $80$ $70$ $60$		Inches.	Inches.	Lbs.	2	3	4	5	6	7	8	9	10	11	12
T183	T 5	1	1	1.0	180	120	90	70	60	50	40				
T187   1½   1½   1.7   350   230   180   140   120   100   90   80	T181	11/8	11/8	1.4	280	190	140	110	90	80	70	60			
T189 $13/8$ $13/6$ 1.9         450         300         220         180         150         130         110         100	T183	$1\frac{3}{16}$	13	1.6-	320	210	160	130	110	90	80	70			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	T187	11/4	11/4	1.7	350	230	180	140	120	100	90	80			
T 39 2 2 4.4 1670 1110 830 670 560 480 420 370 330 300  T 41 2½ 2½ 2½ 5.6 2630 1750 1310 1050 880 750 660 580 530 480 440  T 67 3 3 3 6.8 3930 2620 1970 1570 1310 1120 980 870 790 720 660  T 69 3 3 7.9 4590 3060 2300 1840 1530 1310 1150 1020 920 840 770  T 78 3 3 10.1 5850 3900 2930 2340 1950 1670 1460 1300 1170 1060 980  T 97 3½ 3½ 9.3 6570 4380 3290 2630 2190 1880 1640 1460 1310 1200 1100  UNEQUAL LEGS.  T185 1½ 1½ 3.0 470 310 230 190 160 130 120 100	T189	13/8	18/8	1.9	450	300	220	180	150	130	110	100			
T 49 $2\frac{1}{2}$ $2\frac{1}{2}$ $5.6$ $2630$ $1750$ $1310$ $1050$ $880$ $750$ $660$ $580$ $530$ $480$ $440$ T 67       3       3       6.8       3930 $2620$ $1970$ $1570$ $1310$ $1120$ $980$ $870$ $790$ $720$ $660$ T 69       3       3       7.9 $4590$ $3060$ $2300$ $1840$ $1530$ $1310$ $1150$ $1020$ $920$ $840$ $770$ T 73       3       3 $10.1$ $5850$ $3900$ $2930$ $2340$ $1950$ $1670$ $1460$ $1300$ $1170$ $1060$ $980$ T 97 $3\frac{1}{2}$ $3\frac{1}{2}$ $9.3$ $6570$ $4380$ $3290$ $2630$ $2190$ $1880$ $1640$ $1460$ $1310$ $1200$ $1100$ T 185 $1\frac{1}{4}$ $1\frac{1}{16}$ $1.5$ $250$ $170$ $130$ $100$ $80$ $70$ $60$ .       .       .      <		2 2	2 2												
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		2½ 2½ 2½	2½ 2½												
T 69         3         3         7.9         4590 3060 2300 1840 1530 1310 1150 1020 920 840 770 783 3 3 10.1         5850 3900 2930 2340 1950 1670 1460 1300 1170 1060 980 1670 1460 1300 1170 1060 980           T 97 $3\frac{1}{2}$ $9.3$ $6570$ 4380 3290 2630 2190 1880 1640 1460 1310 1200 1100           UNEQUAL LEGS.           T185 $1\frac{1}{4}$ $1\frac{1}{16}$ $1.5$ $250$ $170$ $130$ $100$ $80$ $70$ $60$	T 49	21/2	21/2	5.6	2630	1750	1310	1050	880	750	660	580	530	480	440
T185   1½   1½   1.5   250   170   130   100   80   70   60	T 69	3 3 3	3	7.9	4590	3060	2300	1840	1530	1310	1150	1020	920	840	770
T185 $1\frac{1}{4}$ $1\frac{1}{16}$ 1.5       250       170       130       100       80       70       60	т 97	3½	3½	9.3	6570	4380	3290	2630	2190	1880	1640	1460	1310	1200	1100
T 22 $2\frac{1}{2}$ $1\frac{1}{4}$ 3.0 $470$ $310$ $230$ $190$ $160$ $130$ $120$ $100$				UN	EC	U	AI	I	E	G٤	5_				
T 65       3       2½       7.2       3200       2130       1600       1280       1070       910       800       710       640       580       530         T140       4½       3½       15.9       11340       7560       5670       4540       3780       3240       2840       2520       2270       2060       1890         T169       5       3       13.6       5670       3780       2840       2270       1890       1620       1420       1260       1130       1030       950         T 84       3       4       9.3       8050       5360       4020       3220       2680       2300       2010       1790       1610       1460       1340	T185	11/4	116	1.5	250	170	130	100	80	70	60				
T140       4½       3½       15.9       11340       7560       5670       4540       3780       3240       2840       2520       2270       2060       1890         T169       5       3       13.6       5670       3780       2840       2270       1890       1620       1420       1260       1130       1030       950         T 84       3       4       9.3       8050       5360       4020       3220       2680       2300       2010       1790       1610       1460       1340	T 22	21/2	11/4	3.0	470	310	230	190	160	130	120	100			
T169     5     3     13.6     5670 3780 2840 2270 1890 1620 1420 1260 1130 1030 950       T 84     3     4     9.3     8050 5360 4020 3220 2680 2300 2010 1790 1610 1460 1340	T 65	3	21/2	7.2	3200	2130	1600	1280	1070	910	800	710	640	580	530
<b>T 84</b> 3 4 9.3 8050 5360 4020 3220 2680 2300 2010 1790 1610 1460 1340	T140	41/2	3½	15.9	11340	7560	5670	4540	3780	3240	2840	<b>2</b> 520	2270	2060	1890
	T169	5	3	13.6	5670	3780	2840	2270	1890	1620	1420	1260	1130	1030	950
<b>T101</b> 3½ 4 10.0 8240 5490 4120 3290 2750 2350 2060 1830 1650 1500 1370		3	4	9.3	8050	5360	4020	3220	2680	2300	2010	1790	1610	1460	1340
	T101	31/2	4	10.0	8240	5490	4120	3290	2750	2350	2060	1830	1650	1500	1370

Safe loads below are figured for fibre stress of 16 000 pounds per square inch and include weight of Z-bar.

#### STANDARD 3" Z-BARS.

Distance between	Sec. N	o. Z 5.	Sec. N	o. Z 9.	Sec. No	o. Z 13.
supports in	1//	5 //	3// 8	$\frac{7}{16}$	$\frac{1}{2}$ //	9 // 16
feet.	6.7 lbs.	8.4 lbs.	9.7 lbs.	11.4 lbs.	12.5 lbs.	14.2 lbs.
	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.
2	10200	12700	13700	15900	16300	18300
3	6800	8470	9130	10600	10870	12200
4	5100	6350	6850	7950	8150	9150
5	4080	5080	5480	6360	6520	7320
6 7 8 9	3400 2910 2550 2270 2040	4230 3630 3180 2820 2540	3910 3430 3040 2740	5300 4540 3980 3530 3180	5430 4660 4080 3620 3260	5230 4580 4070 3 <b>6</b> 60
11	1850	2310	2490	2890	2960	3330
12	1700	2120	2280	2650	2720	3050

## STANDARD 4" Z-BARS.

Distance between	Sec.	No.	Z 21.	Sec.	No.	Z 25.	Sec.	No.	Z 29.
	1//	$\frac{5}{16}$	3//	$\frac{7}{16}$	$\frac{1}{2}$	$\frac{9}{16}$	<u>5</u> //	$\frac{11}{16}$	3//
supports in feet.	8.2 lbs. per ft,	lbs. per ft.	12.4 lbs. per ft.	13.8 lbs. per ft.	15.8 lbs. per ft.	17.9 lbs. per ft.	18.9 lbs. per ft.	20.9 lbs. per ft.	23.0 lbs. per ft.
2 3 4 5	16750 11170 8380 6700	20850 13900 10430 8340	24900 16600 12450 9960	25750 17170 12880 10300	29350 19570 14680 11740	32950 21970 16480 13180	$21530 \\ 16150$	35500 23670 17750 14200	38700 25800 19350 15480
6 7 8 9	5580 4790 4190 3720	6950 5960 5210 4630	8300 7110 6230 5530	8580 7360 6440 5720	9780 8390 7340 6520	10980 9410 8240 7320	10770 9230 8080 7180	11830 10140 8880 7890	12900 11060 9680 8600
10 11 12 13 14	3350 3050 2790 2580 2390	3790 3480 3210 2980	4980 4530 4150 3830 3560	5150 4680 4290 3960 3680	5870 5340 4890 4520 4190	5990 5490 5070 4710	5870 5380 4970 4610	7100 6450 5920 5460 5070	7740 7040 6450 5950 5530

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings  $=\frac{1}{360}$  span.

For complete and exact dimensions of Z-bars see page 39.

Safe loads below are figured for fibre stress of  $16\,000$  pounds per square inch and include weight of Z-bar.

#### STANDARD 5" Z-BARS.

Distance between	Sec. No. Z 37.			Sec. No. Z 41.			Sec. No. Z 45.		
	$\frac{5}{16}$	3// 8	$\frac{7}{16}$	$\frac{1}{2}''$	$\frac{9}{16}$ //	<u>5</u> //	$\frac{11}{16}''$	3//	$\frac{13}{16}$
supports in feet.	11.6 lbs. per ft.	13.9 lbs. per ft.	16.4 lbs. per ft.	17.9 lbs. per ft.	20.2 lbs. per ft.	22.6 lbs. per ft.	23.7 lbs. per ft.	26.0 lbs. per ft.	28.3 lbs. per ft.
2 3 4 5	28500 19000 14250 11400	34100 22730 17050 13640	39700 26470 19850 15880	40950 27300 20480 16380	46000 30670 23000 18400	51050 34030 25530 20420	50500 33670 25250 20200	55100 36730 27550 22040	59750 39830 29880 23900
6 7 8 9	9500 8140 7130 6330 5700	11370 9740 8530 7580 6820	13230 11340 9930 8820 7940	13650 11700 10240 9100 8190	15330 13140 11500 10220 9200	17020 14590 12760 11340 10210	16830 14430 12630 11220 10100	18370 15740 13780 12240 11020	19920 17070 14940 13280 11950
11 12 13 14 15	5180 4750 4380 4070 3800	6200 5680 5250 4870 4550	7220 6620 6110 5670 5290	7450 6830 6300 5850 5460	8360 7670 7080 6570 6130	9280 8510 7850 7290 6810	9180 8420 7770 7210 6730	10020 9180 8480 7870 7350	10860 9960 9190 8540 7970
16	3560	. 4260	4960	5120	<b>5</b> 750	6380	6310	6890	7470

## STANDARD 6" Z-BARS.

Distance between		No. 2	Z 53.	Sec.	No. 2	Z 57.	Sec.	No. 2	
Distance not week	3//	$\frac{7}{16}$	$\frac{1}{2}$ //	9/1 16	<u>5//</u> 8	$\frac{11}{16}$	3//	$\frac{13}{16}$	7/1
supports in	15.6	18.3	21.0	22.7	25.4	28.1	29.3	31.9	34.6
feet.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.	lbs.
	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.	per ft.
2	45000	52450	59850	61600	68400	75200	74900	81150	87450
2 3 4 5	30000	34970	39900	41070	45600		49930		
<b>4</b> 5	22500 18000	26230 20980	29930 23940	$30800 \\ 24640$	$\frac{34200}{27360}$	37600 30080	37450 29960	40580 32460	43730 34980
6	15000	17480	19950	20530	22800	25070	24970	27050	29150
7	12860	14990	17100	17600	19540	$\frac{25070}{21490}$	21400	23190	24990
8	11250	13110	14960	15400	17100	18800	18730	20290	21860
9	10000	11660	13300	13690	15200	16710	16640	18030	19430
10	9000	10490	11970	12320	13680	15040	14980	16230	17490
11	8180	9540	10880	11200	12440	13670	13620	14750	15900
12	7500	8740	9980	10270	11400	12530	12480	13530	14580
13	6920	8070	9210	9480	10520	11570	11520	12480	13450
14 15	6430 6000	7490 6990	8550 7980	8800 8210	9770 9120	10740 10030	10700 9990	$11590 \\ 10820$	12490 11660
16				7700	8550	9400			
17	5630 <b>5</b> 290	6560 6170	7480 7040	7250	8050	885 <b>0</b>	9360 8810	10140 9550	10930 10290
18	5000	5830	6650		7600	8360	8320	9020	9720

For safe loads below heavy lines the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{360}$  span.

For complete and exact dimensions of Z-bars see page 39.

#### GENERAL FORMULÆ FOR FLEXURE OF BEAMS. NOTATION.

A = Area of Section in square inches.

d = Depth of Cross Section in inches.

l = Length of Span in inches.

L = Length of Span in feet.

p = Stress in extreme fibre of section in pounds per square inch.

X<sub>1</sub> = Distance of Center of Gravity of Section from extreme fibre in inches.

W = Total Load. in pounds. Uniformly, Distributed.

W = Total Load, in pounds, Uniformly Distributed, including the Weight of Beam.
W<sub>1</sub> = Total Superimposed or Live Load, in pounds, Uniformly Distributed.
W<sub>2</sub> = Total Weight of Beam, in pounds, Uniformly Distributed.
W<sub>3</sub> = Total Safe Load, in pounds, Uniformly Distributed.
P = Load, in pounds, concentrated at any point

P = Load, in pounds, concentrated at any point.
F = Coefficient of Strength of the Tables of Properties = Safe Load, in pounds, for a fibre stress of 16 000 pounds per square inch for a span of one foot.

F' = Coefficient of Strength of the Tables of Properties = Safe Load, in pounds, for a fibre stress of 12 500 pounds per square inch for a span of one foot.

D = Total Deflection of Beam, in inches, due to weight W.

Dw1 and Dp = Deflections of Beams, in inches, due to the weights W1 and P respectively.

N = Coefficient of Deflection of the Tables of Properties = Deflection, in inches, due to a total load of 1 000 pounds uniformly distributed for a span of one

N' = Coefficient of Deflection of the Tables of Properties = Deflection, in inches, due to a superimposed load of 1 000 pounds, concentrated at the middle of

H = Coefficient of Deflection, in inches, for fibre stress of 16 000 pounds per square inch, for any section used as a Beam subjected to its safe load Uniformly Distributed. (See table, page 68.)

H' = Coefficient of Deflection, in inches, for fibre stress of 12 500 pounds per square inch for any section used as a Beam subjected to its safe load Uniformly Distributed. (See table, page 68.)

M = Total Bending Moment, in inch pounds, due to the Weight of Beam and

Superimposed Load.

 I = Moment of Inertia, in inches<sup>4</sup>, Axis through Center of Gravity.
 I<sub>1</sub> = Moment of Inertia, in inches<sup>4</sup> Axis parallel to above but not through Center of Gravity.

= Distance, in inches, between these Axes.

= Section Modulus in inches<sup>3</sup>.

= Radius of Gyration in inches.

E = Modulus of Elasticity, in pounds, per square inch (Steel = 29 000 000).

#### GENERAL FORMULÆ.

$$S = \frac{I}{X_1} \qquad I_1 = I + Av^2 \qquad r = \sqrt{\frac{I}{A}}$$
 
$$M = \frac{pI}{X_1} = pS \quad \therefore \quad p = \frac{MX_1}{I} = \frac{M}{S} \quad \text{Or for Symmetrical Section } M = \frac{2pI}{d}$$
 For Beam supported at both ends and Uniformly Loaded: 
$$M = \frac{WI}{8} = \frac{(W_1 + W_2)}{8} \stackrel{!}{\cdot} \quad \therefore \quad W = (W_1 + W_2) = \frac{8M}{I} = \frac{8pI}{IX_1} = \frac{8pS}{I}$$
 SAFE LOADS.

SAFE LOADS.  

$$F = \frac{8pS}{l}$$
 where  $p = 16\,000$  pounds and  $l = 12''$  therefore  $F = \frac{2}{3}\,16\,000$  S

$$F' = \frac{8pS}{l}$$
 where p = 12 500 pounds and l = 12" therefore  $F' = \frac{2}{3}$  12 500 S

To obtain the Safe Load for any span in feet, for fibre stress of 16 000 pounds per square inch:

 ${\rm Safe\ Load} = W_s = \frac{2}{3}\,\frac{16\,000\,{\rm S}}{L} = \frac{F}{L}$  To obtain the Safe Load for any span in feet, for fibre stress of 12500 pounds per square inch:

Safe Load =  $W_{\bullet} = \frac{2}{3} \frac{12500 \text{ S}}{L} = \frac{F'}{L}$ 

# GENERAL FORMULÆ FOR FLEXURE OF BEAMS. Continued.

#### DEFLECTIONS.

(1) Beam supported at both ends and Uniformly Loaded:

Deflection for Total Load = 
$$D = \frac{5}{384} \frac{Wl^3}{EI} = \frac{5}{384} \frac{(W_1 + W_2) l^3}{EI}$$

Deflection for Superimposed Load =  $Dw_1 = \frac{5}{384} \frac{W_1 l^3}{EI}$ 

(2) Beam supported at both ends with load concentrated at the middle:

Deflection for Total Load = D = 
$$\frac{Pl^3}{48EI} + \frac{5}{384} \frac{W_2l^3}{EI}$$

Deflection for Superimposed Load =  $D_p = \frac{Pl^3}{48EI}$ 

(3) Beam fixed at one end, unsupported at the other, and Uniformly Loaded:

Deflection for Total Load = D = 
$$\frac{Wl^3}{8EI} = \frac{(W_1 + W_2) l^3}{8EI}$$

Deflection for Superimposed Load =  $Dw_1 = \frac{W_1 l^3}{8EI}$ 

(4) Beam fixed at one end, and unsupported at the other, with load concentrated at the unsupported end:

Deflection for Total Load = D = 
$$\frac{Pl^3}{3EI} + \frac{W_2l^3}{8EI}$$

Deflection for Superimposed Load =  $D_p = \frac{Pl^3}{3El}$ 

 $N = \frac{5}{384} \frac{Wl^3}{EI} = \frac{5}{384} \frac{(W_1 + W_2) l^3}{EI}$ , where  $W = (W_1 + W_2) = 1000$  pounds and l = 12''

$$N' = \frac{Pl^3}{48EI}$$
, where  $P = 1\,000$  pounds and  $l = 12''$ 

Total Deflection, in inches, due to a Beam Uniformly Loaded for any span in feet =  $D = \frac{NWL^3}{1\,000} = \frac{N\,(W_1 + W_2)\,L^3}{1\,000}$ 

Total Deflection, in inches, due to a Superimposed Load P and the Weight of Beam  $W_2$  for any span in feet = D =  $\frac{N'PL^3}{1\,000} + \frac{NW_2L^3}{1\,000}$ 

$$H = \frac{12}{725} L^2$$
  $H' = \frac{3}{232} L^2$ 

#### FOR SYMMETRICAL SECTIONS.

Total Deflection, in inches, for a fibre stress of 16 000 lbs. per square inch =  $D = \frac{H}{d}$ 

Total Deflection, in inches, for a fibre stress of 12 500 lbs. per square inch =  $D = \frac{H'}{d}$ 

## FOR UNSYMMETRICAL SECTIONS.

Total Deflection, in inches, for a fibre stress of 16 000 pounds per square inch

$$= D = \frac{H}{2X_1}$$

Total Deflection, in inches, for a fibre stress of 12500 pounds per square inch

$$= D = \frac{H'}{2X_1}$$

# BENDING MOMENTS AND DEFLECTIONS FOR BEAMS OF UNIFORM SECTION. M = Total Bending Moment, in inch-lbs. $M_{wl}, M_p = Bending$ Moments, in inch-lbs., due to Weights $W_1$ and P respectively. I = Moment of Intertia, in inches<sup>4</sup>. I = Length of Span, in inches. E = Modulus of Elasticity, in lbs. per causer inches. O(0.000) for total.

W = Total Load, in lbs., uniformly distributed, including the weight of

W<sub>1</sub> = Total Superimposed or Live Load, in lbs., uniformly distributed. W<sub>2</sub> = Total Weight of Beam or Dead Load, in lbs., uniformly dis-

tributed.

P,  $P_1$ ,  $P_2$ ,  $P_3 = Loads$ , in lbs., concentrated at any points.

square inch = 29 000 000 for steel.

W<sub>g</sub> = Total Safe Load, in lbs., uniformly distributed, including weight of beam = Total Safe Load of Tables. The ordinates in diagrams give the bending moments for corresponding points on beam. For superimposed load only, make  $W_2$  in formulæ equal to zero.

#### (1) Beam Supported at both ends and Uniformly Loaded,

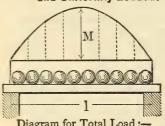


Diagram for Total Load: Draw parabola having M =

# Safe Superimposed Load, in lbs., uniformly distributed, $W'_8 = W_8 - W_2$ .

Maximum Bending Moment at middle of beam =  $M = \frac{W1}{8} = \frac{(W_1 + W_2) 1}{8}$ .

Maximum Deflection =  $\frac{5}{384} \frac{\text{Wl}^3}{\text{EI}}$  $\frac{5}{384} \frac{(W_1 + W_2) l^3}{EI}$ 

#### (2) Beam Supported at both ends with Load Concentrated at the Middle.

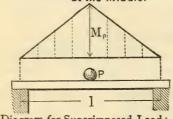


Diagram for Superimposed Load:-Draw triangle having Mp = Diagram for Dead Load similar to Case(1) Safe Superimposed Load, in lbs., concentrated,  $P_s = \frac{W_s - W_2}{2}$ .

Maximum Bending Moment at middle of beam  $=M = \frac{Pl}{4} + \frac{W_2 l}{8}$ .

Maximum Shear at points of support =  $\frac{P+W_2}{2}$ .

Max. Deflection =  $\frac{Pl^3}{48EI} + \frac{5}{384} = \frac{W_2 l^3}{EI}$ .

(3) Beam fixed at one end, Unsupported at the other and

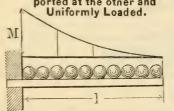


Diagram for Total Load:-Draw Parabola having  $M = \frac{1}{2}$ 

Safe Superimposed Load, in lbs., uniformly distributed,  $W_8 = \frac{W_8}{4} - W_2$ .

Maximum Bending Moment at point of support  $=\frac{Wl}{2}=\frac{(W_1+W_2)l}{2}$ .

Maximum Shear at point of support =  $W = W_1 + W_2$ .

Max. Deflection =  $\frac{Wl^3}{8EI} = \frac{(W_1 + W_2)l^3}{8EI}.$ 

#### BENDING MOMENTS AND DEFLECTIONS FOR BEAMS OF UNIFORM SECTION.

W = Total Load, in lbs., uniformly distributed, including the weight of beam.

 $W_1 = \text{Total Superimposed or Live}$ Load, in lbs., uniformly distributed.  $W_2 = \text{Total Weight of Beam or}$ 

Dead Load, in lbs., uniformly dis-

M = Total Bending Moment, in inch-lbs.  $M_{wl}$ ,  $M_p = Bending$  Moments, in inch-lbs., due to Weights  $W_1$  and P respectively. I = Moment of Inertia, in inches<sup>4</sup>.

Length of Span, in inches.
 E = Modulus of Elasticity, in lbs. per

w<sub>s</sub> = Total Safe Load of Tables.

W<sub>s</sub> = Total Safe Load of Tables.

W<sub>s</sub> = Total Safe Load of Tables.  $P, P_1, P_2, P_3 = Loads$ , in lbs., concentrated at any points. The ordinates in diagrams give the bending moments for corresponding points on beam. For superimposed load only, make  $W_2$  in formulæ equal to zero.

(4) Beam fixed at one end, and Unsupported at the other, with Load Concentrated at the free end. M.

Diagram for Superimposed Load:-Draw triangle having  $M_p = Pl$ . Diagram for Dead Load similar to Case(3) Safe Superimposed Load, in lbs., concentrated,  $P_s = \frac{W_s - 4W_2}{s}$ .

Maximum Bending Moment at point of support =  $Pl + \frac{W_2}{2}$ 

Maximum Shear at point of support = P + W2.

Maximum Deflection =  $\frac{Pl^3}{3EI} + \frac{W_2 l^3}{8EI}$ .

(5) Beam Supported at both ends with Load Concentrated at any point.

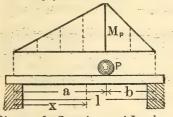


Diagram for Superimposed Load:-Draw triangle having  $M_p = \frac{Pab}{I}$ 

Diagram for Dead Load similar to Case (1)

Safe Superimposed Load, in lbs., concentrated,  $P_s = \frac{W_s l^2 - 4a W_2 (l-a)}{8ab}$ .

Maximum Bending Moment under load  $= \underbrace{a (2 \text{ Pb} + W_2 l - W_2 a)}_{\text{Maximum Bending Moment under load}}$ 

Max. Shear at Sup. near  $a = \frac{Pb}{1} + \frac{W_2}{2}$ .

Max. Shear at Sup. near  $b = \frac{Pa}{1} + \frac{W_2}{2}$ . Deflection at distance x from left

 $\left[ \text{Pb} + \frac{W_2}{8} \left( 2l - \sqrt{\frac{2al - a^2}{3} - \frac{3l^3}{2al - a^2}} \right) \right]$ 

 $x = \sqrt{\frac{2al - a^2}{3}}$  = Distance, from left support, of point of maximum deflection for superimposed load.

(6) Beam Supported at both ends with two Symmetrical Loads.

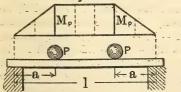


Diagram for Superimposed Load:-Draw trapezoid having M<sub>p</sub> = Pa. Diagram for Dead Load similar to Case(1) Safe Superimposed Load, in lbs., concentrated, each,  $P_s = \frac{W_s l - W_2 l}{8a}$ .

Maximum Bending Moment at center of beam =  $Pa + \frac{W_2l}{8}$ 

Maximum Shear at points of support =  $2P + W_2$ 

Maximum Deflection =  $\frac{\text{Pa}}{24\text{El}} \left( 3l^2 - 4a^2 \right) + \frac{5}{384} \frac{W_2}{\text{El}}$ 

#### BENDING MOMENTS AND DEFLECTIONS FOR BEAMS OF UNIFORM SECTION.

W = Total Load, in lbs., uniformly distributed, including the weight of beam.

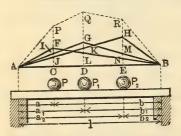
W<sub>1</sub> = Total Superimposed or Live Load, in lbs., uniformly distributed.
W<sub>2</sub> = Total Weight of Beam or Dead Load, in lbs., uniformly distributed.

 $P, P_1, P_2, P_3 = Loads, in lbs., con-$ 

centrated at any points.

The ordinates in diagrams give the bending moments for corresponding points on beam. For superimposed load only, make  $W_2$  in formulæ equal to zero.

(7) Beam Supported at both ends with Loads Concentrated at various Points.



The total bending moment at any point produced by all the weights is equal to the sum of the moments at that point produced by each of the weights separately.

Diagram for Dead Load similar to Case (1)

M = Total Bending Moment, in inch-lbs. M = 1 otal Bending Moment, in inch-lbs., M<sub>p</sub>, Bending Moments, in inch-lbs., due to Weights W<sub>1</sub> and P respectively.

I = Moment of Inertia, in inchest.

I = Length of Span, in inchest.

E = Modulus of Elasticity, in lbs., per square inch = 29 000 000 for steel.

W<sub>s</sub> = Total Safe Load, in lbs., uniformly distributed, including the weight of heam = Total Safe Load of Tables

of beam = Total Safe Load of Tables.

The Maximum Bending Moment occurs at the point where the vertical shear equals zero and will be at one of the loads P, P1, or P2 depending upon their amounts and spacing if W2 is neglected.

Let R = Reaction at Left Support.

Bending Moment at P =

$$M_{p} = Ra - \frac{W_{2} a^{2}}{2l}.$$

Bending Moment at P1 =

$$M_{p1} = Ra_1 - \left[ \frac{W_2 a_1^2}{2l} + P (a_1 - a) \right].$$

Bending Moment at P2 = M2 = Ra2 - $\left[\frac{W_2 a_2^2}{2!} + P_1 (a_2 - a_1) + P (a_2 - a_1)\right].$ 

Shear or Reaction at Left Support =  $\frac{P_2 b_2 + P_1 b_1 + Pb}{1} + \frac{W_2}{2}$ .

Shear or Reaction at Right Support =  $\frac{P_2 a_2 + P_1 a_1 + P_2}{1} + \frac{W_2}{2}$ .

Diagram for Superimposed Load:-Draw as in Case (5) the Ordinates FC, GD and HE representing the bending moments due to loads P, P1 and P2 respectively. Produce FC to P, making PC = FC + IC + JC; GD to Q, making QD = GD + KD + LD; and HE to R, making RE = HE + ME + NE. Join the points A, P, Q, R and B, then the ordinates between A B and polygon A P ORB will represent the bending moments for corresponding points on beam.

#### BENDING MOMENTS AND DEFLECTIONS FOR BEAMS OF UNIFORM SECTION.

W = Total Load, in lbs., uniformly distributed, including the weight of beam.

 $W_1 = Total$  Superimposed or Live Load, in lbs., uniformly distributed.

W2 = Total Weight of Beam or Dead Load, in lbs., uniformly distributed.

P,  $P_1$ ,  $P_2$ ,  $P_3 = Loads$ , in lbs., concentrated at any points.

M= Total Bending Moment, in inch-lbs.  $M_{w1}$ ,  $M_p$  = Bending Moments, in inch-lbs., due to Weights  $W_1$  and P respectively. I = Moment of Inertia, in inches4.

l = Length of Span, in inches. E = Modulus of Elasticity, in lbs., per

square inch =  $29\,000\,000$  for steel.  $W_a = \text{Total Safe Load, in lbs., uniformly distributed, including the weight of beam = Total Safe Load of Tables.$ 

The ordinates in diagrams give the bending moments for corresponding points on beam. For superimposed load only, make  $W_2$  in formulæ equal to zero.

#### (8) Beam Fixed at both ends and Uniformly Loaded.

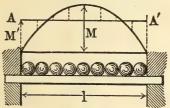


Diagram for Total Load:-Draw parabola having  $M = \frac{W1}{8}$ . Also A A' parallel to base and at a distance The Vertical distances between the parabola and line A A' are the moments for corresponding points on beam.

Safe Superimposed Load, in lbs., uniformly distributed,  $W_s = \frac{3}{2} W_s - W_2$ .

Distance of points of contra-flexure from supports = .21131.

Maximum Bending Moment at points of support =  $\frac{Wl}{12} = \frac{(W_1 + W_2) \, l}{12}$ .

Bending Moment at middle of beam =  $\frac{Wl}{24} = \frac{(W_1 + W_2) l}{24}$ 

Maximum Shear at points of support =  $W_1 + W_2$ 

W13 Maximum Deflection 384EI  $(W_1 + W_2) 1^3$ 384EI

#### (9) Beam Fixed at both ends with Load Concentrated at the Middle.

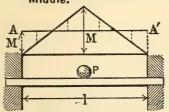


Diagram for Superimposed Load:-Draw triangle having  $M = \frac{Pl}{4}$ . A A' parallel to base and at a distance  $M' = \frac{Pl}{8}$ . The Vertical distances between the triangle and line A A' are the moments for corresponding points

Diagram for Dead Load similar to Case (8)

Safe Superimposed Load, in lbs., concentrated,  $P_s = W_s - \frac{2}{3} W_2$ .

Distance of points of contra-flexure from supports  $= \frac{1}{4}$ l.

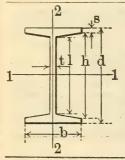
Maximum Bending Moment at points of support =  $\frac{Pl}{8} + \frac{W_2l}{12}$ .

Bending Moment at middle of beam =  $\frac{\mathrm{Pl}}{8} + \frac{\mathrm{W_2l}}{24}$ 

Maximum Shear at points of support =

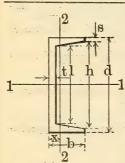
Maximum Deflection =  $\frac{Pl^3}{192EI} + \frac{W_2l^3}{384EI}$ .

# VALUES OF MOMENTS OF INERTIA FOR STAND-ARD AND CAMBRIA SECTIONS.



A = td + 2s (b-t) + 
$$\frac{(b-t)^2}{12}$$
.  
I, Axis 1-1 =  $\frac{bd^3}{12}$  -  $\frac{h^4-l^4}{8}$ .  
I', Axis 2-2 =  $\frac{b^3s}{6}$  +  $\frac{lt^3}{12}$  +  $\frac{b^4-t^4}{288}$ .

Slope of flange  $= g = \frac{h-l}{b-t} = \frac{1}{6}$  for standard sections. h = d-2s. l = h-g(b-t).



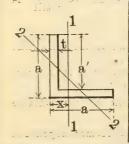
$$A = td + 2s (b-t) + \frac{(b-t)^2}{6}.$$

$$x = \left[b^2s + \frac{ht^2}{2} + \frac{(b-t)^2 (b+2t)}{18}\right] \div A.$$

$$I, Axis 1 - 1 = \frac{bd^3}{12} - \frac{h^4 - l^4}{16}.$$

$$I', Axis 2 - 2 = \frac{1}{3} \left[2sb^3 + lt^3 + \frac{b^4 - t^4}{12}\right] - Ax^2.$$

Slope of flange  $= g = \frac{h-l}{2(b-t)} = \frac{1}{6}$  for standard sections. h = d-2s. l = h-2g(b-t).

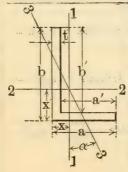


$$A = t (2a - t).$$

$$x = \frac{a^2 + at - t^2}{2(2a - t)}.$$

$$I, Axis 1-1 = \frac{t(a-x)^3 + ax^3 - (a-t)(x-t)^3}{3}.$$

1", Axis  $2-2 = \frac{2x^4-2(x-t)^4+t\left[a-\left(2x-\frac{t}{2}\right)\right]^3}{3}$ 



$$A = t(a + b - t).$$

$$x = \frac{t(2a'+b) + a'^2}{2(a'+b)}. \qquad x' = \frac{t(2b'+a) + b'^2}{2(b'+a)}.$$

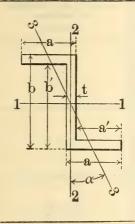
$$Tan. 2a = -\frac{[(2x-t)b(b-2x') + (2x'-t)(a-t)(a+t-2x)]t}{2(l'-l)}.$$

$$I, Axis 1 - 1 = \frac{t(a-x)^3 + bx^3 - (b-t)(x-t)^3}{3}.$$

$$I', Axis 2 - 2 = \frac{t(b-x')^3 + ax'^3 - (a-t)(x'-t)^3}{3}.$$

$$I'', Axis 3 - 3 = \frac{I\cos^2 a - I'\sin^2 a}{\cos^2 a}.$$

## VALUES OF MOMENTS OF INERTIA FOR STAND-ARD AND CAMBRIA SECTIONS.



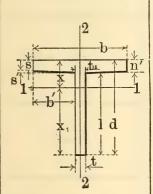
$$A = [b + 2 (a - t)] t.$$

Tan. 
$$2a = -\frac{(bt - t^2)(a^2 - at)}{I - I'}$$
.

I, Axis 
$$1-1=\frac{ab^3-a'(b-2t)^3}{12}$$
.

1', Axis 
$$2-2=\frac{b(a+a')^3-2a'^3b'-6a'a^2b'}{12}$$
.

I" Minimum, Axis 
$$3-3=\frac{I'\cos^2\alpha-I\sin^2\alpha}{\cos^2\alpha}$$
.

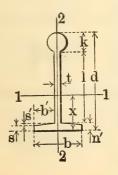


$$A = \frac{1(t + t_1)}{2} + n' t_1 + b' (s + n').$$

$$x = \frac{3s^2(b-t_1) + 2b' \, s' \, (s' + 3s) + 3t_1d^2 - l \, (t_1 - t) \, (3d - l)}{6A}.$$

I, Axis 1-1= 
$$\frac{1^3 (3t+t_1)+4bn'^3-2b's'^3}{12}$$
 - A  $(x-n')^2$ 

I', Axis 2-2 = 
$$\frac{\mathsf{s}\mathsf{b}^3 + \mathsf{s}'\mathsf{t}_1{}^3 + \mathsf{l}\mathsf{t}^3}{12} + \frac{\mathsf{s}'\mathsf{b}'[2\mathsf{b}'^2 + (2\mathsf{b}' + 3\mathsf{t}_1)^2]}{36} + \frac{1(\mathsf{t}_1 - \mathsf{t})[(\mathsf{t}_1 - \mathsf{t})^2 + 2(\mathsf{t}_1 + 2\mathsf{t})^2]}{144}$$
.



e = Area of head.

$$A = e + t (d - k) + (b - t) \left( s + \frac{s'}{2} \right)$$

$$x = \frac{e (2d-k) + t (d-k)^2 + (b-t) \left( s^2 + ss' + \frac{s'^2}{3} \right)}{2A}$$

I, Axis 1-1 = 
$$e^{\left[\frac{k^2}{16} + \left(d - \frac{2s + k}{2}\right)^2\right] + \frac{t(1 + s')^3}{3}}$$
  
+  $\frac{b' s'^3 + 2bs^3}{6} - A(x-s)^2$ .

I', Axis 2-2=
$$\frac{ek^2}{16}$$
+ $\frac{t^3(1+s')+sb^3}{12}$ + $\frac{s'b'[2b'^2+(2b'+3t)^2]}{36}$ 

Sections.	Area of Section.	Distance from Neutral Axis to Extremities of Section. x and x1
a	a <sup>2</sup>	$x_1 = \frac{a}{2}$
	a <sup>g</sup>	$x_1 = a$
	a² — a <sub>1</sub> ²	$x_1 = \frac{a}{2}$
2 8 51	$\mathrm{a}^2$	$x_1 = \frac{a}{\sqrt{2}} = .707a$
d x₁	bd	$x_1=rac{ ext{d}}{2}$
	bd	$x_1 = d$
d₁d b,b, ↓ ↓	$\mathrm{bd}-\mathrm{b}_1\mathrm{d}_1$	$x_1 = \frac{d}{2}$
Q 2/ X,	bd	$x_1 = \frac{b d}{\sqrt{b^2 + d^2}}$

Moment of Inertia.	Section Modulus. $S = \frac{I}{x_1}.$	Radius of Gyration. $r = \sqrt{\frac{I}{A}} \cdot$
$\frac{a^4}{12}$	<u>a<sup>3</sup></u> .6	$\frac{a}{\sqrt{12}} = .289a$
$\frac{a^4}{3}$	$\frac{a^3}{3}$	$\frac{a}{\sqrt{3}} = .577a$
$\frac{a^4 - a_1^4}{12}$	<u>a<sup>4</sup> — a<sub>1</sub><sup>4</sup></u> 6a	$\sqrt{\frac{a^2+a_1^2}{12}}$
- a4 - 12	$\frac{a^3}{6 \sqrt{2}} = .118a^3$	$\frac{a}{\sqrt{12}} = .289a$
$\frac{\mathrm{bd^3}}{12}$	$\frac{\mathrm{bd}^2}{6}$	$\frac{d}{\sqrt{12}} = .289d$
<u>bd</u> 8	$\frac{\mathrm{bd}^2}{3}$	$\frac{\mathrm{d}}{\sqrt{3}} = .577\mathrm{d}$
$\frac{bd^3 - b_1d_1^3}{12}$	$\frac{bd^{3}b_{1}d_{1}^{3}}{6d}$	$\sqrt{\frac{bd^3-b_1d_1^3}{12(bd-b_1d_1)}}$
$\frac{b^3d^3}{6(b^2+d^2)}$	$\frac{b^2d^2}{6\sqrt{b^2+d^2}}$	$\frac{\text{bd}}{1/\overline{6(b^2+d^2)}}$

Sections.	Area of Section.	Distance from Neutral Axis to Extremities of Section. x and x1		
d wx,	bd	$x_1 = \frac{d \cos a + b \sin a}{2}$		
x, d x x b	<u>bd</u> 2	$x = \frac{d}{3}$ $x_1 = \frac{2d}{3}$		
x, d		$x_1 = d$		
$\mathbf{x}_{1}$ $\mathbf{d}$	$\frac{\pi \mathrm{d}^2}{4} = .785 \mathrm{d}^2$	$x_1 = \frac{d}{2}$		
$\begin{array}{c} \uparrow \\ \downarrow \\$	$\frac{\pi \left(d^2 - d_1^2\right)}{4} = .785 \left(d^2 - d_1^2\right)$	$x_1 = \frac{d}{2}$		
$\frac{\mathbf{X}_{1}}{\mathbf{X}}$	$\frac{\pi d^2}{8} = .393 d^2$	$x = \frac{2d}{3\pi} = .212d$ $x_1 = \frac{(3\pi - 4) d}{6\pi} = .288d$		
$\begin{array}{c c} & & & \\ &$	$rac{\mathrm{b}+\mathrm{b}_1}{2}$ . d	$x = \frac{b + 2b_1}{b + b_1} \cdot \frac{d}{3}$ $x_1 = \frac{b_1 + 2b}{b + b_1} \cdot \frac{d}{3}$		

PROPERTIES OF VARIOUS SECTIONS.								
Moment of Inertia.	Section Modulus. $S = \frac{I}{x_1} \cdot$	Radius of Gyration. $r = \sqrt{\frac{I}{A}}$						
$\frac{\mathrm{bd}}{12} \; (\mathrm{d}^2 \cos^2 \alpha + \mathrm{b}^2 \sin^2 \alpha)$	$\frac{\mathrm{d}\mathbf{b}}{6} \left( \frac{\mathrm{d}^2 \mathrm{cos}^2 \mathbf{a} + \mathrm{b}^2 \mathrm{sin}^2 \mathbf{a}}{\mathrm{d} \cos \mathbf{a} + \mathrm{b} \sin \mathbf{a}} \right)$	$\sqrt{\frac{d^2\cos^2\alpha + b^2\sin^2\alpha}{12}}$						
bd <sup>3</sup> 36	$\frac{\mathrm{bd^2}}{24}$	$\frac{\mathrm{d}}{\sqrt{18}} = .236\mathrm{d}$						
$\frac{\mathrm{bd^3}}{12}$	bd <sup>2</sup> 12	$\frac{\mathrm{d}}{\sqrt{6}} = .408\mathrm{d}$						
$\frac{\pi d^4}{64} = .049 d^4$	$\frac{\pi d^3}{32} = .098d^3$	- <u>d</u>						
$\frac{\pi \left(d^4 - d_1^4\right)}{64} = .049 \left(d^4 - d_1^4\right)$	$\frac{\pi}{32} \frac{(d^4 - d_1^4)}{d} = .098 \frac{(d^4 - d_1^4)}{d}$	$\sqrt{rac{{ m d}^2+{ m d}_1{}^2}{4}}$						
$\frac{9\pi^2 - 64}{1152\pi} \cdot d^4 = .007d^4$	$\frac{9\pi^2 - 64}{192(3\pi - 4)} d^3 = .024d^3$	$\frac{\sqrt{9\pi^2 - 64}}{12\pi} \cdot d = .132d$						
$\frac{b^2 + 4bb_1 + b_1^2}{36 (b + b_1)} \cdot d^3$	$\frac{b^2 + 4bb_1 + b_1^2}{12(b_1 + 2b)} \cdot d^2$	$\frac{d}{6(b+b_1)}\sqrt{rac{2(b^2+4bb_1+b_1^2)}{2(b^2+4bb_1+b_1^2)}}$						

Sections.	Area of Section.	Distance from Neutral Axis to Extremities of Section. x and x <sub>1</sub>
$\frac{1}{d} \sum_{\substack{x \\ x, y}} $	$\frac{3}{2}$ d <sup>2</sup> tan. 30° = .866d <sup>2</sup>	$x_1 = \frac{d}{2}$
\$\frac{1}{x},	$\frac{3}{2} d^2 \tan 30^\circ = .866d^2$	$x_1 = \frac{d}{2 \cos 30^{\circ}} = .577d$
$\begin{array}{c c} & & \\ \hline & & \\ \hline & & \\ \hline & & \\ \hline & & \\ \end{array}$	2d² tan. 22½° = .828d²	$x_1 = \frac{d}{2}$
d x,	$\frac{\pi \mathrm{bd}}{4} = .785 \; \mathrm{bd}$	$x_1 = \frac{d}{2}$
	td + 2b' (s + n')	$x_1 = \frac{d}{2}$
$ \begin{array}{c c}  & & & & & & \\ \hline  & & & & & \\$	td + 2b' (s + n')	$x_1 = \frac{b}{2}$
x,d + bo	td + b' (s + n')	$x_1 = \frac{d}{2}$
$\begin{array}{c c}  & & & & & \\  & & & & \\  & & & & \\  & & & &$	td + b' (s + n')	$x = [b^{2}s + \frac{ht^{2}}{2} + \frac{g}{3}(b-t)^{2}]$ $(b + 2t)] \div A$ $x_{1} = b - x$

2 200 2 2220 2	110011111111111111111111111111111111111								
Moment of Inertia.	Section Modulus. $S = \frac{I}{x_1}$	Radius of Gyration. $r = \sqrt{\frac{I}{A}}$							
$\frac{A}{12} \left[ \frac{d^2 (1 + 2 \cos^2 30^\circ)}{4 \cos^2 30^\circ} \right] = .06d^4$	$\frac{A}{6} \left[ \frac{d(1+2\cos^2 30^\circ)}{4\cos^2 30^\circ} \right] = .12d^3$	$\frac{d}{4\cos 30^{\circ}} \sqrt{\frac{1 + 2\cos^{2}30^{\circ}}{3}} = .264d$							
$\frac{A}{12} \left[ \frac{d^2 (1 + 2 \cos^2 30^\circ)}{4 \cos^2 30^\circ} \right]$ = .06d <sup>4</sup>	$\frac{A}{6} \left[ \frac{d(1 + 2\cos^2 30^\circ)}{4\cos 30^\circ} \right] = .104d^3$	$\frac{d}{4 \cos 30^{\circ}} \sqrt{\frac{1 + 2 \cos^{2} 30^{\circ}}{3}} = .264d$							
$\frac{A}{12} \left[ \frac{d^2 \left( 1 + 2 \cos^2 22\frac{1}{2}^{\circ} \right)}{4 \cos^2 22\frac{1}{2}^{\circ}} \right] = .055d^4$	$\frac{A}{6} \left[ \frac{d \left( 1 + 2 \cos^2 22\frac{1}{2}^{\circ} \right)}{4 \cos 22\frac{1}{2}^{\circ}} \right]$ = .109d <sup>3</sup>	$\frac{d}{4\cos 22\frac{1}{2}^{\circ}} \sqrt{\frac{1+2\cos^2 22\frac{1}{2}^{\circ}}{3}}$ = .257d							
$\frac{\pi b d^3}{64} = .049 b d^3$	$\frac{\pi b d^2}{32} = .098bd^2$	<u>d</u>							
$\frac{1}{12} \left[ bd^3 - \frac{1}{4g} \left( h^4 - l^4 \right) \right]$	2 <u>1</u> d	$r = \sqrt{\frac{I}{A}}$							
$\frac{1}{12} \left[ b^3 (d - h) + lt^3 + \frac{g}{4} (b^4 - t^4) \right]$	2 <u>I</u>	$r = \sqrt{\frac{I}{A}}$							
$\frac{1}{12} \left[ bd^3 - \frac{1}{8g} (h^4 - l^4) \right]$	2 <u>I</u>	$r = \sqrt{\frac{1}{A}}$							
$\frac{1}{3} \left[ 2sb^3 + lt^3 + \frac{g}{2} (b^4 - t^4) \right] - Ax^2$	$\frac{1}{b-x}$	$r = \sqrt{\frac{I}{A}}$							

Sections.	Area of Section.	Distance from Neutral Axis to Extremities of Section. x and x <sub>1</sub>
	bd — h (b — t)	$x_1 = \frac{d}{2}$
$\begin{array}{c} \xrightarrow{\searrow} S \longleftarrow & \downarrow t \\ & \stackrel{\searrow}{\searrow} & \stackrel{\downarrow}{\longrightarrow} & \stackrel{\downarrow}{\searrow} \\ & \stackrel{\downarrow}{\longrightarrow} & \stackrel{\downarrow}{\longrightarrow} & \stackrel{\downarrow}{\longrightarrow} & \stackrel{\downarrow}{\longrightarrow} \\ & & \stackrel{\downarrow}{\longrightarrow} & \stackrel{\downarrow}$	bd — h (b — t)	$x_1 = \frac{b}{2}$
x, d by	bd — h (b — t)	$x_1 = \frac{d}{2}$
X $X$ $A$	bd — h (b — t)	$x = \frac{2b^2s + ht^2}{2A}$ $x_1 = b - x$
x <sub>1</sub> b d	td + s (b - t)	$x_1 = \frac{d}{2}$
$ \begin{array}{c c}  & \downarrow \\  & \downarrow \\$	bs + ht	$x = \frac{d^2t + s^2(b - t)}{2A}$ $x_1 = d - x$
	$bs + ht + b_1s$	$x = \frac{td^{2} + s^{2}(b-t) + s(b_{1}-t)(2d-s)}{2A}$ $x_{1} = d - x$
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$bs + \frac{h(t + t_1)}{2}$	$x=\frac{3bs^2+3th(d+s)+h(t_1-t)(h+3s)}{6A}$ $x_1 = d - x$

Moment of Inertia.	Section Modulus.	Radius of Gyration.
I	$S = \frac{I}{x_1}$	$r = \sqrt{\frac{I}{A}}$
$\frac{bd^3 - h^3 (b - t)}{12}$	bd <sup>3</sup> — h <sup>3</sup> (b — t) 6d	$\sqrt{\frac{bd^3 - h^3 (b - t)}{12 [bd - h (b - t)]}}$
$\frac{2\mathrm{sb}^3 + \mathrm{ht}^3}{12}$	$\frac{2sb^3 + ht^3}{6b}$	$\sqrt{\frac{2\mathrm{s}\mathrm{b}^3 + \mathrm{h}\mathrm{t}^3}{12[\mathrm{bd} - \mathrm{h}(\mathrm{b} - \mathrm{t})]}}$
$\frac{bd^{3}-h^{3}(b-t)}{12}$	$\frac{\mathrm{bd}^3 - \mathrm{h}^3  (\mathrm{b} - \mathrm{t})}{6\mathrm{d}}$	$\sqrt{\frac{bd^3 - h^3 (b - t)}{12 [bd - h (b - t)]}}$
$\frac{2{ m s}{ m b}^3 + { m h}{ m t}^3}{3} - { m A}{ m x}^2$	I b-x	$\sqrt{\frac{1}{A}}$
$\frac{td^3 + s^3 (b - t)}{12}$	$\frac{\operatorname{td}^3 + \operatorname{s}^3(b - \operatorname{t})}{\operatorname{6d}}$	$\sqrt{\frac{td^3 + s^3 (b - t)}{12 [td + s (b - t)]}}$
$\frac{tx_1^3 + bx^3 - (b - t)(x - s)^3}{3}$	$\frac{1}{d-x}$	$\sqrt{\frac{tx_1^3 + bx^3 - (b - t)(x - s)^3}{3(bs + ht)}}$
$\frac{bx^3 + b_1x_1^3 - (b - t)(x - s)^3}{3}$ $\frac{(b_1 - t)(x_1 - s)^3}{3}$	$\frac{1}{d-x}$	$-\frac{\left[\frac{bx^3 + b_1x_1^3 - (b - t)(x - s)^3}{3(bs + ht + b_1s)} - \frac{(b_1 - t)(x_1 - s)^3}{3(bs + ht + b_1s)}\right]^{\frac{1}{2}}$
$\frac{4bs^3 + h^3 (3t + t_1)}{12} - A(x - s)^2$	$\frac{I}{d-x}$	$\sqrt{\frac{I}{A}}$

EXPLANATIONS OF THE TABLES OF PROPERTIES OF STANDARD AND SPECIAL I-BEAMS,
STANDARD AND SPECIAL CHANNELS,
STANDARD AND SPECIAL ANGLES
WITH EQUAL AND UNEQUAL
LEGS, Z-BARS AND T-BARS.

### PROPERTIES OF I-BEAMS.

PAGES 156 TO 159 INCLUSIVE.

The figures or values in the various columns give the section numbers, dimensions, weights, areas and properties of the sections as noted in the different headings.

The columns which require special explanation are as follows:

SECTION MODULUS-Column 8.

This is obtained from the moment of inertia in column 7 by dividing it by the distance from the neutral axis to the most remote fibre, which in this case is one-half the depth of the beam.

COEFFICIENTS OF STRENGTH-Columns 13 and 14.

The coefficients of strength F and F' have been computed for fibre stresses of 16000 and 12500 pounds per square inch respectively, as stated in the headings of the columns, and are the safe loads in pounds uniformly distributed, including its own weight for a beam one foot long. Thus the safe load for any span may be obtained by dividing the proper coefficient by the length of the span in feet.

The coefficients of strength were obtained from the following for-

$$F = \frac{2}{3} \times 16\,000 \times S$$
  
 $F' = \frac{2}{3} \times 12\,500 \times S$ 

in which S is the section modulus.

## COEFFICIENTS OF DEFLECTION—Columns 15 and 16.

The coefficients of Deflection N and N' for uniform and center loads, respectively, were obtained from the following formulæ:

$$N = \frac{Wl^3}{76.8EI}$$
  $N' = \frac{Pl^3}{48EI}$ 

in which

P and W = 1000 pounds.

1 = 12 inches.

E = 29 000 000.

I = moment of inertia about axis 1-1.

These coefficients are therefore the deflections in inches of a beam one foot long with a load of 1 000 pounds. The deflection of a beam for any load and span may therefore be obtained by multiplying the proper coefficient by the cube of the span in feet, and by the number of 1 000-pound units in the given load.

## PROPERTIES OF STANDARD AND SPECIAL CHANNELS.

## PAGES 160 TO 163 INCLUSIVE.

The various columns in the Tables of Properties of Standard Channels are similar to those in the Tables of Properties of I-Beams, as explained above, with the addition of column 11, which gives the Section Modulus about an axis through the center of gravity parallel to the web, and column 13, which gives the distance of the center of gravity from the outside of the web. In this case the Section Modulus  $S' = \frac{I'}{b-x}$  the notation being as given at the heads of the columns.

## PROPERTIES OF T-BARS.

A Table of Properties of Cambria T-Bars is also given on pages 178 and 179.

#### PROPERTIES OF ANGLES.

The values in the Tables of Properties of Standard and Special Angles, with Equal Legs, pages 164 to 169, are as stated in the headings, and those in the Tables of Properties of Standard and Special Angles, with Unequal Legs, on pages 170 to 177, are similar, but with the addition of values for I", S" and r" about the inclined axis 3-3, the position of which, in order to give the minimum values, was determined by the formula on page 140 for the value of the tangent of  $2\infty$ . After determining the position of the inclined axis, the properties corresponding thereto were obtained by the formula on page 140.

#### PROPERTIES OF Z-BARS.

The Tables of Properties of Z-Bars, on pages 180 and 181, are similar to those for Beams and Channels with the addition of values in column 13 for determining the position of the inclined axis 3-3 to give the minimum values of the radius of gyration, as shown in column 14, these values being obtained in a manner similar to that used in calculating like quantities for the Tables of Properties of Angles with Unequal Legs, as explained above.

## MOMENTS OF INERTIA OF RECTANGLES.

A Table of Moments of Inertia of Rectangles is added on pages 182 and 183 for convenience in calculating the Moments of Inertia, Section Moduli, and Radii of Gyration for compound shapes in which plates are used.

# GENERAL FORMULÆ FOR PROPERTIES AND FLEXURE.

Formulæ for obtaining the Properties of Standard Sections are given on pages 140 and 141, and for various usual sections on pages 142 to 149 inclusive.

General formulæ for Flexure of Beams, Bending Moments, and Deflections for various cases of loading are given on pages 134 to 139 inclusive.

# EXAMPLES OF APPLICATION OF THE TABLES OF PROPERTIES.

#### EXAMPLE I.

What is the proper size of I-Beam to carry a load of 35 000 pounds concentrated at the center of a span of 25 feet, the fibre stress not to exceed 16 000 pounds per square inch?

In the Tables of Properties of Standard I-Beams, the column headed F gives the coefficient of strength for a uniform load corresponding to a fibre stress of 16 000 pounds per square inch.

The coefficient of strength for a concentrated load at the center is twice that for the same load uniformly distributed, hence the coefficient necessary to meet the conditions is  $35\,000\times25\times2=1\,750\,000$ . From the Table of Properties of Standard I-Beams, page 159, column 13, the coefficient F for a 24-inch 80-pound beam is found to be 1855 310. The weight of the beam itself is  $80\times25=2000$  pounds, which corresponds to a coefficient of  $2000\times25=50\,000$ , which deducted from 1855 310 gives a net coefficient of 1800 310. A 24-inch beam weighing 80 pounds per foot is therefore the proper size.

## EXAMPLE II.

What is the deflection of the beam in the preceding example under the given load?

In the Table of Properties of Standard I-Beams, pages 156 to 159 inclusive, the coefficient of deflection for beams with center loads is given in column 15. To obtain the required deflection it is only necessary to multiply the coefficient by the cube of the span and the number of 1 000 pound units contained in the load.

Thus for the given example the deflection in inches =

$$.0000006 \times 25^3 \times \frac{35000}{1000} = .328 \text{ inch.}$$

#### EXAMPLE III.

What is the safe load uniformly distributed that can be placed on an 8-inch standard channel weighing 11.25 pounds per foot, with a clear span of 15 feet for a maximum fibre stress of 12 500 pounds per square inch, the web to be placed vertically?

From the Table of Properties of Standard Channels, page 161, column F', the coefficient of strength for the given channel under the conditions named is found to be 67 300. Hence the total load may be 67 300 ÷ 15 = 4487 pounds, and as the channel itself weighs 169 pounds, the net superimposed load which it can safely carry under the given conditions is 4318 pounds.

#### EXAMPLE IV.

What is the fibre stress in a 5" x 3" angle weighing 8.2 pounds per foot if loaded at the center with a weight of 1500 pounds, used as a beam with a span of 6 feet, the 5-inch leg to be placed vertically?

The bending moment at the center will be

$$\frac{W_1 l}{4} + \frac{W_2 l}{8} = \frac{1500 \times 72}{4} + \frac{8.2 \times 6 \times 72}{8} = 27443$$
 inch pounds.

Referring to the Table of Properties of Standard Angles, Unequal Legs, on page 173, the Section Modulus for this angle, corresponding to the axis 2—2, is found to be 1.89.

The maximum fibre stress is obtained by dividing the bending moment by the section modulus, thus:  $\frac{27\,443}{1.89} = 14\,520$ , which is the maximum fibre stress in pounds per square inch at the point most remote from the neutral axis, which in this case is the extremity of the longer leg of the angle.

The second term in the above expression for the bending moment is that due to the weight of the angle itself and is inconsiderable, so that in practice it might be neglected for short spans, but should be taken into consideration for the longer ones.

#### PROPERTIES OF COMPOUND SHAPES.

The moments of inertia, section moduli and radii of gyration of compound shapes used as beams or columns, composed of plates and angles, channels, beams, Z-bars, T-bars, or any combination of these, may be obtained with the aid of the Tables of Properties as follows:

The first step is to find the center of gravity of the proposed section, which in the case of symmetrical sections is at the center of the figure.

For unsymmetrical sections the position of the center of gravity may be determined by multiplying the areas of the component parts by the distances of their centers of gravity from any convenient line, taken as an axis, and dividing this product by the sum of the areas, which will give the distance of the centre of gravity of the compound section from the assumed axis.

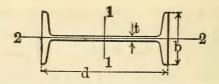
The position of the center of gravity for all sizes of angles, channels, and T-bars is given in the Tables of Properties for these shapes, and is given for various geometrical sections on pages 142 to 149 inclusive, in connection with their other properties.

After determining the position of the center of gravity of a compound shape as explained above, the moment of inertia about an axis through its center of gravity may be found by taking the sums of the moments of inertia of each component part about an axis through its own center of gravity parallel to the axis of the compound section, and the sums of products of the area of each component part by the square of the distance of its center of gravity from the axis of the compound section.

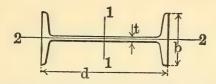
Having thus obtained the moment of inertia of the compound section, the section modulus may be obtained by dividing this moment of inertia by the distance from the neutral axis to the most remote extremity of the section.

The square of the radius of gyration for the compound section may be obtained by dividing the moment of inertia by the total area.

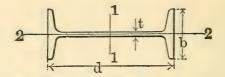
The moment of inertia of a compound section about any axis other than that through its center of gravity may be found in a manner similar to that above described.



1	2	3	4	5	6	7	8	9	10	11
Section Number.	Depth of Beam.	Weight per Foot.	Area of Section.	Thick- ness of Web.	Flange.	Moment of Inertia Axis 1-1.	Section Modulus Axis 1-1.	Radius of Gyra- tion Axis 1-1.	Moment of Inertia Axis 2-2.	Radius of Gyra- tion Axis 2-2.
	d		A	t	b	I	S	r	I'	$\mathbf{r}'$
	Inches.	Pounds.	Sq.Inches	Inches.	Inches.	Inches.4	Inches.3	Inches.	Inches.4	Inches
B. 5	3 "	5.50 6.50 7.50	1.63 1.91 2.21	.17 .26 .36	2.33 2.42 2.52	2.5 2.7 2.9	1.7 1.8 1.9	1.23 1.19 1.15	.46 .53 .60	.53 .52 .52
в 9	4 "	7.50	2.21	.19	2.66	6.0	3.0	1.64	.77	.59
66		8.50	2.50	.26	2.73	6.4	3.2	1.59	.85	.58
66	66	9.50	2.79	.34	2.81	6.7 7.1		1.54	.93	.58
•••	•	10.50	3.09	.41	2.88	7.1	3.0	1.52	1.01	.57
B13	5	9.75	2.87	.21	3.00	12.1	4.8	2.05	1.23	.65
6.6		12.25	3.60	.36	3.15	12.1 13.6	5.4	1.94	1.45	.63
66	66	14.75	4.34	.50	3.29	15.1	6.1	1.87	1.70	.63
B17	6	12.25	3.61	.23	3.33	21.8	<b>₩</b> 9	2.46	1.85	.72
PI.	66	14.75	4.34	.35	3.45	24.0	8.0	2.35	2.09	.69
66	66	17.25	5.07	.47	3.57	26.2		2.27	2.36	.68
B21	7	15.00	4.42	.25	3.66	36.2	10.4	2.86	2.67	.78
66	66	17.50 20.00	5.15 5.88	.35	3.76 3.87	39.2 42.2	11.2 12.1	2.76	2.94	.76
	-	20.00	5.00	•#0	0.07	42.2	12.1	2.00	3.24	.74
B25	8	18.00	5.33	.27	4.00	56.9	14.2	3.27	3.78	.84
66	66	20.25	5.96	.35	4.08	60.2	15.0	3.18	4.04	.82
66	66	22.75	6.69	.44	4.17	64.1	16.0	3.10	4.36	.81
		25.25	7.43	.53	4.26	68.0	17.0	3.03	4.71	.80
B29	9	21.00	6.31	.29	4.33	84.9	18.9	3.67	5.16	.90
66	6.6	25.00	7.35	.41	4.45	91.9	20.4	3.54	5.65	.88
66	66	30.00	8.82	.57	4.61	101.9	22.6		6.42	.85
		35.00	10.29	.73	4.77	111.8	24.8	3.30	7.31	.84
B33	10	25.00	7.37	.31	4.66	122.1	24.4	4.07	6.89	.97
66	66	30.00	8.82	.45	4.80	134.2	26.8	3.90	7.65	.93
66	66	35.00	10.29	.60	4.95	146.4	29.3	3.77	8.52	.91
66	66	40.00	11.76	.75	5.10	158.7	31.7	3.67	9.50	.90
B41	19	31.50	9.26	.35	5.00	215.8	36.0	4 93	9.50	1 01
19.41	12	35.00	10.29	.44	5.09	228.3	38.0		10.07	.99
66	66	40.00	11.76	.56	5.21	245.9	41.0	4.57	10.95	.96
70.50	1.5	40.00	10.40	4.7	==0	4410	F0.0	= 0=	14.00	1.00
B53	15	42.00 45.00	13 94	.41	5.50 5.55	441.8 455.8	58.9 60.8	5.85	14.62 15.09	1.08
66	66	50.00	14.71	.56	5.65	483.4	64.5	5.73	16.04	1.04
6.6	66	55.00	16.18	.66	5.75	511.0	68.1	5.62	16.04 17.06	1.03
66	66	60.00	17.65	.75	5.84	538.6	71.8	5.52	18.17	1.01



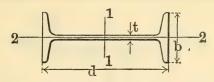
12	13	14	15	16	1
Increase of	Coefficient	of Strength.	Coefficient of	f Deflection.	
Thickness of Web for each Pound Increase	For Fibre Stress of 16 000 Pounds per Square Inch for	For Fibre Stress of 12 500 Pounds per Square Inch for	Uniform Load.	Center Load.	Section Number.
in Weight	Buildings.	Bridges.	N	N'	
	.E	TE,		N'	
.098	17650 19140 20710	13790 14950 16180	.00031253 .00028827 .00026644	.00050006 .00046124 .00042630	B.,5
.074	31810 33890 35980 38070	24850 26480 28110 29750	.00013009 .00012209 .00011500 .00010868	.00020815 .00019535 .00018400 .00017389	B.9
.059	51590 58100 64630	40300 45390 50490	.00006417 .00005698 .00005122	.00010267 .00009117 .00008195	B13
.049	77460 85270 93110	60520 66610 72740	.00003561 .00003235 .00002963	.00005698 .00005177 .00004741	B17
.042	110410 119400 128560	86260 93290 100430	.00002142 .00001980 .00001839	.00003427 .00003168 .00002943	B21
.037	151660 160510 170970 181430	118490 125400 133570 141740	.00001364 .00001289 .00001210 .00001140	.00002183 .00002062 .00001936 .00001825	B25
.033	201300 217930 241460 264990	157260 170260 188640 207020	.00000914 .00000844 .00000762 .00000694	.00001462 .00001350 .00001219 .00001110	B29 "
.029	260470 286250 312390 338530	203500 223630 244050 264480	.00000635 .00000578 .00000530 .00000489	.00001017 .00000925 .00000848 .00000782	B33
.025	383670 405800 437170	299740 317030 341540	.00000360 .0000340 .0000316	.00000575 .00000544 .00000505	B41
.020	628270 648310 687530 726740 765960	490840 506490 537130 567770 598410	.00000176 .00000170 .00000161 .00000152 .00000144	.00000281 .00000272 .00000257 .00000243 .00000231	B53



1	2	3	4	5	6	7	8	9	10	11
Section	Depth of Beam,	Weight per Foot.	Area of Section.	Thick- ness of Web.	Width of Flange.	Moment of Inertia Axis 1-1.	Section Modulus Axis 1-1.	Radius of Gyra- tion Axis 1-1.	Moment of Inertia Axis 2-2.	Radius of Gyration Axis 2-2.
	d		A	t	b	I	S	r	I'	$\mathbf{r}'$
	Inches.	Pounds.	Sq.Inches	Inches.	Inches.	Inches.4	Inches.3	Inches.	Inches.4	Inches.
B 65	18	55.0 60.0 65.0 70.0	15.93 17.65 19.12 20.59	.46 .56 .64 .72	6.00 6.10 6.18 6.26	795.6 841.8 881.5 921.2	93.5 97.9 102.4	6.91 6.79 6.69		1.13 1.11 1.09
В 73	20	65.0 70.0 75.0	19.08 20.59 22.06	.50 .58 .65	6.33	1169.5 1219.8 1268.8	122.0	7.70	29.04	1.19
B 89	24	80.0 85.0 90.0 95.0 100.0	23.32 25.00 26.47 27.94 29.41	.50 .57 .63 .69	7.07 7.13 7.19	2087.2 2167.8 2238.4 2309.0 2379.6	180.7 186.5 192.4	9.31 9.20 9.09	44.35 45.70 47.10	1.33 1.31 1.30

# PROPERTIES OF SPECIAL I-BEAMS.

B105	12	40.0 45.0 50.0 55.0	11.84 13.24 14.71 16.18	.58	5.25 5.37 5.49 5.61	268.9 285.7 303.4 321.0	47.6 50.6	4.65	13.81 14.89 16.12 17.46	1.06 1.05
B109	15	60.0 65.0 70.0 75.0 80.0	17.67 19.12 20.59 22.06 23.53		6.00 6.10 6.19 6.29 6.39	609.0 636.1 663.7 691.2 718.8	84.8 88.5 92.2	5.77 5.68 5.60	25.96 27.42 29.00 30.68 32.46	1.20 1.19 1.18
B113	15	80.0 85.0 90.0 95.0 100.0	23.57 25.00 26.47 27.94 29.41	.90 .99 1.09	6.40 6.50 6.59 6.69 6.79	815.9 843.4 871.0	108.8 112.5 116.1	5.71 5.64 5.58	41.31 43.46 45.79 48.25 50.84	1.32 1.32 1.31
B121	20	80.0 85.0 90.0 95.0 100.0	23.73 25.00 26.47 27.94 29.41	.60 .66 .74 .81 .88	7.06 7.14 7.21	1466.3 1508.5 1557.5 1606.6 1655.6	150.9 155.8 160.7	7.77 7.67 7.58	47.25 48.98 50.78	1.37 1.36 1.35

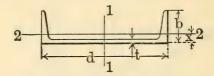


12	13	14	15	16	1	
Increase of	Coefficient	of Strength.	Coefficient of			
Thickness of Web for each Pound Increase in Weight.	For Fibre Stress of 16 000 Pounds per Square Inch for Buildings.	For Fibre Stress of 12 500 Pounds per Square Inch for Bridges.	Uniform Load.	Center Load.	Section Number.	
f	E	IF'	N	N'		
.016	942880 997680 1044740 1091800	736620 779440 816200 852970	.00000098 .00000092 .00000088 .00000084	.00000156 .00000148 .00000141 .00000135	B 65	
.015	1247490 1301110 1353400	974600 1016490 1057340	.00000066 .00000064 .00000061	.00000106 .00000102 .00000098	В 73	
.0123	1855310 1926950 1989700 2052440 2115190	1449460 1505430 1554450 1603470 1652490	.00000037 .00000036 .00000035 .00000034 .00000033	.00000060 .00000057 .00000056 .00000054 .00000052	B 89	

# PROPERTIES OF SPECIAL I-BEAMS.

478130	373540	.00000288	.00000462	B105
539300	421320			6.6
570670	445830	.00000242	.00000387	6.6
866130	676670	.00000127	.00000204	B109
				66
				66
				66
1022000	100010	.00000100	.00000175	
1122290	876790	.00000098	.00000157	B113
1160340	906520	.00000095	.00000152	6.6
				66
				66
1277980	990420	.00000086	.00000138	
1564060	1221920	.00000053	.00000085	B121
1609100	1257110	.00000051	.00000082	6.6
1661390	1297960	.00000050	.00000080	66
				66
1765960	1379660	.00000047	.00000075	•••
	507930 539300 570670 866130 904660 943870 983090 1022300 1122290 1160340 1199550 1238770 1277980	507930         396820           539300         421320           570670         445830           866130         676670           904660         706770           943870         737400           983090         768040           1022300         798670           1122290         876790           160340         906520           199550         937150           238770         967790           1277980         998420           1564060         1221920           1609100         1257110           1661390         1297960           1713670         1338810	507930         396820         .00000272           539300         421320         .00000256           570670         445830         .00000242           866130         676670         .00000127           904660         706770         .00000127           943870         737400         .00000112           983090         768040         .00000112           1022300         798670         .00000098           160340         906520         .0000098           199550         937150         .00000092           1277980         998420         .00000086           1564060         1221920         .00000051           1661390         1297960         .00000050           1713670         1338810         .00000048	$\begin{array}{cccccccccccccccccccccccccccccccccccc$

# PROPERTIES OF STANDARD CHANNELS.



1	2	3	4	5	6	7	8	9	10	111	12
Section Number	Depth of Channel.	Weight per Foot.	Area of Section.	Thick- ness of Web.	Width of Flange.	Moment of Inertia Axis 1-1.	Section Mod- ulus Axis 1-1.	Radius of Gyra- tion Axis 1-1.	Moment of Inertia Axis 2-2.	Section Mod- ulus Axis 2-2.	Radius of Gyra- tion Axis. 2-2.
	d		A	t	b	I	S	r	I'	S'	r'
	Inches.	Pounds.	Sq. Ins.	Inches.	Inches.	Inches.4	Inch's3	Inches.	Inches.4	Inches <sup>3</sup>	Inches.
C 5	3	4.00 5.00 6.00	1.19 1.47 1.76	.17 .26 .36	1.41 1.50 1.60	1.6 1.8 2.1	1.1 1.2 1.4	1.17 1.12 1.08	.20 .25 .31	.21 .24 .27	.41 .41 .42
C,9	4	5.25 6.25 7.25	1.55 1.84 2.13	.18 .25 .33	1.58 1.65 1.73	3.8 4.2 4.6	1.9 2.1 2.3	1.56 1.51 1.46	.32 .38 .44	.29 .32 .35	.45 .45 .46
C13	5 "	6.50 9.00 11.50	1.95 2.65 3.38	.19 .33 .48	1.75 1.89 2.04	7.4 8.9 10.4	3.0 3.5 4.2	1.95 1.83 1.75	.48 .64 .82	.38 .45 .54	.50 .49 .49
C17	6	8.00 10.50 13.00	2.38 3.09 3.82	.20 .32 .44	1.92 2.04 2.16	13.0 15.1 17.3	5.0 5.8	2.34 2.21 2.13	.70 .88 1.07	.50 .57 .65	.54 .53 .53
c21	7	15.50 9.75 12.25	4.56 2.85 3.60	.56 .21 .32	2.28 2.09 2.20	19.5 21.1 24.2	6.0	2.07 2.72 2.59	1.28 .98 1.19	.74 .63 .71	.53 .59 .57
66	66	14.75 17.25 19.75	4.34 5.07 5.81	.42 .53 .63	2.30 2.41 2.51	27.2 30.2 33.2	8.6 9.5	2.50 2.44 2.39	1.40 1.62 1.85	.71 .79 .87 .96	.57 .56 .56
C25	8	11.25 13.75 16.25	3.35 4.04 4.78	.22 .31 .40	2.26 2.35 2.44		9.0		1.33 1.55 1.78	.79 .87 .95	.63 .62 .61
66	"	18.75 21.25	5.51 6.25	.49	2.53 2.62	43.8 47.8	11.0 11.9	2.76		1.02	.60
c%9	9 "	13,25 15.00 20.00	3.89 4.41 5.88	.23 .29 .45	2.43 2.49 2.65	47.3 50.9 60.8	10.5 11.3 13.5	$\frac{3.40}{3.21}$	2.45	.97 1.03 1.19	.67 .66 .65
c33	10	25.00 15.00	7.35	.61	2.81	70.7	15.7 13.4			1.36	.64
6.6	66	20.00	5.88	.38	2.74	78.7	15.7	3.66	2.85	1.34	.70
66	66	25.00 30.00 35.00	7.35 8.82 10.29	.53 .68 .82	2.89 3.04 3.18	103.2	18.2 20.6 23.1		3.40 3.99 4.66	1.50 1.67 1.87	.68 .67 .67
C41	12	20.50 25.00 30.00	6.03 7.35 8.82	.28 .39 .51	3.05	128.1 144.0 161.6	24.0	4.43	4.53	1.75 1.91 2.09	.81 .78 .77
66	66	35.00	10.29	.64	3.30	179.3 196.9	29.9	4.17	5.90	2.27	.76 .75
C53	15	40.00	9.90	.76		312.6			6.63		.75
"	"	35.00	10.29	.43	3.43	319.9	42.7	5.57	8.48	3.22	.91
66	6.6	40.00 45.00	13.24	.52	3.62	347.5 375.1	50.0	5.44 5.32		3.63	.89
66	66	50.00 55.00		.72 .82	3.72 3.82	402.7 430.2	53.7 57.4	5.23 5.16	11.22 12.19	3.85	.87

#### PROPERTIES OF STANDARD CHANNELS.



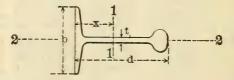
13	14	15	16	17	18	1
Distance	Increase of	Coef. of	Strength.	Coef. of I	Deflection.	
of Center of Gravity from	Thickness of Web for each	Fibre Stress 16 000 Pounds	Fibre Stress 12 500 Pounds	Uniform	Center	Section
Outside of Web.	Pound Increase in Weight.	per Sq. Inch for Buildings.	per Sq. Inch. for Bridges.	Load.	Load.	Number.
X	f	F	F'	N	N'	
Inches.	Inches.					
.44 .44 .46	.098	11630 13140 14710	9090 10270 11490	.0004743 .0004199 .0003751	.0007589 .0006718 .0006001	C 5
.46 .46	.074	20230 22270 24360	15800 17400 19030	.0002046 .0001858 .0001698	.0003273 .0002973 .0002717	C.9
.49 .48 .51	.059	31640 37860 44390	24720 29570 34680	.0001046 .0000875 .0000746	.0001674 .0001399 .0001193	c13
.52 .50 .52	.049	46210 53750 61600	36100 42000 48120	.0000597 .0000513 .0000448	.0000855 .0000821 .0000717	C17 "
.55 .55 .53	.042	69440 64270 73650	54250 50210 57540	.0000397 .0000368 .0000321	.0000636 .0000588 .0000714	C21
.53 .55		82740 91950 101100	64690 71840 78990	.0000286 .0000257 .0000234	.0000457 .0000411 .0000374	66 66
.58	.037	86140	67300	.0000240	.0000384	C25
.56 .56 .57		95990 106450 116910 127370	75000 83170 91340 99510	.0000216 .0000194 .0000177 .0000162	.0000345 .0000311 .0000283 .0000260	66
.61 .59 .58	.033	112170 120540 144070	87630 94170 112550	.0000164 .0000153 .0000128	.0000262 .0000244 .0000204	c29
.62 .64	.029	167590 142680	130930	.0000110	.0000176	C33
.61 .62 .65	.029	167940 194090 220230	131210 151630 172060	.0000099 .0000085 .0000075	.0000158 .0000136 .0000120	"
.69 .70 .68	.025	246380 227750 256000 287370	192480 177930 200000 224510	.0000067 .0000061 .0000054 .0000048	.0000107 .0000097 .0000086 .0000077	C41
.69 .72		318750 350120	249020 273530	.0000043	.0000069	66
.79 .79 .78	.020	444520 455030 494250	347280 355500 386130	.0000025 .0000024 .0000022	.0000040 .0000039 .0000036	C53
.79 .80 .82		533470 572680 611900	416770 447410 478050	.0000021 .0000019 .0000018	.0000033	66 66
.02		011000	±78090	.0000018	.0000029	

#### PROPERTIES OF SPECIAL CHANNELS.



1	2	3	4	5	6	7	8	9	10	11	12	13
Sec- tion Num- ber.	Depth of Chan'l.	W'ght per Foot.	Area of Section.	Thick- ness of Web.	Width of Flange	Thick- ness of Flange	Slope of Flange	Moment of Inertia Axis 1-1.	Section Mod- ulus Axis 1-1.	Radius of Gyra- tion Axis 1-1.	Moment of Inertia Axis 2-2.	Section Mod- ulus Axis 2-2.
	d		A	t	b	S		I	8	r	I'	S'
	Ins.	Lbs.	Sq. Ins.	Inches.	Inches	Inches.	g	Inches.4	Ins.3	Inches	Inches,4	Ins.3
C91	66	21.4 23.9 26.4 28.9 31.4 33.9	6.30 7.03 7.77 8.50 9.24 9.97	.31 .37 .44 .50 .56	2.64 2.70 2.76 2.82 2.89 2.95	.34	.17	128.2 137.0 145.9 154.7 163.5 172.3	22.8 24.3 25.8 27.3	4.41 4.33 4.27 4.21	3.80 4.09 4.38	1.69 1.78 1.86
C95		32.0		.38	4.00	.34	.15				11.54	
66	66		10.29	.45	4.08	66	66	251.5			12.54	
66			10.88	.50	4.12	66	66				$13.10 \\ 13.94$	
66			11.76 $13.24$	.56	$\frac{4.19}{4.30}$	66	66	292.9			15.32	
66		TU.0	14.71	.79	4.42	66	66				16.71	
66			16.18	.90	4.53	66	66				18.14	
			'									

#### PROPERTIES OF BULB BEAMS.



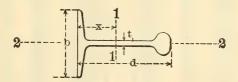
1	2	3	4	5	6	7	8	9
Section Number.	Depth of Beam.	Weight per Foot.	Area of Section.	Thickness of Web.	Width of Flange.	Moment of Inertia Axis 1-1.	Modulus Axis 1-1.	Radius of Gyration Axis 1-1.
	d		A	t	b	I	S	r
	Inches.	Pounds.	Sq. Ins.	Inches.	Inches.	Inches.4	Inches.3	Inches.
B171	5 7 3 2	11.5	3.37	3/8	27/8	11.39	3.71	1.84
B173	6	14.0	4.11	9 32	43/8	21.52	6.12	2.29
66	66	15.3 18.4	4.48 5.42	9 32 132 1/2	43/8 47/8 419 419	22.73 25.72	6.55 7.59	2.25

#### PROPERTIES OF SPECIAL CHANNELS.



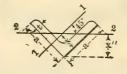
14	15	16	17	18	19	20	1
		Increase of		strength.	Coef. of I	Deflection.	
of Gyra- tion Axis 2-2.	Center of Gravity from Outside of Web.	Thickness of Web for each Lb. Increase in Weight.	Fibre Stress	Fibre Stress 12 500 Pounds per Sq. Inch for Bridges.	Uniform Load.	Center Load.	Section Number.
Inches.	Inches.	Inches.	F	F′	N	N'	
.72 .71 .70 .69 .69	.63 .62 .62 .63 .64 .65	.024	227950 243630 259320 275000 290690 306380	190340 202590 214850 227100	.0000061 .0000057 .0000053 .0000050 .0000048	.0000091 .0000085 .0000080 .0000076	C91
1.11 1.10 1.10 1.09 1.08 1.07	1.01 .99 .98 .97 .97 .98 1.00	.023	389710 412750 426340 446740 480720 514710 548700	322460 333080 349010 375560 402120	.0000027	.0000049 .0000048 .0000046 .0000042	C95

#### PROPERTIES OF BULB BEAMS.



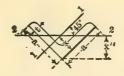
10	11	12	13	14	15	1 .
Distance of	Increase of	Coef. of	Strength.	Coef. of D	eflection.	
Center of Gravity from Outside of Flange.	Thickness of	16 000 Pounds	Fibre Stress 12 500 Pounds per Sq. Inch for Bridges.	Uniform Load.	Center Load.	Section Number.
X Inches.	f	F	F'	N	N'	
2.15		39600	30940	.0000681	.0001090	B171
2.49 2.53 2.61	.049	65320 69860 80930	51030 54580 63230	.0000341	.0000577 .0000546 .0000483	В173

### PROPERTIES OF STANDARD ANGLES.



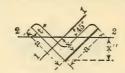
1	2	3	4	5	6	7	8
Section Number.	Dimensions.	Thickness.	Weight per Foot.	Area of Section.	Distance of Center of Gravity from Back of Leg.	Moment of Inertia Axis 1-1.	Section Modulus Axis 1-1.
	ara	t		A	X	I	S
	Inches.	Inches.	Pounds.	Sq. Ins.	Inches.	Inches.4	Inches.3
A.,5 A.,7	3/4 x 3/4 1 x 1	1/8 3 1 6 1/8 8 3 6	.6 .9 .8 1.2 1.5	.18 .25 .24 .34	.23 .25 .30 .32	.009 .012 .022 .030	.017 .024 .031
		74		.44	.34	.037	.056
A 9 "	1¼ x 1¼	1/8 3 1 6 1/4 1/8 3 1 6 1/4 5 1 6	1.1 1.5 2.0 2.4	.30 .44 .57 .69	.36 .38 .40 .42	.044 .061 .077 .090	.049 .071 .091 .109
A11	1½ x 1½	1/8	1.3	.36 .53	.42	.08	.072
66	66	1/8 3 1/4 5 1/4 5 1/6 3/8	1.8	.53	.44	.11	.104
6.6	66	74 5	2.4	.84	.49	.16	.134 .162 .188
6.6	6.6	3/8	3.4	.99	.51	.16	.188
66	66		3.9	1.13	.53	.21	.214
A13	13/4 x 13/4	3 16	2.2	.63	.51	.18	.14
66	66	4_5	2.8 3.4	.82 1.00 1.18	.53	.23 .27 .31	.19 .23
66	66	3/2	4.0	1.18	.55	.31	.26
66	66	3 16 1/4 5 6 3/8 7 7 16 1/2	4.6	1.34	.59	.35	.30
		1/2	5.1	1.50	.61	.38	.33
A15	2 x 2	3 16 1/4 5 16 3/8 76 1/2	2.5 3.2	.72	.57	.27	.19 .25
66	66	5	4.0	.94 1.16	.61	.35	.30
66	66	3/8	4.7 5.3	1.36	.64	.48	.35
66	66	16	5.3	1.56	.66	.54	.40
		1/2	6.0	1.75	.68		745
A17	2½ x 2½	3 16 14 5 13 8 7 16 12 2 9	3.1 4.1	.91	.69 .72	.55 .70	.30
66	66	5 16	5.0	1.47	.74	.85 .98	.48
66	66	3/8	5.9 6.8	1.74	.76	.98	.57
66	66	16	7.7	2.00	.78	1.11 1.23	.72
66	6.6	72	8.5	2.50	.83	1.34	.80
A19	3 x 3	1/4	4.9	1.44	.84	1.24	.58
	66	5 16	6.1	1.78	.87	1.51 1.76	.71
66	66	1/4 5 6 8 7 6 1/2 9 6 5 8 118	7.2	2.11	.89	1.76	.83 .95
66	66	16	9.4	2.44 2.75	.91 .93	1.99 2.22	1.07
6.6	66	9 16	10.4	3.06	.95	2.43	1.19
66	. 66	5/8	11.5	3.36	.98	2.62	1.30
	1	18	12.5	3.66	1.00	2.81	1.40

#### PROPERTIES OF STANDARD ANGLES.



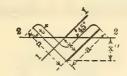
9	10	11	12	13	1
Radius of Gyration Axis 1-1.	Distance of Center of Gravity from External Apex.	Least Moment of Inertia Axis 2-2.	Section Modulus Axis 2-2.	Least Radius of Gyration Axis 2-2.	Section Number.
r	x''	1"	S''	r''	
Inches.	Inches.	Inches,4	Inches.3	Inches.	
.22 .22 .30 .30	.33 .36 .42 .45	.004 .005 .009	.011 .014 .021 .028	.14 .14 .19 .19	A.,5 A.,7
.29	.48	.013 .016	.034	.19	66
.38 .38 .37 .36	.51 .54 .57 .60	.018 .025 .033 .040	.035 .047 .057 .066	.24 .24 .24 .24	A 9
.47 .46 .45 .44	.60 .63 .66 .69	.031 .045 .058 .070 .082	.053 .072 .088 .101	.30 .29 .29 .29	A11
.43	.75	.094	.126	.29	66
.54 .53 .52 .51 .51	.72 .75 .78	.073 .094	.10 .13 .15	.34 .34	A13
.52 .51	.81	.094 .113 .133	.15 .16	.34	66
.51 .50	.84 .87	.152 .171	.18 .20	.34 .34	66
.62 .61 .60	.80 .84	.11 .14 .17	.14 .17 .20 .22 .25 .27	.39 .39	A15
.60	.87 .90	.17 .20	.20	.39	66
.59 .59 .58	.93 .96	.23 .26	.25	.38	66
.78	.98 1.01	.22	.22 .28	.49	A17
.76	1.05	.29 .35	.33	.49	6.6
.75 .75	1.08	.41 .46	.38 .42	.48 .48	66
.74	1.14	.52	.46	.48	66
.73	1.17	.58	.49	.48	410
.93 .92	1.19 1.22 1.26	.50 .61	.42 .50	.59 .59	A19
.92 .91 .91	1.26	.72	.57 .64	.58	66
.90	1.29 1.32	.82 .92	.70	.58 .58	66
.89	1.35 1.38	$\frac{1.02}{1.12}$	.76 .81	.58	66
.88 .88	1.41	1.22	.86	.58 .58	66

## PROPERTIES OF STANDARD ANGLES. EQUAL LEGS.

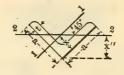


1	2	3	4	5	6	7	8
Section Number.	Dimensions.	Thickness	Weight per Foot.	Area of Section.	Distance of Center of Gravity from Back of Leg.	Moment of Inertia Axis 1-1.	Section Modulus Axis 1-1.
	ara	t		A	X	I	S
	Inches.	Inches.	Pounds.	Sq. Ins.	Inches.	Inches.4	Inches.3
A21	3½ x 3½ 3½	6-00/5-10/20/10/10/4-00/00/00/00/00/00/00/00/00/00/00/00/00/	7.2 8.5 9.8 11.1 12.4 13.6 14.8 16.0 17.1 18.3	2.09 2.49 2.88 3.25 3.63 3.99 4.34 4.69 5.03 5.36	.99 1.01 1.04 1.06 1.08 1.10 1.12 1.15 1.17	2.45 2.87 3.26 3.69 4.33 4.65 4.96 5.25 5.53	.98 1.15 1.32 1.49 1.65 1.81 1.96 2.11 2.25 2.39
A28	4 x 4	6,00,7 10,00	8.2 9.8 11.3 12.8 14.3 15.7 17.1 18.5 19.9 21.2	2.41 2.86 3.31 3.75 4.19 4.62 5.44 5.84 6.24	1.12 1.14 1.16 1.18 1.21 1.23 1.25 1.27 1.29 1.31	3.71 4.36 4.97 5.56 6.12 6.66 7.17 7.66 8.14 8.59	1.29 1.52 1.75 1.97 2.19 2.40 2.61 2.81 3.01 3.20
A27	6 x 6	8/7H/20H8/80H8/80H8/80H8/	14.9 17.2 19.6 21.9 24.2 26.5 28.7 31.0 35.3 37.4	4.36 5.06 5.75 6.44 7.11 7.78 8.44 9.09 9.74 10.38 11.00	1.64 1.66 1.68 1.71 1.73 1.75 1.78 1.80 1.82 1.84 1.86	15.39 17.68 19.91 22.07 24.16 26.19 28.15 30.06 31.92 33.72 35.46	3.53 4.07 4.61 5.14 5.66 6.17 6.66 7.15 7.63 8.11 8.57
A35	8 x 8	1/2/2 E / S1-E / 4/3/E / S1-E / 1-E / 8/3/E / S1-E	26.4 29.6 32.7 35.8 38.9 42.0 45.0 48.1 51.0 54.0 56.9	7.75 8.69 9.61 10.53 11.44 12.34 13.24 14.13 15.00 15.88 16.74	2.19 2.21 2.23 2.25 2.28 2.30 2.32 2.34 2.37 2.39 2.41	48.65 54.09 59.43 64.64 74.72 79.58 84.34 88.98 93.53 97.97	8.37 9.34 10.30 11.25 12.18 13.11 14.02 14.91 15.80 16.67 17.53

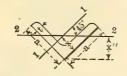
#### PROPERTIES OF STANDARD ANGLES.



9	10	11	12	13	1
Radius of Gyration Axis 1-1.	Distance of Center of Gravity from External Apex.	Least Moment of Inertia Axis 2-2.	Section Modulus Axis 2-2.	Least Radius of Gyration Axis 2-2.	Section Number.
r	x''	I''	S''	r''	Humbor.
Inches.	Inches.	Inches.4	Inches.3	Inches.	
1.08 1.07 1.07 1.06 1.05 1.04 1.04 1.03 1.02	1.40 1.43 1.46 1.50 1.53 1.56 1.59 1.62 1.65 1.68	.99 1.16 1.33 1.50 1.66 1.82 1.97 2.13 2.28 2.43	.71 .81 .91 1.00 1.09 1.17 1.24 1.31 1.38 1.45	.69 .68 .68 .68 .68 .67 .87 .67	A21
1.24 1.23 1.23 1.22 1.21 1.20 1.19 1.19 1.18	1.58 1.61 1.64 1.67 1.71 1.74 1.77 1.80 1.83	1.50 1.77 2.02 2.28 2.52 2.76 3.00 3.23 3.46 3.69	.95 1.10 1.23 1.36 1.48 1.59 1.70 1.80 1.89 1.99	.79 .79 .78 .78 .78 .77 .77 .77 .77	A23
1.88 1.87 1.86 1.85 1.84 1.83 1.83 1.82 1.81 1.80 1.80	2.32 2.34 2.38 2.41 2.45 2.54 2.54 2.560 2.64	6.19 7.13 8.04 8.94 9.81 10.67 11.52 12.35 13.17 13.98 14.78	2.67 3.04 3.37 3.70 4.01 4.31 4.59 4.86 5.12 5.37 5.61	1.19 1.18 1.18 1.17 1.17 1.17 1.17 1.16 1.16	A27
2.51 2.50 2.49 2.48 2.47 2.46 2.45 2.44 2.44 2.43 2.43	3.09 3.12 3.16 3.19 3.22 3.25 3.28 3.35 3.35 3.38 3.41	19.56 21.79 23.97 26.13 28.24 30.33 32.38 34.40 36.40 38.38 40.33	6.33 6.98 7.60 8.20 8.77 9.33 9.86 10.38 10.38 11.36 11.36	1.59 1.58 1.58 1.57 1.57 1.56 1.56 1.56 1.56	A35

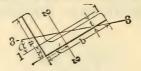


1	2	3	4	5	6	7	8
Section Number.	Dimensions.	Thickness.	Weight per Foot.	Area of Section.	Distance of Center of Gravity from Back of Leg.	Moment of Inertia Axis 1-1,	Section Modulus Axis 1-1.
	ara	t		A	x	I	S
	Inches.	Inches.	Pounds.	Sq. Ins.	Inches.	Inches.4	Inches,3
A61	1½ x 1½	1/8 3 16	1.3 1.8	.36 .53	.42	.08	.072
A41	2½ x 2½	3 1 4 4 5 1 6 3 8 7 7 8	2.8 3.7 4.5 5.3 6.1	.81 1.07 1.31 1.55 1.78	.63 .65 .68 .70	.39 .50 .61 .70	.24 .32 .39 .45
A43	2 <sup>3</sup> / <sub>4</sub> x 2 <sup>3</sup> / <sub>4</sub>	3 16 1/4 5 18 3/8 17 17	3.4 4.5 5.6 6.6 7.6 8.5	1.00 1.32 1.63 1.93 2.22 2.50	.76 .78 .80 .82 .85	.73 .95 1.15 1.33 1.51 1.67	.37 .48 .59 .69 .79
A45	4½ x 4½ 	5 e / 8 7 e / 2 9 e / 8 1 e /	9.3 11.0 12.8 14.5 16.2 17.8 19.5	2.72 3.24 3.75 4.25 4.75 5.24 5.72	1.24 1.26 1.29 1.31 1.33 1.35 1.35	5.36 6.30 7.20 8.07 8.91 9.71 10.48	1.64 1.95 2.24 2.53 2.81 3.09 3.35
A47	5 × 5	3/8 76 122 9 6 5/8 115	12.3 14.3 16.2 18.1 20.0 21.8	3.61 4.19 4.75 5.31 5.86 6.41	1.39 1.41 1.43 1.46 1.48 1.50	8.74 10.02 11.25 12.44 13.58 14.68	2.42 2.79 3.16 3.51 3.86 4.20



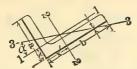
9	10	11	12	13	1
Radius of Gyration. Axis 1-1.	Distance of Center of Gravity from External Apex.	Least Moment of Inertia Axis 2-2.	Section Modulus Axis 2-2.	Least Radius of Gyration Axis 2-2.	Section Number,
r	<b>x</b> ''	I''	S''	r''	
Inches.	Inches.	Inches.4	Inches,3	Inches.	
.47 .46	.60 .63	.031 .045	.053 .072	.30	A61
.70 .69 .68 .67	.89 .92 .96 .99	.16 .21 .25 .29 .33	.18 .22 .26 .30	.44 .44 .44 .43 .43	A41
.86 .85 .83 .83 .82	1.07 1.10 1.13 1.17 1.20 1.23	.30 .38 .47 .55 .63	.28 .35 .41 .47 .52	.54 .54 .53 .53 .53	A43
1.40 1.40 1.39 1.38 1.37 1.36 1.35	1.75 1.79 1.82 1.85 1.88 1.91 1.95	2.16 2.54 2.92 3.29 3.64 3.99 4.34	1.23 1.42 1.61 1.78 1.94 2.03 2.23	.89 .89 .88 .88 .88 .87	A45
1.56 1.55 1.54 1.53 1.52 1.51	1.96 2.00 2.03 2.06 2.09 2.12	3.53 4.05 4.56 5.06 5.55 6.03	1.79 2.03 2.25 2.46 2.66 2.84	.99 .98 .98 .98 .97	A47

### PROPERTIES OF STANDARD ANGLES.



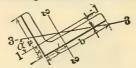
1	2	3	4	5	6	7	8
Section	Dimensions.	Thickness.	Weight per Foot.	Area of Section.	Distance of Center of Gravity from Back of Longer Leg.	Moment of Inertia Axis 1-1.	Section Modulus Axis 1-1.
Number.	bra	t		A	x	I	S
	Inches.	Inches.	Pounds.	Sq. Ins.	Inches.	Inches.4	Inches.3
A91	2½ x 2	3 6 /4 6 6 7 6 /2 9 6	2.8 3.7 4.5 5.3 6.1 6.8 7.6	.81 1.07 1.31 1.55 1.78 2.00 2.22	.51 .54 .56 .58 .60 .63	.29 .37 .45 .51 .58 .64	.20 .25 .31 .36 .41 .46
A93	3 x 2½	1/4 -56/8 -76/2 -6/8 -6/8 -6/8	4.5 5.6 6.6 7.6 8.5 9.5 10.4	1.32 1.63 1.93 2.22 2.50 2.78 3.05	.66 .68 .71 .73 .75 .77	.74 .90 1.04 1.18 1.30 1.42 1.53	.40 .49 .58 .66 .74 .82
A95	3½ x 2½	1/45/6/6/6/6/6/6/6/46/4	4.9 6.1 7.2 8.3 9.4 10.4 11.5 12.5 13.4	1.44 1.78 2.11 2.44 2.75 3.06 3.36 3.66 3.94	.61 .64 .66 .68 .70 .73 .75 .77	.78 .94 1.09 1.23 1.36 1.49 1.61 1.72 1.83	.41 .50 .59 .68 .76 .84 .92 .99
A97	3½ x 3	5 6 0 7 5 20 6 0 16 4 19 6 0	6.6 7.9 9.1 10.2 11.4 12.5 13.6 14.7 15.8 16.8	1.94 2.30 2.66 3.00 3.34 3.68 4.00 4.32 4.63 4.93	.81 .83 .85 .88 .90 .92 .94 .96 .98	1.58 1.85 2.09 2.33 2.55 2.76 2.96 3.15 3.33 3.50	.72 .85 .98 1.10 1.21 1.33 1.44 1.54 1.65 1.75
A99	4 x 3	5-10/0-16/29-16/29-16/4-186/8	7.2 8.5 9.8 11.1 12.4 13.6 14.8 16.0 17.1 18.3	2.09 2.49 2.88 3.25 3.63 3.99 4.34 4.69 5.03 5.36	.76 .78 .80 .83 .85 .87 .89 .92 .94	1.65 1.92 2.18 2.42 2.66 2.87 3.08 3.28 3.47 3.66	.73 .87 .99 1.12 1.23 1.35 1.46 1.57 1.68 1.79

### PROPERTIES OF STANDARD ANGLES. UNEQUAL LEGS.



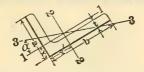
9	10	11	12	13	14	15	1
Radius of Gyration Axis 1-1.	Distance of Center of Gravity from Back of Shorter Leg.	Moment of Inertia Axis 2-2.	Section Modulus Axis 2-2.	Radius of Gyration Axis 2-2.	Tangent of Angle	Least Radius of Gyration Axis 3-3.	Section
r	x'	I'	S'	$\mathbf{r}'$	œ	r''	Number.
Inches.	Inches.	Inches.4	Inches.3	Inches.		Inches.	
.60 .59 .58 .58 .57 .56	.76 .79 .81 .83 .85 .88	.51 .65 .79 .91 1.03 1.14 1.24	.29 .38 .47 .55 .62 .70	.79 .788 .7765 .775 .775	.632 .626 .620 .614 .607 .600	.43 .42 .42 .42 .42 .42 .42	A91
.75 .74 .73 .72 .72 .71	.91 .93 .96 .98 1.00 1.02 1.04	1.17 1.42 1.66 1.88 2.08 2.28 2.46	.56 .69 .81 .93 1.04 1.15 1.26	.95 .94 .93 .91 .91	.684 .680 .676 .672 .666 .661	.53 .52 .52 .52 .52 .52	A98
.74 .73 .72 .70 .69 .69	1.11 1.14 1.16 1.18 1.20 1.23 1.25 1.27 1.29	1.80 2.19 2.56 2.91 3.24 3.55 3.85 4.13 4.40	.75 .93 1.09 1.26 1.41 1.56 1.71 1.85	1.12 1.11 1.10 1.09 1.09 1.08 1.07 1.06 1.06	.506 .501 .496 .491 .486 .480 .472 .468 .461	.54444 .554455 .553 .553 .554	A95
.90 .99 .89 .87 .87 .85 .85 .85	1.06 1.08 1.10 1.13 1.15 1.17 1.19 1.21 1.23 1.25	2.33 2.72 3.10 3.45 3.79 4.11 4.41 4.70 4.98 5.24	.95 1.13 1.29 1.45 1.61 1.76 1.91 2.05 2.20 2.33	1.10 1.09 1.08 1.07 1.07 1.06 1.05 1.04 1.04	.724 .721 .718 .714 .711 .707 .703 .698 .694 .689	.632 .622 .622 .622 .632 .632	A97
.89 .88 .87 .86 .85 .84 .83 .83	1.26 1.28 1.30 1.33 1.35 1.37 1.39 1.42 1.44	3.38 3.96 4.52 5.55 6.03 6.49 6.93 7.35	1.23 1.46 1.68 1.89 2.09 2.30 2.49 2.68 2.87 3.05	1.27 1.26 1.25 1.25 1.24 1.23 1.22 1.22 1.21	.554 .5547 .543 .538 .529 .524 .518 .512	.65 .64 .64 .64 .64 .64 .64 .64	A99

#### PROPERTIES OF STANDARD ANGLES.

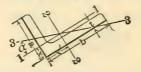


1	2	3	4	5	6	7	8
Section Number.	Dimensions.	Thickness.	Weight per Foot.	Area of Section.	Distance of Center of Gravity from Back of Longer Leg.	Moment of Inertia Axis 1-1.	Section Modulus Axis 1-1.
number.	bra	t		A	x	I	S
	Inches.	Inches.	Pounds.	Sq. Ins.	Inches.	Inches.4	Inches.3
A101	5 x 3	56 8 5 29 6 6 16 4 6 6 6 7	8.2 9.8 11.3 12.8 15.7 17.1 18.5 19.9 21.2	2.41 2.86 3.31 3.75 4.19 4.61 5.03 5.44 5.84 6.24	.68 .70 .73 .75 .770 .82 .84 .86 .88	1.75 2.04 2.32 2.58 2.83 3.06 3.29 3.51 3.71 3.91	.75 .89 1.02 1.15 1.27 1.39 1.51 1.62 1.74
A108	5 x 3½	5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	8.7 10.4 12.0 13.6 15.2 16.8 18.3 19.8 21.3 22.7 24.2	2.56 3.53 4.00 4.47 4.93 5.38 6.25 6.68 7.09	.84 .86 .88 .91 .93 .95 .97 1.00 1.02 1.04 1.06	2.72 3.18 3.63 4.05 4.45 4.83 5.20 5.55 6.21 6.52	1.02 1.21 1.39 1.56 1.73 1.90 2.06 2.22 2.37 2.52 2.67
A105	6 x 3½	3/7-1-/0-16/0-16/4-36/0-16-1	11.7 13.5 15.3 17.1 18.9 20.6 22.4 24.0 25.7 27.3 28.9	3.43 3.97 4.50 5.03 5.55 6.06 6.57 7.55 8.03 8.50	.79 .81 .83 .86 .88 .90 .93 .95 .97 .99	3.34 3.81 4.25 4.67 5.08 5.47 5.82 6.55 6.88 7.21	1.23 1.41 1.59 1.77 1.94 2.11 2.27 2.43 2.59 2.74 2.90
A107	6 x 4	3/20/6/8-40/40/8/85/40/1	12.3 14.3 16.2 18.1 20.0 21.8 23.6 25.4 27.2 28.9 30.6	3.61 4.19 4.75 5.31 5.86 6.41 6.94 7.47 7.99 8.50 9.00	.94 .96 .99 1.01 1.03 1.06 1.08 1.10 1.12 1.14	4.90 5.60 6.27 6.91 7.52 8.11 8.68 9.23 9.75 10.26 10.75	1.60 1.85 2.08 2.31 2.54 2.76 2.97 3.18 3.39 3.59 3.79

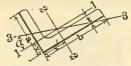
## PROPERTIES OF STANDARD ANGLES. UNEQUAL LEGS.



9	10	11	12	13	14	15	1
Radius of Gyration Axis 1-1.	Distance of Center of Gravity from Back of Shorter Leg.	Moment of Inertia Axis 2-2.	Section Modulus Axis 2-2.	Radius of Gyration Axis 2-2.	Tangent of Angle	Least Radius of Gyration Axis 3-3.	Section Number.
r	x'	I'	S'	r'	$\propto$	r''	Trumbor,
Inches.	Inches.	Inches.4	Inches.3	Inches.		Inches.	
.85 .84 .84 .83 .82 .82 .81 .80 .80	1.68 1.70 1.73 1.75 1.77 1.80 1.82 1.84 1.86 1.88	6.26 7.37 8.43 9.45 10.43 11.37 12.28 13.15 13.98 14.78	1.89 2.24 2.58 2.591 3.23 3.55 3.86 4.16 4.46 4.75	1.61 1.60 1.59 1.58 1.57 1.56 1.55 1.55	.368 .364 .361 .357 .353 .349 .345 .340 .336	.66 .65 .65 .65 .65 .64 .64 .64	A101
1.03 1.02 1.01 1.01 1.00 .99 .98 .98 .97 .96	1.59 1.61 1.63 1.68 1.70 1.72 1.75 1.77 1.79	6.60 7.78 8.90 9.99 11.03 12.03 12.99 13.92 14.81 15.67 16.49	1.94 2.29 2.64 2.99 3.32 3.65 4.28 4.58 4.58 5.17	1.61 1.60 1.59 1.58 1.57 1.56 1.55 1.54 1.53 1.53	.489 .485 .482 .479 .476 .472 .468 .464 .455 .451	.7665.7555.775.775.775.7755555555555555	A103
.99 .98 .97 .96 .95 .95 .93 .93 .93	2.04 2.06 2.08 2.11 2.13 2.15 2.18 2.20 2.22 2.24 2.26	12.86 14.76 16.59 18.37 20.08 21.74 23.34 24.89 26.39 27.84 29.15	3.24 3.75 4.24 4.72 5.65 6.10 6.55 6.98 7.41 7.80	1.94 1.93 1.92 1.91 1.90 1.89 1.89 1.88 1.87 1.86	.350 .347 .344 .341 .338 .334 .331 .327 .323 .320 .317	.77665555555555555555555555555555555555	A105
1.17 1.16 1.15 1.14 1.13 1.13 1.12 1.11 1.11 1.10	1.94 1.96 1.99 2.01 2.03 2.06 2.08 2.10 2.12 2.14 2.17	13.47 15.46 17.40 19.26 21.07 22.82 24.51 26.15 27.73 29.26 30.75	3.32 3.83 4.83 4.83 5.31 5.78 6.25 6.70 7.15 7.59 8.02	1.93 1.92 1.91 1.90 1.89 1.88 1.87 1.86 1.85	.446 .443 .440 .438 .434 .431 .428 .425 .421 .418	.87 .87 .87 .86 .86 .86 .86 .86	A107



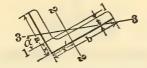
1	2	3	4	5	6	7	8
Section			Weight per Foot.	Area of Section.	Distance of Center of Gravity from Back of Longer Leg.	Moment of Inertia Axis 1-1.	Section Modulus Axis 1-1.
2.0044.0	bra	t		A	X	1	S
	Inches.	Inches.	Pounds.	Sq. Ins.	Inches.	Inches.4	Inches.3
A17	, ,	1	1.0	.28	.24	.020	.003
A16	37 1½ x 3	4 1/8	1.0	.27	.17	.011	.018
A16	35 13/4 x 11/	8 16	2.8	.81	.33	.073	.093
A16	33 13/4 x 11/2	4 16	1.8	.53	.33	.07	.07
A18	21 2 x 13/	3 16 1/4 5 13 3 8 7 16	2.1 2.7 3.3 3.9 4.4	.60 .79 .96 1.13 1.29	.35 .37 .39 .42 .44	.10 .12 .14 .16 .18	.10 .12 .14 .17
A12	23 2 x 11	1/8 3/6 1/4 5/6 3/8 7/6	1.5 2.2 2.8 3.4 4.0 4.6	.43 .63 .82 1.00 1.18 1.34	.37 .39 .41 .44 .46 .48	.08 .12 .15 .18 .21 .23	.07 .11 .14 .17 .20
A1	$2\frac{5}{16} \times 1\frac{1}{1}$		2.1	.60	.30	.08	.08
A18		-	2.3 3.0 3.7 4.4 5.0	.67 .88 1.08 1.27 1.45	.28 .30 .33 .35 .37	.07 .09 .11 .13	.08 .10 .12 .14 .16
A1:	27 2½ x 1½	2 16 1/4 5 16 3/8 7/6	2.5 3.2 4.0 4.7 5.3	.72 .94 1.16 1.36 1.56	.35 .38 .40 .42 .44	.13 .16 .19 .22 .24	.11 .14 .17 .20 .23
A16	31 2½ x 13	4 16 14	2.6 3.4	1.00	.43 .45	.20 .25	.15 .20
A13	28 23/4 x 11/	2 3 16 1/4 5 16 3/8 76	2.6 3.4 4.2 5.0 5.7	.77 1.00 1.24 1.46 1.67	.34 .36 .38 .41 .43	.13 .17 .20 .22 .25	.11 .14 .18 .21 .23
A13	29 3 x 2	3 16 1/4 5 6 8 7 16 1/2	3.1 4.1 5.0 5.9 6.8 7.7	.91 1.19 1.47 1.74 2.00 2.25	.47 .49 .51 .54 .56	.31 .39 .47 .54 .61 .67	.20 .26 .32 .37 .42 .47



9	10	11	12	13	14	15	1
	7 0.0				1.7		
Radius of Gyration Axis 1-1.	Distance of Center of Gravity from Back of Shorter Leg.	Moment of Inertia Axis 2-2.	Section Modulus Axis 2-2.	Radius of Gyration Axis 2-2.	Tangent of Angle	Radius of Gyration Axis 3-3.	Section
r	x'	I'	S'	r'	$\propto$	r''	Number.
Inches.	Inches.	Inches.4	Inches.3	Inches.		Inches.	
.27	.46	.052	.057	.44	.458	.20	A170
.20	.55	.061	.064	.48	.261	.16	A167
.30	.65	.140	.127	.42	.104	.30	A165
.36	.58	.16	.14	.55	.496	.27	A163
.41 .39 .38 .38	.66 .68 .71 .73 .75	.24 .31 .37 .42 .47	.18 .23 .28 .33 .38	.63 .62 .61 .60	.475 .455 .445 .434 .421	.31 .30 .29 .29 .30	A121
.45 .44 .43 .42 .42	.62 .64 .66 .69 .71	.17 .25 .32 .38 .43 .48	.13 .18 .24 .29 .34 .38	.64 .63 .62 .62 .61	.558 .551 .543 .534 .524 .512	.33 .32 .32 .32 .32	A123
.36	.80	.33	.22	.74	.330	.29	A155
.33 .33 .32 .32 .31	.91 .93 .95 .97 1.00	.43 .55 .66 .77	.27 .35 .43 .50	.80 .79 .79 .78 .77	.264 .256 .247 .238 .228	.27 .27 .26 .26 .27	A125
.42 .41 .41 .40 .40	.85 .88 .90 .92	.46 .59 .71 .82 .92	.28 .36 .44 .52	.80 .79 .79 .78	.364 .357 .349 .340 .331	.33 .32 .32 .32	A127
.51 .50	.81 .83	.49 .62	.29 .37	.80 .79	.486 .479	.38 .38	A161
.41 .40 .39 .39	.96 .98 1.01 1.03 1.05	.60 .77 .93 1.08 1.21	.33 .44 .53 .63	.89 .88 .87 .86 .85	.309 .302 .295 .287 .279	.33 .32 .32 .32	A128
.58 .57 .56 .55 .55	.97 .99 1.02 1.04 1.06 1.08	.84 1.09 1.32 1.53 1.73 1.92	.41 .54 .66 .78 .89	.97 .96 .95 .94 .93	.446 .440 .434 .428 .421 .414	.44 .43 .43 .43 .43 .43	A129



1	2	3	4	5	6	7	8
Section Number.	Dimensions,	Thickness.	Weight per Foot.	Area of Section.	Distance of Center of Gravity from Back of Longer Leg.	Moment of Inertia Axis 1-1.	Section Modulus Axis 1-1.
	bra	t		A	x	I	S
	Inches.	Inches.	Pounds.	Sq. Ins.	Inches.	Inches.4	Inches.3
A151	3½ x 2 " " " "	1/4 5/6 3/8 7/16/29/6 5/8	4.5 5.6 6.6 7.6 8.5 9.5 10.4	1.32 1.63 1.93 2.22 2.50 2.78 3.05	.46 .48 .50 .53 .55 .57	.41 .49 .57 .64 .70 .76 .82	.26 .32 .38 .43 .48 .54
A131	4 x 3½	5.6 / 8 / 16 / 9 16 / 8 / 16	7.7 9.1 10.6 11.9 13.3 14.7 16.0	2.25 2.68 3.09 3.50 3.91 4.30 4.69	.93 .96 .98 1.00 1.02 1.04 1.07	2.55 2.99 3.40 3.79 4.17 4.49 4.86	.99 1.17 1.35 1.52 1.68 1.83 2.00
A133	4½ x 3	3/8 7/6 1/22 9/6 5/8 1/6	9.1 10.6 11.9 13.3 14.7 16.0	2.68 3.09 3.50 3.91 4.30 4.69	.74 .76 .79 .81 .83	1.98 2.25 2.51 2.75 2.98 3.19	.88 1.01 1.13 1.25 1.37 1.49
A135	5 x 4	3/8 76 1/2 9 15/8 116	11.0 12.8 14.5 16.2 17.8 19.5	3.24 3.75 4.25 4.75 5.24 5.72	1.03 1.05 1.07 1.10 1.12 1.14	4.66 5.32 5.96 6.56 7.14 7.70	1.57 1.81 2.04 2.26 2.48 2.69
A109 "" "" "" "" "" "" "" "" "" "" "" "" ""	7 x 3½	76/296/816/456/856	15.0 17.0 19.1 21.0 23.0 24.9 26.8 28.7 30.5 32.3	4.41 5.00 5.59 6.18 6.75 7.32 7.88 8.43 8.97 9.50	.75 .78 .80 .82 .85 .87 .89 .91	3.95 4.41 4.86 5.28 5.69 6.08 6.46 6.83 7.18	1.44 1.62 1.80 1.97 2.14 2.31 2.48 2.64 2.80 2.96



9	10	11	12	13	14	15	1
Radius of Gyration Axis 1-1.	Distance of Center of Gravity from Back of Shorter Leg.	Moment of Inertia Axis 2-2.	Section Modulus Axis 2-2.	Radius of Gyration Axis 2-2.	Tangent of Angle	Radius of Gyration Axis 3-3.	Section
r	x'	I'	S'	r'	•	r''	
Inches.	Inches.	Inches.4	Inches.3	Inches.		Inches.	
.56 .55 .54 .54 .53 .52 .52	1.21 1.23 1.25 1.28 1.30 1.32 1.34	1.67 2.02 2.36 2.68 2.98 3.27 3.54	.73 .89 1.05 1.21 1.36 1.50 1.64	1.13 1.12 1.11 1.10 1.09 1.08 1.08	.335 .329 .324 .318 .312 .305 .298	.44 .43 .43 .43 .43 .43	A151 ""
1.07 1.06 1.05 1.04 1.03 1.02 1.02	1.18 1.21 1.23 1.25 1.27 1.29 1.32	3.56 4.18 4.76 5.32 5.86 6.37 6.86	1.26 1.49 1.72 1.94 2.15 2.35 2.56	1.26 1.25 1.24 1.23 1.23 1.22 1.21	.757 .755 .753 .750 .747 .742	.73 .73 .72 .72 .72 .72	A131 " " " " "
.86 .85 .85 .84 .83	1.49 1.51 1.54 1.56 1.58 1.60	5.50 6.29 7.04 7.75 8.44 9.10	1.83 2.10 2.37 2.64 2.89 3.14	1.44 1.43 1.42 1.41 1.40 1.39	.440 .437 .431 .428 .424 .419	.65 .65 .64 .64	A133
1.20 1.19 1.18 1.18 1.17 1.16	1.53 1.55 1.57 1.60 1.62 1.64	8.14 9.32 10.46 11.55 12.61 13.62	2.34 2.70 3.05 3.39 3.73 4.05	1.59 1.58 1.57 1.56 1.55 1.54	.631 .629 .626 .623 .620	.85 .85 .85 .84 .84	A135
.95 .94 .93 .93 .92 .91 .91 .90 .89	2.50 2.53 2.55 2.57 2.60 2.62 2.64 2.66 2.69 2.71	22.56 25.41 28.18 30.86 33.47 35.99 38.45 40.82 43.13 45.37	5.01 5.68 6.34 6.96 7.60 8.22 8.83 9.42 10.00 10.58	2.26 2.25 2.25 2.24 2.23 2.22 2.21 2.20 2.19	.267 .264 .262 .259 .257 .253 .250 .247 .244 .241	.76 .755 .755 .744 .744 .744 .74	A109

#### PROPERTIES OF T-BARS.



#### EQUAL LEGS.

1	2	3 -	4	5	6	7	- 8	9
		Dimer	isions.				Distance of	
	Width	Depth	Thickness	Thickness	Weight	Area	Center of Gravity	Moment of Inertia
Section	of	of	of	of	per	Section.	from Outside	Axis 1-1.
Number.	Flange.	Bar.	Flange.	Stem.	Foot.	,	of Flange.	
	b ·	d	s to n' t to t'			A	x	I
	Inches.	Inches.	Inches.	Inches.	Pounds.	Sq. Ins.	Inches.	Inches.4
<b>T</b> 5	1	1	1/8 to 5/32	1/8 to 5/32	1.0	.27	.29	.02
T181	11/8	11/8	3 " 7 16 32	$\frac{5}{32}$ " $\frac{7}{32}$	1.4	.41	.33	.04
T183	1 3	1 3 16	3 " 1/4	5 " 7 32 32	1.6	.45	.34	.05
T187	11/4	11/4	3 " 1/4	5 " 1/4	1.7	.48	.36	.06
T189	13/8	13/8	3 " 1/4	5 "1/4	1.9	.55	.39	.08
T 37 T 39	2	2 2	1/4 " 5 5 " 3/8	1/4 " 5 5 " 3/8	3.7 4.4	1.07 1.28	.59 .61	.37 .43
T 41 T 42	2½ 2½	2½ 2½	1/4 " 5 5 " 3/8	1/4 " 5 16 " 3/8	4.2 5.0	1.21 1.46	.68 .67	.51 .64
T 49	$2\frac{1}{2}$	21/2	5 "3/8	5 "3/8	5.6	1.63	.73	.87
T 67 T 69 T 73	3 3 3	3 3 3	5 "3/8 3/8 "7 1/2 "9 1/2 "9	5 " 3/8 3/8 " 7 1/2 " 9 1/6	6.8 7.9 10.1	1.99 2.31 2.96	.86 .88 .93	1.58 1.82 2.27
T 97	3½	3½	3/8 " 7/16	3/8 " 7/16	9.3	2.74	.99	3.10

T185	11/4	$1_{\frac{1}{16}}$	3 to 1/4	$\frac{5}{32}$ to $\frac{7}{32}$	1.5	.44	.29	.04
T 22	$2\frac{1}{2}$	11/4	3 " 9 16 32	3 " 5 16 16	3.0	.86	.30	.08
<b>T</b> 65	3	$2\frac{1}{2}$	3/8 " 7/16	3/8 " 7/16	7.2	2.11	.71	1.08
T 84	3	4	3/8 " 7	3/8 " 7	9.3	2.74	1.27	4.12
T101	$3\frac{1}{2}$	4	3/8 " 7/16	3/8 " 7/16	10.0	2.94	1.20	4.33
T140	41/2	3½	7 " 9 16 16	11 " 7/8	15.9	4.65	1.11	5.08
<b>T</b> 169	5	3	1/2 " 9/16	13 "5/8	13.6	3.99	.72	2.42

#### PROPERTIES OF T-BARS.

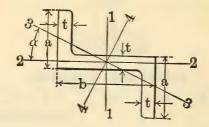


#### EQUAL LEGS.

10	11	12	13	14	15	16	17
					Coef. of	Strength.	
Section Modulus Axis 1-1.	Radius of Gyration Axis 1-1.	Moment of Inertia Axis 2-2.	Section Modulus Axis 2-2.	Radius of Gyration Axis 2-2.	For Fibre Stress of 16 000 lbs. per Square Inch.	For Fibre Stress of 12 500 lbs. per Square Inch.	Section Number.
S	r	I'	S'	r'	F	F'	
Inches.3	Inches.	Inches.4	Inches.3	Inches.			
.03	.30	.01	.02	.21	350	270	<b>T</b> 5
.05	.32	.02	.04	.25	560	440	T181
.06	.33	.03	.05	.26	630	490	<b>T</b> 183
.07	.35	.03	.05	.27	700	550	T187
.08	.39	.05	.07	.29	890	690	T189
.26 .31	.59 .59	.18 .23	.18 .23	.42 .42	2770 3330	2160 2600	T 37 T 39
.32 .40	.65 .66	.24 .32	.21 .29	.45 .47	3440 4300	2690 3360	T 41 T 42
.49	.74	.44	.35	.52	5250	4100	T 49
.74 .86 1.10	.90 .90 .88	.75 .92 1.20	.50 .61 .80	.62 .64 .64	7860 9180 11710	6140 7180 9150	T 67 T 69 T 73
1.23	1.08	1.42	.81	.73	13140	10260	Т 97

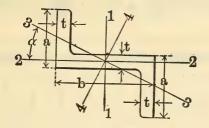
.05	.29	.03	.01	.28	500	390	T185
.09	.31	.28	.22	.58	930	730	T 22
.60	.64	.90	,60	.66	6400	5000	T 65
1.51	1.24	.90	.60	.58	16090	12570	T 84
1.54	1.23	1.42	.81	.70	16470	12860	T101
2.13	1.05	3.73	1.66	.90	22690	17720	T140.
1.06	.78	5.42	2.17	1.17	11340	8860	T169

#### PROPERTIES OF Z-BARS.



_1_	2	3	4	5	6	7	8	9	10	11	12
Section Num- ber.	Depth of Bar.	Length of Legs.	Thick- ness of Web and Legs.	W'ght per Foot.	Area of Section.	Moment of Inertia Axis 1-1.	Section Modulus Axis 1-1.	Radius of Gyra- tion Axis 1-1.	Moment of Inertia Axis 2-2.	Section Mod- ulus Axis 2-2.	Radius of Gyra- tion Axis 2-2.
	b	a	t		A	1	S	r	I'	S'	r'
	Inches.	Inches.	Inches.	Lbs.	Sq. Ins.	Inches.4	Inches.3	Ins.	Inches.4	Ins.3	Inches.
Z .,5	3 3 1 1 6	2 <sup>11</sup> / <sub>18</sub> 2 <sup>3</sup> / <sub>4</sub>	1/4 5 16	6.7 8.4	1.97 2.48	2.87 3.64		1.21 1.21	2.81 3.64	1.10 1.40	1.19 1.21
Z,,9	3 31 6	$2^{\frac{11}{16}}_{2\frac{3}{4}}$	3/8 16	$9.7 \\ 11.4$	2.86 3.36	$\frac{3.85}{4.57}$	2.57 2.98	$\frac{1.16}{1.17}$	3.92 4.75	1.57 1.88	1.17 1.19
Z13	$\frac{3}{3\frac{1}{16}}$	$2^{11}_{16}$ $2^{3}_{4}$	1/2 9 16	$12.5 \\ 14.2$	3.69 4.18	4.59 5.26	3.06 3.43	$\frac{1.12}{1.12}$	4.85 5.68	1.99 2.30	1.15
Z21	4	31/16	1/4	8.2	2.41	6.28	3.14	1.62	4.23	1.44	
66	41/8 41/8	$3\frac{1}{16}$ $3\frac{1}{8}$ $3\frac{3}{16}$	1/4 5 16 3/8	$10.3 \\ 12.4$	3.03 3.66	7.94 9.63	3.91 4.67	$\frac{1.62}{1.62}$	5.46 6.77	$\frac{1.84}{2.26}$	1.34 1.36
Z25	4	31	7 16	13.8	4.05	9.66	4.83	1.54	6.73	2.37	1.29
6.6	41/8	$3^{\frac{1}{16}}_{18} \ 3^{\frac{3}{8}}_{16}$	$\frac{7}{16}$ $\frac{7}{16}$ $\frac{9}{16}$	15.8 $17.9$	4.66 5.27	11.18 $12.74$	5.50 6.18	1.55 1.55	7.96 9.26	$\frac{2.77}{3.19}$	1.31 1.32
Z29	4	31/8 31/8	5/8	18.9	5.55	12.11	6.05	1.48	8.73	3.18	1.25
6.6	41/8 41/8	$3_{16}^{3}$	5/8 11/6 9/4	20.9 23.0	6.14 6.75	13.52 $14.97$	6.65 7.26	1.48 1.49	9.95 11.24	$\frac{3.58}{4.00}$	1.27 1.29
Z37	5 5 1 5 1/8	3½ 3½ 3½ 3 <sup>5</sup> 3 <sup>8</sup>	5 3/8 7 16	11.6 13.9 16.4	3.40 4.10 4.81	13.36 16.18 19.07	6.39	1.98 1.99 1.99	6.18 7.65 9.20	2.00 2.45 2.92	1.35 1.37 1.38
Z41	5	31/4	1/2 9 16 5/8	17.9 20.2		19.19 21.83	7.68 8.62	1.91 1.92	9.05 10.51	$\frac{3.02}{3.47}$	1.31
66	5 <sup>1</sup> / <sub>16</sub> 5 <sup>1</sup> / <sub>8</sub>	3 18 3 8 3 8	5/8	22.6	6.64	24.53	9.57	1.92	12.06	3.94	1.35
Z45	5 5 1 5 1/8	$3\frac{1}{4}$ $3\frac{5}{16}$ $3\frac{3}{8}$	116 3/4 13 16	23.7 26.0 28.3	7.64	23.68 26.16 28.70	9.47 10.34 11.20	1.84 1.85 1.86	12.83	3.91 4.37 4.84	1.28 1.30 1.31
<b>Z53</b>	6	31/2	3/8	15.6	4.59	25.32	8.44	2.35	9.11	2.75	1.41
66	6 <sup>1</sup> / <sub>16</sub> 6 <sup>1</sup> / <sub>8</sub>	$3\frac{1}{2}$ $3\frac{9}{16}$ $3\frac{5}{8}$	3/8 7 16 1/2	18.3 21.0		29.80 34.36		$\frac{2.35}{2.36}$	10.94 $12.87$	3.27 $3.81$	1.43 1.44
Z57	6	$3\frac{1}{2}$ $3\frac{9}{16}$ $3\frac{5}{8}$	9 16 5/8 11 13	22.7 25.4		34.64 38.87	11.55 12.82	2.28 2.28	12.59 14.41	$3.91 \\ 4.44$	
66	61/8 61/8	35/8	11 13	28.1	8.25	43.18	14.10	2.29	16.34	4.98	1.41
Z61	6	$3\frac{1}{2}$ $3\frac{9}{16}$ $3\frac{5}{8}$	3/4	29.3 31.9		42.12 46.13	$14.04 \\ 15.22$		15.44 $17.27$		1.34
66	61/8		3/4 136 7/8	34.6	10.17	50.22	16.40	2.22	19.18	6.02	1.37
Z67	71/2	3	3/8	16.3	- 1		10.18		5.59		1.08
Z73	8	3	3/8	16.9	4.97	44.64	11.16	3.00	5.60	1.99	1.06

#### PROPERTIES OF Z-BARS.



13	14	15	16	17	18	1
	Least Radius	Coef. of S	Strength.	Coef. of I	eflection.	
Tangent of Angle	of Gyration Axis 3-3.	For Fibre Stress of 16 000 Pounds per Square Inch.	For Fibre Stress of 12500 Pounds per Square Inch.	Uniform Load.	Center Load.	Section Number.
, oc	Inches.	F	F'	N	N'	
.986 1.000	.55 .55	20400 25400	16000 19800	.000270	.000432 .000341	Z <sub>66</sub> 5
.990 .975	.54 .55	27400 31800	21400 24800	.000201	.000322	Z,,9
.965 .951	.53 .54	32600 36600	25500 28600	.000169	.000271 .000236	Z13
.778 .788 .798	.67 .68 .69	33500 41700 49800	26200 32600 38900	.000124 .000098 .000081	.000198 .000156 .000129	Z21
.794 .804 .814	.66 .67 .68	51500 58700 65900	40200 45900 51500	.000080 .000069 .000061	.000129 .000111 .000098	Z25
.808 .818 .828	.65 .67	64600 71000 77400	50500 55500 60500	.000064 .000057 .000052	.000103 .000092 .000083	Z29
.611 .619 .628	.75 .76	57000 68200 79400	44500 53300 62000	.000058 .000048 .000041	.000093 .000077	Z37
.616 .623 .631	.74 .75	81900 92000	64000 71900	.000040	.000065	Z41
.619 .626	.73 .74	102100 101000 110200	79800 78900 86100	.000032	.000052	Z45
.633 .519 .526	.76 .83 .83	90000 104900	93300 70300 81900	.000027 .000031 .000026	.000043 .000049 .000042	Z53
.532 .520 .526	.84 .81 .82	119700 123200 136800	93500 96200 106800	.000023 .000020	.000036 .000032	Z57
.532 .519 .525	.84 .81 .82	150400 149800 162300	117500 117000 126800	.000018 .000017	.000029	Z61
.530	.83	174900	136700	.000015	.000025	66
.29 .27	.72 .72	108600 119000	93000	.000020	.000033	Z67 Z73

#### MOMENTS OF INERTIA OF RECTANGLES.



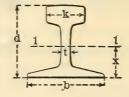
Depth		Widt	h of R	ectangl	le in In	iches.	
in Inches.	$\frac{1}{4}$	<u>5</u> 16	38	$\frac{7}{16}$	$\frac{1}{2}$	$\frac{9}{16}$	<u>5</u> 8
2	.17	.21	.25	.29	.33	.38	.42
3	.56	.70	.84	.98	1.13	1.27	1.41
4	1.33	1.67	2.00	2.33	2.67	3.00	3.33
5	2.60	3.26	3.91	4.56	5.21	5.86	6.51
6	4.50	5.63	6.75	7.88	9.00	10.13	11.25
7	7.15	8.93	10.72	12.51	14.29	16.08	17.86
8	10.67	13.33	16.00	18.67	21.33	24.00	26.67
9	15.19	18.98	22.78	26.58	30.38	34.17	37.97
10	20.83	26.04	31.25	36.46	41.67	46.87	52.08
11	27.73	34.66	41.59	48.53	55.46	62.39	69.32
12	36.00	45.00	54.00	63.00	72.00	81.00	90.00
13	45.77	57.21	68.66	80.10	91.54	102.98	114.43
14	57.17	71.46	85.75	100.04	114.33	128.63	142.92
15	70.31	87.89	105.47	123.05	140.63	158.20	175.78
16	85.33	106.67	128.00	149.33	170.67	192.00	213.33
17	102.35	127.94	153.53	179.12	204.71	230.30	255.89
18	121.50	151.88	182.25	212.63	243.00	273.38	303.75
19	142.90	178.62	214.34	250.07	285.79	321.52	357.24
20	166.67	208.33	250.00	291.67	333.33	375.00	416.67
21	192.94	241.17	289.41	337.64	385.88	434.11	482.34
22	221.83	277.29	332.75	388.21	443.67	499.13	554.58
23	253.48	316.85	380.22	443.59	506.96	570.33	633.70
24	288.00	360.00	432.00	504.00	576.00	648.00	720.00
25	325.52	406.90	488.28	569.66	651.04	732.42	813.80
26	366.17	457.71	549.25	640.79	732.33	823.88	915.42
27	410.06	512.58	615.09	717.61	820.13	922.64	1025.16
28	457.33	571.67	686.00	800.33	914.67	1029.00	1143.33
29	508.10	635.13	762.16	889.18	1016.21	1143.23	1270.26
30	562.50	703.13	843.75	984.38	1125.00	1265.63	1406.25
32	682.67	853.33	1024.00	1194.67	1365.33	1536.00	1706.67
34	818.83	1023.54	1228.25	1432.96	1637.67	1842.38	2047.08
36	972.00	1215.00	1458.00	1701.00	1944.00	2187.00	2430.00
38	1143.17	1428.96	1714.75	2000.54	2286.33	2572.13	2857.92
40	1333.33	1666.67	2000.00	2333.33	2666.67	3000.00	3333.33
42	1543.50	1929.38	2315.25	2701.13	3087.00	3472.88	3858.75
44	1774.67	2218.33	2662.00	3105.67	3549.33	3993.00	4436.67
46	2027.83	2534.79	3041.75	3548.71	4055.67	4562.63	5069.58
48	2304.00	2880.00	3456.00	4032.00	4608.00	5184.00	5760.00
50	2604.17	3255.21	3906.25	4557.29	5208.33	5859.38	6510.42
52	2929.33	3661.67	4394.00	5126.33	5858.67	6591.00	7323.33
54	3280.50	4100.63	4920.75	5740.88	6561.00	7381.13	8201.25
56	3658.67	4573.33	5488.00	6402.67	7317.33	8232.00	9146.67
58	4064.83	5081.04	6097.25	7113.46	8129.67	9145.87	10162.08
60	4500.00	5625.00	6750.00	7875.00	9000.00	10125.00	11250.00

#### MOMENTS OF INERTIA OF RECTANGLES.



	Width o	of Recta	angle in	Inches	•	Depth				
116	3/4	$\begin{array}{c c} \underline{1} \ \underline{3} \\ \overline{1} \ \underline{6} \end{array}$	7/8	15 16	1	in Inches.				
.46	.50	.54	.58	.63	.67	2				
1.55	1.69	1.83	1.97	2.11	2.25	3				
3.67	4.00	4.33	4.67	5.00	5.33	4				
7.16	7,81	8.46	9.11	9.77	10.42	5				
12.38	13,50	14.68	15.75	16.88	18.00	6				
19.65	21,44	23.22	25.01	26.80	28.58	7				
29.33	32,00	34.67	37.33	40.00	42.67	8				
41.77	45,56	49.36	53.16	56.95	60.75	9				
57.29	62.50	67.71	72.92	78.13	83.33	10				
76.26	83.19	90.12	97.05	103.98	110.92	11				
99.00	108.00	117.00	126.00	135.00	144.00	12				
125.87	137.31	148.75	160.20	171.64	183.08	13				
157.21	171.50	185.79	200.08	214.38	228.67	14				
193.36	210.94	228.52	246.09	263.67	281.25	15				
234.67	256.00	277.33	298.67	320.00	341.33	16				
281.47	307.06	332.65	358.24	383.83	409.42	17				
334.13	364.50	394.88	425.25	455.63	486.00	18				
392.96	428.69	464.41	500.14	535.86	571.58	19				
458.33	500.00	541.67	583.33	625.00	666.67	20				
530.58	578.81	627.05	675.28	723.52	771.75	21				
610.04	<b>66</b> 5.50	720.96	776.42	831.87	887.33	22				
697.07	760.44	823.81	887.18	950.55	1013.92	23				
792.00	864.00	936.00	1008.00	1080.00	1152.00	24				
895.18	976.56	1057.94	1139.32	1220.70	1302.08	25				
1006.96	1098.50	1190.04	1281.58	1373.13	1464.67	26				
1127.67	1230.19	1332.70	1435.22	1537.73	1640.25	27				
1257.67	1372.00	1486.33	1600.67	1715.00	1829.33	28				
1397.29	1524.31	1651.34	1778.36	1905.39	2032.42	29				
1546.88	1687.50	1828.13	1968.75	2109.38	2250.00	30				
1877.33	2048.00	2218.67	2389.33	2560.00	2730.67	32				
2251.79	2456.50	2661.21	2865.92	3070.63	3275.33	34				
2673.00	2916.00	3159.00	3402.00	3645.00	3888.00	36				
3143.71	3429.50	3715.29	4001.08	4286.88	4572.67	38				
3666.67	4000.00	4333.33	4666.67	5000.00	5333.33	40				
4244.63	4630.50	5016.38	5402.25	5788.13	6174.00	42				
4880.33	5324.00	5767.67	6211.33	6655.00	7098.67	44				
5576.54	6083.50	6590.46	7097.42	7604.38	8111.33	46				
6336.00	6912.00	7488.00	8064.00	8640.00	9216.00	48				
7161.46	7812.50	8463.54	9114.58	9765.63	10416.67	50				
8055.67	8788.00	9520.33	10252.67	10985.00	11717.33	52				
9021.38	9841.50	10661.63	11481.75	12301.88	13122.00	54				
10061.33	10976.00	11890.67	12805.33	13720.00	14634.67	56				
11178.29	12194.50	13210.71	14226.92	15243.12	16259.33	58				
12375.00	13500.00	14625.00	15750.00	16875.00	18000.00	60				

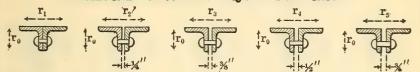
### PROPERTIES AND PRINCIPAL DIMENSIONS OF STANDARD T-RAILS.



		Weight							Axis	1-1.
	Section Jumber.	per Yard.	Area.	b	d	k	t	x	Moment of Inertia.	Section Modulus.
		Pounds.	Sq. Ins.	Inches.	Inches.	Inches.	Inches.	Inches.	1	S
_	522	8	0.78	11/2	1½	13	<u>5</u>	0.75	0.23	0.31
	523	12	1.18	17/8	17/8	116	3 16	0.92	0.55	0.58
	524	16	1.57	21/4	21/4	1 3	7 32	1.10	1.13	0.99
	525	20	2.0	23/8	23/8	13/8	1/4	1.2	1.5	1.2
	526	25	2.5	23/4	23/4	1½	19 64	1.4	2.4	1.7
	544	30	2.9	3	. 3	15/8	21 64	1.4	3.6	2.3
	546	35	3.4	31/4	31/4	13/4	23 64	1.6	4.9	2.9
	545	40	3.9	3½	3½	17/8	25 64	1.7	6.6	3.6
	549	45	4.4	311 16	$3\frac{11}{16}$	2	27 64	1.8	8.1	4.2
	542	50	4.9	31/8	31/8	21/8	7 16	1.9	10.1	5.1
	537	55	5.4	41	416	21/4	$\frac{15}{32}$	2.0	12.2	5.9
	533	60	5.9	41/4	41/4	23/8	31 64	2.1	14.7	6.7
	534	65	6.4	4 7 16	4 7 16	$2\frac{13}{32}$	1/2	2.1	17.0	7.4
	532	70	6.9	45/8	<b>4</b> 5/8	2 7 16	33 64	2.2	20.0	8.4
	529	75	7.4	413 16	413	2 15 32	17 32	2.3	23.0	9.1
	530	80	7.8	5	5	21/2	35 64	2.4	26.7	10.1
	531	85	8.3	5 3 16	5 3 1 6	2 9 16	9 16	2.5	30.5	11.2
	535	90	8.8	53/8	53/8	25/8	9	2.6	35.2	12.6
	550	95	9.3	5 g 16	5 9 1 6	211	9 16	2.7	38.8	13.3
	536	100	9.8	53/4	53/4	23/4	9 16	2.8	44.4	15.0
	539	150	14.7	6	6	41/4	1	3.0	69.3	22.9

Sections No. 529 to 537 and 542 to 549 inclusive, are Am. Soc. C. E. Standard. For detail dimensions of Section No. 539 see page 18.

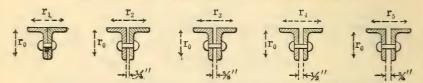
# RADII OF GYRATION FOR TWO ANGLES PLACED BACK TO BACK. ANGLES WITH EQUAL LEGS.



Radii of gyration correspond to directions indicated by arrowheads.

Section	Dimensions.	Thickness.	Area of	Radii of Gyration.						
Number.	Inches.	Inches.	Two Angles. Sq. Ins.	<b>r</b> <sub>0</sub>	r <sub>1</sub>	r <sub>2</sub>	<b>r</b> <sub>3</sub>	r <sub>4</sub>	<b>r</b> <sub>5</sub>	
A11	1½ x 1½	3 16 3/8	1.06 1.98	0.46 0.44	0.64 0.67	0.73	0.78 0.82	0.83 0.88	0.94	
A13	13/4 x 13/4	3 16 7 16	1.26 2.68	$0.54 \\ 0.51$	0.74	0.83 0.88	0.88	0.93	1.03	
A15	2 x 2	3 16 16 7 16	1.44 2.32 3.12	0.62 0.60 0.59	0.84 0.86 0.88	0.93 0.95 0.98	0.98 1.00 1.03	1.03 1.05 1.08	1.13 1.16 1.19	
*A41	21/4 x 21/4	3 16 3/8	1.62 3.10	0.70 0.67	0.94 0.97	1.03 1.06	1.08 1.11	1.12 1.16	1.22 1.27	
A17	2½ x 2½	1/4 3/8 1/2	2.38 3.48 4.50	0.77 0.75 0.74	1.05 1.07 1.09	1.14 1.16 1.19	1.19 1.21 1.24	1.24 1.26 1.29	1.34 1.36 1.39	
*A43	2 <sup>3</sup> / <sub>4</sub> x 2 <sup>3</sup> / <sub>4</sub>	3 16 5 16 7 16	2.00 3.26 4.44	0.86 0.84 0.83	1.14 1.16 1.18	1.23 1.25 1.28	1.28 1.30 1.32	1.32 1.35 1.37	1.42 1.45 1.47	
A19	3 x 3	16 1/4 7 16 5/8	2.88 4.88 6.72	0.93 0.91 0.88	1.26 1.28 1.32	1.34 1.37 1.41	1.39 1.42 1.46	1.43 1.47 1.51	1.53 1.57 1.61	
A21	3½ x 3½	78 3/8 5/8 13 16	4.98 7.98	1.07 1.04	1.48 1.52	1.56 1.61	1.61 1.66	1.66 1.71	1.75 1.81	
A23	4 × 4	5 16 9 163 163	10.06 4.82 8.38	1.02 1.24 1.21	1.55 1.67 1.71	1.65 1.76 1.80	1.70 1.80 1.85	1.75 1.85 1.89	1.85 1.94 1.99	
* <b>A4</b> 5	4½ x 4½	136 5 166 172 5/8	11.68 5.44 8.50	1.18 1.40 1.38	1.75 1.87 1.90	1.85 1.96 1.99	1.89 2.00 2.04	1.94 2.05 2.08	2.04 2.14 2.18	
*A47	5 x 5	5/8 3/8	7.22 9.50	1.36 1.56 1.54	1.92 2.09 2.10	2.01 2.17 2.19	2.06 2.22 2.24	2.10 2.26 2.28	2.20 2.35 2.38	
II A OP	6 x 6	3/8 1/2 5/8	11.72	1.52 1.87	2.12 2.50	2.21	2.26 2.63	2.30	2.40 2.76	
A27	"	7 16 5/8 7/8	14.22 19.48	1.84 1.81	2.53 2.57	2.62 2.66	2.66 2.70	2.71 2.75	2.80 2.85	
A35	8 x 8	1/2 5/8	15.50 19.22	2.51 2.49	3.32 3.34	3.41 3.43	3.45 3.47	3.49 3.51	3.58 3.60	
66	66	1/2 5/8 3/4 7/8 <b>1</b>	22.88 26.47 30.00	2.47 2.45 2.44	3.36 8.88 3.40	3.44 3.46 3.48	3.49 3.51 3.53	3.53 3.55	3.62 3.64	
66	"	11/8	33.47	2.42	3.42	3.51	3.55	3.57 3.60	3.67 3.69	

## RADII OF GYRATION FOR TWO ANGLES PLACED BACK TO BACK. ANGLES WITH UNEQUAL LEGS.

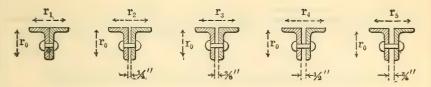


Radii of gyration correspond to directions indicated by arrowheads.

Section	Dimensions.	Thickness.	Area of Two							
Number.	Inches.	Inches.	Angles. Sq. Ins.	r <sub>0</sub>	<b>r</b> <sub>1</sub>	$\mathbf{r}_2$	r <sub>3</sub>	r <sub>4</sub>	r <sub>5</sub>	
*A121	2 × 13/8	3 16 3/8	1.20 2.26	0.63 0.61	0.54 0.56	0.62 0.66	0.67 0.71	0.72 0.76	0.83 0.88	
*A123	2 x 1½	3 16 3/8	1.26 2.36	0.63 0.61	0.59 0.62	0.68 0.72	0.73 0.77	0.78 0.82	0.88 0.93	
*A125	2½ x 1¼	3 16 3/8	1.34 2.54	0.80 0.78	0.44 0.47	0.52 0.57	0.58 0.62	0.63 0.68	0.74 0.79	
*A127	2½ x 1½	3 16 3/8	1.44 2.72	0.80 0.78	0.55 0.58	0.64 0.68	0.69 0.73	0.74 0.78	0.84 0.89	
*A161	2½ x 1¾	3 16 1/4	1.54 2.00	0.80 0.79	0.67 0.68	0.75 0.77	0.80 0.81	0.85 0.86	0.95 0.97	
A91 "	2½ x 2	3 16 3/ 8 1/2	1.62 3.10 4.00	0.79 0.77 0.75	0.79 0.82 0.84	0.88 0.91 0.94	0.92 0.96 0.99	0.97 1.01 1.04	1.07 1.12 1.15	
*A128	2¾ x 1½	3 16 16 7 16	1.54 2.48 3.34	0.89 0.87 0.85	0.53 0.55 0.58	0.62 0.65 0.68	0.67 0.70 0.73	0.72 0.75 0.78	0.82 0.86 0.89	
*A129	3 × 2	3 16 5 16 7 16	1.82 2.94 4.00	0.97 0.95 0.93	0.75 0.76 0.79	0.83 0.85 0.88	0.88 0.90 0.93	0.93 0.95 0.98	1.03 1.05 1.09	
A93	3 × 2½ "	1/4 3/8 16	2.64 3.86 5.56	0.95 0.93 0.91	1.00 1.02 1.05	1.09 1.11 1.15	1.13 1.16 1.20	1.18 1.21 1.25	1.28 1.31 1.35	
*A151	3½ x 2	1/4 7 16 5/8	2.63 4.43 6.10	1.13 1.10 1.08	.72 .75 .79	.81 .84 .89	.85 .89 .94	.90 .94 .99	1.00 1.05 1.10	
A95	3½ x 2½	1/4 1/2 116	2.88 5.50 7.32	1.12 1.09 1.06	0.96 1.00 1.03	1.04 1.09 1.13	1.09 1.14 1.18	1.13 1.19 1.23	1.23 1.29 1.33	
A97	3½ x 3	5 16 16 16 16	3.88 6.68 9.26	1.10 1.07 1.04	1.21 1.25 1.30	1.30 1.34 1.40	1.35 1.39 1.45	1.39 1.44 1.50	1.49 1.54 1.60	

## RADII OF GYRATION FOR TWO ANGLES PLACED BACK TO BACK.

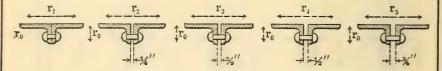
#### ANGLES WITH UNEQUAL LEGS.



Radii of gyration correspond to directions indicated by arrowheads.

Section	Dimensions.	Thickness.	Area of Two	Radii of Gyration.						
Number.	Inches.	Inches.	Angles. Sq. Ins.	$\mathbf{r}_{0}$	<b>r</b> <sub>1</sub>	$\mathbf{r}_2$	$\mathbf{r}_3$	r <sub>4</sub>	r <sub>5</sub>	
A99 "	4 × 3	5 16 9 16 13 16	4.18 7.26 10.06	1.27 1.24 1.21	1.17 1.21 1.25	1.25 1.30 1.35	1.30 1.34 1.40	1.34 1.39 1.45	1.44 1.49 1.55	
*A131	4 × 3½	5 16 1/2 5/8	4.50 7.00 8.60	1.26 1.23 1.22	1.42 1.44 1.46	1.50 1.53 1.55	1.55 1.58 1.60	1.59 1.63 1.65	1.69 1.72 1.75	
*A133	4½ x 3	3/8 1/2 5/8	5.36 7.00 8.60	1.44 1.42 1.40	1.14 1.15 1.18	1.22 1.24 1.27	1.27 1.29 1.31	1.31 1.34 1.36	1.41 1.44 1.46	
A101	5 x 3	5 16 9 16 13 16	4.82 8.38 11.68	1.61 1.58 1.55	1.09 1.13 1.17	1.17 1.22 1.27	1.22 1.26 1.32	1.26 1.31 1.37	1.36 1.41 1.47	
A103	5 × 3½	3/8 5/8 7/8	6.10 9.86 13.36	1.60 1.56 1.53	1.34 1.37 1.42	1.42 1.46 1.51	1.46 1.51 1.56	1.51 1.56 1.61	1.60 1.66 1.71	
*A135	5 x 4	3/8 1/2 5/8	6.48 8.50 10.48	1.59 1.57 1.55	1.58 1.60 1.62	1.66 1.68 1.71	1.71 1.73 1.75	1.75 1.78 1.80	1.85 1.87 1.90	
A105	6 x 3½	3/8 5/8 7/8	6.86 11.10 15.10	1.94 1.90 1.87	1.26 1.30 1.34	1.34 1.39 1.44	1.39 1.43 1.49	1.43 1.48 1.53	1.53 1.58 1.64	
A107	6 x 4	3/8 5/8 7/8	7.22 11.72 15.98	1.93 1.90 1.86	1.50 1.53 1.58	1.58 1.62 1.67	1.62 1.67 1.71	1.67 1.71 1.76	1.76 1.81 1.86	
*A109	7 × 3½	76 112 558 1136	8.82 10.00 12.36 15.76 19.00	2.26 2.25 2.24 2.21 2.19	1.16 1.22 1.24 1.27 1.31	1.29 1.30 1.32 1.36 1.40	1.33 1.35 1.37 1.41 1.45	1.38 1.39 1.42 1.46 1.50	1.47 1.48 1.51 1.56 1.60	

## RADII OF GYRATION FOR TWO ANGLES PLACED BACK TO BACK. ANGLES WITH UNEQUAL LEGS.

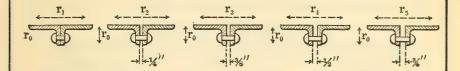


Radii of gyration correspond to directions indicated by arrowheads.

Section	Dimensions.	Thickness.	Area of Two		R	Radii of	Gyration		
Number.	Inches.	Inches.	Angles. Sq. Ins.	r <sub>o</sub>	<b>r</b> <sub>1</sub>	$\mathbf{r}_2$	r <sub>3</sub>	r <sub>4</sub>	r <sub>5</sub>
*A121	2 × 13/8	3 16 3/8	1.20 2.26	0.41 0.38	0.92 0.95	1.01 1.05	1.06 1.10	1.11 1.15	1.22 1.26
*A123	2 x 1½	3 16 3/8	1.26 2.36	0.44 0.42	0.90 0.93	0.99	1.05 1.14	1.09 1.19	1.20 1.29
*A125	2½ x 1¼	3 16 3/8	1.34 2.54	0.33 0.32	1.21 1.25	1.31 1.35	1.36 1.40	1.41 1.45	1.51 1.56
*A127	2½ x 1½	3 16 3/8	1.44 2.72	0.42 0.40	1.17 1.20	1.26 1.30	1.31 1.35	1.36 1.40	1.47 1.51
*A161	2½ x 1¾	3 16 1/4	1.54 2.00	0.51 0.50	1.13 1.14	1.23 1.24	1.27 1.29	1.32 1.34	1.43 1.44
A91 "	2½ x 2	3 16 3/8 1/2	1.62 3.10 4.00	0.60 0.58 0.56	1.10 1.13 1.15	1.19 1.23 1.25	1.24 1.28 1.30	1.29 1.33 1.35	1.39 1.43 1.46
*A128	23/4 x 11/2	3 16 5 16 7 16	1.54 2.48 3.34	0.41 0.40 0.39	1.31 1.33 1.36	1.40 1.43 1.45	1.45 1.48 1.51	1.50 1.53 1.56	1.60 1.63 1.66
*A129	3 × 2	3 16 5 16 7	1.82 2.94 4.00	0.58 0.57 0.55	1.37 1.39 1.41	1.46 1.48 1.51	1.51 1.53 1.56	1.56 1.58 1.61	1.66 1.68 1.71
A93	3 x 2½	1/4 3/8 9 16	2.64 3.86 5.56	0.75 0.74 0.72	1.31 1.33 1.37	1.40 1.42 1.46	1.45 1.47 1.51	1.50 1.52 1.56	1.60 1.63 1.66
*A151	3½ x 2	1/4 7 16 5/8	2.63 4.43 6.10	.56 .54 .52	1.65 1.69 1.72	1.75 1.78 1.82	1.79 1.83 1.87	1.84 1.88 1.92	1.94 1.99 2.03
A95	3½ x 2½	1/4 1/2 116	2.88 5.50 7.32	0.74 0.70 0.69	1.58 1.62 1.66	1.67 1.72 1.75	1.72 1.77 1.80	1.76 1.81 1.86	1.86 1.92 1.96
A97	3½ x 3	5 16 9 16 13	3.88 6.68 9.26	0.90 0.87 0.85	1.52 1.57 1.61	1.61 1.66 1.71	1.66 1.71 1.76	1.71 1.76 1.81	1.80 1.86 1.91

## RADII OF GYRATION FOR TWO ANGLES PLACED BACK TO BACK.

#### ANGLES WITH UNEQUAL LEGS.



Radii of gyration correspond to directions indicated by arrowheads.

Section	Dim	ensi	ons.	Thickness.	Area of Two		]	Radii of	Gyration	l.	
Number.	In	nche	S.	Inches.	Angles. Sq. Ins.	r <sub>o</sub>	<b>r</b> <sub>1</sub>	$\mathbf{r}_2$	r <sub>3</sub>	<b>r</b> <sub>4</sub>	<b>r</b> <sub>5</sub>
A99 "	4	X 66	3 -	76 9 76 13 16	4.18 7.26 10.06	0.89 0.86 0.83	1.79 1.83 1.88	1.88 1.93 1.97	1.93 1.97 2.02	1.97 2.02 2.08	2.07 2.12 2.18
*A131	4	X 66	$3\frac{1}{2}$	5 16 12 5/8	4.50 7.00 8.60	1.07 1.04 1.02	1.73 1.76 1.78	1.81 1.85 1.87	1.86 1.89 1.92	1.91 1.94 1.97	2.00 2.04 2.07
*A133	41/2	X 66	3	3/8 1/2 5/8	5.36 7.00 8.60	0.86 0.85 0.83	2.07 2.09 2.11	2.16 2.18 2.21	2.21 2.23 2.26	2.26 2.28 2.31	2.35 2.38 2.41
A101	5	X "	3	5 16 9 16 13 16	4.82 8.38 11.68	0.85 0.82 0.80	2.33 2.37 2.42	2.42 2.47 2.52	2.47 2.52 2.57	2.52 2.57 2.62	2.61 2.67 2.72
A103	5	X 66	3½	3/8 5/8 7/8	6.10 9.86 13.36	1.02 0.99 0.96	2.27 2.31 2.36	2.36 2.40 2.45	2.41 2.45 2.50	2.45 2.50 2.55	2.55 2.60 2.65
*A135	5	X	4	3/8 1/2 5/8	6.48 8.50 10.48	1.20 1.18 1.17	2.20 2.22 2.24	2.29 2.31 2.33	2.34 2.36 2.38	2.38 2.41 2.43	2.48 2.50 2.53
A105	6	X "	3½	3/8 5/8 7/8	6.86 11.10 15.10	0.99 0.96 0.93	2.81 2.86 2.90	2.90 2.95 3.00	2.95 3.00 3.05	3.00 3.05 3.10	3.09 3.15 3.20
A107	6	X 66	4	3/8 5/8 7/8	7.22 11.72 15.98	1.17 1.13 1.11	2.74 2.78 2.82	2.83 2.87 2.92	2.87 2.92 2.97	2.92 2.97 3.02	3.02 3.06 3.12
*A109	7	X 66 66 66	3½	76/22/826	8.82 10.00 12.36 15.76 19.00	0.95 0.94 0.93 0.91 0.89	3.37 3.39 3.40 3.45 3.48	3.47 3.48 3.50 3.54 3.58	3.52 3.53 3.55 3.59 3.63	3.56 3.58 3.60 3.64 3.68	3.66 3.67 3.70 3.74 3.78

For various values of  $\frac{L}{r}$  in which L = length in feet and r = radius of gyration in inches.

P = ultimate strength in lbs. per square inch.

#### FOR SOFT STEEL.

$$P = \frac{45\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}} \quad P = \frac{45\ 000}{1 + \frac{(12\ L)^2}{24\ 000\ r^2}} \quad P = \frac{45\ 000}{1 + \frac{(12\ L)^2}{18\ 000\ r^2}}$$

To obtain safe unit stress:

$\frac{\mathbf{L}_{t}}{\mathbf{r}}$	1	e Strengt Square I		L <sub>r</sub>	Ultimate Strength in lbs. per Square Inch.			
1	Square.	Pin and Square.	Pin.		Square.	Pin and Square.	Pin.	
3.0	43437	42694	41978	7.6	36554	33419	30779	
3.2	43230	42395	41593	7.8	36193	32966	30268	
3.4	43011	42081	41190					
3.6	42782	41754	40773	8.0	35828	32514	29762	
3.8	42543	41412	40340	8.2	35462	32064	29260	
				8.4	35095	31615	28763	
4.0	42294	41058	39893	8.6	34727	31169	28272	
4.2	42035	40693	39435	8.8	34358	30724	27787	
4.4	41765	40317	38966	0.0	22222	20222	02000	
4.6	41488	39930	38485	9.0	33988	30282	27306	
4.8.	41203	39534	37998	9.2	33611	29844	26832	
- 0	10010	90490	07400	9.4	33249	29408	26364	
5.0	40910	39130	37500	9.6	32880	28977	25903	
5.2	40608	38807	36997	9.8	32511	28549	25448	
5.4	40299	38300	36488	100	201.49	90195	05000	
5.6	39984 39663	37874 37443	35975 35457	10.0	32143 31776	28125 27706	25000	
5.8	99009	0(440	00407	10.2		27290	24559	
6.0	39335	37006	34938	10.4 10.6	31411 31054	26879	24125 23698	
6.2	39003	36566	34416	10.8	30684	26474	23279	
6.4	38665	36122	33894	10.0	90004	20414	20219	
6.6	38323	35676	33371	11.0	30324	26072	22866	
6.8	37976	35219	32849	11.2	29965	25675	22460	
0.0	01010	00510	05010	11.4	29608	25285	22063	
7.0	37616	34776	32328	11.6	29247	24899	21671	
7.2	37272	34324	31809	11.8	28903	24517	21288	
7.4	36914	33872	31292	2110		22321	21300	

For various values of  $\frac{L}{r}$  in which L = length in feet and r = radius of gyration in inches.

P = ultimate strength in lbs. per square inch.

#### FOR SOFT STEEL.

Square bearing Pin and square bearing Pin bearing P = 
$$\frac{45\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$$
 P =  $\frac{45\ 000}{1 + \frac{(12\ L)^2}{24\ 000\ r^2}}$  P =  $\frac{45\ 000}{1 + \frac{(12\ L)^2}{18\ 000\ r^2}}$ 

To obtain safe unit stress:

L,		e Streng Square I	th in 1bs.	L,	Ultimate Strength in 1bs. per Square Inch.			
•	Square.	Pin and Square.	Pin.		Square.	Pin and Square.	Pin.	
12.0	28553	24142	20911	16.6	21406	16960	14043	
12.2	28207	23771	20542	16.8	21137	16708	13812	
12.4	27863	23406	20179					
12.6	27522	23046	19823	17.0	20872	16459	13584	
12.8	27185	22693	19474	17.2	20611	16216	13366	
	:			17.4	20353	15977	13150	
13.0	26850	22343	19133	17.6	20098	15742	12938	
13.2	26524	22005	18797	17.8	19847	15512	12731	
13.4	26189	21662	18469					
13.6	25864	21329	18148	18.0	19599	15286	12528	
13.8	25543	21002	17833	18.2	19351	15063	12329	
				18.4	19114	14845	12135	
14.0	25224	20680	17523	18.6	18878	14630	11944	
14.2	24909	20363	17221	18.8	18644	14420	11757	
14.4	24598	20052	16925					
14.6	24290	19746	16634	19.0	18418	14218	11579	
14.8	23985	19445	16350	19.2	18185	14010	11394	
				19.4	17961	13811	11219	
15.0	23684	19148	16071	19.6	17740	13616	11048	
15.2	23387	18858	15799	19.8	17519	13422	10877	
15.4	23093	18572	15532					
15.6	22803	18288	15270	20.0	17308	13235	10715	
15.8	22516	18015	15105	20.2	17096	13050	10553	
				20.4	16888	12868	10434	
16.0	22234	17744	14764	20.6	16682	12690	10249	
16.2	21954	17478	14518	20.8	16480	12515	10087	
16.4	21678	17216	14279					

For various values of  $\frac{L}{r}$  in which L = length in feet and r = radius of gyration in inches.

P = ultimate strength in 1bs. per square inch.

#### FOR MEDIUM STEEL.

Square bearing Pin and square bearing P = 
$$\frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$$
 P =  $\frac{50\ 000}{1 + \frac{(12\ L)^2}{24\ 000\ r^2}}$  P =  $\frac{50\ 000}{1 + \frac{(12\ L)^2}{18\ 000\ r^2}}$ 

To obtain safe unit stress:

L/r		Square I		L <sub>r</sub>	Ultimate Strength in 1bs. per Square Inch.			
	Square.	Pin and Square.	Pin.		Square.	Pin and Square.	Pin.	
3.0	48263	47438	46642	7.6	40616	37132	34199	
3.2	48033	47106	46214	7.8	40214	36629	33631	
3.4	47790	46757	45767					
3.6	47536	46393	45303	8.0	39809	36127	33069	
3.8	47270	46013	44822	8.2	39402	35627	32511	
				8.4	38994	35128	31959	
4.0	46993	45620	44325	8.6	38585	34632	31413	
4.2	46705	45214	43817	8.8	38175	34138	30874	
4.4	46406	44797	43295					
4.6	46098	44367	42761	9.0	37764	33647	30340	
4.8	45781	43927	42220	9.2	37345	33160	29813	
				9.4	36943	32676	29293	
5.0	45455	43478	41667	9.6	36533	32197	28781	
5.2	45120	43119	41108	9.8	36123	31721	28275	
5.4	44777	42555	40542					
5.6	44427	42082	39972	10.0	35714	31250	27778	
5.8	44070	41603	39397	10.2	35307	30784	27288	
				10.4	34901	30322	26806	
6.0	43706	41118	38820	10.6	34504	29866	26331	
6.2	43337	40629	38240	10.8	34093	29415	25865	
6.4	42961	40136	37660					
6.6	42581	39640	37079	11.0	33693	28969	25407	
6.8	42196	39132	36499	11.2	33294	28528	24956	
~ .		20012	02000	11.4	32898	28094	24514	
70	41796	38640	35920	11.6	32497	27665	24079	
7.2	41413	38138	35343	11.8	32114	27241	23653	
7.4	41016	37635	34769					

For various values of  $\frac{L}{r}$  in which L = length in feet and r = radius of gyration in inches.

P = ultimate strength in lbs. per square inch.

#### FOR MEDIUM STEEL.

$$P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}} \quad P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{24\ 000\ r^2}} \quad P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{18\ 000\ r^2}} \quad P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{18\ 000\ r^2}}$$

To obtain safe unit stress:

L/r		e Strengt Square I	h in 1bs. nch.	L,	Ultimate Strength in 1bs. per Square Inch.			
	Square.	Pin and Square.	Pin.		Square.	Pin and Square.	Pin.	
12.0	31726	26824	23234	16.6	23784	18844	15603	
12.2 12.4	31341 30959	26412 26007	22824 22421	16.8	23486	18564	15347	
12.6	30580	25607	22026	17.0	23191	18288	15093	
12.8	30205	25214	21638	17.2 17.4	22901 22614	18018 17752	14851 14611	
13.0	29833	24826	21259	17.6	22331	17491	14376	
13.2 13.4	29471 29099	24450 24069	20886 20521	17.8	22052	17235	14145	
13.6	28738	23699	20164	18.0	21777	16984	13920	
13.8	28381	23336	19814	18.2 18.4	21501 21238	16737 $16494$	13699	
14.0	28027	22978	19470	18.6	20975	16256	13483 13271	
14.2	27677	22626	19134	18.8	20715	16022	13063	
14.4 14.6	27331 26989	22280 21940	18805 18482	19.0	20464	15798	12865	
14.8	26650	21605	18167	19.2	20206	15567	12661	
15.0	26316	21276	17857	19.4 19.6	19957 19711	15346 15129	12466 12275	
15.2	25985	20953	17554	19.8	19466	14913	12086	
15.4 15.6	25659 25337	20636 20320	17258 16967	20.0	19231	14706	11905	
15.8	25018	20017	16683	20.2	18996	14500	11725	
16.0	24704	19716	16404	$20.4 \\ 20.6$	18764 18536	14298 14100	11549 11377	
16.2	24393	19420	16131	20.8	18311	13905	11208	
16.4	24087	19129	15865					

# EXAMPLE OF THE USE OF THE TABLES OF RADII OF GYRATION FOR TWO ANGLES PLACED BACK TO BACK AND THE TABLES OF STRENGTH OF STEEL COLUMNS OR STRUTS.

#### PAGES 185 TO 193 INCLUSIVE.

What is the size of truss member required to safely sustain 50 000 pounds in compression, the safety factor being 4, the unsupported length 8

feet, the gusset plates at each end being 3/11 thick?

Assume for trial two  $4'' \times 3'' \times \frac{5}{16}''$  angles with the long legs together. Referring to page 187, the least Radius of Gyration, comparing values in columns  $r_0$  and  $r_3$ , is found to be 1.27. The ratio of the length of the column in feet to the Least Radius of Gyration in inches,  $\frac{L}{r}$  is therefore

Referring to the table of Strength of Steel Columns or Struts for

 $\frac{8}{1.27} = 6.3.$ 

medium steel, page 192, the ultimate strength of a column in which  $\frac{L}{r} = 6.3$  is found by interpolation between the values for 6.2 and 6.4 to be 43 149 pounds per square inch, which, divided by the safety factor 4, gives 10 787 pounds as the safe unit stress per square inch. Multiplying the safe unit stress per square inch: 10 787 pounds by 4.18, the area of the two angles in square inches, gives 45 090 pounds as the total safe load. This is slightly less than the specified load of 50 000 pounds, and therefore it will be necessary to increase the assumed section. Assume the angles to be  $4'' \times 3'' \times 3''$ , for which the Least Radius of Gyration is found by interpolation to be 1.26, and by the same process used above,  $\frac{L}{r}$  is found to be 6.35, which corresponds to an ultimate strength of 43 055

pounds per square inch, or a safe unit stress of 10 764 pounds per square inch, which multiplied by the area of the two angles: 4.96 square inches, gives a safe total load of 53 389 pounds, which is ample to meet the conditions stated.

#### EXPLANATION OF TABLES RELATING TO DI-MENSIONS AND SAFE LOADS OF STEEL COLUMNS OF VARIOUS SECTIONS.

#### PAGES 196 TO 277 INCLUSIVE.

Tables of Dimensions for Plate and Angle Columns are given on pages 196 and 197, the Moments of Inertia and Section Moduli about two rectangular axes are given on pages 198 to 200, and the safe loads for various lengths, calculated for the Radius of Gyration about each of the two rectangular axes, are given on pages 222 to 241 inclusive.

Tables of Dimensions for Z-bar Columns with Side Plates are given on page 202, the Moments of Inertia and Section Moduli about two rectangular axes are given on page 203, and the safe loads for various lengths, based upon the Least Radius of Gyration, are given on pages 244 and 245.

Tables of Dimensions for Latticed Channel Columns are given on page 204, the Moments of Inertia and Section Moduli about two rectangular

axes are given on page 205, the Safe Loads for various lengths, based upon the Least Radius of Gyration, are given on pages 246 to 249, and data relating to the proper sizes of lattice bars and stay-plates to be used with these

columns are given on pages 248 and 249.

On pages 206 and 207 are given the Principal Dimensions of Plate and Channel Columns with comparatively narrow plates, called, for convenience of reference, Series A, and on pages 208 and 209 for Series B, which differs from Series A, in having wider plates. Moments of Inertia and Section Moduli about two rectangular axes are given for Series A and B on pages 210 to 216, and the safe loads for different lengths, based upon the Least Radius of Gyration, are given on pages 250 to 277 inclusive.

Safe loads for I-beams used as Columns or Struts are given on pages 218 to 221, and the dimensions of these sections can be obtained from the

tables on pages 156 to 159 inclusive.

The Plate and Channel Columns given in Series A are particularly useful in buildings or locations in which it is desired to keep the extreme dimensions of the cross section as small as possible for this style of column, although in this series the Radius of Gyration about the central axis parallel to the channel webs is somewhat smaller than the Radius of Gyration about the axis perpendicular to the channel webs. This makes the narrower columns of Series A somewhat less economical of material than the wider columns of Series B, which, however, is small in amount for columns of ordinary story lengths of 10 feet to 14 feet, such as are used in skeleton buildings.

In Series B of Plate and Channel Columns with wider plates, the Radii of Gyration about the two axes are practically equal for the intermediate thicknesses and these columns are slightly more economical of material than those of Series A, although they require somewhat more space on account

of their wider sections.

The Safe Loads for columns of various kinds, as given on pages 218 to 277 inclusive, are expressed in thousands of pounds, and have been figured by the use of Gordon's formula, as stated at the heads of the various tables, using the safety factor 4, which relates to static or quiescent loads such as occur in ordinary buildings.

On page 217 is given a table showing the Distances Back to Back for Spacing two Channels of the same size in order to produce equal Moments of Inertia about the two rectangular axes. This table will be found to be

useful in designing compression members of trusses, etc.

The Safe Loads of the tables are assumed to be centrally applied, and for convenience in computing the proper sizes required to support eccentric loads, the tables of Moments of Inertia and Section Moduli for the different sections of columns are given.

The Safe Loads of the various tables are figured for extreme ratios from

30 to 150 for  $\frac{1}{r}$ , in which 1 is the length of the column and r the Least

Radius of Gyration, both expressed in inches.

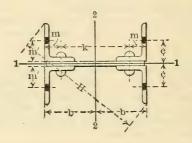
The weights of columns stated in the tables are per lineal foot of shaft, and do not include any allowances for bases, brackets or other connections, as these depend upon the particular details and requirements of each case.

Loads for other safety factors can be figured from the tables by inverse

proportion, thus:

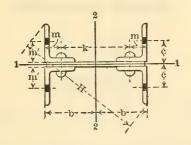
New safety factor: 4:: load from tables: new loads. Drawings of typical details of steel columns are given on pages 298 and 299.

## DIMENSIONS FOR PLATE AND ANGLE COLUMNS.



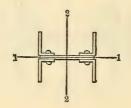
Size of Angles.	Size of Plates.	Weight of Column.	Area of Column Section.	b	c	m	m′	k	н
Inches.	Inches.	Lbs.per Ft.	Sq. Ins.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
3 x 2½ x ½ x ½ 5%	6 x 1/4 6 5/8	24.9 56.1	6.79 15.94	31/8	$2\frac{1\%}{16}$	1,1/2	13/4	31/2	813 91/8
3 x 2½ x ¼ 5/8	8 x 1/4 5/8	26.6 60.4	7.29 17.19	41/8	$2\frac{1}{16}$	1,1/2	13/4	51/2	$10\frac{3}{8} \\ 10\frac{9}{16}$
3 x 21/2 x 1/4 5/8	10 x 1/4 5/8	28.3 64.6	7.79 18.44	51/8	$2\frac{1}{16}$	1,1/2	13/4	71/2	$^{12}_{12_{\bar{1}\bar{6}}}$
3 x 2½ x ½ 5/8	12 x 1/4 5/8	30.0 68.9	8.29 19.69	61/8	$2\frac{1}{16}$	11/2	13/4	91/2	$13\frac{3}{4} \\ 13\frac{15}{16}$
3½ x 2½ x ¼ x ¼ 3¼	7 x 1/4 3/4	27.4 73.3	7.50 21.00	35/8	23/8 25/8	11/2	21/4	41/2	10½ 10½ 10½
3½ x 2½ x ¼ "2 x 3¼	8 x 1/4 " 3/4	28.3 75.9	7.75 21.75	41/8	23/8 25/8	11/2	21/4	51/2	$\frac{11}{11\frac{5}{16}}$
3½ x 2½ x ¼ x ¼ 3¼	10 x 1/4	30.0 81.0	8.25 23.25	51/8	23/8 25/8	1,1/2	21/4	71/2	12 ½ 12 ½
3½ x 2½ x ¼ "2 x 3¼	12 x 1/4	31.7 86.1	8.75 24.75	61/8	23/8 25/8	11/2	21/4	91/2	$14\frac{1}{4}$ $14\frac{1}{2}$
4 x 3 x 1 8 1 8 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	8 x 5 16 7/8	39.3 98.6	10.86 28.44	41/8	$2^{\frac{7}{16}}_{\frac{11}{16}}$	13/4	21/4	43/4	${ 11_{16}^{11} \atop 12 \frac{1}{8} }$
4 x 3 x 15 7/8	10 x 5/8	41.4 104.6	11.49 30.19	51/8	$2^{\frac{7}{16}}_{16}$	13/4	21/4	63/4	$13_{\frac{16}{16}}^{\frac{3}{16}}\\13_{\frac{9}{16}}^{\frac{9}{16}}$
4 x 3 x 5 7/8	12 x 5 16 7/8	43.5 110.5	12.11 31.94	61/8	$2^{\frac{7}{16}}_{1\frac{1}{16}}$	13/4	21/4	83/4	$14\frac{13}{16} \\ 15\frac{1}{8}$
4 x 3 x 15 7/8	14 x 5 78	45.6 116.5	12.74 33.69	71/8	$2^{\frac{7}{16}}_{16}$	13/4	21/4	103/4	$\begin{array}{c} 16\frac{1}{2} \\ 16\frac{13}{16} \end{array}$

Dimensions m' and c may be varied to suit requirements.

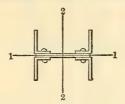


Size of Angles.	Size of Plates.	Weight of Column.	Area of Column Section.	b	c	m	m′	k	н
Inches.	Inches.	Lbs.per Ft.	Sq. Ins.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
5 x 3½ x 5 16 15 16	$10 \times \frac{5}{16}$	47.4 130.6	13.36 37.74	51/8	$2^{\frac{7}{16}}_{2^{\frac{3}{4}}}$	21/4	21/4	53/4	14 <sup>9</sup> 15
$5 \times 3^{1/2} \times \frac{5}{16}$	12 x 5 16 15 16	49.5 137.0	13.98 39.61	61/8	$2^{\frac{7}{16}}_{2\frac{3}{4}}$	21/4	21/4	73/4	${}^{16}_{16_{\overline{16}}}$
$5 \times 3^{1/2} \times \frac{5}{16}$	14 x 5 16 15 15	51.6 143.4	14.61 41.49	71/8	$2^{\frac{7}{16}}_{2\frac{3}{4}}$	21/4	21/4	93/4	$^{17\frac{9}{16}}_{17\frac{15}{16}}$
$ \frac{5}{6} \times \frac{3}{16} \times \frac{5}{16} $	16 x 5 16 15 16	53.7 149.8	15.23 43.36	81/8	$2^{\frac{7}{16}}_{2\frac{3}{4}}$	21/4	21/4	113/4	$19\frac{1}{4} \\ 19\frac{9}{16}$
6 x 3½ x 3/8	12 × 3/8	64.2 158.3	18.23 46.00	61/8	2 <sup>7</sup> / <sub>16</sub> 2 <sup>3</sup> / <sub>4</sub>	21/4	21/4	73/4	17 <sup>7</sup> / <sub>16</sub> 17 <sup>7</sup> / <sub>8</sub>
6 x 3½ x 3/8	14 × 3/8	66.7 165.1	18.98 48.00	71/8	$2^{\frac{7}{16}}_{2\frac{3}{4}}$	21/4	21/4	93/4	$18\frac{7}{8} \\ 19\frac{5}{16}$
6 x 3½ x 3/8	1,6 x 3/8	69.3 171.9	19.73 50.00	81/8	$2^{\frac{7}{16}}_{2\frac{3}{4}}$	21/4	21/4	113/4	$\begin{array}{c} 20\frac{7}{16} \\ 20\frac{13}{16} \end{array}$
6 x 3½ x 3/8	18 x 3/8	71.8 178.7	20.48 52.00	91/8	2 <sup>7</sup> / <sub>16</sub> 2 <sup>3</sup> / <sub>4</sub>	21/4	21/4	133/4	$\begin{array}{c} 22\frac{1}{16} \\ 22\frac{7}{16} \end{array}$
$7 \times 31/2 \times 716$	14 × 7 16	82.6 178.7	23.74 52.00	71/8	2½ 2¾	21/4	21/4	93/4	$\begin{array}{c} 20\frac{5}{16} \\ 20\frac{11}{16} \end{array}$
$7 \times 3\frac{1}{2} \times \frac{7}{16}$	16 x 7 16	85.6 185.5	24.61 54.00	81/8	2½ 2¾	21/4	21/4	113/4	21 <sup>3</sup> / <sub>4</sub> 22 <sup>1</sup> / <sub>8</sub>
$7 \times 3\frac{1}{2} \times \frac{7}{16}$	18 x 7 1 1	88.6 192.3	25.49 56.00	91/8	2½ 2¾	21/4	21/4	1,33/4	23½ 23½ 23½
$\frac{7}{6} \times \frac{31}{2} \times \frac{7}{16}$	20 x 7	91.6 199.1	26.40 58.00	101/8	2½ 2¾	21/4	21/4	153/4	247/8 25 16

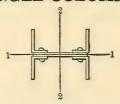
Dimensions m' and c may be varied to suit requirements.



		Axis	1-1.	Axis	2-2.		Axis	1-1.	Axis	2-2.
Size of Angles.	Size of Plate.	Moment of Inertia.	Section Modulus.	Moment of Inertia.	Section Modulus.	Size of Plate.	Moment of Inertia.	Section Modulus.	Moment of Inertia.	Section Modulus.
Inches.	Inches.	Ins.4	Ins.3	Ins.4	Ins.3	Inches.	Ins.4	Ins.3	Ins.4	Ins.3
3 x 2½ x½ x½ x½ x 1/4 x 1/5 x	6x1/4 6x1/4 6x1/6 6x	10.3 13.4 16.7 20.2 24.0 28.1 32.4	3.3 4.3 5.2 6.3 7.4 8.6 9.8	39.4 47.9 55.9 63.5 70.6 77.3 83.7	12.6 15.3 17.9 20.3 22.6 24.8 26.8	8x1/4 6 16 6 8/8 7 76 6 1/2 6 1/2 6 5/8 6 5/8	10.3 13.4 16.7 20.3 24.0 28.1 32.4	3.3 4.3 5.3 6.3 7.4 8.6 9.8	76.7 93.7 110.1 125.6 140.5 154.6 168.1	18.6 22.7 26.7 30.5 34.1 37.5 40.8
3 x 2½ x¼	10x <sup>1</sup> / <sub>4</sub>	10.3 13.4 16.7 20.3 24.1 28.1 32.5	3.3 4.3 5.3 6.3 7.4 8.6 9.8	128.4 157.5 185.6 212.5 238.3 263.1 286.9	25.1 30.7 36.2 41.5 46.5 51.3 56.0	12x <sup>1</sup> / <sub>4</sub> <sup>5</sup> / <sub>16</sub> <sup>7</sup> / <sub>16</sub> <sup>7</sup> / <sub>16</sub> <sup>7</sup> / <sub>16</sub> <sup>1</sup> / <sub>2</sub> <sup>9</sup> / <sub>16</sub> <sup>5</sup> / <sub>8</sub>	10.3 13.4 16.7 20.3 24.1 28.2 32.5	3.3 4.3 5.3 6.3 7.4 8.6 9.8	195.7 240.5 284.0 325.8 366.1 405.1 442.7	32.0 39.3 46.4 53.2 59.8 66.1 72.3
3½ x 2½ x½ "" 55 "" 75 "" 75 "" 15 "" 1	7x <sup>1</sup> / <sub>4</sub>	16.0 20.7 25.6 30.8 36.3 42.1 48.3 54.8 61.6	4.4 5.7 6.9 8.3 9.7 11.1 12.7 14.3 15.9	62.4 76.2 89.3 101.7 113.6 124.8 135.5 145.6 155.2	17.2 21.0 24.6 28.1 31.3 34.4 37.4 40.2 42.8	8x14 	16.0 20.7 25.6 30.8 36.3 42.1 48.3 54.8 61.6	4 4 5.7 6.9 8.3 9.7 11.1 12.7 14.3 15.9	84.7 103.6 121.7 138.9 155.5 171.2 186.3 200.6 214.3	20.5 25.1 29.5 33.7 37.7 41.5 45.2 48.6 52.0
3½ x 2½ x¼ "	10x14 76 38 77 16 1	16.0 20.7 25.6 30.8 36.3 42.2 48.3 54.9 61.7	4.4 5.7 6.9 8.3 9.7 11.2 12.7 14.3 15.9	140.9 173.0 203.9 233.5 262.1 289.4 315.9 341.2 365.6	27.5 33.8 39.8 45.6 51.1 56.5 61.7 66.6 71.3	12x <sup>1</sup> / <sub>4</sub> 6 16 6 16 6 176 6 1	16.0 20.7 25.6 30.8 36.4 42.2 48.4 54.9 61.8	4.4 5.7 7.0 8.3 9.7 11.2 12.7 14.3 15.9	213.7 262.9 310.5 356.2 400.7 443.4 484.9 524.8 563.3	34.9 42.9 50.7 58.2 65.4 72.4 79.2 85.7 92.0

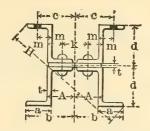


		Axis	1-1.	Axis	2-2,		Axis	1-1.	Axis	2-2.
Size of Angles.	Size of Plate.	Moment of Inertia.	Section Modulus.	Moment of Inertia.	Section Modulus.	Size of Plate.	Moment of Inertia.	Section Modulus.	Moment of Inertia.	Section Modulus.
Inches.	Inches.	Ins.4	Ins.3	Ins.4	Ins.3	Inches.	Ins.4	Ins.3	Ins.4	Ins.3
4 x 8 x 5 6 7 8 6	8 X 18 6 6 7 6 6 7 7 8 6 6 7 7 8 6 6 7 7 8 6 6 7 7 8 6 6 7 7 8 6 6 7 7 8 7 8	30.3 37.4 44.8 52.6 60.8 69.5 78.6 88.1 98.1 108.5	7.3 8.9 10.6 12.4 14.2 16.1 18.1 20.1 22.3 24.4	114.6 134.8 154.0 172.4 190.0 206.9 223.0 238.3 253.0 267.0	27.8 32.7 37.3 41.8 46 1 50 2 54.1 57.8 61.3 64.7	10 x 5/6 (1/6 1/6 1/6 1/6 1/6 1/6 1/6 1/6 1/6 1/6	30.3 37.4 44.8 52.6 60.9 69.5 78.6 88.2 98.2 108.6	7.3 8.9 10.6 12.4 14.2 16.1 18.1 20.2 22.3 24.5	192.0 226.4 259.5 291.5 322.2 352.0 380.5 408.0 434.4 459.8	37.5 44.2 50.6 56.9 62.9 68.7 74.2 79.6 84.7 89.7
4×3 x 56  11 12 12 12 12 12 12 12 12 12 12 12 12 1	12 x 5 6 6 7 6 7 6 7 6 7 6 6 7 6 7 6 6 7 6 7	30.3 37.4 44.8 52.6 60.9 69.6 78.7 88.2 98.2 108.7	7.3 8.9 10.6 12.4 14.2 16.1 18.1 20.2 22.3 24.5	292.3 345.5 396.7 446.6 494.7 541.5 586.5 630.1 672.2 713.1	47.7 56.4 64.8 72.9 80.8 88.4 95.8 102.9 109.8 116.4	14 x 5 6 6 6 7 6 6 7 6 6 7 6 6 7 6 6 7 6 6 7 6 7 6 6 7	30.3 37.4 44.8 52.7 60.9 69.6 78.7 88.3 98.3 108.8	7.3 8.9 10.6 12.4 14.2 16.1 18.1 20.2 22.3 24.5	416.8 493.4 567.4 639.7 709.6 777.8 843.7 907.7 969.8 1030.1	58.5 69.3 79.6 89.8 99.6 109.2 118.4 127.4 136.1 144.6
5 x 31/2 x 5 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	10 x 56 (13/8) (16/14) (16/14) (17/8)	57.6 70.6 84.1 98.2 112.9 128.2 144.1 160.6 177.8 195.7 214.2	11.2 13.6 16.1 18.7 21.4 24.1 27.0 29.9 32.9 36.0 39.2	225.0 265.7 304.8 342.6 379.1 414.4 448.2 481.1 512.6 543.1 572.5	43.9 51.8 59.5 66.9 74.0 80.9 87.5 93.9 100.0 106.0 111.7	12 x 5 6 6 7 6 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6	57.6 70.6 84.1 98.2 112.9 128.2 144.1 160.7 177.9 195.8 214.3	11.2 13.6 16.1 18.7 21.4 24.1 27.0 29.9 32.9 36.0 39.2	341.9 404.6 465.2 524.0 581.0 636.4 689.8 741.8 792.1 841.0 888.2	55.8 66 1 75.9 85.5 94.9 103.9 112.6 121.1 129.3 137.3 145.0
5 x 31/2 x 56 6 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7		57.6 70.6 84.1 98.2 112.9 128.3 144.2 160.8 178.0 195.9 214.4	11.2 13.6 16.1 18.7 21.4 24.1 27.0 29.9 32.9 36.0 39.2	486.8 576.9 664.2 749.3 832.1 912.7 990.8 1067.1 1141.0 1213.2 1283.1	68.3 81.0 93.2 105.2 116.8 128.1 139.1 149.8 160.1 170.3 180.1	16 x 5 6 6 7 6 6 7 6 6 7 6 6 7 6 6 7 6 7 6 7	57.6 70.6 84.1 98.3 113.0 128.3 144.2 160.8 178.1 196.0 214.6	11.2 13.6 16.1 18.7 21.4 24.2 27.0 29.9 32.9 36.0 39.2	660.8 784.0 903.8 1020.6 1134.7 1245.9 1354.0 1459.8 1562.6 1663.3 1761.0	81.3 96.5 111.2 125.6 139.7 153.3 166.6 179.7 192.3 204.7 216.7



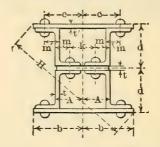
		Axis	1-1.	Axis	2-2.		Axis	1-1.	Axis	2-2.
Size of Angles.	Size of Plate.	Moment of Inertia.	Section Modulus.	Moment of Inertia.	Section Modulus.	Size of Plate.	Moment of Inertia.	Section Modulus.	Moment of Inertia.	Section Modulus.
Inches.	Inches.	Ins.4	Ins.3	Ins.4	Ins.3	inches.	Ins.4	Ins.3	Ins.4	Ins.3
6 x 31/2 x 3/8 11/10 2	12 x 3/8 to 1/2	119.2 141.5 164.5 188.3 212.9 238.3 264.5 291.5 319.5 348.2 377.5	19.3 22.8 26.3 50.0 33.7 37.6 41.5 49.6 53.8 58.1	457.5 526.2 593.0 657.9 720.9 781.8 841.2 898.5 954.4 1008.4 1060.8	74.7 85.9 96.8 107.4 117.7 127.6 137.3 146.7 155.8 164.6 173.2	14 x 3/8 16 1/2 16 1/2 16 16 16 16 16 16 16 16 16 16 16 16 16	119.2 141.5 164.5 188.3 212.9 238.3 264.6 291.6 319.6 348.4 377.7	19.3 22.8 26.3 30.0 33.7 37.6 41.5 45.5 49.6 53.9 58.1	649.1 747.7 843.9 937.6 1028.8 1117.3 1203 9 1287.9 1370.0 1449.5 1526.9	91.1 104.9 118.4 131.6 144.4 156.8 169.0 180.8 192.3 203.4 214.3
6 x 3 ½ x 3 x 3	16 x 3/8 1/7 1/8 1/8 1/9 1/9 1/9 1/9 1/9 1/9 1/9 1/9 1/9 1/9	119.2 141.5 164.5 188.4 213.0 238.4 264.6 291.7 319.7 348.5 377.8 220.8	19.3 22.8 26.3 30.0 33.7 37.6 41.5 45.5 49.7 53.9 58.1 30.6	878.6 1013.2 1144.7 1273.2 1398.6 1520.6 1640.2 1756.4 1870.4 1981.1 2089.1 831.2	108.1 124.7 140.9 156.7 172.1 187.2 201.9 216.2 230.2 243.8 257.1 116.7	18 x 3/8 1/6 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2		19.3 22.8 26.3 30.0 33.7 37.6 41.5 45.5 49.7 53.9 58.2 30.6	1147.4 1324.4 1497.5 1667.1 1832.8 1994.3 2152.9 2307.4 2459.2 2606.8 2751.3 1122.6	125.7 145.1 164 1 182.7 200.9 218.6 235 9 252.9 269 5 285.7 301.5 138.2
66 96 66 96 66 96 66 96 66 96 96 96 96 9		1	35.3 40.2 44.9 50.0 55.1 60.4 65.7 71.1 76.6	938.4 1043.0 1144.6 1243.9 1340.7 1434.8 1526.7 1615.9 1702.8	131.7 146 4 160.7 174.6 188.2 201.4 214.3 226 8 239.0	16 x 76 6 1 2 9 6 1 5 8 6 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		35.3 40.2 44.9 50.0 55.1 60.4 65.7 71.1 76.6	1268.8 1411.6 1550.9 1687.2 1820.5 1950.3 2077.4 2201.1 2322.0	156.2 173.7 190.9 207.7 224.0 240.0 255.7 270.9 285.8
7 × 3½× 7	18 x 76 4 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	220.8 255.9 292.8 328.6 367.4 406.7 447.4 488.5 531.0 574.7	30.6 35.3 40.2 44.9 50.0 55.2 60.4 65.7 71.1 76.6	1463.2 1655.1 1843.0 2026.6 2206.4 2382.7 2554.7 2723.5 2888.1 3049.1	160 4 181.4 202.0 222.1 241.8 261.1 280 0 298.5 316.5 334.2	20 x 76	220.8 255.9 292.8 328.6 367.5 406.8 447.5 488.6 531.2 574.8	30.6 35.3 40.2 44.9 50.0 55.2 60.4 65.7 71.1 76.6	1854.8 2099.4 2339.4 2574.2 2804.4 3030.5 3251.4 3468.5 3680.5 3888.3	183.2 207.4 231.1 254.2 277.0 299.3 321.1 342.6 363.5 384.0

#### DIMENSIONS FOR Z-BAR COLUMNS.



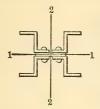
Section of	t	a	b	d	н	c	k	m	A
Column.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
4-3" Z-Bars and Web-plate 534" wide.	1/4 5 16 3/8 77 16 1/2 91	2116/416 222416 223/416 223/416 223/4	576 576 515 515 516 516 516 516	31/8 37/2 31/8 31/9 31/4 31/4 31/2	12 <sup>9</sup> / <sub>16</sub> 12 <sup>5</sup> / <sub>8</sub> 12 <sup>3</sup> / <sub>8</sub> 12 <sup>1</sup> / <sub>2</sub> 12 <sup>1</sup> / <sub>4</sub> 12 <sup>1</sup> / <sub>6</sub>	43/8 41/6 41/4 43/16 41/8 41/8	23/4	15/8	3
4-4'' Z-Bars and Web-plate 634'' wide.	14 5 6 8 7 6 2 9 6 8 16 8 16 8 16 8 16 8 16 8 16 8 16	31-6 31-6 31-6 31-6 31-6 31-6 31-6 31-6	6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	41/87 43/24 43/24 41/32	15 16 3 16 15 15 15 15 15 15 15 15 15 15 15 15 15	5 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	31/2	134	3½ " " " " " "
4-5" Z-Bars and Web-plate 7" wide.	10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	6 1 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	55555555555555555555555555555555555555	16161616 1661616 1661616 1661616 1661616 16616 1	555555544783416 44164416	31/2	17/8	3 <sup>5</sup> / <sub>8</sub>
4-6" Z-Bars and Web-plate 734" wide.	3076-296-30-60-496-8	3355/2965/801/2965/80	71/8 71/8/8 71/8/8 611-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1	61696 6386 6386 6386 6386 6152 6152 6152 6152 6152	$18\frac{7}{8}$ $19\frac{1}{8}$ $18\frac{3}{4}$ $18\frac{13}{16}$ $18\frac{9}{16}$ $18\frac{11}{16}$ $18\frac{7}{8}$	55555555555555555555555555555555555555	4	2	4

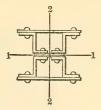
## DIMENSIONS FOR Z-BAR AND PLATE COLUMNS.



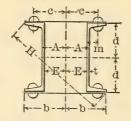
		Cover	Plates.							
Section of Column.	Thickness of Web-plate and Z-Bars.	Width.	Thick- ness. t'	ь	đ	н	c	k	m	A
	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
	11 16 66 66 66 66 66	14	3/7-B/29-B/20-B/49-B/20	66 66 66 66 66 66 66	7 Paralization 1 Para	$\begin{array}{c} 19\frac{9}{16}\\ 19\frac{11}{16}\\ 19\frac{3}{4}\\ 19\frac{13}{16}\\ 20\\ 20\frac{3}{16}\\ 20\frac{5}{16} \end{array}$	5,5   	4	2	4
4-6'' 2-Bars	3/4	14	3/7-6/21-6/8-1-6/4-3-6/8	66 66 66	63/45/6/05/6/6/17/05/6/6/17/77/1/4	$\begin{array}{c} 19\frac{7}{16} \\ 19\frac{9}{16} \\ 19\frac{1}{5} \\ 819\frac{13}{16} \\ 19\frac{13}{16} \\ 20\frac{1}{16} \\ 20\frac{1}{8} \end{array}$	51/4	4	2	4
and 1 Web-plate 734" wide.	13	14	3/876/296/816/496/8	66 66 66 66 66 66 66 66 66 66 66 66 66	7.225/21-12	$\begin{array}{c} 19\frac{9}{16} \\ 19\frac{11}{16} \\ 19\frac{11}{16} \\ 19\frac{13}{16} \\ 19\frac{15}{16} \\ 20\frac{3}{16} \\ 20\frac{5}{16} \end{array}$	5 3 6 CC C	4	2	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
	7/8	14	3/76/296/81/6/436/8	7   	6156 7166 7186 7186 7186 7186 7186 7186 718	1911636 19178 2016 2016 20178 2016 20176	51/8	4	2	4

#### PROPERTIES OF Z-BAR COLUMNS.



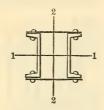


	<b>Z</b> -1	Bar C	olum	ns.		Z-Bar (	olu	mnsw	vith C	over P	lates.
Section	of Web-Z-Bars.	Axis	1-1.	Axis	2-2.	Section	of tes.	Axis	1-1.	Axis	2-2.
of Column.	Thickness of plate and Z-	Moment of Inertia.	Section Mod- ulus.	Moment of Inertia.	Section Mod- ulus.	of Column.	Thickness of Cover Plates.	Moment of Inertia.	Section Mod- ulus.	Moment of Inertia.	Section Mod- ulus.
	Ins.	Ins.4	Ins.3	Ins.4	Ins.3		Ins.	Ins.4	Ins.3	Ins.4	Ins.3
4-3" Z-Bars and Web- plate 534" wide.	1/4 5 6 3/8 7 16 1/2 9 16	32.3 42.8 48.0 59.5 63.6 76.1	10.3 13.3 15.1 18.1 19.6 22.8	80.3 99.8 112.1 130.0 138.9 155.3	14.8 18.3 21.1 24.5 26.8 29.9	4 Z-Bars 6½" x 3½"x½½" and 1 Web-plate 7¾"x½"	3/8/7/6/22/6/81/6/43/6/8/15/8/15/8/15/8/15/8/15/8/15/8/15/8/	1021.1 1103.9 1188.1 1273.8 1361.1 1450.0 1540.4	149.2 159.8 170.5 181.2 191.9 202.6 213.4 224.2	704.7 733.3 761.8 790.4 819.0 847.6 876.2	100.7 104.8 108.8 112.9 117.0 121.1 125.2
4-4" Z-Bars and Web- plate 634" wide.	1/4 5/6 /8 /7/5 1/2 /9/6 /8 1/6 /4	68.6 89.7 112.6 118.4 141.7 166.9 167.2 192.9 220.5	16.6 21.3 26.1 28.1 32.9 37.9 38.8 43.8 49.0	133 0 165.2 197.2 212.4 241.4 270.0 276.4 302.3 327.9	21.1 26.2 31.2 34.7 39.4 44.1 46.5 50.9 55.2	4 Z-Bars 6" x 3½" x ¾" and 1 Web-plate 7¾" x ¾"	3/8/6/29/6/81/6/43/6/8	1632.4 1725.9 1014.0 1094.5 1176.5 1259.9 1344.9 1431.5 1519.5 1609.1 1700.3	224.2 235.0 150.2 160.7 171.1 181.6 192.1 202.7 213.3 223.9 234.5	904.8 933.3 715.7 744.3 772.9 801.5 830.1 858.6 887.2 915.8 944.4	129.3 133 3 102.2 106.3 110.4 114.5 118.6 122.7 126.7 130.8 134.9
4-5" Z-Bars and Web- plate 7" wide.	56/87/6/22/6/00/16/43/6/5/00/16/43/6	149.4 186.0 225.2 235.6 275.4 317.8 320.1 363.0 408.7	29.0 35.4 42.4 44.9 51.5 58.4 59.9 66.8 73.9	197.2 235.2 272.7 289.7 323.8 357.6 364.9 395.6 425.8	30.1 35.8 41.5 45.4 50.8 56.1 59.0 63.9 68.8	4 Z-Bars 616' x 316' x 13'' x 13'' and 1 Web-plate 73'' x 13'' x 13''	8 3/8/16/29/16/81/16/4/3/6/8	1094 2 1176.9 1261.2 1346.9 1434.2 1523.0 1613.4 1705.4 1799.0	159.9 170.4 181.0 191.6 202.2 212.8 223.5 234.2 245.0	757.4 786.0 814.6 843.2 871.7 900.3 928.9 957.5 986.1	108.2 112.3 116.4 120.5 124.5 128.6 132.7 136.8 140.9
4-6" Z-Bars and Web- plate 734" wide.	3/8/7/6/29/6/8/16/43/6/8/15/8/15/8/15/8/15/8/15/8/15/8/15/8/	288.0 346.8 409.1 426.3 489.3 555.8 561.7 628.9 699.7	46.5 55.2 64.2 67.9 76.8 85.9 88.1 97.7 107.7	318.1 368.8 418.9 441.7 487.7 533.2 544.2 585.9 627.1	44.6 51.8 58.8 63.7 70.3 76.9 80.6 86.8 92.9	4 Z-Bars 6½" x 3½" x ½" and 1 Web-plate 7¾" x ½"	3/8 7/6/29/6/8/15/8/15/8/15/8/15/8/15/8/15/8/15/8/	1178.3 1263.3 1349.8 1437.8 1527.5 1618.7 1711.4 1805.8 1901.8	169.8 180.5 191.1 201.8 212.5 223.3 234.0 244.9 255.7	798.6 827.1 855.7 884.3 912.9 941.5 970.1 998.6 1027.2	114.1 118.2 122.2 126.3 130.4 134.5 138.6 142.7 146.7

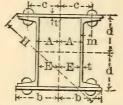


Depth of Channel and Section	Weight per Foot.	t	ь	d	н	c	Œ	A	m
Number.	Pounds.	Inches.	Inches.	Inches,	Inches.	Inches.	Inches.	Inches.	Inches.
6" C17	8.00 10.50 13.00 15.50	.20 .32 .44 .56	3¾ "	8,,,	9,9	27/8	$\begin{array}{c} 1_{\frac{13}{16}} \\ 1_{\frac{11}{16}} \\ 1_{\frac{9}{16}} \\ 1_{\frac{7}{16}} \end{array}$	2	$egin{array}{c} egin{array}{c} \egin{array}{c} egin{array}{c} \egin{array}{c} \egin{array}$
7" C21	9.75 12.25 14.75 17.25 19.75	.21 .32 .42 .53 .63	41/4	3½ " "	11	33/8	$2\frac{3}{16}$ $2\frac{1}{16}$ $1\frac{1}{16}$ $1\frac{1}{1}$ $1\frac{3}{4}$	23/8	$\begin{array}{c} 1 \frac{3}{16} \\ 1 \frac{5}{16} \\ 1 \frac{7}{16} \\ 1 \frac{1}{2} \\ 1 \frac{5}{8} \end{array}$
8" C25	11.25 13.75 16.25 18.75 21.25	.22 .31 .40 .49 .58	413 (16 (16 (16 (16 (16	4	121/2	33/4	$2\frac{1}{2}$ $2\frac{7}{16}$ $2\frac{3}{8}$ $2\frac{1}{4}$ $2\frac{3}{16}$	23/4	$\begin{array}{c c} 1\frac{1}{4} \\ 1\frac{5}{16} \\ 1\frac{3}{8} \\ 1\frac{1}{2} \\ 1\frac{9}{16} \end{array}$
9″ C29	13.25 15.00 20.00 25.00	.23 .29 .45 .61	5 <sub>16</sub>	4½ "	133/4	41/8	23/4 2116 29/16 23/8	3,	$1\frac{3}{8}$ $1\frac{7}{16}$ $1\frac{9}{16}$ $1\frac{3}{4}$
10" C33	15.00 20.00 25.00 30.00 35.00	.24 .38 .53 .68 .82	53/4	5,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	151/4	45/8	$3\frac{1}{8}$ $3\frac{7}{8}$ $2\frac{11}{16}$ $2\frac{9}{16}$	33/8	11/2 15/8 13/4 11/5 21/6
12" C41	20.50 25.00 30.00 35.00 40.00	.28 .39 .51 .64 .76	613	6	181/8	55/8	37/8 33/4 35/8 31/2 33/8	41/8	13/4 17/8 2 21/8 21/4
15" C53	33.00 35.00 40.00 45.00 50.00 55.00	.40 .43 .52 .62 .72 .82	81/8	71/2	221/8	65/8	43/4 4116 45/8 41/2 47/6 45/8 47/6 45/8	51/8	17/8 1 <sup>15</sup> / <sub>16</sub> 2 <sup>1</sup> / <sub>8</sub> 2 <sup>1</sup> / <sub>4</sub> 2 <sup>1</sup> / <sub>16</sub>

#### PROPERTIES OF LATTICED CHANNEL COLUMNS.

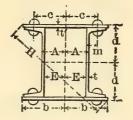


		Axis	s 1-1 <b>.</b>	Axis	s 2-2.
Depth of Channel and	Weight per Foot.	Moment of Inertia.	Section Modulus.	Moment of Inertia.	Section Modulus.
Section Number.	Pounds.	Inches.4	Inches,3	Inches.4	Inches.3
6″ C17	8.00 10.50 13.00 15.50	26.0 30.2 34.6 39.0	8.7 10.1 11.5 13.0	27.0 31.1 35.2 38.7	7.3 8.4 9.5 10.4
7'' <b>c</b> 21	9.75 12.25 14.75 17.25 19.75	42.2 48.4 54.4 60.4 66.4	12.1 13.8 15.5 17.3 19.0	44.0 50.5 56.4 61.4 66.5	10.3 11.9 13.3 14.4 15.6
8″ c25	11.25 13.75 16.25 18.75 21.25	64.6 72.0 79.8 87.7 95.6	16.2 18.0 20.0 21.9 23.9	67.5 75.8 84.5 92.3 99.7	14.0 15.8 17.6 19.3 20.8
9′′ <b>C</b> 29	13.25 15.00 20.00 25.00	94.6 101.8 121.6 141.4	21.0 22.6 27.0 31.4	92.4 100.0 120.1 139.1	17.8 19.2 23.1 26.8
10″ <b>C</b> 33	15.00 20.00 25.00 30.00 35.00	133.8 157.4 182.0 206.4 231.0	26.8 31.5 36.4 41.3 46.2	106.2 158.5 183.3 205.4 226.0	18.5 27.6 32.0 35.8 39.4
12" C41	20.50 25.00 30.00 35.00 40.00	256.2 288.0 323.2 358.6 393.8	42.7 48.0 53.9 59.8 65.6	256.9 295.6 335.8 370.5 405.7	37.9 43.6 49.5 54.6 59.8
15″ C53	33.00 35.00 40.00 45.00 50.00 55.00	625.2 639.8 695.0 750.2 805.4 860.4	83.4 85.3 92.7 100.0 107.4 114.7	618.7 636.1 700.8 763.0 819.5 874.3	76.1 78.3 86.3 93.9 100.9 107.6



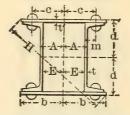
#### SERIES A.

Depth	Weight	Size of	Plates.								
of Channel and Section	per Foot.	Width.	Thick- ness. t'	t	b	d	н	c	E	A	m
No.	Pounds,	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
6" C17	\$.0 10.5 13.0 15.5	8	1/4/8/4/8/4/8/1/4/8/1/4/8	.20 .32 .44 .56	4 66 66 66 66 66 66	31/4/8 35/8/4/8 31/4/8 31/4/8 31/4/8 31/4/8 35/8	$10^{\frac{5}{163}}_{10^{\frac{1}{13}}}$ $10^{\frac{5}{163}}_{10^{\frac{1}{13}}}$ $10^{\frac{5}{163}}_{10^{\frac{1}{13}}}$ $10^{\frac{5}{163}}_{10^{\frac{1}{13}}}$ $10^{\frac{5}{163}}_{10^{\frac{1}{13}}}$	27/8	$ \begin{array}{c} 1\frac{13}{16} \\ 1\frac{11}{16} \\ 1\frac{9}{16} \\ 1\frac{7}{16} \end{array} $	2	$1_{\frac{1}{1}6}^{\frac{1}{1}6}$ $1_{\frac{5}{1}6}^{\frac{5}{1}6}$ $1_{\frac{7}{1}6}^{\frac{5}{1}6}$ $1_{\frac{7}{1}6}^{\frac{7}{1}6}$
7" C21	9.75 12.25 14.75 17.25 19.75	9	1478/478/478/478/478	.21 .32 .42 .53	41/2	33/4/8/4/8/4/8/4/8/4/8/4/8/4/8/4/8/4/8/4	$\begin{array}{c} 11^{3/4} \\ 12^{3/6} \\ 11^{3/6} \\ 12^{3/6} \\ 12^{3/6} \\ 12^{3/6} \\ 12^{3/6} \\ 11^{3/6} \\ 12^{3/6} \\ 11^{$	31/4     	2 1 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	21/4	$ \begin{array}{c} 1,\frac{3}{16} \\ 1,\frac{5}{16} \\ 1,\frac{7}{16} \\ 1,\frac{7}{16} \\ 1,\frac{7}{2} \\ 1,\frac{5}{8} \end{array} $
8″ C25	11,25 13,75 16,25 18,75 21,25	10	1478/478/478/478/478	.22 .31 .40 .49 .58	5	45,874,874,874,874,474,874,474,4	$13^{1/8}$ $13^{5/8}$ $13^{1/8}$ $13^{5/8}$ $13^{1/8}$ $13^{5/8}$ $13^{1/8}$ $13^{5/8}$	35/8	2 <sup>3</sup> / <sub>8</sub> 2 <sup>5</sup> / <sub>1</sub> / <sub>6</sub> 2 <sup>1</sup> / <sub>4</sub> 2 <sup>1</sup> / <sub>8</sub> 2 <sup>1</sup> / <sub>1</sub> / <sub>6</sub>	25/8	1½4 1,56 13% 1½2 1,96
9" C29	13,25 15,00 20,00 25,00	11	1/4/ 5/8 1/4/ 5/8 1/4/ 5/8 1/4/ 5/8	.23 .29 .45 .61	51/2	43/4 51/8 43/4 51/8 43/4 51/8 43/4 51/8 43/4 51/8	$\begin{array}{c} 14\frac{1}{2} \\ 15\frac{1}{16} \\ 14\frac{1}{2} \\ 15\frac{1}{16} \\ 14\frac{1}{2} \\ 15\frac{1}{16} \\ 14\frac{1}{2} \\ 15\frac{1}{16} \end{array}$	41/8	23/4 2116 216 23/8	3 "" "" "" "" "" "" "" "" "" "" "" "" ""	13/8 1.7/15 1.7/15 1.7/15 1.7/15 13/4



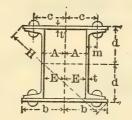
#### SERIES A.

Depth	Weight	Size of	Plates.							*	
Channel and Section	per Foot.	Width.	Thick- ness.	t	b	d	H	C	Œ	A	m
No.	Pounds.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
10" c33	15.0 20.0 25.0 30.0 35.0 20.5 25.0 30.0 35.0 40.0	12	14040400400400400 1400400400400400400	.24 .38 .53 .68 .82 .28 .39 .51 .64 .76	6	55555555555555555555555555555555555555	155, 16, 16, 16, 16, 16, 16, 16, 16, 16, 16	41/2 "" "" "" "" "" "" "" "" "" "" "" "" ""	3. 2.7/8 2.7/8 2.7/8 2.7/8 3.7/8 3.7/8 3.7/8 3.7/8 3.7/8 3.7/8 3.7/8	31/4 · · · · · · · · · · · · · · · · · · ·	1;/2 1;/8 1;/4 1;15 2;16 1;/6 2;16 1;/8 2;/4
15″ C53	35.0 40.0 45.0 50.0 55.0	17	3/3/4/0/4/0/4/0/4/0/4/0/4/0/4/0/4/0/4/0/	.40 .43 .52 .62 .72 .82	81/ <sub>2</sub>	77/8 144 177/8 177	23146 3646 31446 3166 316	63/4	47/8 41/3 43/4 45/8 40/16 47/6	51/4	1.78 1.156 2 2.18 2.14 2.14 2.14



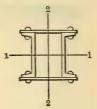
#### SERIES B.

Depth	Weight	Size of	Plates.								-
of Channel and Section	per Foot.	Width.	Thick- ness. t'	t	ь	d	н	c	E	<b>A</b>	m
No.	Pounds.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
6" C17	8 10.5 13.0 15.5	66	1/4/8/4/8/4/8/4/8	.20 .32 .44 .56	41/2	31/4/8/44/8/14/8/14/8/35/8/35/8/35/8/35/8/35/8/35/8/35/8/3	$\begin{array}{c} 11\frac{1}{8} \\ 11\frac{9}{16} \\ 11\frac{1}{8} \\ 11\frac{9}{16} \\ 11\frac{1}{8} \\ 11\frac{9}{16} \\ 11\frac{1}{8} \\ 11\frac{9}{16} \end{array}$	33/8	2 16 2 16 2 16 1 16 1 16 1 16 1 16 1 16	21/2	$ \begin{array}{c} 1, \frac{1}{16} \\ 1, \frac{3}{16} \\ 1, \frac{5}{16} \\ 1, \frac{5}{16} \\ 1, \frac{7}{16} \end{array} $
7" C21	9.75 12.25 14.75 17.25 19.75	11	1-5-1-6-1-6-1-5-1-5-8	.21 .32 .42 .53 .63	5 <sup>1</sup> / <sub>2</sub>	33/4 41/8 33/4 41/8 41/8 41/8 41/8 41/8	$\begin{array}{c} 13^{\frac{5}{16}}_{13}^{5$	41/4	3 16 2 15 2 16 2 13 2 14 2 14 2 14 2 18	31/4    	$   \begin{array}{c}     1_{\frac{3}{1}6} \\     1_{\frac{5}{1}6} \\     1_{\frac{7}{1}6} \\     1_{\frac{7}{1}6} \\     1_{\frac{1}{2}2} \\     1_{\frac{5}{8}} \\   \end{array} $
8" C25	11.25 13.75 16.25 18.75 21.25	12	145/8/47/8/47/8/47/8/47/8	.22 .31 .40 .49 .58	66	41,57,47,87,47,47,47,47,47,47,47,47,47,47,47,47,47	14 1 1 2 1 6 2 1 6 2 1 6 1 1 1 1 1 1 1 1 1	45/8	3,16 3,16 3,16 3,14 3,18 3,18 3,16	35/8	1 <sup>1</sup> / <sub>4</sub> 1 <sup>5</sup> / <sub>1</sub> 6 1 <sup>3</sup> / <sub>8</sub> 1 <sup>1</sup> / <sub>2</sub> 1 <sup>1</sup> / <sub>1</sub> 6
9" C29	13,25 15,00 20,00 25,00	13	1/4/8/4/8/1/4/8/1/4/8	.23 .29 .45 .61	61/2	43/45 51/8 43/45 51/8 43/4 51/8 51/8	16 <sup>1</sup> / <sub>8</sub> , 16 <sup>1</sup> / <sub>16</sub> , 16 <sup>1</sup> / <sub>8</sub> , 16 <sup>1</sup> / <sub>16</sub> , 16 <sup>1</sup> / <sub>8</sub> , 16 <sup>1</sup> / <sub>16</sub> , 16 <sup>1</sup> / <sub>8</sub> , 16 <sup>1</sup> / <sub>16</sub>	5½8   	3 <sup>3</sup> / <sub>4</sub> 3 <sup>1</sup> / <sub>16</sub> 3 <sup>1</sup> / <sub>16</sub> 3 <sup>3</sup> / <sub>8</sub>	4 "" "" "" "" "" "" "" "" "" "" "" "" ""	13/8 17/6 19/6 13/4

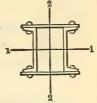


#### SERIES B.

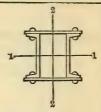
Depth		Size of	Plates.								
of Channel and Section	Weight per Foot.	Width.	Thick-ness.	t	b	d	н	C	E	A	m
No.	Pounds.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
10" C33 12" C41	15.0 20.0 25.0 30.0 35.0 20.5 25.0 35.0 40.0 35.0 40.0	15	1/5/1/6/4/6/4/6/4/6/4/6/4/6/4/6/4/6/4/6/4/6	.24 .38 .53 .68 .82 .28 .39 .51 .64 .76 .40 .43 .52	88 66 66 66 66 66 66 66 66 66 66 66 66 6	1458448044804480458 1458480480480488 7878787878	1884-54-54-54-54-54-54-54-54-54-554-555-55-	65/8	41/2 43/8 41/4 41/6 31/6 43/4 41/2 43/8 63/8 61/4 61/4	43/4 51/8	1½ 1½ 1½ 1½ 1½ 1¼ 1¼ 1¼ 1¼ 1¼ 1¼ 1¼ 1¼ 1¼ 1¼ 1¼ 1¼ 1¼
C53	45.0 50.0 55.0	66	3/3/4/0/4/0/4/0/4/0/4/0/4/0/4/0/4/0/4/0/	.62	66	7/8/4/8/4/8/4/8/4/8/7/14/8/4/8/4/8/4/8/4/8/4/8/4/8/4/8/4/8/4/	765676567656765676565656565656565656565	66	6½8 6½6 5½6	66 66 66 66	2½8 2¼4 2½4 2,5



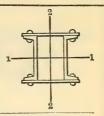
			٤	SER	IE:	5 A	-		4	SEF	RIE:	5 B	-
Depth of	Weight		late.	Axis	1-1.	Axis	2-2.		late.	Axis	1-1.	Axis	2-2.
Channel and Section Num- ber.	per Foot.	Width of Plate.	Thickness of Plate.	Mo- ment of Inertia.	Section Mod- ulus.	Mo- ment of Inertia.	Section Mod- ulus.	Width of Plate.	Thickness of Plate.	Mo- ment of Inertia.	Section Mod- ulus.	Mo- ment of Inertia.	Section Mod- ulus.
	Lbs.	Ins.	In.	Ins.4	Ins.3	Ins.4	Ins.3	Ins.	In.	Ins.4	Ins,3	Ins.4	Ins.3
6'' C 17	8.00	8	1/4 5 16 3/8 7 16 1/2 9 16 5/8	65.1 75.9 87.0 98.6 110.7 123.1 136.1	20.0 22 9 25 8 28.7 31.6 34 6 37.5	48.4 53.7 59.0 64.4 69.7 75.0 80.4	12.1 13.4 14.8 16.1 17.4 18.8 20.1	9	1/4/5/16/3/8/7/16/29/16/8	70.0 82 1 94.7 107.8 121.3 135.3 149.8	21.5 24.8 28.1 31.4 34.6 38.0 41.3	69.6 77.2 84.8 92.4 100.0 107.6 115.2	15.5 17.2 18.9 20.5 22.2 23.9 25.6
6'' C 17	10.50	8	1/4 5 16 3/8 7 16 1/2 9 16 5/8	69.3 80.1 91 2 102 8 114.9 127.3 140.3	21.3 24.2 27.0 29.9 32.8 35.7 38.7	52.5 57.8 63.1 68.5 73.8 79.1 84.5	13.1 14.5 15.8 17.1 18.5 19.8 21.1	9	1/4 563/8 761/29/6 5/8	74 2 86.3 98.9 112 0 125.5 139.5 154.0	22.8 26.1 29.3 32.6 35.8 39.2 42.5	76 5 84 1 91.7 99 3 106.9 114.5 122 1	17.0 18.7 20.4 22.1 23.8 25.4 27.1
6" C 17	13.00	8 66 66 66	1/4 5 16 3/8 7 16 1/2 9 16 5/8	73.7 84.5 95.6 107.2 119.3 131.7 144.7	22.7 25.5 28.3 31.2 34.1 37.0 39.9	56.5 61.9 67.2 72.5 77.9 83.2 88.5	14.1 15.5 16.8 18.1 19.5 20.8 22.1	9	1/4 5 16 3/8 7 16 1/2 9 16 5/8	78.6 90.7 103.3 116.4 129.9 143.9 158.4	24.2 27.4 30.6 33.9 37.1 40.4 43.7	83.4 91.0 98.6 106.2 113 7 121.3 128.9	18.5 20.2 21.9 23.6 25.3 27.0 28.7
6" C 17	15.50	8 66 66 66	1/4 5/6/3/8 7/6/1/2 9/16/8	78.1 88.9 100.0 111.6 123.7 136.1 149.1	24.0 26.8 29.6 32.5 35.3 38.2 41.1	60.0 65.4 70.7 76.0 81.4 86 7 92.0	15.0 16.3 17.7 19.0 20.3 21.7 23.0	9 ""	1/4 5 16 3/8 7 6 1/2 9 16 5/8	83.0 95.1 107.7 120.8 134.3 148.3 162.8	25.5 28.7 31.9 35.1 38.4 41.6 44.9	89.5 97.1 104.7 112.3 119.9 127.4 135.0	19.9 21.6 23.3 25.0 26.6 28.3 30.0



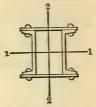
	1	1	1	SEF	HE:	SA		1		SEI	3100	SB	
Depth		te,			1-1.		2-2.	je.			1-1.		2-2.
of Channel and Section Num-	Weight per Foot.	Width of Plate,	Thickness Plate.	Mo- ment of Inertia.	Section Mod- ulus.	Mo- ment of Inertia.	Section Mod- ulus.	Width of Plate.	Thickness Plate.	Mo- ment of Inertia.	Section Mod- ulus.	Mo- ment of Inertia.	Section Mod- ulus.
ber.	Lbs.	Ins.	In.	Ins.4	Ins.3	Ins.4	Ins.3	Ins.	In.	Ins.4	Ins.3	Ins.4	Ins.3
7" C 21	9.75	9	1/4 5/6 3/8 7/6 1/2 9/6 5/8 1/3 4	101.4 117.4 134.1 151.3 169.0 187.2 206.2 225.6 245.5	27.0 30.8 34.6 38.4 42.2 46.1 50.0 53.9 57.8	70.6 78.1 85.8 93.4 101.0 108.5 116.1 123.8 131.3	15.7 17.4 19.1 20.8 22.4 24.1 25.8 27.5 29.2	111	1/4 563/8 76/29 15/8 11/3/4	114.5 134.2 154.5 175.5 197.1 219.5 242.5 266.3 290.7	30.5 35.2 39.9 44.6 49.3 54.0 58.8 63.6 68.4	130.9 144.7 158.6 172.5 186.3 200.2 214.1 227.9 241.8	23.8 26.3 28.8 31.4 33.9 36.4 38.9 41.4 44.0
c 21	12.25	9 44 44 44 44 44 44 44 44 44 44 44 44 44	1/4 5/6/8 7/6/29/6/81/6/3/4	107.6 123.6 140.3 157.5 175.2 193.4 212.4 231.8 251.7	28.7 32.4 36.2 40.0 43.8 47.6 51.5 55.4 59.2	76.3 83.9 91.5 99.1 106.7 114.3 121.9 129.5 137.1	17.0 18.6 20.3 22.0 23.7 25.4 27.1 28.8 30.5	11	1/4 5 6 8 7 6 8 1	120.7 140.4 160.7 181.7 203.3 225.7 248.7 272.5 296.9	32.2 36.8 41.5 46.1 50.8 55.6 60.3 65.1 69.9	144.0 157.9 171.8 185.6 199.5 213.4 227.2 241.1 255.0	26.2 28.7 31.2 33.8 36.3 38.8 41.3 43.8 46.4
7'' C 21	14.75	66 66 66 66 66 66 66 66 66 66 66 66 66	1/456/8/76/296/816/4	113.6 129.6 146.3 163.5 181.2 199.4 218.4 237.8 257.7	30.3 34.0 37.7 41.5 45.3 49.1 53.0 56.8 60.6	81.5 89.1 96.7 104.3 111.9 119.5 127.1 134.7 142.3	18.1 19.8 21.5 23.2 24.9 26.5 28.2 29.9 31.6	11	1/4 5 16 3/8 7 6 1/2 9 16 8/4	126.7 146.4 166.7 187.7 209.3 231.7 254.7 278.5 302.9	33.8 38.4 43.0 47.7 52.3 57.0 61.8 66.5 71.3	156.3 170.1 184.0 197.8 211.7 225.6 239.4 253.3 267.2	28.4 30.9 33.5 36.0 38.5 41.0 43.5 46.1 48.6
7'' C 21	17.25	9	1/4 5/6/8 7/6/29/6/81/6/4	119.6 135.6 152.3 169.5 187.2 205.4 224.4 243.8 263.7	31.9 35.6 39.3 43.1 46.8 50.6 54.4 58.2 62.1	85.9 93.4 101.1 108.7 116.2 123.8 131.4 139.1 146.6	19.1 20.8 22.5 24.2 25.8 27.5 29.2 30.9 32.6	11	1/4 5 6 3/8 7 6 1/2 9 6 5/8 1 1 6/3 4	132.7 152.4 172.7 193.7 215.3 237.7 260.7 284.5 308.9	35.4 40.0 44.6 49.2 53.8 58.5 63.2 67.9 72.7	167.1 181.0 194.9 208.7 222.6 236.5 250.3 264.2 278.1	30.4 32.9 35.4 38.0 40.5 43.0 45.5 48.0 50.6
c 21	19.75	66 66 66 66 66 66 66 66 66 66 66 66 66	1/4 5/6 3/8 7/6 1/2 9/6 1/8 1/8 1/8 1/8 1/8 1/8 1/8 1/8	125.6 141.6 158.3 175.5 193.2 211.4 230.4 249.8 269.7	33.5 37.1 40.8 44.6 48.3 52.0 55.9 59.7 63.5	90.3 97.9 105.5 113.1 120.7 128.3 135.9 143.5 151.1	20.1 21.8 23.4 25.1 26.8 28.5 30 2 31.9 33.6	11	1/4:56 13/8 76 11/29 15/8 16/4	138.7 158.4 178.7 199.7 221.3 243.7 266.7 290.5 314.9	37.0 41.5 46.1 50.7 55.3 60.0 64.7 69.4 74.1	178.2 192.0 205.9 219.7 233.6 247.5 261.3 275.2 289.1	32.4 34.9 37.4 40.0 42.5 45.0 47.5 50.0 52.6



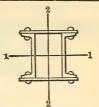
		1	1	EF	IE	SA		1	5	SEF	RIE	S B	_
Depth	Wainh	ate.	ate.	Axis	1-1.	Axis	2-2.	ate.	ate.	Axis	1-1.	Axis	2-2.
of Channel and Section Num-	Weight per Foot.	Width of Plate.	Thickness Plate.	Mo- ment of Inertia.	Section Mod- ulus.	Mo- ment of Inertia.	Section Mod- ulus.	Width of Plate.	Thickness Plate.	Mo- ment of Inertia.	Section Mod- ulus.	Mo- ment of Inertia.	Section Mod- ulus.
ber.	Lbs.	Ins.	In.	Ins.4	Ins.3	Ins.4	Ins.3	Ins.	In.	Ins.4	Ins.3	Ins.4	Ins.3
8′′ C 25	11.25	10	1/456/876/296/816/4	149.7 172.6 196.2 220.5 245.4 271.1 297.5 324.6 352.4	35.2 40.0 44.9 49.7 54.5 59.4 64.3 69.2 74.2	104.0 114.4 124.9 135.3 145.7 156.1 166.5 176.9 187.4	20.8 22.9 25.0 27.1 29.1 31.2 33.3 35.4 37.5	12 "" "" "" "" "" "" "" "" "" "" "" "" ""	1/4 5/6/3/8 7/6/29/6/8 1/6/4	166.7 194.2 222.5 251.7 281.6 312.4 344.1 376.6 410.0	39.2 45.0 50.9 56.7 62.6 68.5 74.4 80.3 86.3	181.1 199.1 217.1 235.1 253.1 271.1 289.1 307.1 325.1	30.2 33.2 36.2 39.2 42.2 45.2 48.2 51.2 54.2
8″ C 25	13.75	10	1/4 5 16/8 7 16/2 9 16/8 116/4	157.1 180.0 203.6 227.9 252.8 278.5 304.9 332.0 359.8	37.0 41.7 46.5 51.4 56.2 61.0 65.9 70.8 75.8	111.6 122.0 132.4 142.8 153.2 163.6 174.1 184.5 194.9	22.3 24.4 26.5 28.6 30.6 32.7 34.8 36 9 39.0	12	1/4 5 16/8 7 16/2 9 16/8 116/4	174.1 201.6 229.9 259.1 289.0 319.8 351.5 384.0 417.4	41.0 46.8 52.6 58.4 64.2 70.1 76 0 81.9 87.9	196.4 214.4 232.4 250.4 268.4 286.4 304.4 322.4 340.4	32.7 35.7 38.7 41.7 44.7 47.7 50.7 53.7 56.7
8'' C 25	16 25	10	1/4 5 6 76 12 9 6 15/8 116/4	164.9 187.8 211.4 235.7 260.6 286.3 312.7 339.8 367.6	38.8 43.6 48.3 53.1 57.9 62.8 67.6 72.5 77.4	119.4 129.8 140.2 150.6 161.0 171.5 181.9 192.3 202.7	23.9 26.0 28.0 30 1 32.2 34.3 36.4 38.5 40.5	12	1/4 5/6/8 7/6/2 9/6/81/6/4	181.9 209.4 237.7 266.9 296.8 327.6 359.3 391.8 425.2	42.8 48.6 54.3 60.1 66.0 71.8 77.7 83.6 89.5	212.5 230.5 248.5 266.5 284.5 302.5 320.5 338.5 356.5	35.4 38.4 41.4 44.4 47.4 50.4 53.4 56.4 59.4
8" C 25	18.75	10	1/4 56/8 716/2 915/816/4	172.7 195.6 219.2 243.5 268.4 294.1 320.5 347.6 375.4	40.6 45.4 50.1 54.9 59.7 64.5 69.3 74.2 79.0	126.3 136.7 147.2 157.6 168.0 178.4 188.8 199.2 209.7	25.3 27.4 29.4 31.5 33.6 35.7 37.8 39 9 41.9	12	1/4 563/8 761/2 96/8 16/4	189.7 217.2 245.5 274.7 304.6 335.4 367.1 399.6 433.0	44.6 50.4 56.1 61.9 67.7 73.5 79.4 85.2 91.2	227.3 245.3 263.3 281.3 299.3 317.3 335.3 353.3 371.3	37.9 40.9 43.9 46.9 49.9 52.9 55.9 58.9 61.9
8'' C 25	21.25	10	1/4 563/8 76/2 95/816/4	180.7 203.6 227.2 251.5 276.4 302.1 328.5 355.6 383.4	42.5 47.2 51.9 56.7 61.4 66.2 71.0 75.9 80.7	133.0 143.4 153.8 164.2 174.6 185.0 195.5 205.9 216.3	26.6 28.7 30.8 32.8 34.9 37.0 39.1 41.2 43.3	12	1/4 5 16 3/8 76 1/2 96 5/8 116 3/4	197.7 225.2 253.5 282.7 312.6 343.4 375.1 407.6 441.0	46.5 52.2 58.0 63.7 69.5 75.3 81.1 87.0 92.8	241 7 259.7 277.7 295.7 313.7 349.7 367.7 385.7	40.3 43.3 46.3 49.3 52.3 55.3 58.3 61.3 64.3



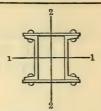
			5	eer	le:	5 A	-			EF	HE	s B	-
Depth of	Weight		Plate.	Axis	1-1.	Axis	2-2,		ate.	Axis	1 1.	Axis	2-2.
Channel and Section Num- ber.	per Foot.	Width of Plate.	Thickness of Pl	Mo- ment of Inertia.	Section Mod- ulus.	Mo- ment of Inertia.	Section Mod- ulus.	Width of Plate.	Thickness of Plate.	Mo- ment of Inertia.	Section Mod- ulus.	Mo- ment of Inertia.	Section Mod- ulus.
	Lbs.	Ins.	In.	Ins.4	Ins.3	Ins.4	Ins.3	Ins.	In.	Ins.4	Ins.3	Ins.4	Ins.3
9″ C 29	13.25	11 66 66 66 66 66 66	1/4 56 3/8 76 1/2 96 5/8 116 3/4	212.3 243.8 276.0 309.0 343.0 377.9 413.5 449.9 487.5	44.7 50.7 56.6 62.6 68.6 74.7 80.7 86.7 92.9	147.9 161.8 175.6 189.4 203.3 217.3 231.1 244.9 258.8	26.9 29.4 31.9 34.4 37.0 39.5 42.0 44.5 47.1	13	1/4 5 16 2/8 16 1/2 9 16 5/8 116 3/4	233.7 270.8 308.9 348.1 388.2 429.3 471.5 514.7 558.9	49.2 56.3 63.4 70.5 77.6 84.8 92.0 99.2 106.5	244.3 267.2 290.1 313.0 335.9 358.8 381.6 404.5 427.4	37.6 41.1 44.6 48.2 51.7 55.2 58.7 62.2 65.8
9′′ C 29	15.00	11	1/4 5/6/3/8 7/6/2 9/6/5/8 11/6/4	219.5 251.0 283.2 316.2 350.2 385.1 420.7 457.1 494.7	46.2 52.2 58.1 64.0 70.0 76.1 82.1 88.1 94.2	155.4 169.3 183.1 197.0 210.9 224.8 238.6 252.4 266.3	28.3 30.8 33.3 35.8 38.3 40.9 43.4 45.9 48.4	13	1/4 5/6 3/8 7/6 1/2 9/16 5/8 11/6 3/4	240.9 278.0 316.1 355.3 395.4 436.5 478.7 521.9 566.1	50 7 57.8 64.9 72.0 79.1 86.2 93.4 100.6 107.8	258.5 281.4 304.3 327.2 350.1 373.0 395.8 418 7 441.6	39.8 43.3 46.8 50.3 53.9 57.4 60.9 64.4 67.9
9″ C 29	20.00	11	1/4 5/6 7/6 1/2 9/6 5/8 1/16 3/4	239.3 270.8 303.0 336.0 370.0 404.9 440.5 476.9 514.5	50.4 56.3 62.2 68.0 74.0 80.0 86.0 91.9 98.0	175.6 189.5 203.3 217.1 231.0 244.9 258.8 272.6 286.5	31.9 34.5 37.0 39.5 42.0 44.5 47.1 49.6 52.1	13	$\begin{array}{c} 1/4 \\ \frac{5}{16} \\ \frac{3}{8} \\ \frac{7}{16} \\ \frac{9}{16} \\ \frac{1}{16} \\ \frac{3}{4} \\ \end{array}$	260.7 297.8 335.9 375.1 415.2 456.3 498.5 541.7 585.9	54.9 61.9 68.9 76.0 83.0 90.1 97.3 104.4 111.6	297.0 319.9 342.8 365.7 388.6 411.5 434.3 457.2 480.1	45.7 49 2 52.7 56 3 59.8 63.3 66.8 70.3 73.9
9″ C 29	25.00	11	1/4 5 16 3/8 7 16 1/2 9 16 5/8 116 3/4	259.1 290.6 322.8 355.8 389.8 424.7 460.3 496.7 534.3	54.5 60.4 66 2 72.1 78.0 83.9 89.8 95.8 101.8	194.6 208.5 222.3 236.1 250.1 264.0 277.8 291.6 305.5	35.4 37.9 40 4 42.9 45.5 48.0 50.5 53.0 55.6	13	1/4 5/6/3/8 7/6/1/29 16/8 1/6/4 1/6/4	280.5 317 6 355.7 394.9 435.0 476.1 518.3 561.5 605.7	59.1 66.0 73.0 80.0 87.0 94.1 101.1 108.2 115.4	333.9 356.8 379.7 402.5 425.4 448.3 471.2 494.1 517.0	51.4 54.9 58.4 61.9 65.5 69.0 72.5 76.0 79.5



			5	SID R	TE	5 A			ş	FF	RIE	SB	
Donth		- e	_	Axis		Axis	2-2.	.0.		Axis		Axis	
Depth of Channel and Section Num-	Weight per Foot.	Width of Plate.	Thickness Plate.	Mo- ment of Inertia.	Section Mod- ulus.	Mo- ment of Inertia.	Section Mod- ulus.	Width of Plate.	Thickness Plate.	Mo- ment of Inertia.	Section Mod- ulus.	Mo- ment of Inertia.	Section Mod- ulus.
ber.	Lbs.	Ins.	In.	Ins.4	Ins.3	Ins.4	Ins.3	Ins.	In.	Ins.4	Ins.3	Ins.4	Ins.3
10" C 33	15.0	12 "" "" "" "" "" "" "" "" "" "" "" "" ""	1/4 5/6/3/8 7/6/2 9/6/8 1/6/4	291.4 333.3 376.1 419.9 464.8 510.7 557.6 605.6 654.7	55.5 62.7 70.0 77.2 84.5 91.8 99.1 106.5 113.9	195.4 213.4 231.4 249.4 267.4 285.4 303.4 321.4 339.4	32.6 35.6 38.6 41.6 44.6 47.6 50.6 53.6 56.6	15	1/4 5/6 3/8 7/6 1/2 9/6 5/8 1/6 4	330.8 383 3 436.7 491.6 547.6 605.1 663.6 723.7 784.9	63.0 72.1 81.2 90.4 99.6 108.8 118.0 127.3 136.5	381.8 417.0 452.1 487.3 522.4 557.6 592.7 627.9 663.1	50.9 55.6 60.3 65.0 69.7 74.3 79.0 83.7 88.4
10″ C 33	20.0	12	1/4 56/8 76/1/2 96/8 16/4	315.0 356.9 399.7 443.5 488.4 534.3 581.2 629.2 678.3	60.0 67.2 74.4 81.6 88.8 96.1 103.3 110.6 118.0	220.1 238 1 256.1 274.1 292.1 310.1 328.1 346.1 364.1	36 7 39.7 42.7 45.7 48.7 51.7 54.7 57.7 60.7	15	1/4 5/6 3/8 7/6 1/2 9/6 16/8 16/3/4	354.4 406.9 460.3 515.2 571.2 628.7 687.2 747.3 808.5	67.5 76.6 85.6 94.8 103.9 113.0 122.2 131.4 140.6	438.0 473.1 508.3 543.4 578.6 613.8 648.9 684.1 719.2	58.4 63.1 67.8 72.5 77.2 81.8 86.5 91.2 95.9
10″ c 33	25 0	12	1/4 5/6/3/8 7/6/2 9/6/81/6/4	339.6 381.5 424.3 468.1 513.0 558.9 605.8 653.8 702.9	64.7 71.8 78.9 86.1 93.3 100.5 107.7 115.0 122.2	242.8 260.8 278.8 296.8 314.8 332.8 350.8 368.8 386.8	40.5 43.5 46.5 49.5 52.5 55.5 58.5 61.5 64.5	15	1/4 5/16/3/8 7/16/1/29/16/5/81/6/3/4	379.0 431.5 484.9 539.8 595.8 653.3 711.8 771.9 833.1	72.2 81.2 90.2 99.3 108.3 117.4 126.5 135.7 144.9	491.8 526.9 562.1 597.3 632.4 667.6 702.7 737.9 773.0	65.6 70.3 75.0 79.6 84.3 89.0 93.7 98.4 103.1
10″ C 33	30.0	12	1/4 563/8 761/2 965/8 1163/4	364.0 405.9 448.7 492.5 537.4 583.3 630.2 678.2 727.3	69.3 76.4 83.5 90.6 97.7 104.9 112.0 119.3 126.5	262.9 280.9 298.9 316.9 334.9 352.9 370.9 388.9 406.9	43.8 46.8 49.8 52.8 55.8 58.8 61.8 64.8	15	1/4 5/6 3/8 7/6 1/2 9/6 5/8 1/16 1/2 1/6 1/6 1/6 1/6 1/6 1/6 1/6 1/6	403.4 455.9 509.3 564.2 620.2 677.7 736.2 796.3 857.5	76.8 85.8 94.8 103.8 112.8 121.8 130.9 140.0 149.1	541.6 576.8 611.9 647.1 682.2 717.4 752.5 787.7 822.9	72.2 76.9 81.6 86.3 91.0 95.7 100.3 105.0 109.7
10" C 33	35.0	12	1/4 5 16 3/8 7 16 1/2 9 16/8 116/3/4	388.6 430.5 473.3 517.1 562.0 607.9 654.8 702.8 751.9	74.0 81.0 88.1 95.1 102.2 109.3 116.4 123.6 130.8	281.7 299.7 317.7 335.7 353.7 371.7 389.7 407.7 425.7	46.9 49.9 52.9 55.9 58.9 61.9 64.9 70.9	15	1/4 5 6 8 7 6 1/2 9 16 5/8 1 6 5/8 1 6 3/4	428.0 480.5 533.9 588.8 644.8 702.3 760.8 820.9 882.1	81.5 90.4 99.3 108.3 117.2 126.3 135.3 144.3 153.4	589.2 624.4 659.5 694.7 729.8 765.0 800.2 835.3 870.5	78.6 83.3 87.9 92.6 97.3 102.0 106.7 111.4 116.1

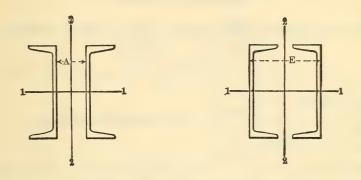


					and transit	emai 400						2	
				EF						SEI			
Depth of Channel and Section Num-	Weight per Foot.	Width of Plate.	Thickness Plate.	Mo- ment of Inertia.	Section Mod- ulus.	Mo- ment of Inertia.	Section Mod- ulus.	Width of Plate.	Thickness Plate.	Mo- ment of Inertia.	Section Mod- ulus.	Mo- ment of Inertia.	Section Mod- ulus.
ber.	Lbs.	Ins.	In.	Ins.4	Ins.3	Ins.4	Ins.3	Ins.	In.	Ins.4	Ins.3	Ins.4	Ins.3
12" C 41	20.5	14	1/4 56 3/8 76 11/2 96 5/8 11/3/4	518.9 587.9 658.3 730.1 803 4 878.0 954.1 1031.6 1110.6	83.0 93.1 103.3 113.4 123.6 133.8 144.0 154.3 164.5	371.3 399.9 428.4 457.0 485.6 514.2 542.8 571.4 599.9	53.0 57.1 61.2 65.3 69.4 73.5 77.5 81.6 85.7	16	1/4 <sup>5</sup> 13/8 <sup>76</sup> /2 <sup>9</sup> 15/8 <sup>16</sup> /3/4	556.4 635.3 715.8 797.8 881.5 966.9 1053.8 1142.4 1232.7	89.0 100.6 112.3 123.9 135.6 147.3 159.1 170.8 182.6	549.3 592.0 634.6 677.3 720.0 762.6 805.3 848.0 890.6	68.7 74.0 79.3 84.7 90.0 95.3 100.7 106.0 111.3
12″ C <b>4</b> 1	25.0	14	1/4 5 6 8 7 6 1/2 9 6 8 1 7 8 1 7 8 1 8 8 1	550.7 619.7 690.1 761.9 835.2 909.8 985.9 1063.4 1142.4	88.1 98.2 108.3 118.4 128.5 138.6 148.8 159.0 169.3	409.9 438.5 467.1 495.7 524.3 552.9 581.4 610.0 638.6	58.6 62.7 66.7 70.8 74.9 79.0 83.1 87.2 91.2	16	1/4 5/6 3/8 7/6 1/2 9/6 5/8 11/3/4	588.2 667.1 747.6 829.6 913.3 998.7 1085.6 1174.2 1264.5	94.1 105.7 117.3 128.9 140.5 152.2 163.9 175.6 187.3	610.8 653.4 696.1 738.8 781.4 824.1 866.8 909.4 952.1	76.4 81.7 87.0 92.4 97.7 103.0 108.4 113.7 119.0
12" C 41	30.0	14	1/4 5 16 3/8 7 16/8 15/8 116/4	585.9 654.9 725.3 797.1 870.4 945.0 1021.1 1098.6 1177.6	93.7 103.7 113.8 123.8 133.9 144.0 154.1 164.3 174.5	450.2 478.8 507.3 535.9 564.5 593.1 621.7 650.3 678.8	64.3 68.4 72.5 76.6 80.6 84.7 88.8 92.9 97.0	16	1/4 56 3/8 76 12 96 15/8 118/4	623.4 702.3 782.8 864.8 948.5 1033.9 1120.8 1209.4 1299.7	99.7 111.3 122.8 134.3 145.9 157.5 169.2 180.9 192.6	675.7 718 3 761.0 803.7 846.3 889.0 931.6 974.3 1017.0	84.5 89.8 95.1 100.5 105.8 111.1 116.5 121.8 127.1
12'' C 41	35.0	14	1/4 5/6 3/8 7/6 1/2 9/6 5/8 11/6 3/4	621.3 690.3 760.7 832.5 905 8 980.4 1056.5 1134.0 1213.0	159.5 169.6 179.7	484.9 513.4 542.0 570.6 599.2 627.8 656.4 684.9 713.5	69.3 73.4 77.4 81.5 85.6 89.7 93.8 97.9 101.9	16	1/4 5 16 3/8 7 16 1/2 9 16 5/8 116 176 176 176 176 176 176 176	658.8 737.7 818 2 900.2 983.9 1069 3 1156.2 1244.8 1335.1	105.4 116.9 128.3 139.8 151.4 162.9 174.5 186.1 197.8	733.6 776.3 818.9 861.6 904.3 946.9 989.6 1032.3 1074.9	91.7 97.0 102.4 107.7 113 0 118.4 123.7 129.0 134.4
12" C 41	40.0	14	1/4 5 6 3/8 7 6 1/2 9 6 5/8 1 16 3/4	656.5 725.5 795.9 867.7 941.0 1015.6 1091.7 1169.2 1248.2	105.0 114.9 124.9 134.8 144.8 154.8 164.8 174.8 184.9	520.1 548.7 577.2 605.8 634.4 663.0 691.6 720.2 748.7	74.3 78.4 82.5 86.6 90.6 94.7 98.8 102.9 107.0	16	1/4:56 3/8 76 1/2 96 5/8 146 3/4	694.0 772.9 853.4 935.4 1019.1 1104.5 1191.4 1280.0 1370.3	111.0 122.4 133.9 145.3 156.8 168.3 179.8 191.4 203.0	792.1 834.8 877.4 920.1 962.8 1005.4 1048.1 1090.8 1133.4	99.0 104.3 109.7 115.0 120.3 125.7 131.0 136.3 141.7



		1	5	EF	103	S A	-	1	5	BEF	RIE	S B	
			1		1-1,		2-2.	-			3 1-1,		2-2.
Depth of Channel and Section Number.	Weight per Foot	Width of Plate.	Thickness of Plate.	Mo- ment of Inertia.	Section Mod- ulus.	Mo- ment of Inertia.	Section Mod- ulus.	Width of Plate.	Thickness of Plate.	Mo- ment of Inertia.	Section Mod- ulus.	Mo- ment of Inertia.	Section Mod- ulus.
	Lbs.	Ins.	In.	Ins.4	Ins.3	Ins.4	Ins.3	Ins.	In.	Ins.4	Ins.3	Ins.4	Ins.3
15″ C 53	33.0	17	3/8 716 1/2 916 5/8 116 3/4	1378.9 1512.0 1646.6 1783.4 1922.9 2064.6 2207.8	175.1 190.5 205 8 221 2 236.7 252.2 267.6	953.4 1004.7 1055.7 1106.8 1158.1 1209.4 1260.4	112.2 118.2 124.2 130.2 136.2 142.3 148.3	20	3/8/7/6/29/6/8/16/4 1/29/16/8/16/4	1511.8 1668.1 1826.9 1988.1 2151.9 2318.2 2487.1	192 0 210.2 228 4 246.6 264.9 283.1 301.5	1525.9 1609.2 1692.5 1775.9 1859.2 1942.5 2025.9	152.6 160.9 169.3 177.6 185.9 194.3 202.6
15″ C 53	35.0	17	3/8 7/6/2 16/2 16/8 11/6/4	1393.5 1526.6	177.0 192.3 207.7 223.0 238.5 254.0 269.4	971.7 1023.0 1074.1 1125.1 1176.4 1227.7 1278.8	114.3 120.4 126.4 132.4 138.4 144.4 150.4	20	3/8 16/2 16/8 16/8 16/8 16/8	1526.4	193.8 212.0 230.2 248.4	1557.3 1640.7 1724.0 1807.3 1890.7 1974.0 2057.3	155.7 164.1 172.4 180.7 189.1 197.4 205.7
15″ C 53	40.0	17	3/8 7 16/2 9 16/8 11/8 4		184.0 199.3 214.6 229.9 245.3 260.7 276.1	1039.9 1091.2 1142.3 1193.3 1244.6 1295.9 1347.0	122.3 128.4 134.4 140.4 146.4 152.5 158.5	20	3/8 7/6 1/2 9/6 5/8 1/6	1581.6 1737.9 1896.7 2057.9 2221.7 2388.0 2556.9	255.3 273.4 291.7	1674.6 1757.9 1841.2 1924.6 2007.9 2091.2 2174.6	167.5 175.8 184.1 192.5 200.8 209.1 217.5
15″ C 53	45.0	17	3/8 7/16/1/2 9/16/5/81/16/3/4	1503.9 1637.0 1771.6 1908.4 2047.9 2189.6 2332.8	191.0 206.2 221.5 236.7 252.0 267.4 282.8	1105.4 1156.8 1207.9 1258.9 1310.2 1361.5 1412.6	130.1 136.1 142.1 148.1 154.2 160.2 166.2	20	3/8 7 16 1/2 9	1636.8 1793.1 1951.9 2113.1 2276 9 2443.2 2612.1	207.9 225.9 244.0 262.1 280.2 298.4	1788.6 1871.9 1955.3 2038.6 2121.9 2205.3 2288.6	178.9 187.2 195.5 203.9 212.2 220.5 228.9
15″ C 53	50.0	17	3/8/76/296/8/116/4	1559.1 1692.2 1826.8 1963.6 2103.1 2244.8 2388.0	198.0 213.2 228.4 243.5 258.8 274.2 289.5	1165.3 1216.6 1267.7 1318.7 1370.0 1421.3 1472.4	137.1 143.1 149.1 155.1 161.2 167.2 173.2	20	3/8 7/6 1/2 9/6 5/8 1/6	1692.0 1848.3 2007.1 2168.3 2332.1 2498.4 2667.3	214.9 232.9 250.9 268.9 287.0 305.2	1894.9 1978.2 2061.5 2144.9 2228.2 2311.5 2394.9	189.5 197.8 206.2 214.5 222.8 231.2 239.5
15'' C 53	55.0	17	3/8 7/6 1/2 9/6 5/8 11/6 13/4	1614.1 1747.2 1881.8 2018.6 2158.1 2299.8 2443.0	205.0 220.1 235.2 250.4 265.6 280.9	1223.4 1274.7 1325.7 1376.8 1428.1 1479.4 1530.4	143.9 150.0 156.0 162.0 168.0 174.0 180.1	20	3/8/16/29/6/81/6	1747.0 1903.3 2062.1 2223.3 2387.1 2553.4 2722.3	221.9 239.8 257.8 275.8 293.8 311.9	1998.8 2082.1 2165.5 2248.8 2332.1 2415 5	199.9 208.2 216.6 224.9 233.2 241.6 249.9

#### SPACING OF CHANNELS FOR EQUAL MOMENTS OF INERTIA ABOUT THE TWO REC-TANGULAR AXES 1-1 AND 2-2.



Section Num- ber.	Depth of Channel.	Weight per ft. of one Chan- nel.	Area of Section of one Chan- nel.	A	E	Section Num- ber.	Depth of Chan- nel.	Weight per ft. of one Chan- nel.	Area of Section of one Chan- pel.	A	Е
	Inches.	Pounds.	Sq. Ins.	Inches.	Inches.		Inches.	Pounds.	Sq. Ins.	Inches.	Inches.
C 5	3	5.00	1.19 1.47 1.76	1.17	2.93	C 25	8	18.75 21.25	5.51 6.25	4.37 4.22	6.65 6.58
C 9.	4 "	6.25	1.55 1.84 2.13	1.96	3.92 3.80 3.72	C 29 "	9 "	13.25 15.00 20.00 25.00	3.89 4.41 5.88 7.35	5.48 5.14	8.06 7.84 7.46 7.31
C 13	5	6.50 9.50 11.50	1.95 2.65 3.38	2.57	4.49	66	10	15.00 20.00 25.00 30.00	4.46 5.88 7.35 8.82	5.96 5.66	8.89 8.40 8.14 8.01
C 17	6	8.00 10.50 13.00 15.50	3.82	3.29 3.08	5.16	" C 41	12	35.00 20.50	10.29	5.18	7.94
C 21	7 "		2.85 3.60	4.21 4.00	6.41 6.12	" " "	66	25.00 30.00 35.00 40.00	7.35 8.82 10.29 11.76	7.35 7.06 6.83	10.07 9.78 9.59 9.48
66	66	17.25 19.75	5.07	3.65	5.85	C 53	15	33.00 35.00	10.29	9.42	12.67 12.58
C 25	8 "	11.25 13.75 16.25	4.04	4.72	6.96	66	66	40.00 45.00 50.00 55.00	13.24 14.71 16.18	8.92 8.72 8.53	12.08 11.92 11.81

Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 L)^2}{36000 r^2}}$ . Safety factor 4.

Depth of Beam and Section	Weight per Foot,	Area of Section.	Least Radius of Gyration.		L,e	engtl	h in	Fee	t.	
Number.	Pounds.	Sq. Ins.	Inches.	2	3	4	5	6	7	8
3" B5	5.5 6.5 7.5	1.63 1.91 2.21	.53 .52 .52	19 23 26	18 21 24	17 19 22	15 17 20	13 16 18	12 14 16	11 12 14
4" B9	7.5 8.5 9.5 10.5	2.21 2.50 2.79 3.09	.59 .58 .58 .57	26 30 33 37	25 28 31 35	23 26 29 32	21 24 27 29	20 22 24 27	18 20 22 24	16 18 20 22
5" B13	9.75 12.25 14.75	2.87 3.60 4.34	.65 .63 .63	35 43 52	33 41 50	31 39 47	29 36 43	27 33 40	24 30 36	22 27 33
6" B17	12.25 14.75 17.25	3.61 4.34 5.07	.72 .69 .68	44 52 61	42 51 59	40 48 56	38 45 52	35 42 48	33 39 44	30 35 41
7" B21	15.0 17.5 20.0	4.42 5.15 5.88	.78 .76 .74	54 63 71	52 61 69	50 58 66	47 55 62	45 52 58	42 48 54	39 45 50
8″ B25	18.00 20.25 22.75 25,25	5.33 5.96 6.69 7.43	.84 .82 .81 .80	65 73 82 91	63 71 79 88	61 68 76 84	58 65 72 80	55 61 69 76	52 58 65 71	49 54 60 66
9" B29	21.0 25.0 30.0 35.0	6.31 7.35 8.82 10.29	.90 .88 .85 .84	77 90 108 126	76 88 105 122	73 85 101 118	70 81 97 112	67 78 92 107	63 73 87 101	60 69 81 95
10" B33	25.0 30.0 35.0 40.0	7.37 8.82 10.2.) 11.76	.97 .93 .91 .90	91 108 126 144	89 106 123 141	86 103 119 136	83 99 115 131	80 94 110 125	76 90 104 118	73 85 98 112
12" B41	31.5 35.0 40.0	9.26 10.29 11.76	1.01 .99 .96	114 127 144	112 124 142	109 121 137	105 117 133	102 112 127	97 107 121	93 102 115

Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 L)^2}{36000 r^2}}$ . Safety factor 4.

		I.,	engt	h in	Fee	et.	ı		Weight per Foot.	Depth of Beam and Section
9	10	11	12	17	Pounds.	Number.				
9 11 13									5.5 6.5 7.5	3′′ B5
14 16 18 19	13 14 16 17								7.5 8.5 9.5 10.5	4′′ B9
20 25 30	18 22 27	17 20 24							9.75 12.25 14.75	5" B13
28 32 37	25 29 34	23 27 31	21 25 28						12.25 14.75 17.25	6" B17
36 41 46	33 38 43	31 35 39	28 32 36	26 30 33					15.0 $17.5$ $20.0$	7" B21
46 50 56 61	43 47 52 57	40 43 48 53	37 40 45 49	34 37 41 45	31 34 38 42				18.00 20.25 22.75 25.25	8" B25
56 65 76 88	53 60 71 82	49 57 66 76	46 53 61 71	43 49 57 66	40 46 53 61	37 43 49 56			21.0 25.0 30.0 35.0	9″ B29
68 80 92 105	65 75 87 98	61 71 81 92	57 66 76 86	54 62 71 80	50 58 66 74	47 54 62 69	44 50 57 65		25 0 30.0 35.0 40.0	10" B33
88 97 109	83 91 103	78 86 96	74 81 90	69 76 85	65 72 79	61 67 74	58 63 69	54 59 65	31.5 35.0 40.0	12" B41

Based on Gordon's Formula  $P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$ . Safety factor 4.

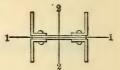
Depth of Beam and Section	Weight per Foot.	Area of Section.	Least Radius of Gyra- tion.			L,en	gth i	in F	eet.		
Number.	Pounds.	Sq. Ins.	Inches.	2	3	4	5	6	7	8	9
12" B105	40.0 45.0 50.0 55.0	11.84 13.24 14.71 16.18	1.08 1.06 1.05 1.04	146 163 181 199	144 160 178 196	140 156 174 191	136 152 168 185	132 146 163 178	127 141 156 171	121 135 149 163	116 128 142 155
15" B 53	42.0 45.0 50.0 55.0 60.0	12.48 13.24 14.71 16.18 17.65	1.08 1.07 1.04 1.03 1.01	154 163 181 199 217	151 160 178 196 213	148 157 174 191 207	144 152 168 185 201	139 147 162 178 194	133 142 156 171 185	128 135 149 163 177	122 129 141 155 167
15" B109	60.0 65.0 70.0 75.0 80.0	17.67 19.12 20.59 22.06 23.53	1.21 1.20 1.19 1.18 1.17	218 236 254 273 291	215 233 251 269 286	212 229 246 264 281	207 223 240 258 274	201 217 234 250 266	195 211 226 242 257	188 203 218 233 248	181 195 209 224 238
15" B113	80.0 85.0 90.0 95.0 100.0	23.57 25.00 26.47 27.94 29.41	1.32 1.32 1.32 1.31 1.31	292 309 328 346 364	289 306 324 342 360	284 302 319 336 354	279 295 313 330 348	273 289 306 322 339	265 281 297 314 330	256 272 288 304 320	249 264 279 293 309
18" B 65	55.0 60.0 65.0 70.0	15.93 17.65 19.12 20.59	1.15 1.13 1.11 1.09	197 218 236 254	194 214 232 250	190 210 227 244	185 205 221 237	180 198 214 230	173 191 206 221	166 184 198 212	160 176 189 202
20" B 73	65.0 70.0 75.0	19.08 20.59 22.06	1.21 1.19 1.17	236 254 273	233 251 268	229 246 264	223 240 257	217 234 250	210 226 241	203 218 233	196 209 223
20″ B121	80.0 85.0 90.0 95.0 100.0	23.73 25.00 26.47 27.94 29.41	1.39 1.37 1.36 1.35 1.34	294 309 328 346 364	291 307 325 343 361	287 302 320 337 355	282 297 314 331 349	276 290 307 324 340	270 283 300 315 332	261 275 290 307 321	254 266 282 296 312
24" B 89	80.0 85.0 90.0 95.0 100.0	23.32 25.00 26.47 27.94 29.41	1.36 1.33 1.51 1.30 1.28	289 309 328 346 364	286 306 324 342 360	282 302 319 336 354	276 295 313 330 347	271 289 305 322 338	264 281 297 313 328	256 273 288 303 317	248 264 278 293 307

Based on Gordon's Formula  $P = \frac{50\,000}{1 + \frac{(12\,\mathrm{L})^2}{36\,000\,\mathrm{r}^2}}$ . Safety factor 4.

			Weight per Foot.	Depth of Beam and Section							
10	11	12	13	14	15	16	17	18	19	Pounds.	Number.
110 122 135 148	105 116 128 140	99 110 121 132	94 103 114 124	88 98 108 117	83 92 101 111	79 87 96 104	75 82 90 98	70 77 85 92	• • •	40.0 45.0 50.0 55.0	12" B105
116 123 134 147 158	110 116 127 139 150	105 110 120 131 141	99 104 113 124 132	93 98 106 116 124	88 93 101 109 117	83 87 94 103 110	79 82 89 97 104	74 78 84 91 97		42.0 45.0 50.0 55.0 60.0	15" B 53
173 187 201 214 228	166 179 192 205 217	159 171 183 195 206	152 163 174 186 197	144 154 165 176 187	137 147 157 168 178	130 140 150 158 168	124 132 142 151 160	117 126 135 142 151	111 120 127 135 143	60.0 65.0 70.0 75.0 80.0	15" B109
239 254 269 284 299	231 245 259 272 287	221 235 249 261 275	213 226 239 251 264	203 216 228 240 252	194 206 218 228 240	186 197 209 219 230	177 188 199 208 219	169 180 190 199 210	161 171 181 190 200	80.0 85.0 90.0 95.0 100.0	15" B113
153 168 181 192	145 160 172 183	139 152 163 173	132 144 154 164	125 137 146 155	119 129 138 146	112 122 131 138	106 116 123 130	100 110 117 123	95 104 110 116	55.0 60.0 65.0 70.0	18″ B 65
187 201 214	179 192 204	171 183 194	164 174 185	155 165 175	148 157 167	141 150 158	134 142 150	126 135 142	120 127 135	65.0 70.0 75.0	20″ B 73
246 258 271 286 300	237 249 262 277 290	229 239 253 265 278	219 230 241 255 267	211 221 232 244 257	202 212 223 234 245	194 202 213 223 235	186 194 204 214 223	177 185 195 205 214	169 176 185 195 203	80.0 85.0 90.0 95.0 100.0	20″ B121
239 255 269 282 296	231 245 258 271 284	223 236 247 261 272	213 226 238 249 260	*205 217 227 239 249	196 207 216 228 238	187 198 207 218 226	179 189 197 207 215	172 181 189 198 205	163 172 180 188 196	80.0 85.0 90.0 95.0 100.0	24" B 89

CALCULATED FOR LEAST RADIUS OF GYRATION AXIS I-I.

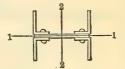
Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 L)^2}{36000 r^2}}$ .



Size of Angles.	Size of Plates.	Weight of Column.	Area of Column Section.	Least Radius of Gyration Axis 1-1.	Radius of Gyration Axis 2-2.	Length in Feet		
Inches.	Inches.	Lbs.per Ft.	Sq. Ins.	Inches.	Inches.	2	4	6
3 x 2½ x ½ x ¼	6 x 1/4 5 6 6 7 6 6 7 6 6 7 6 6 7 6 6 7 6 6 7 6 6 7 6 6 7 6 6 7 6 6 7 6 7 6 6 7 6	23.1 28.8 34.1 39.3 44.2 49.5 54.4	6.79 8.40 9.98 11.53 13.00 14.49 15.94	1.24 1.27 1.30 1.33 1.36 1.39 1.43	2.41 2.39 2.37 2.35 2.33 2.31 2.29	84 103 123 142 161 180 198	81 100 120 139 157 175 193	77 96 114 133 151 169 186
3½ x 2½ x ½	7 x 1/4 56 66 3/6 7 6 66 66 66 66 66 66 66 66 66 66 66 6	25.6 31.8 37.7 43.6 49.5 55.0 60.9 66.4 71.5	7.50 9.30 11.07 12.83 14.50 16.17 17.82 19.46 21.00	1.46 1.49 1.52 1.55 1.58 1.61 1.65 1.68 1.71	2.88 2.86 2.84 2.82 2.80 2.78 2.76 2.74 2.72	93 115 137 159 180 201 221 241 261	91 113 135 156 177 197 218 237 257	88 109 130 151 171 192 212 231 250
4 x 3 x 5 c c c c c c c c c c c c c c c c c c	8 X X X 1 1 2 6 8 1 6 1 7 8 1 8 1 8 1 8 1 8 1 8 1 8 1 8 1 8 1	37.3 44.2 51.1 58.0 64.9 71.4 77.9 84.4 90.5 97.0	10.86 12.98 15.02 17.00 19.02 20.98 22.86 24.75 26.61 28.44	1.67 1.70 1.73 1.76 1.79 1.82 1.85 1.89 1.92 1.95	3.25 3.23 3.21 3.18 3.16 3.14 3.12 3.10 3.08 3.06		133 158 183 208 233 257 281 304 327 350	129 154 179 203 227 251 274 297 320 343
5 x 3 <sup>1</sup> / <sub>2</sub> x <sup>5</sup> / <sub>6</sub> (1 1 1 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2	10 x	45.4 54.4 62.9 71.4 79.9 88.5 96.6 104.7 112.8 120.6 128.7	13.36 15.94 18.49 21.00 23.53 25.98 28.40 30.79 33.11 35.48 37.74	2.08 2.10 2.13 2.16 2.19 2.22 2.25 2.29 2.35 2.38	4.10 4.08 4.06 4.04 4.02 4.00 3.98 3.96 3.93 3.91 3.89		165 196 228 259 290 320 350 380 409 438 466	162 193 224 255 285 315 345 374 403 432 460
6 x 31/2 x 3/4 x 3	12 x 8/6 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2	62.1 71.9 81.6 91.4 101.1 110.5 120.2 129.2 138.5 147.5 156.4	18.23 21.15 24.00 26.86 29.69 32.48 35.29 37.98 40.69 43.36 46.00	2.56 2.59 2.62 2.65 2.68 2.71 2.74 2.77 2.80 2.83 2.86	5.01 4.99 4.97 4.95 4.93 4.91 4.88 4.86 4.84 4.82 4.80		225 261 297 333 368 402 437 471 505 538 571	222 258 294 329 364 398 432 466 499 532 565

CALCULATED FOR LEAST RADIUS OF GYRATION AXIS I-I.

Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 L)^2}{36000 r^2}}$ .

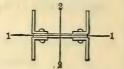


#### Length in Feet.

8	10	12	14	16	18	20	22	24	26	28	30	32	34
72 90 108 125 143 160 177 84 104 125 145 164 124 223 241 124 149 172 196 220 243 266 289 311 333	67 84 100 117 134 150 166 79 99 118 137 156 175 194 213 231 119 142 165 188 211 234 256 278 300 322	61 77 93 108 124 140 155 74 92 111 129 147 166 184 202 219 113 135 157 179 201 223 245 268 309	56 70 85 99 114 129 144 69 86 103 121 138 155 173 190 207 106 127 148 170 191 212 233 254 274 295	51 644 77 91 105 119 132 63 80 96 112 129 145 162 178 195 99 119 139 160 180 220 240 240 280	58 73 89 104 119 135 151 166 182 93 112 131 150 169 188 208 227 246 265	54 68 82 96 111 125 140 155 170 86 104 122 140 158 177 195 213 232 250	80 97 114 131 131 148 165 183 200 2018 236	74 90 106 122 138 155 171 188 205 222			30	32	34
196 220 243	165 188 211 234	157 179 201 223	148 170 191 212	139 160 180 200	131 150 169 188	122 140 158 177	114 131 148 165	106 122 138 155					• • • • • • • • • • • • • • • • • • • •
196 220 243 266 289	211 234 256 278	201 223 245 266	191 212 233 254	180 200 220 240	169 188 208 227	158 177 195 213	148 165 183 200	138 155 171 188					• • • • • • • • • • • • • • • • • • • •
333 158 188 219	322 153 183 212	309 147 176 205	295 141 169 197	280 135 162 189	265 128 154 180	250 122 146 171	236 115 139 162	222 109 131 153	103 124 145	97 117 137			
249 279 308 337 366 395	242 271 300 329 357 385	234 262 290 318 346 374	225 252 280 307 334 361	215 242 269 295 321 348	206 231 257 282 308 333	196 220 245 270 294 319	186 209 233 257 280 304	176 198 221 244 267 290	166 188 210 231 253 275	157 178 198 219 240 261			
423 451 219 254 289	413 441 214 249 283	401 428 209 243 277	388 414 203 236 269	374 400 197 229 261	359 384 190 221 252	343 368 183 213 243	328 352 176 205 234	313 336 168 196 225	297 320 161 188 215	283 304 154 180 206	147 172 197	140 164 188	133 156 179
289 324 358 392 426 459	318 352 385 418 451	310 344 376 409 442	302 335 367 399 431	293 325 356 388 419	283 314 345 376 406	273 303 333 363 393	263 292 321 350 379	253 281 309 337 365	242 269 297 324 351	232 258 284 311 337	222 247 272 298 323	212 236 261 285 310	202 226 249 273 296
493 525 558	484 516 548	474 506 537	462 494 525	450 481 511	437 467 497	423 452 481	408 437 465	393 421 449	378 405 432	363 390 416	349 374 400	334 359 384	320 344 368

CALCULATED FOR LEAST RADIUS OF GYRATION AXIS I-I.

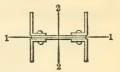
Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 L)^2}{36000 r^2}}$ 



Size of Angles,	Size of Plates.	Weight of Column.	Area of Column Section.	Least Radius of Gyration Axis 1-1.	Radius of Gyration Axis 2-2.		engt:	
Inches.	Inches.	Lbs.perFt.	Sq. Ins.	Inches.	Inches.	2	4	6
3 x 2½ x ¼ x 1/4 x	8 x 1/4 5/16 3/8 7/8 1/2 9 1/6 1/6	24.8 30.9 36.6 42.3 47.6 53.3 58.6	7.29 9.02 10.73 12.40 14.00 15.61 17.19	1.19 1.22 1.25 1.28 1.31 1.34 1.37	3.25 3.23 3.21 3.19 3.17 3.15 3.13	90 111 132 153 173 193 213	87 108 128 149 169 188 208	82 102 122 142 161 181 200
3½ x 2½ x ¼	8 x 1/4 6 16 8 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	26.4 32.9 39.0 45.1 51.2 56.9 63.0 68.7 74.0	7.75 9.61 11.44 13.27 15.00 16.73 18.44 20.15 21.75	1.44 1.47 1.50 1.53 1.56 1.59 1.62 1.65 1.68	3.31 3.28 3.26 3.24 3.22 3.20 3.18 3.16 3.14	96 119 142 164 186 208 229 250 270	94 117 139 161 183 204 225 246 266	91 113 134 156 177 198 218 239 259
4 x 3 x 5 x 5 x 5 x 5 x 5 x 5 x 5 x 5 x 5	116 34 116 116 116	39.4 46.8 54.1 61.4 68.7 75.7 82.6 89.5 96.0 103.0	11.49 13.73 15.90 18.00 20,15 22.23 24.24 26.25 28.24 30.19	1.62 1.65 1.68 1.71 1.74 1.77 1.80 1.83 1.86 1.90	4.09 4.07 4.04 4.02 4.00 3.98 3.96 3.94 3.92 3.90		140 167 194 220 246 272 297 322 347 371	136 163 189 214 240 265 290 315 339 363
5 x 3½ x 56 3/8 3/8 3/8 3/8 3/8 3/8 3/8 3/8 3/8 3/8	12 X 9 6 8 8 9 1 6 9 1 6 9 1	47.6 56.9 65.9 74.8 83.8 92.7 101.3 109.8 118.4 126.5 135.1	13.98 16.69 19.36 22.00 24.65 27.23 29.77 32.29 34.73 37.23 39.61	2.03 2.06 2.08 2.11 2.14 2.17 2.20 2.23 2.26 2.29 2.33	4.95 4.92 4.90 4.88 4.86 4.84 4.82 4.80 4.78 4.76 4.74		172 206 238 271 303 335 367 398 429 459 489	169 202 234 266 298 330 361 392 422 452 482
6 x 3½ x 3/6	14 x 3/3 %	64.7 74.8 85.0 95.2 105.3 115.1 125.3 134.7 144.5 153.8 163.2	18.98 22.03 25.00 27.99 30.94 33.86 36.79 39.61 42.44 45.24 48.00	2.51 2.54 2.57 2.59 2.62 2.65 2.68 2.71 2.74 2.77 2.81	5.85 5.83 5.81 5.79 5.77 5.74 5.72 5.70 5.68 5.66 5.64		234 272 309 347 383 419 455 491 526 561 595	231 269 306 343 379 415 450 486 521 555 589

CALCULATED FOR LEAST RADIUS OF GYRATION AXIS I-I.

Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 L)^2}{36000 r^2}}$ .

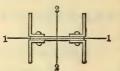


#### Length in Feet.

8	10	12	14	16	18	20	22	24	26	28	30	32	34
77 96 115	71 89 106	65 81 98	58 74 89	53 67 81									
134 152 171 189	124 142 160 177	114 131 148 165	105 120 136 152	95 110 124 139						• •			• •
86 107 128 149 170	81 101 121 141 161	76 95 114 133 151	70 88 106 124 142	65 81 98 115 132	60 75 91 106 122	55 69 83 98 113							
190 210 230 249	180 200 219 238	170 189 208 226	159 177 195 213	149 166 183 200	138 154 170 187	128 143 158 174							• •
131 156 182 207 232	125 149 174 198	118 141 165 188 211	111 133 155 177	103 124 145 167	96 116 136 156	89 108 127 145	83 100 118 135	77 93 109 126					
232 256 281 305 329	222 246 270 293 317	211 234 257 280 303	200 222 244 266 288	188 209 230 251 273	176 196 216 237 257	164 184 203 222 242	153 171 190 208 227	143 160 177 195 212					• • •
352 165 197 229	340 159 191 222	325 153 184 214	310 147 176 205	294 140 168	277 133 160	261 126 151 177	245 119 143 167	230 112 135 158	105 127 149	99 120 141			
260 291 322 353 383	252 283 313 343 373	244 273 303 332	234 263 291 320	196 224 251 279 307	186 213 240 267 293	202 228 254 279	192 216 241 266	181 205 228 252	171 194 216 239	162 183 204 226			
413 443 473	403 432 461	361 390 419 447	348 376 405 432	334 362 389 416	320 346 373 399	305 331 357 382	290 315 340 365	276 299 323 347	261 284 307 330	247 269 291 313	121	149	
228 264 301 337 373	223 259 295 330 366	217 252 287 322 357	211 245 279 313 347	204 237 270 304 337	196 229 261 293 325	189 220 251 283 314	181 211 241 272 302	173 202 231 261 290	166 194 221 250 278	158 185 212 239 266	151 176 202 228 254	143 168 193 217 242	136 160 184 207 231
408 444 478 513	400 435 470 504	391 425 459 493	381 414 447 480	369 402 435 467	357 389 421 453	345 376 407 438	332 362 392 422	319 348 377 406	306 334 362 390	293 320 347 375	280 306 333 359	268 293 318 344	255 280 304 329
547 581	538 571	526 559	513   546	499 531	484 515	468   499	452 482	435 464	419 447	402 429	385 412	369 395	353 378

CALCULATED FOR LEAST RADIUS OF GYRATION AXIS 1-1.

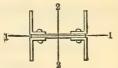
Based on Gordon's Formula P= $\frac{50\,000}{1+\frac{(12\,\mathrm{L})^2}{36\,000\,\mathrm{r}^2}}$ .



Size of Angles.	Size of Plates.	Weight of Column.	Area of Column Section.	Least Radius of Gyration Axis 1-1.	Radius of Gyration Axis 2-2.	1	engtl	
Inches.	Inches.	Lbs.per Ft.		Inches.	Inches.	2	4	6
3 x 2½ x ½ 	10 x 1/4  5 7 16 1/2 18 6/8 10 x 1/4	26.5 33.0 39.2 45.3 51.0 57.1 62.9	7.79 9.65 11.48 13.28 15.00 16.74 18.44 8.25	1.16 1.18 1.21 1.24 1.27 1.30 1.33 1.39	4.07 4.05 4.03 4.01 3.99 3.96 3.94 4.13	96 119 141 164 186 207 228 102	92 115 137 159 180 202 222 100	87 109 130 151 172 193 213 96
(; (; 36) (; (; 76) (; (; 176) (; 176) (; (; 176) (; 176)	16 16 17 16 17 16 17 16 17 16 17 16 17 16 17 16 17 16 17 16 17 17 17 17 17 17 17 17 17 17 17 17 17	35.0 41.6 48.1 54.6 60.7 67.3 73.4 79.1 41.6	10.24 12.19 14.15 16.00 17.86 19.69 21.53 23.25 12.11	1.42 1.45 1.48 1.51 1.54 1.57 1.60 1.63 1.58	4.11 4.09 4.07 4.05 4.03 4.01 3.99 3.97 4.91	127 151 175 199 222 245 267 289	124 148 171 195 217 240 262 284 148	119 143 165 188 210 232 254 276 143
4 x 3 x 56 3/8 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	12 x 56 8 76 8 76 12 12 12 12 12 12 12 12 12 12 12 12 12	49.3 57.1 64.8 72.6 79.9 87.3 94.6 101.6 108.9	14.48 16.77 19.00 21.27 23.48 25.61 27.75 29.86 31.94	1.61 1.64 1.66 1.69 1.72 1.75 1.78 1.81 1.84	4.89 4.87 4.85 4.83 4.81 4.79 4.77 4.74 4.72		176 204 232 260 287 314 340 366 392	171 198 226 253 279 306 332 358 383
5 x 3½ x 56 x x 52	14 x 56 8 8 7 16 8 12 8 12 8 12 8 12 8 12 8 12 8 12 8	49.7 59.5 68.8 78.2 87.6 96.9 105.9 114.9 123.9 132.5 141.4	14.61 17.44 20.24 23.00 25.78 28.48 31.15 33.79 36.36 38.98 41.49	1.98 2.01 2.04 2.07 2.09 2.12 2.15 2.18 2.21 2.24 2.27	5.77 5.75 5.73 5.71 5.69 5.67 5.64 5.62 5.60 5.58 5.56		180 215 249 283 317 351 384 416 449 481 512	176 211 245 278 312 345 377 410 442 473 505
6 x 3\frac{1}{2} x \frac{3}{7}\frac{1}{1}\frac{1}{2} x \frac{3}{7}\frac{1}{1}\frac{1}{1}\frac{1}{2}} \frac{1}{1}\frac{1}{1}\frac{1}{2}} \frac{1}{1}\frac{1}{1}\frac{1}{2}} \frac{1}{1}\frac{1}{1}\frac{1}{2}\frac{1}{1}\frac{1}{2}\frac{1}{1}\frac{1}{2}\frac{1}\frac{1}{2}\frac{1}{2}\frac{1}{2}\frac{1}{2}\frac{1}{2}\frac{1}	16 x 2/8  16 1/2  17 1/2  18 1	67.2 77.8 88.4 99.0 109.6 119.8 130.4 140.2 150.4 160.2 170.0	19.73 22.90 26.00 29.11 32.19 35.23 38.29 41.23 44.19 47.11 50.00	2.46 2.49 2.52 2.54 2.57 2.60 2.63 2.66 2.69 2.72 2.75	6.68 6.66 6.64 6.61 6.59 6.57 6.55 6.53 6.51 6.48		244 283 322 360 399 436 474 511 548 584 620	240 279 318 356 394 431 468 505 542 578 613

CALCULATED FOR LEAST RADIUS OF GYRATION AXIS I-I.

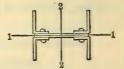
Based on Gordon's Formula  $P = \frac{50\,000}{1 + \frac{(12\,L)^2}{36\,000\,r^2}}$ .



#### Length in Feet.

CALCULATED FOR LEAST RADIUS OF GYRATION AXIS 1-1.

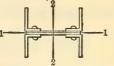
Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 L)^2}{36000 r^2}}$ .



Size of Angles,	Size of Plates.	Weight of Column.	Area of Column Section.	Least Radius of Gyration Axis 1-1.	Radius of Gyration Axis 2-2.		engt:	
Inches.	Inches.	Lbs.per Ft.		Inches.	Inches.	2	4	6
3 x 2½ x ¼ 	12 x <sup>1</sup> / <sub>4</sub> <sup>5</sup> / <sub>16</sub> <sup>3</sup> / <sub>8</sub> <sup>7</sup> / <sub>16</sub>	28.2 35.2 41.7 48.3 54.4 61.0 67.1	8.29 10.27 12.23 14.15 16.00 17.86 19.69	1.12 1.15 1.17 1.20 1.23 1.26 1.28	4.87 4.85 4.83 4.81 4.78 4.76 4.74	102 126 151 174 198 221 244	98 122 146 169 192 215 237	92 115 138 160 183 205 226
3½ x 2½ x ½, x ¼, x ¼, x ¼, x ¼, x ¼, x ¼, x ¼	12 x <sup>1</sup> / <sub>4</sub> 56 66 77 67 77 67 78 67 78 67 78 67 78 78 78 78 78 78 78 78 78 78 78 78 78	29.8 37.2 44.1 51.1 58.0 64.6 71.5 78.1 84.2	8.75 10.86 12.94 15.02 17.00 18.98 20.94 22.90 24.75	1.35 1.38 1.41 1.43 1.46 1.49 1.52 1.55 1.58	4.94 4.92 4.90 4.88 4.85 4.83 4.81 4.79 4.77	108 135 160 186 211 236 260 284 307	106 131 157 182 206 231 255 278 302	101 126 151 175 199 223 246 270 292
4 x 3 x 5 8 38 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	14 x 5 6 6 7 8 6 7 16 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	43.7 51.9 60.0 68.2 76.4 84.1 91.9 99.7 107.1 114.9	12.74 15.23 17.65 20.00 22.40 24.73 26.99 29.25 31.49 33.69	1.54 1.57 1.60 1.62 1.65 1.68 1.71 1.74 1.77	5.72 5.70 5.68 5.66 5.63 5.61 5.59 5.57 5.55		155 185 215 244 273 302 330 358 386 413	150 179 208 237 265 294 322 349 376 403
5 x 31/2 x 5/8 x 6/8 x 6	16 x 5 5 6 8 7 8 7 2 9 6 7 6 7 4 7 6 7 6 7 7 6 7 7 6 7 7 6 7 7 7 7	51.8 62.0 71.8 81.6 91.4 101.2 110.6 120.0 129.4 138.4 147.8	15.23 18.19 21.11 24.00 26.90 29.73 32.52 35.29 37.98 40.73 43.36	1.94 1.97 2.00 2 02 2.05 2.08 2.11 2.14 2.17 2.19 2.22	6.59 6.57 6.54 6.52 6.50 6.48 6.46 6.44 6.41 6.39 6.37		187 224 260 295 331 366 400 435 468 502 535	183 219 255 290 325 359 393 427 461 494 527
6 x 31/2 x 3/6  4 4 1/2 x 3/6  4 4 1	18 x 3/7-6/00 x 1/2 x 1/	69.8 80.8 91.8 102.8 113 9 124.5 135.5 145.7 156.4 166.6 176.8	20.48 23.78 27.00 30.24 33.44 36.61 39.79 42.86 45.94 48.99 52.00	2.42 2.44 2.47 2.50 2.52 2.55 2.58 2.61 2.64 2.67 2.70	7.49 7.47 7.45 7.42 7.40 7.38 7.36 7.34 7.32 7.29 7.27		253 294 334 374 414 453 492 531 569 607 644	249 290 330 369 409 448 486 525 563 600 637

CALCULATED FOR LEAST RADIUS OF GYRATION AXIS I-I.

Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 L)^2}{36000 r^2}}$ .

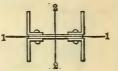


#### Length in Feet.

-8	10	12	14	16	18	20	122	24	26	28	30	32	34
8	10	12	14	10	18	20	22	24	20	20	30	32	34
86	78	71	63	57				1					
107	98	89	80	72									
128	118	107	97	87			: :						
150	138	126	114	103									
171	158	145	131	119									
192	178	164	149	135									
213	198	182	167	152									
96	90	83	77	70	64	58						١	
120	112	104	96	88	81	74							
143	135	125	116	107	98	- 89							
167	157	146	136	125	115	105							
190	179	167	156	144	132	122							
213	201	188	175	162	150	138							
236	223	210	195	181	168	155							
258	245	230	215	200	186	171							
281	267	251	235	219	204	188					6 4		
144	136	128	120	111	103	95	88	81					
172	163	154	144	134	124	115	106	98					
200	190	180	168	157	146	135	125	116					
228	217	205	193	180	168	156	144	133	• •			• •	
255	244	231	217	203	189	176	163	151		• •		• •	
283 310	270 297	$\frac{256}{282}$	241 266	226 250	$\frac{211}{234}$	$\frac{197}{218}$	$\frac{183}{203}$	170 188		• •	• •	• •	
337	323	307	290	273	256	239	223	207		• •			
364	349	332	315	296	278	260	243	226					• •
390	375	357	339	320	301	282	263	246					
178	172	165	158	150	142	134	126	118	111	104			• •
213	206	198	189	180	170	161	152	143	134	126			
248	240	231	220	210	199	188	178	167	157	148			
282	273	263	252	240	228	216	204	192	181	170			
316	307	295	283	270	257	243	230	217	204	192			
350	340	327	314	300	286	271	256	242	228	215			
384	372	359	345	330	314	298	283	267	252	238			
417	405	391	376	360	343	326	309	293	277	261			
450	437	423	407	390	372	354	336	318	301	284			
483	470	454	437	419	401	382	363	344	326	308			
515	501	485	468	449	430	410	390	370	350	332	• •		
245	239	233	225	217	209	201	192	183	175	166	158	150	143
285	278	271	262	253	244	234	224	214	204	194	185	176	167
324	317	308	299	289	278	267	256	245	234	223	212	202	192
363	355	346	336 372	325 360	313	301	288 321	276 307	264	251	$\frac{240}{267}$	228 254	217
402 440	393 431	383 420	408	395	$\frac{347}{382}$	334 367	353	338	293 323	280 309	267 295	281	$\frac{242}{268}$
478	469	457	445	431	416	401	385	369	353	338	323	308	293
516	506	494	480	466	450	434	417	400	383	367	350	334	319
554	543	530	516	501	484	467	449	431	414	396	378	362	345
591	580	567	552	535	518	500	481	463	444	425	407	389	371
628	616	602	587	570	552	533	513	494	474	454	435	416	397
,					,		,		'	,		,	

CALCULATED FOR LEAST RADIUS OF GYRATION AXIS 1-1.

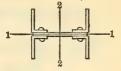
Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 L)^2}{36000 r^2}}$ .



	Size of Angles.	Size Weight of of Plates. Column.		Area of Radius of Gyration Section, Axis 1-1.		Radius of Gyration Axis 2-2.	in Feet.			
	Inches.	Inches.	Lbs.per Ft.	Sq. Ins.	Inches.	Inches.	6	8	10	
66 66 66 66 66	x 31/2 x 7/8	14 x 776 2 96 0 80-16 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	80.8 91.8 103.2 113.7 124.7 135.3 145.9 156.5 166.6 176.8	23.78 27.00 30.24 33.48 36.61 39.79 42.90 45.98 49.03 52.00	3.05 3.08 3.11 3.13 3.17 3.20 3.23 3.26 3.29 3.32	5.92 5.90 5.87 5.85 5.83 5.81 5.79 5.76 5.74 5.72	292 332 372 412 451 490 528 567 604 642	289 329 368 407 446 485 523 561 598 635	285 324 363 402 449 478 516 553 591 627	
66	X 31/2 X 7 8 1/2 2 X 7 8 1/2 2 X 1/2 2	16 x 76 12 29 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	83.8 95.2 107.0 118.0 129.4 140.4 151.4 162.4 173.0 183.6	24.65 28.00 31.36 34.73 37.98 41.29 44.52 47.73 50.90 54.00	3.00 3.02 3.06 3.08 3.11 3.14 3.17 3.20 3.23 3.26	6.75 6.73 6.71 6.69 6.67 6.64 6.62 6.60 6.58 6.56	303 345 386 427 468 508 548 588 627 666	299 340 382 422 463 503 542 582 621 659	294 335 376 416 456 496 535 574 612 651	
	X 31/2 X 7/10/2 0/10 8/10/2 1/	18 x 76	86.8 98.6 110.8 122.3 134.1 145.5 156.9 168.4 179.4 190.4	25.53 29.00 32.49 35.98 39.36 42.79 46.15 49.48 52.78 56.00	2.94 2.97 3.00 3.02 3.06 3.08 3.11 3.14 3.17 3.20	7.58 7.55 7.53 7.51 7.49 7.47 7.44 7.42 7.40 7.38	313 357 400 442 485 526 568 609 650 690	309 352 395 437 479 520 562 602 643 683	305 347 389 430 472 513 554 594 634 674	
17 66 66 66 66 66 66 66	x 31/2 x 7/6/2 4/6/2 x 1/6/2 x	20 x 7/6 / 2 / 6 / 6 / 6 / 6 / 6 / 6 / 6 / 6 /	89.8 102.0 114.7 126.5 138.7 150.6 162.5 174.3 185.8 197.2	26.40 30.00 33.61 37.23 40.73 44.29 47.77 51.23 54.65 58.00	2.89 2.92 2.95 2.97 8.00 3.03 3.06 3.09 3.12 3.15	8.39 8.37 8.34 8.32 8.30 8.28 8.25 8.23 8.21 8.19	324 369 413 457 501 545 588 630 673 715	320 364 408 452 495 538 581 623 665 707	314 358 402 445 488 530 572 614 656 697	

CALCULATED FOR LEAST RADIUS OF GYRATION AXIS (-1.

Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 L)^2}{36000 r^2}}$ .

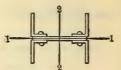


#### Length in Feet.

12	14	16	18	20	22	24	26	28	30	32	34	36	38	40
		10					~~		-00	-02				
279	274	267	260	253	246	238	230	222	214	206	198	191	183	176
318	312	305	297	289	280	271	263	254	245	236	227	218	210	201
357 395	350	342	333	324	315	305	295	286	276	266	256	246	237	228
395	387	379	369	359	349	339	328	317	306	295	284	274	263	253
433	424	415	405	395	384	372	360	349	337	325	313	302	290	279
470	462	452	441	430	418	406	393	380	368	355	342	330	318	306
508	498	488	477	465	452	439	425	412	398	385	371	358	345	332
545	535	524	512	499	486	472	458	443	429	415	400	386	372	358
581	571	559	547	534	520	505	490	475	460	444	429	414	399	385
613	607	595	582	568	553	538	522	506	490	474	458	442	427	412
289	283	276	269	261	253	245	236	228	220	211	203	195	187	180
329	322	315	307	298	289	280	270	261	251	242	232	223	214	206
369	362	353	344	335	325	314	304	293	283	272	262	252	242	233
409	400	391	381	371	360	349	337	326	314	303	291	280	269	259
448	439	429	419	407	396	383	371	359	346	334	321	309	297	286
487	478	467	456	444	431	418	405	391	378	364	351	338	325	313
526	516	505	493	480	466	452	438	424	409	395	381	367	353	340
564	554	542	529	516	501	487	472	456	441	426	411	396	381	367
603 640	591	579	566	551 587	536	521	505	489	473	457	441	425	409	394
040	629	616	602	981	571	555	538	521	504	487	471	454	437	421
299	292	285	277	269	260	252	243	234	255	216	208	199	191	
340	333	325	316	307	297	287	277	267	257	248	238	228	219	
382	374	365	355	345	334	323	312	301	290	279	268	258	247	
423	414	404	393	382	371	359	347	335	322	310	298	287	275	
463	454	443	432	420	407	395	382	368	355	342	329	316	304	
504	494	483	470	457	444	430	416	402	388	374	360	346	333	
544	533	521	508	495	481	466	451	436	420	405	390	376	361	
584	573	560	546	532	517	501	485	469	453	437	421	405	390	* , *
624	612	598	584	569	553	536	520	503	486	469	452	435	419	• •
663	650	636	622	606	589	572	554	536	518	500	483	465	448	• •
308	301	294	285	277	268	258	249	240	230	221	212	204	195	
351	343	335	326	316	306	295	285	274	264	253	243	233	224	
394	385	376	366	355	344	332	321	309	297	286	274	263	253	
436	427	417	405	394	381	369	356	343	330	318	305	293	281	
479	468	457	445	432	419	406	392	378	364	350	337	323	310	
521	510	498	485	471	457	442	427	412	397	383	368	354	340	
562	551	538	524	510	495	479	463	447	431	415	400	384	369	
603 644	591 632	578 618	563 602	548 586	532 569	515 552	499 534	482	465	448	431	415	399	• •
685	672	657	641	624	607	588	570	516 551	498 532	480 513	463 494	445 476	428 458	• •
000	012	007	0.11	024	007	900	910	991	992	919,	494	470	-100	

### CALCULATED FOR RADIUS OF GYRATION AXIS 2-2.

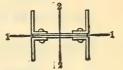
Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 L)^2}{36000 r^2}}$ .



D	arecy rac				_	1	•	
Size of Angles.	Size of Plates.	Weight of Column.	Area of Column Section.	Least Radius of Gyration Axis 1-1.	Radius of Gyration Axis 2-2.		engtl	
Inches.	Inches.	Lbs.per Ft.	Sq. Ins.	Inches.	Inches.	4	6	8
of Angles.  Inches.  Inches.  3 x 21/2 x 1/4 s s s s s s s s s s s s s s s s s s s	of Plates.  Inches.  6 x 1/4  4 5 6 6 7 7 x 1/4  6 7 x 1/4  7 x 1/4  7 x 1/4  8 x 1/5  10 x	of Column, Lbs.per Ft.  23.1 28.8 34.1 39.3 44.2 49.5 54.4 25.6 31.8 37.7 43.6 49.5 55.0 60.9 66.4 71.5 37.3 44.2 51.1 58.0 64.9 71.4 77.9 84.4 90.5 97.0 45.4 62.9 71.4 79.9 88.5	of Column Section. Sq. Ins.  6.79 8.40 9.98 11.53 13.00 14.49 15.94 7.50 9.30 11.07 12.83 14.50 16.17 17.82 19.46 21.00 10.86 12.98 15.02 17.00 19.02 20.98 22.86 24.75 26.61 28.44 13.36 15.94 18.49 21.00 23.53 25.98	Radius of Gyration Axis 1-1. Inches.  1.24 1.27 1.30 1.33 1.36 1.39 1.43 1.46 1.49 1.52 1.55 1.58 1.61 1.65 1.68 1.71 1.67 1.70 1.73 1.76 1.79 1.82 1.85 1.89 1.92 1.95 2.08 2.10 2.13 2.16 2.19 2.22	Gyration Aris 2-2. Inches.  2.41 2.39 2.37 2.35 2.33 2.31 2.29 2.88 2.86 2.84 2.82 2.80 2.78 2.76 2.74 2.72 3.25 3.21 3.18 3.16 3.14 3.12 3.10 3.08 3.06 4.10 4.08 4.06 4.04 4.02 4.00	in	82 102 121 140 158 176 194 92 114 136 157 178 198 219 238 257 134 160 185 210 234 228 305 328 350 166 198 229 260 291	81 100 119 137 155 173 190 91 113 134 155 176 196 216 235 254 133 158 207 231 255 278 301 324 346 165 196 228 228 289 319
66 66 1496 66 66 1496 66 66 1496 66 66 1496 66 66 1496	1 1 2 6 8 1	96.6 104.7 112.8 120.6 128.7	28.40 30.79 33.11 35.48 37.74	2.25 2.25 2.29 2.32 2.35 2.38	3.98 3.96 3.93 3.91 3.89		351 381 410 439 467	349 378 407 436 464
6 x 3½ x 3/8	12 x 3/8 1/8 1/9 9 5 8 1 6 7 8	62.1 71.9 81.6 91.4 101.1 110.5	18.23 21.15 24.00 26.86 29.69 32.48	2.56 2.59 2.62 2.65 2.68 2.71	5.01 4.99 4.97 4.95 4.93 4.91			225 261 297 332 367 402
(6 (6 136 14 16 16 16 16 16 16 16 16 16 16 16 16 16	1 3/4 1 13/6 1 1/8 1 1/8 1 1/8 1 1/8	120.2 129.2 138.5 147.5 156.4	35.29 37.98 40.69 43.36 46.00	2.74 2.77 2.80 2.83 2.86	4.88 4.86 4.84 4.82 4.80			436 470 503 536 569

## CALCULATED FOR RADIUS OF GYRATION AXIS 2-2.

Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 L)^2}{36000 r^2}}$ .

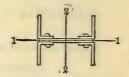


#### Length in Feet.

10	12	14	16	18	20	22	24	26	28	30	32	34	36	38	40
79	77	74	72	69		63	60	58	55	52					
98	95	92	89	85		78	75	71	68	64					
116	113	109	105	101	97	92	88	84	80	76			• •		
134 151	130 147	126 142	121 137	116 131	111 126	106 120	101 114	96 108	92 103	87 98			• •		
169	163	158	152	146		133	127	120	1114	108					
185	180	173	167	160	153	146	138	132	125	118					
89	88	86	83	81	79	76	73	71	68	65	63	60	58		
111	109	106	103	100	97	94	91	87	84	81	77	74	71		
132	129	126	123	119	115	112	108	104	100	96	92	88	84		
152	149	146	142	137	133	129	124	119	115	110	106		97		
172	169	165	160	156	151	145	140	135	129	124	119				
192	188	183	178	173	167 184	162 178	156	150	144	138 151	132 145		121 132		
212 230	207 225	202 220	196 214	190 207	200	178	171 186	164 178	158 171	164	157	150	132		• •
230	244	237	231	$\frac{207}{223}$	216	208	200	192	184	177	169		154		
131	129	126	124	121	118	115	111	108	105	101	98		91	88	85
156	153	150	147	144	140	136	132	128	124	120	116		108		
180	177	174	170	166	162	158	153	148	143	139	134	129	124	120	115
204	201	197	193	188	184	178	173	168	162	157	151	146	141	135	130
228	224	220	215	210	205	199	193	187	181	175	168	162	156	150	
252	247	243	237	231	225	219	212	206	199	192	185	178	172	165	
274	270	264	259 280	252 273	245 265	238	231	224	216 233	209 225	$\frac{201}{217}$	194 209	187 201	179	173
297 319	292 314	286 307	300	273 293	285	258 276	250 268	$\begin{vmatrix} 242 \\ 259 \end{vmatrix}$	250	225	$\frac{217}{232}$	$\frac{209}{224}$	201	193 207	186 199
341	335	328	321	312	304	295	285	276	266	257	248	238	229	220	211
163	161	160	157	155	153	150	147	144	141	138	134	131	128	124	121
195	193	190	188	185	182	179	175	171	168	164	160	156	152	148	144
226	223	221	218	214	211	207	203	199	194	190	185	181	176	171	166
256	254	250	247	243	239	235	230	225	220	215	210	205	199	194	189
287	284	280	276	272	267	262	257	251	246	240	234	228	222	216	210
316	313	309	305	300	295	289	283	277	271	265	258	251	245	238	232
346 375	342 371	338 366	333	328 355	322 349	316 342	309 335	303	296 320	289 312	282 305	274 297	267 289	260 281	252 273
403	399	394	388	382	375	368	360	352	344	336	305	319	310	301	293
432	427	421	415	408	401	393	385	377	368	359	350	340	331	322	313
460	454	449	442	435	427	418	410	400	391	381	371	362	352	342	332
224	222	221	218	216	214	211	208	205	202	199	196	192	189	185	181
260	258	256	253	251	248	245	242	238	234	231	227	223	218	214	210
295	293	291	288	285	282	278	274	270	266	262	257	253	248	243	238
330	328	325	322	319	315	311	307	302	$\frac{298}{329}$	293	288	282	277	272	266
365	363	360	356 389	352 385	348 381	344 376	339	334	329	323	318	312	306	300	294
399 433	397 430	393 427	422	418	413	408	371 402	365 396	359 389	353 383	347 376	341	334 362	327 355	321 347
467	463	460	455	450	445	439	433	426	419	412	405	397	389	382	374
500	496	492	487	482	476	470	463	456	449	441	433	425	417	408	400
533	529	524	519	513	507	500	493	486	478	469	461	452	443	434	425
565	561	556	551	544	538	530		515	506					460	

CALCULATED FOR RADIUS OF GYRATION AXIS 2-2.

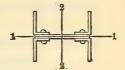
Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 L)^2}{36000 r^2}}$ .



	Size of Angles.	Size of Plates.	Weight of Column.	of Column Section.	Radius of Gyration Axis 1-1,	Radius of Gyration Axis 2-2.		engti Fee	
	Inches.	Inches.	Lbs.per Ft.	Sq. Ins.	Inches,	Inches.	4	6	8
3	x 21/2 x 1/4 15/6 16/7 17/7 17/7 17/7 17/7 17/7 17/7 18/7	8 x 1/4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	24.8 30.9 36.6 42.3 47.6 53.3 58.6	7.29 9.02 10.73 12.40 14.00 15.61 17.19	1.19 1.22 1.25 1.28 1.31 1.34 1.37	3.25 3.23 3.21 3.19 3.17 3.15 3.13	90 112 133 154 174 194 213	89 111 132 152 173 192 212	88 110 130 151 171 190 209
31	2 x 21/2 x 1/4	8 x 1/4/5/16 (1/2)	26.4 32.9 39.0 45.1 51.2 56.9 63.0 68.7 74.0	7.75 9.61 11.44 13.27 15.00 16.73 18.44 20.15 21.75	1.44 1.47 1.50 1.53 1.56 1.59 1.62 1.65 1.68	3.31 3.28 3.26 3.24 3.22 3.20 3.18 3.16 3.14		96 119 141 163 185 206 227 248 268	95 117 140 161 183 204 225 245 265
66 66 66	X 3 X 5 6 6 8 7 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6 7	10 x 5 5 8 7 5 8 1 8 1 8 1 8 1 8 1 8 1 8 1 8 1 8 1 8	39.4 46.8 54.1 61.4 68.7 75.7 82.6 89.5 96.0 103.0	11.49 13.73 15.90 18.00 20.15 22.23 24.24 26.25 28.24 30.19	1.62 1.65 1.68 1.71 1.74 1.77 1.80 1.83 1.86 1.90	4.09 4.07 4.04 4.02 4.00 3.98 3.96 3.94 3.92 3.90		142 170 197 223 249 275 300 325 350 374	141 169 195 222 247 273 298 323 347 371
5	* 31/2 X 31/2 X 4 6 6 7 6 6 6 7 6 6 6 6 7 6 6 6 6 7 6 6 6 6 7 6 6 6 6 7 6	12 x 5 6 3 8 7 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6 7	47.6 56.9 65.9 74.8 83.8 92.7 101.3 109.8 118.4 126.5 135.1	13.98 16.69 19.36 22.00 24.65 27.23 29.77 32.29 34.73 37.23 39.61	2.03 2.06 2.08 2.11 2.14 2.17 2.20 2.23 2.26 2.29 2.33	4.95 4.92 4.90 4.88 4.86 4.84 4.82 4.80 4.78 4.76 4.74			173 206 239 272 304 336 368 399 429 460 490
6	X 31/2 X 3/8 11/2 X 3/	14 x 3/0   16/29   16/	64 7 74.8 85.0 95.2 105.3 115.1 125.3 134.7 144.5 153.8 163.2	18.98 22.03 25.00 27.99 30.94 33.86 36.79 39.61 42.44 45.24 48.00	2.51 2.54 2.57 2.59 2.62 2.65 2.68 2.71 2.74 2.77 2.81	5.85 5.83 5.81 5.79 5.77 5.74 5.72 5.70 5.68 5.66 5.64			

# CALCULATED FOR RADIUS OF GYRATION AXIS 2-2.

Based on Gordon's Formula P= $\frac{50\,000}{1+\frac{(12\,L)^2}{36\,000\,r^2}}$ .

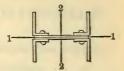


#### Length in Feet.

10	12	14	16	18	20	22	24	26	28	30	32	34	36	38	40
87	86	84	83	81	79	77	74	72	70	68	65	63	61	59	56
108	106	104	102	100	97	95	92	89	86	83	81	78	75	72	70
129	127	124	122	119	116	112	109	106	102	99	96	92	89	86	82
149	146	143	140	137	133	130	126	122	118	114	110	106	102	99	95
168	166	162	159	155	151	147	142	138	133	129	124	120	115	111	107
188	184	181	177	173	168	163	158	153	148	143	138	133	128	123	119
206	203	199	195	190	185	179	174	168	163	157	151	146	140	135	130
93	92	90	189	87	85	82	80	78	75	73	70	68	66	63	61
116	114	112	110	108	105	102	99	96	93	90	87	84	81	78	75
138	136	133	130	127	124	121	118	114	110	107	103	100	96	93	89
159	157	154	151	147	144	140	136	132	127	123	119	115	111	107	103
181	178	174	171	167	162	158	153	149	144	139	134	130	125	120	116
201	198	194	190	186	181	176	171	165	160	155	149	144	139	134	129
222	218	214	209	204	199	193	188	182	176	170	164	158	152	147	141
242	238	233	228	222	217	211	204	198	191	185	178	172	165	159	153
261	257	252	246	240	234	227	220	213	206	199	192	185	178	171	165
140	139	137	135	133	131	129	126	124	121	118	115	112	110	107	104
167	165	163	161	159	156	153	150	147	144	141	137	134	130	127	123
194	192	189	187	184	181	177	174	170	166	162	159	155	151	147	143
220	217	215	212	208	205	201	197	193	189	184	180	175	170	166	161
245	243	240	236	233	229	224	220	215	210	205	200	195	190	185	180
271	268	264	261	256	252	247	242	237	232	226	220	215	209	203	198
295	292	289	284	280	275	270	264	258	253	246	240	234	228	222	215
320	316	312	308	303	298	292	286	280	273	266	260	253	246	239	232
344	340	336	331	326	320	314	307	300	293	286	279	271	264	257	249
368	364	359	354	348	342	335	328	320	313	305	297	289	282	274	266
172	171	169	168	166	164	162	160	157	155	152	150	147	144	141	139
205	204	202	200	198	196	193	191	188	185	182	178	175	172	168	165
238	236	234	232	230	227	224	221	218	214	210	207	203	199	195	191
270	269	266	264	261	258	254	251	247	243	239	235	230	226	221	217
303	300	298	295	292	288	284	280	276	272	267	262	257	252	247	242
334	332	329	326	322	318	314	309	305	300	295	289	284	278	273	267
365	363	359	356	352	348	343	338	333	327	322	316	310	304	298	291
396	393	390	386	382	377	372	366	361	355	349	342	336	329	322	315
427	423	420	415	411	406	400	394	388	382	375	368	361	354	346	339
457	453	449	445	440	434	428	422	415	408	401	394	386	378	370	362
486	483	478	474	468	462	456	449	442	434	427	419	410	402	394	385
234	233	231	230	228	226	224	222	219	217	214	211	209	206	203	199
272	270	269	267	265	263	260	257	255	252	249	245	242	239	235	231
309	307	305	303	301	298	296	293	289	286	282	279	275	271	267	263
346	344	342	340	337	334	331	327	324	320	316	312	307	303	298	294
382	380	378	375	372	369	365	362	358	353	349	344	340	335	330	324
418	416	413	411	407	404	400	396	391	387	382	377	371	366	360	355
454	451	449	445	442	438	434	429	424	419	414	408	403	397	391	384
489	487	483	480	476	472	467	462	457	452	446	440	433	427	420	414
524	521	518	514	510	505	500	495	490	484	477	471	464	457	450	443
559	556	552	548	544	539	533	528	521	515	508	501	494	487	479	471
593	589	586	581	577	571	566	559	553	546	539	532	524	516	508	500

CALCULATED FOR RADIUS OF GYRATION AXIS 2-2.

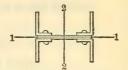
Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 \text{ L})^2}{36000 \text{ r}^2}}$ .



Size of Angles,	Size of Plates.	Weight of Column.	Area of Column Section.	Least Radius of Gyration Axis 1-1.	Radius of Gyration Axis 2-2.		engti Fee	t.
Inches.	Inches.	Lbs.per Ft.	Sq. Ins.	Inches.	Inches.	6	8	10
3 x 2½ x ¼	10 x 1/4 3/8 7/8 1/8 9 1/8 5/8	26.5 33.0 39.2 45.3 51.0 57.1 62.9	7.79 9.65 11.48 13.28 15.00 16.74 18.44	1.16 1.18 1.21 1.24 1.27 1.30 1.33	4.07 4.05 4.03 4.01 3.99 3.96 3.94	96 119 142 164 186 207 228	95 118 141 163 185 206 227	95 117 140 161 183 204 225
3/2 x 2/2 x /4 	10 x 1/4  16 05/8  17 16 16 16 16 16 16 16 16 16 16 16 16 16	28.1 35.0 41.6 48.1 54.6 60.7 67.3 73.4 79.1	8.25 10.24 12.19 14.15 16.00 17.86 19.69 21.53 23.25	1.39 1.42 1.45 1.48 1.51 1.54 1.57 1.60 1.63	4.13 4.11 4.09 4.07 4.05 4.03 4.01 3.99 3.97	102 127 151 175 198 221 244 266 288	102 126 150 174 197 220 242 264 286	101 125 149 172 195 218 240 262 283
4 x 3 x 5 6 8 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	12 x 5 6 8 8 7 6 8 7 6 1 1 2 9 1 5 8 8 1 6	41.6 49.3 57.1 64.8 72.6 79.9 87.3 94.6 101.6 108.9	12.11 14.48 16.77 19.00 21.27 23.48 25.61 27.75 29.86 31.94	1.58 1.61 1.64 1.66 1.69 1.72 1.75 1.78 1.81 1.84	4.91 4.89 4.87 4.85 4.83 4.81 4.79 4.77 4.74 4.72		150 179 207 235 262 290 317 343 369 395	149 178 206 234 261 288 315 341 367 392
5 x 3\frac{1}{2} x \frac{5}{3}\frac{6}\frac{6}{3}\frac{6}{3}\frac{6}{3}\frac{6}{3}\frac{6}{3}\frac{6}{3}\frac{6}{3}\frac{6}{3}\frac{6}{3}\frac{6}{3}\frac{6}{3}	14 x 5 6 / 6 / 6 / 2 6 / 8 / 8 / 8 / 8 / 8 / 8 / 8 / 8 / 8 /	49.7 59.5 68.8 78.2 87.6 96.9 105.9 114.9 123.9 132.5 141.4	14.61 17.44 20.24 23.00 25.78 28.48 31.15 33.79 36.36 38.98 41.49	1.98 2.01 2.04 2.07 2.09 2.12 2.15 2.18 2.21 2.24 2.27	5.77 5.75 5.73 5.71 5.69 5.67 5.64 5.62 5.60 5.58 5.56			180 215 250 284 318 351 384 417 449 481 512
6 x 3½ x 34	16 x 3/8 (1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	67.2 77.8 88.4 99.0 109.6 119.8 130.4 140.2 150.4 160.2 170.0	19.73 22.90 26.00 29.11 32.19 35.23 38.29 41.23 44.19 47.11 50.00	2.46 2.49 2.52 2.54 2.57 2.60 2.63 2.66 2.69 2.72 2.75	6.68 6.66 6.64 6.61 6.59 6.57 6.55 6.53 6.51 6.48 6.46			

CALCULATED FOR RADIUS OF GYRATION AXIS 2-2.

Based on Gordon's Formula P= $\frac{50\,000}{1+\frac{(12\,\mathrm{L})^2}{36\,000\,\mathrm{r}^2}}$ .



#### Length in Feet.

12	14	16	18	20	22	24	26	28	30	32	34	36	38	40
94	92	91	90	88	87	85	83	81	80	78	76	74	72	70
116	115	113	111	109	107	105	103	101	98	96	94	91	89	86
138	136	135	132	130	128	125	123	120	117	114	111	108	105	103
160	158	156	153	150	148	145	142	138	135	132	128	125	122	118
181	179	176	173	170	167	164	160	157	153	149	145	141	138	134
202	199	196	193	190	186	183	179	174	170	166	162	157	153	149
222	219	216	213	209	205	201	196	192	187	182	178	173	168	163
100	99	97	96	94	93	91	89	87	85	83	81	79	77	75
124	122	121	119	117	115	113	110	108	106	103	101	98	95	93
147	146	144	141	139	137	134	131	128	125	122	119	116	113	110
170	168	166	164	161	158	155	152	148	145	141	138	134	131	127
193	191	188	185	182	179	175	172	168	164	160	156	152	148	144
216	213	210	207	203	199	195	191	187	183	178	174	169	165	160
238	235	231	228	224	220	215	211	206	201	196	191	186	181	176
259	256	252	248	244	239	235	230	224	219	214	208	203	197	191
280	277	273	268	264	259	253	248	242	236	231	225	219	213	207
148	147	145	144	142	140	138	136	134	132	129	127	125	122	120
176	175	173	171	169	167	165	162	160	157	154	151	148	145	142
204	202	200	198	196	193	191	188	185	182	178	175	172	168	165
232	230	228	225	222	219	216	213	210	206	202	198	195	191	187
259	257	254	251	248	245	242	238	234	230	226	221	217	213	208
286	283	281	277	274	270	266	262	258	254	249	244	239	234	229
312	310	306	303	299	295	291	286	282	277	272	266	261	256	250
338	335	332	328	324	320	315	310	305	299	294	288	282	277	271
364	361	357	353	348	344	339	333	328	322	316	310	303	297	291
389	386	382	377	373	367	362	356	350	344	337	331	324	317	310
180	178	177	176	174	173	171	169	167	165	163	160	158	156	153
214	213	211	210	208	206	204	202	199	197	194	191	188	186	183
249	247	245	243	241	239	236	234	231	228	225	222	218	215	212
283	281	279	277	274	271	269	265	262	259	255	252	248	244	240
316	314	312	309	307	304	300	297	293	290	286	281	277	273	269
349	347	345	342	339	335	332	328	324	320	315	311	306	301	296
382	380	377	374	370	367	363	358	354	349	345	340	334	329	324
414	412	409	405	402	398	393	389	384	379	373	368	362	357	351
446	443	440	436	432	428	423	418	413	408	402	396	390	384	378
478	475	471	467	463	458	453	448	442	436	430	424	417	411	404
509	506	502	498	493	488	483	477	471	465	458	451	444	437	430
243	242	241	239	238	236	234	232	230	228	225	223	221	218	215
282	281	279	278	276	274	272	269	267	264	262	259	256	253	250
321	319	318	316	314	311	309	306	303	300	297	294	291	287	284
359	357	356	353	351	348	346	343	340	336	333	329	325	321	317
397	395	393	391	388	385	382	379	375	372	368	364	359	355	351
435	433	430	428	425	421	418	414	411	406	402	398	393	388	384
472	470	467	464	461	457	454	450	446	441	436	432	427	421	416
509	506	503	500	497	493	489	485	480	475	470	465	459	454	448
545	542	539	536	532	528	524	519	514	509	504	498	492	486	480
581	578	575	571	567	563	558	553	548	542	537	531	524	518	511
617	613	610	606	602	597	592	587	581	575	569	563	556	549	542

CALCULATED FOR RADIUS OF GYRATION
AXIS 2-2,

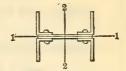
Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 L)^2}{36000 r^2}}$ .



D	arcty rac	101 4.		30 000 1		A	<u> </u>	
Size of Angles,	Size of Plates.	Weight of Column,	Area of Column	Least Radius of Gyration Axis 1-1.	Radius of Gyration Axis 2-2.		engtl Fee	
			Section,			- 0	0	10
Inches.	Inches.	Lbs.per Ft.	Sq. Ins.	Inches.	Inches.	6	8	10
3 x 2½ x ½ x ½ §	12 x 1/4	28.2 35.2 41.7 48.3 54.4 61.0 67.1	8.29 10.27 12.23 14.15 16.00 17.86 19.69	1.12 1.15 1.17 1.20 1.23 1.26 1.28	4.87 4.85 4.83 4.81 4.78 4.76 4.74	103 127 151 175 199 222 245	102 126 151 174 198 221 243	101 126 150 173 197 219 242
3½ x 2½ x ½	12 x 14	29.8 37.2 44.1 51.1 58.0 64.6 71.5 78.1 84.2	8.75 10.86 12.94 15.02 17.00 18.98 20.94 22.90 24.75	1.25 1.35 1.38 1.41 1.43 1.46 1.49 1.52 1.55 1.58	4.74 4.94 4.92 4.90 4.88 4.85 4.83 4.81 4.79 4.77		108 134 160 185 210 235 259 283 306	108 134 159 184 209 233 257 281 304
4 x 3 x 5 8 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	14 x 3/8 7/8 1/2 9/8 1	43.7 51.9 60.0 68.2 76.4 84.1 91.9 99.7 107.1 114.9	12.74 15.23 17.65 20.00 22.40 24.73 26.99 29.25 31.49 33.69	1.54 1.57 1.60 1.62 1.65 1.68 1.71 1.74 1.77	5.72 5.70 5.68 5.66 5.63 5.61 5.59 5.57 5.55		158 188 218 248 277 306 335 363 390 418	157 188 217 247 276 305 333 361 389 416
5 x 31/2 x 76 x 11/2 x 1	16 x 3/3/3/6 (10 10 10 10 10 10 10 10 10 10 10 10 10 1	51.8 62.0 71.8 81.6 91.4 101.2 110.6 120.0 129.4 138.4 147.8	15.23 18.19 21.11 24.00 26.90 29.73 32.52 35.29 37.98 40.73 43.36	1.94 1.97 2.00 2.02 2.05 2.08 2.11 2.11 2.17 2.19 2.22	6.59 6.57 6.54 6.52 6.50 6.48 6.46 6.44 6.39 6.37			189 225 261 297 333 368 402 436 470 504 537
6 x 3 ½ x 3/2 x 3/	18 x 3/8 (17 6 17 6 18 18 18 18 18 18 18 18 18 18 18 18 18	69.8 80.8 91.8 102.8 113.9 124.5 135.5 145.7 156.4 166.6 176.8	20.48 23.78 27.00 30.24 33.44 36.61 39.79 42.86 45.94 48.99 52.00	2 42 2.44 2.47 2.50 2.52 2.55 2.58 2.61 2.64 2.67 2.70	7.49 7.47 7.45 7.42 7.40 7.38 7.36 7.34 7.32 7.29 7.27			

### CALCULATED FOR RADIUS OF GYRATION AXIS 2-2.

Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 L)^2}{36000 r^2}}$ .

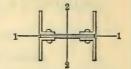


#### Length in Feet.

12	14	16	18	20	22	24	26	28	30	32	34	36	38	40
					22	~=	20	20	-50	-02	-01	-00	-00	-10
101	100	99	98	97	95	94	93	91	90	88	86	85	83	81
125 149	124 147	123 146	121	120	118	116	115 137	113	111 132	109	$\frac{107}{127}$	105   125	103	$\frac{101}{120}$
172	171	169	$\frac{144}{167}$	143 165	141 163	139 160	158	134 155	153	130 150	147	144	122 141	138
195	193	191	189	187	184	182	179	176	173	170	166	163	160	156
218	216	214	211	209	206	203	199	196	193	189	185	182	178	174
240	238	235	233	230	227	223	220	216	212	208	204	200	196	192
107	106	105	104	103	101	100	98	97	95	94	92	90	88	87
133 158	131 157	130 155	129 153	$\frac{127}{152}$	126 150	124 148	122 145	120 143	118 141	116 138	114 136	112 133	110 130	$\frac{107}{128}$
183	181	180	178	175	173	171	168	165	163	160	157	154	151	148
207	206	204	201	199	196	194	191	188	184	181	178	174	171	167
232	230	227	225	222	219	216	213	209	206	202	198	194	190	186
255 279	253 276	251 274	248 270	245 267	242 264	238 260	234 256	$\frac{231}{251}$	227 247	222 242	218 238	214 233	$\frac{210}{228}$	$\frac{205}{223}$
302	299	296	293	289	285	$\frac{280}{281}$	277	272	267	262	257	252	247	241
156	156	154	153	152	150	149	147	145	143	142	140	137	135	133
187	185	184	183	181	179	177	175	173	171	169	166	164	161	159
216	215	213	212	210	208	205	203	201	198	195	193	190	187	184
246 275	$\frac{244}{273}$	$   \begin{array}{c c}     242 \\     271   \end{array} $	240 269	238 266	236 263	233 261	231 258	228 254	225 251	222 248	218 244	215 240	212 236	208 233
303	301	299	296	294	291	288	284	281	277	273	269	265	$\frac{260}{261}$	$\frac{253}{257}$
331	329	327	324	321	318	314	311	307	303	298	294	289	285	280
359	357	354	351	348	344	340	336	332	328	323	318	313	308	303
$\frac{386}{413}$	384 411	381   407	378 404	374 400	370 396	366 392	362 387	357 382	352 377	347 371	342 366	337 360	331 354	326 348
188	187	186	185	184	182	181	179	178	176	174	172	170	168	166
224	223	222	221	219	218	216	214	212	210	208	205	203	201	198
260	259	258	256	254	252	250	248	246	243	241	238	235	233	230
296	295	293	291	289	287	285	282	279	277	274	271	267	264	261
331 366	330 364	328 362	326 360	324 357	321 355	318 352	316 349	313 345	309 342	306 338	303 334	299 330	295 326	292 322
400	399	396	394	391	388	385	381	378	374	370	365	361	357	352
435	432	430	427	424	421	417	414	410	405	401	396	392	387	382
468	466	463	460	457	453	450	445	441	437	432	427	422	416	411
502 534	499 532	496 529	493 525	489 521	486 517	481 513	477 508	472 503	467 498	462 492	457 487	451 481	446 475	440 468
253	252	251	250	248	247	245	244	242	240	238	236	234	232	229
294	293	291	290	288	287	285	283	281	279	276	274	272	269	266
334	333	331	330	328	326	324	322	319	317	314	312	309	306	303
374 414	373 412	371 410	369 408	367 406	365 404	363 401	360	358 395	355 392	352 389	349 385	346 382	342 378	339 374
414 453	451	410	447	445	404	439	398 436	433	429	426	422	418	414	410
492	490	488	485	483	480	477	473	470	466	462	458	453	449	444
530	528	526	523	520	517	514	510	506	502	498	493	489	484	479
568 606	566 603	563 601	561 598	558 595	554 591	551 587	547 583	542 578	538 574	533 569	529 563	524 558	518 552	513 547
643	641	638	634	631	$\frac{591}{627}$	623	618	614	609	603	598	592	586	580
		-000	,	-002	~_,	0201	010	011	0001					

## CALCULATED FOR RADIUS OF GYRATION AXIS 2-2.

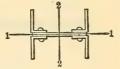
Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 \text{ L})^2}{36000 \text{ r}^2}}$ .



Size of Angles,	Size of Plates.	Weight of Column.	Area of Column Section.	Least Radius of Gyration Axis 1-1.	Radius of Gyration Axis 2-2.	Len in F	
Inches.	Inches.	Lbs.per Ft.	Sq. Ins.	Inches.	Inches.	10	12
7 x 3½ x 7 c 1/2 x 7 c 1/2 x 7 c 1/2 x 1/2 x 1/2 x 1/2 x 1/2 c 1/2	14 x x 7 8 2 9 6 8 9 16 8 16 16 16 16 16 16 16 16 16 16 16 16 16	80.8 91.8 103.2 113.7 124.7 135.3 145.9 156.5 166.6 176.8	23.78 27.00 30.24 33.48 36.61 39.79 .42.90 45.98 49.03 52.00	3.05 3.08 3.11 3.13 3.17 3.20 3.23 3.26 3.29 3.32	5.92 5.90 5.87 5.85 5.83 5.81 5.79 5.76 5.74 5.72	293 334 374 413 452 491 529 567 605 642	292 332 372 411 450 489 527 564 602 639
7 x 3½ x 7/16  11 11 16  11 11 16  11 11 16  11 11 16  11 11 16  11 11 16  11 11 16  11 11 16  11 11 16  11 11 16  11 11 16  11 11 16  11 11 16  11 11 16  11 11 16  11 11 16  11 11 16  11 11 16  11	16 x 76 29 6 8 16 8 16 16 16 16 16 16 16 16 16 16 16 16 16	83.8 95.2 107 0 118.0 129.4 140.4 151.4 162.4 173.0 183.6	24.65 28.00 31.36 34.73 37.98 41 29 44.52 47.73 50.90 54.00	3.00 3.02 3.06 3.08 3.11 3.14 3.17 3.20 3.23 3.26	6.75 6.73 6.71 6.69 6.67 6.64 6.62 6.60 6.58 6.56		304 346 387 428 469 509 549 588 627 666
7 x 3½ x 76 12 x 176	18 x 76 / 20 6 / 16 / 20 6 / 16 / 20 6 / 16 / 20 6 / 16 / 20 6 / 16 / 20 6 / 20	86.8 98.6 110.8 122.3 134.1 145.5 156.9 168.4 179.4 190.4	25.53 29.00 32.49 35.98 39.36 42.79 46.15 49.48 52.78 56.00	2.94 2.97 3.00 3.02 3.06 3.08 3.11 3.14 3.17 3.20	7.58 7.55 7.53 7.51 7.49 7.47 7.44 7.42 7.40 7.38		315 359 402 445 487 529 570 612 652 693
7 x 3½ x 7e 1/2 x 7e 1/2 x 1/2	20 x 75 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	89.8 102.0 114.7 126.5 138.7 150.6 162.5 174.3 185.8 197.2	26.40 30.00 33.61 37.23 40.73 44.29 47.77 51.23 54.65 58.00	2.89 2.92 2.95 2.97 3.00 3.03 3.06 3.09 3.12 3.15	8.39 8.37 8.34 8.32 8.30 8.28 8.25 8.23 8.21 8.19		

CALCULATED FOR RADIUS OF GYRATION AXIS 2-2.

Based on Gordon's Formula P= $\frac{50\,000}{1+\frac{(12\,\mathrm{L})^2}{36\,000\,\mathrm{r}^2}}$ .



#### Length in Feet.

14	16	18	20	22	24	26	28	30	32	34	36	38	40
290	288	286	284	281	278	275	272	269	266	262	258	255	251
330	328	325	323	320	317	313	310	306	302	298	294	289	285
370 409	367 406	364 403	361 399	358 396	354 392	351 387	347 383	342 378	338 373	333 368	329 363	324 358	$\frac{319}{352}$
447	444	441	437	433	429	424	419	414	408	403	397	391	385
486 523	482 520	478 516	474 511	470 506	465 501	460 496	455 490	449 484	443 477	$\frac{437}{471}$	$\frac{431}{464}$	424 457	418 450
561	557	553	548	543	537	531	525	518	511	504	497	489	482
598 635	594 630	589 <b>625</b>	584 620	578 614	572 607	566 600	559 593	552 586	545 <b>5</b> 78	537 570	529 561	521 553	513 544
302	301	299	297	295	293	290	288	285	282	279	276	273	270
344 385	342 383	340 381	338 379	336 376	333 373	330 370	327 366	324 363	321 359	$\frac{318}{355}$	$\frac{314}{352}$	$\frac{310}{347}$	$\frac{307}{343}$
426	424	421	419	416	412	409	405	401	397	393	389	384	379
467 507	464 504	461 501	458 498	455 494	451 490	448 486	443 481	439 477	$\frac{435}{472}$	$\frac{430}{467}$	$\frac{425}{461}$	420 456	415 450
546	543	540	536	532	528	524	519	514	509	503	497	491	485
586 624	582 621	579 617	575 613	571 609	566 604	561 598	556 593	551 587	545 581	539 574	533 568	526 561	520 554
663	659	655	651	646	641	635	629	623	616	609	602	595	588
314	313	312	310	308	306	304	302	300	297	295	292	290	287
358 401	356 399	354 397	353 395	351 393	348 390	$\frac{346}{388}$	344	341 382	338 379	335 376	$\frac{332}{372}$	329 369	326 365
443	441	439	437	434	432	429	426	422	419	415	411	408	403
485 527	483 525	481 522	478 519	476 516	473 513	469 51 <b>0</b>	466 506	462 502	459 498	455 493	450 489	446 484	442 479
568	566	563	560	557	553 593	550	546	541	537 575	532	527	522	517
609 650	607	604 644	601 641	597 637	593 633	589 628	585 624	580 619	575 613	570 608	565 602	559 596	554 590
690	687	684	680	676	672	667	662	657	651	645	639	633	626
326 371	325 370	324 368	322 367	321	319	317	315	313	311	309	307	305	302
415	414	412	411	365 409	363 407	361 404	359 402	357 399	354 397	352 394	349 391	346 388	344 385
460 503	458 502	456	454	452	450	447	445	442	439	436	432	429	426
547	545	500 543	498 541	495 538	493 535	490 532	487 529	484 526	$\frac{481}{522}$	477 518	473 514	470 510	466 506
590 633	588 630	585	583	580	577	574	570	567	563	559	554	550	545
675	672	628 670	625 667	622 664	619 660	615 656	612	608 648	603 644	599 639	594 634	590 629	585 623
717	714	711	708	705	701	697	693	688	683	678		667	662

### SAFE LOADS IN THOUSANDS OF POUNDS FOR Z-BAR COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 \cdot L)^2}{36000 r^2}}$ . Safety factor 4.



Section	Thickness of Web- plate and Z-Bars.	Area of Column Section.	Weight of Column per Foot.	Least Radius of Gyra- tion.		L,en	igth	in F	eet.	
Column.	Inches.	Sq. Ins.	Pounds.	Inches.	4	6	8	10	12	14
4-3" Z-Bars and Web-plate 534" wide.	1/4 5 16 3/8 7 16 1/2 916	9.31 11.72 13.59 15.97 17.62 19.97	31.7 39.7 46.1 54.2 59.8 67.8	1.86 1.91 1.88 1.93 1.90 1.95	114 144 167 196 216 245	112 141 163 192 212 240	108 137 158 187 206 234	104 132 153 180 198 226	100 126 146 173 190 216	95 121 139 165 181 207
4-4" Z-Bars and 1 Web-plate 634" wide,	1/4-16/87-6/9-16/81-6/4-16/9-16/9-16/9-16/9-16/9-16/9-16/9-16/9	11.31 14.22 17.16 19.14 22.00 24.89 26.41 29.22 32.06	38.5 48.4 58.2 65.2 74.7 84.5 89.9 99.4 109.2	2.46 2.51 2.56 2.49 2.54 2.59 2.52 2.57 2.62	140 176 212 237 272 308 327 362 397	138 174 210 234 269 505 323 358 392	135 171 207 230 265 300 317 352 386	132 167 202 225 259 293 310 344 379	129 163 197 219 253 287 302 336 369	125 158 191 213 245 279 293 327 360
4-5" Z-Bars and Web-plate 7" wide.	5 G C C G C C G C C C C C C C C C C C C	15.78 19.03 22.31 24.50 27.70 30.94 32.66 35.81 39.00	52.8 64.5 76.0 83.5 94.2 105.3 111.2 121.9 132.5	3.08 3.13 3.18 3.10 3.15 3.21 3.13 3.18 3.24		194 234 275 302 341 381 402 441 481	192 232 272 298 338 377 398 437 476	189 229 269 294 333 372 392 431 469	186 225 264 289 327 367 386 423 462	182 220 259 283 321 359 378 415 454
4-6" Z-Bars and 1 Web-plate 734" wide.	3/8-16/29/6-16/8-16/49/6-8	21.28 24.94 28.62 31.08 34.69 38.33 40.31 43.87 47.47	72.3 84.7 97.2 105.6 118.1 130.5 137.0 149.0 161.5	3.68 3.73 3.78 3.70 3.75 3.67 3.65 3.63		263 309 354 385 429 474 499 543 587	261 306 352 381 426 471 494 538 582	258 303 348 377 421 466 490 533 575	255 299 344 373 417 460 483 525 569	251 295 339 367 411 453 476 519 559

Thick-

### SAFE LOADS IN THOUSANDS OF POUNDS FOR Z-BAR COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 L)^2}{36000 r^2}}$  Safety factor 4.



			I.	engt	h in	Fee	et.				ness of Web- plate and Z-Bars.
16	18	20	22	24	26	28	30	32	34	36	Inches.
90 114 132 157 172 197	85 108 124 148 162 186	79 102 117 139 153 175			• • •						1/4 5 16 3/8 76 1/2 9
121 153 186 206 237 270 285 317 349	117 147 179 198 229 260 275 305 337	112 142 173 190 220 251 264 294 326	107 136 166 183 211 241 253 282 313	102 130 158 175 203 231 243 271 299	98 124 151 167 194 222 232 259 288						1/4 56 1/5 1/2 1/2 1/5 1/6 1/6 1/6 1/6 1/6 1/6 1/6 1/6 1/6 1/6
178 215 254 276 314 352 370 407 445	174 210 247 270 306 344 360 396 433	169 204 241 262 299 335 351 386 423	164 199 234 255 289 325 341 376 411	159 192 228 248 248 281 316 330 365 400	154 186 220 239 271 306 320 353 388	148 181 213 231 263 297 310 342 376	143 174 206 223 254 287 298 331 362	138 168 198 215 245 276 288 318 350	133 161 191 206 236 267 277 307 338		5 6 8 7 6 2 6 8 1 6 4 3 6 1 6 4 3 6 1 6 1 6 1 6 1 6 1 6 1 6 1 6 1 6 1 6
248 290 334 362 404 446 468 509 551	243 285 328 354 397 439 460 500 539	238 279 322 348 390 429 451 489 529	233 274 315 341 381 421 440 479 516	228 268 309 332 373 412 431 467 505	221 261 300 325 364 401 419 456 491	216 254 293 316 354 391 409 443 480	210 248 286 308 345 381 397 432 465	204 241 278 300 336 370 387 419 453	199 234 270 290 326 360 374 407 438	192 227 263 282 317 348 364 394 426	3/87 6/29 6/80-60/406/8

# SAFE LOADS IN THOUSANDS OF POUNDS FOR Z-BAR AND PLATE COLUMNS.

Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 L)^2}{36000 r^2}}$ . Safety Factor 4.



#### SQUARE ENDS.

Section of Column.	Thick- ness of Cover Plates.	Area of Column Section.	Weight of Column.	Least Radius of Gyra- tion	Length in Feet.  Les. 10 12 14 16 18 20  80 594 587 579 570 560 549 81 615 608 600 591 580 569 82 657 629 621 611 601 589 82 658 650 642 632 621 609 83 679 671 662 652 641 629 84 701 693 683 673 661 649 85 743 735 725 714 702 689 85 765 756 746 735 722 709  75 618 610 602 592 582 570 76 639 631 623 613 602 590 77 660 653 643 633 622 610 78 682 674 664 654 643 630 79 703 695 685 675 663 650 80 724 716 706 695 683 670 80 746 737 727 716 703 690						
	Inches.	Sq. Ins.	Lbs.per Ft.	Inches.	10	12	14	16	18	20	22
4 Z-Bars 61/8" x 35/8" x 1/16" and 1 Web-plate 73/4" x 1/16"	3/7-6/20-6/20-16/4006/20 15/1-0/1-0/1-17/	48.83 50.58 52.33 54.08 55.83 57.58 59.33 61.08 62.83	166.2 172.2 178.1 184.1 190.0 196.0 201.9 207.9 213.8	3.80 3.81 3.82 3.82 3.83 3.84 3.84 3.85 3.85	615 637 658 679 701 722 743	608 629 650 671 693 714 735	600 621 642 662 683 704 725	591 611 632 652 673 694 714	580 601 621 641 661 682 702	569 589 609 629 649 669 689	538 558 577 597 616 636 656 675 695
4 7-Bars 6" x 31/" x 3/4" and 1 Web-plate 73/4" x 3/4"	3/7-11/9-6/81-6/4-9-6/8	50.81 52.56 54.31 56.06 57.81 59.56 61.31 63.06 64.81	172.7 178.6 184.6 190.5 196.5 202.4 208.4 214.3 220.3	3.75 3.76 3.77 3.78 3.79 3.80 3.80 3.81 3.82	639 660 682 703 724	631 653 674 695 716	623 643 664 685 706	613 633 654 675 695	602 622 643 663 683	590 610 630 650 670	558 578 598 617 637 656 676 696 715
4 Z-Bars 6 16" x 3 16" x 13" 3 16" x 13" Web-plate 734" x 13"	33 7 6 22 6 8 16 4 6 8 1 1 1 7 8 1 1 1 1 7 8 1 1 1 1 7 8 1 1 1 1	54.37 56.12 57.87 59.62 61.37 63.12 64.87 66.62 68.37	184.7 190.7 196.6 202.6 208.5 214.5 220.4 226.4 232.3	3.73 3.74 3.75 3.76 3.77 3.78 3.78 3.79 3.80	661 682 703 725 746 768 789 810 832	653 674 695 716 737 758 780 801 822	643 664 685 706 727 748 769 790 811	633 654 674 695 716 736 757 777 798	622 642 662 683 703 723 744 764 784	610 630 650 670 690 709 729 749 769	597 616 636 656 675 695 714 734 754
4 Z-Bars 61/" x 35/8" x 7/8" and 1 Web-plate 73/4" x 7/8"	116	57.97 59.72 61.47 63.22 64.97 66.72 68.47 70.22 71.97	197.2 203.1 209 1 215.0 221.0 226.9 232.9 238.8 244.8	3.71 3.72 3.73 3.74 3.75 3.76 3.76 3.77 3.78	704 726 747 768 790 811 832 854 875	696 717 738 759 780 801 822 844 865	686 706 727 748 769 790 811 832 853	674 695 716 736 757 778 798 819 839	662 683 703 723 744 764 784 804 825	649 669 689 709 729 749 769 789 809	635 655 675 694 714 733 753 773 792

# SAFE LOADS IN THOUSANDS OF POUNDS FOR Z-BAR AND PLATE COLUMNS.

Based on Gordon's Formula  $P = \frac{50\,000}{1 + \frac{(12\,L)^2}{36\,000\,r^2}}$ . Safety factor 4.



#### SQUARE ENDS.

Length in Feet.												Thick- ness of Cover Plates.
24	26	28	30	32	34	36	38	40	42	44	46	Inches.
526 546 565 584 603 622 642 661 580 546 563 642 661 680 700	514 533 552 570 589 608 627 646 664 533 552 571 589 608 627 646 665 683	501 520 538 557 575 593 612 630 648 520 538 556 575 593 612 630 648 667	489 506 524 560 578 596 614 632 506 578 596 614 632 650	475 493 510 528 546 563 581 598 616 492 510 527 545 562 580 597 615	462 479 496 514 531 548 565 582 599 478 495 512 530 547 564 581 598 615	449 466 482 499 516 532 549 566 582 464 481 498 511 548 564 581	436 452 468 485 501 517 533 549 565 450 467 483 499 515 532 548 564 580	423 439 454 470 486 502 517 533 549 437 453 468 484 500 516 531 547 563	410 425 441 456 471 487 502 517 532 423 439 454 469 485 500 515 531 546	397 412 427 442 457 472 487 501 516 410 425 440 455 469 484 499 514 529	385 399 414 428 443 457 471 486 500 397 411 426 440 455 469 484 498 512	3/9-6/2-8-6/4-38/8 3/9-6/2-8-6/4-38/8 3/9-6/2-8-6/4-38/8
583 6022 6226 641 660 679 699 718 737 621 640 659 678 678 678 675 717	569 588 607 626 644 663 682 701 720 606 625 643 662 681 700 719 738 756	555 573 592 610 628 647 665 684 702 590 627 646 664 682 701 719 738	540 558 576 594 612 630 648 666 684 574 592 610 628 646 682 700 718	525 543 560 578 595 613 631 648 666 559 576 594 611 629 646 664 681 699	510 527 545 562 579 596 613 630 647 548 560 577 594 611 628 645 662 679	495 512 529 545 562 579 595 612 629 526 543 560 577 593 610 627 643 660	480 497 513 529 545 562 578 594 610 511 527 543 559 576 592 608 624 640	466 482 497 513 529 545 560 576 592 495 511 526 542 558 574 690 605 621	451 467 482 497 513 528 543 559 574 479 495 510 525 541 556 571 587 602	437 452 467 482 496 511 526 541 556 464 479 494 509 524 538 553 568 583	423 437 452 466 481 495 510 524 539 449 463 478 492 507 521 536 550 565	

Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 \text{ L})^2}{36000 \text{ r}^2}}$ . Safety factor 4.



Depth of Channels.	Weight of each Channel.	Area of Column Section.	Least Radius of Gyration.		Len	igth	in F	eet.	
Inches.	Lbs. per Foot.	Sq. Ins.	Inches.	4	6	8	10	12	14
6	8.0 10.5 13.0 15.5	4.76 6.18 7.64 9.12	2.34 2.21 2.13 2.06	59 76 94 112	58 75 93 110	57 73 90 107	55 71 88 104	54 69 85 100	52 67 81 96
7	9.75 12.25 14.75 17.25 19.75	5.70 $7.20$ $8.68$ $10.14$ $11.62$	2.72 2.59 2.50 2.44 2.39	71 89 107 125 144	70 88 106 124 142	69 87 104 121 139	68 85 102 119 136	66 83 99 116 132	65 81 96 112 128
8	11.25 13.75 16.25 18.75 21.25	$\begin{array}{c} 6.70 \\ 8.08 \\ 9.56 \\ 11.02 \\ 12.50 \end{array}$	3.11 2.99 2.89 2.82 2.77	\$3 100 119 137 155	83 99 117 135 153	82 98 116 134 151	80 97 114 131 149	79 95 112 128 145	77 93 109 125 142
.9	13.25 15.00 20.00 25.00	7.78 8.82 11.76 14.70	3.45 3.37 3.20 3.08		96 109 145 181	95 108 143 179	94 107 142 177	93 105 139 173	91 103 137 170
10	15.0 20.0 25.0 30.0 35.0	8.92 11.76 14.70 17.64 20.58	3.84 3.66 3.52 3.41 3.31		110 146 182 218 254	110 144 180 216 251	109 143 178 213 248	107 141 176 210 245	106 139 173 207 240
12	20.5 25.0 30.0 35.0 40.0	12.06 14.70 17.64 20.58 23.52	4.61 4.43 4.28 4.17 4.09			149 181 217 254 289	148 180 216 251 287	147 179 214 249 284	146 177 211 246 281
15 " " "	33.0 35.0 40.0 45.0 50.0 55.0	19.80 20.58 23.52 26.48 29.42 32.36	5.59 5.56 5.44 5.32 5.23 5.16			246 255 291 328 364 400	244 254 290 326 363 399	243 252 288 324 360 396	241 251 286 322 357 393

Based on Gordon's Formula  $P = \frac{50\,000}{1 + \frac{(12\ L)^2}{36\,000\,r^2}}$ . Safety factor 4.



,			Weight of each Channel.	Depth of Channels.					
16	18	20	22	24	26	28	30	Lbs. per Foot.	Inches.
50 64 78 92	48 61 74 88	46 58 71 83	44 55 67 78	42 52 63 74			• • •	8.0 10.5 13.0 15.5	6
63 78 93 108 123	61 76 90 104 119	58 73 86 100 113	56 70 83 96 108	54 67 79 92 104	52 64 76 87 98		• • • •	9.75 12.25 14.75 17.25 19.75	7  
76	74	72	70	68	65	63	61	11.25	8
90	88	86	83	80	78	75	72	13.75	
107	104	100	97	94	90	87	83	16.25	
122	118	115	111	107	103	99	95	18.75	
138	134	129	124	120	115	111	106	21.25	
90	88	86	84	82	80	77	75	13.25	9
101	99	97	94	92	90	87	84	15.00	
134	131	127	124	120	116	113	109	20.00	
166	162	157	153	149	143	139	134	25.00	
- 104	102	101	99	97	95	93	90	15.0	10
136	134	131	128	125	122	119	116	20.0	
170	166	163	159	155	151	146	143	25.0	
203	198	194	189	185	179	174	168	30.0	
236	230	225	219	213	207	201	194	35.0	
144	142	140	138	136	134	131	129	20.5	12
175	172	170	167	165	161	159	155	25.0	
209	206	203	200	196	192	187	184	30.0	
243	240	236	231	227	223	218	213	35.0	
277	273	268	263	258	253	248	243	40.0	
240	238	235	233	230	228	225	222	33.0	15
249	247	245	242	240	236	234	230	35.0	
284	282	279	276	273	269	266	262	40.0	
319	316	313	310	306	302	298	294	45.0	
354	352	348	344	339	334	329	325	50.0	
390	386	381	377	372	368	362	357	55.0	

Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 L)^2}{36000 r^2}}$ . Safety factor 4.



Depth of Channels.	Weight of each Channel.	Area of Column Section.	Least Radius of Gyration.	Length in Feet.					
Inches.	Lbs. per Foot.	Sq. Ins.	Inches.	32	34	36	38	40	
9	13.25 15.00 20.00 25.00	7.78 8.82 11.76 14.70	3.45 3.37 3.20 3.08	73 81 106 129	71 79 101 124				
10	15.0 20.0 25.0 30.0 35.0	8.92 11.76 14.70 17.64 20.58	3.84 3.66 3.52 3.41 3.31	87 113 138 163 188	85 109 134 158 183	83 106 130 153 176			
12,	20.5 25.0 30.0 35.0 40.0	12.06 14.70 17.64 20.58 23.52	4.61 4.43 4.28 4.17 4.09	127 152 180 208 236	124 149 176 203 231	121 146 172 199 224	119 142 167 193 218	116 139 164 188 212	
15	33.0 35.0 40.0 45.0 50.0 55.0	19.80 20.58 23.52 26.48 29.42 32.36	5.59 5.56 5 44 5.32 5.23 5.16	219 228 258 289 320 351	215 224 254 284 315 344	213 220 250 279 309 338	209 217 246 275 303 332	206 213 241 270 299 325	

For detail dimensions see page 204.

# SIZE OF LATTICE BARS TO BE USED WITH LATTICED CHANNEL COLUMNS.

Depth of Channels.	Dimensions Ba	s of Lattice	Weight of Lattice Bars per Foot.	Center of Hole to End of Bar. (a)	Distance Center to Center of Rivets, (d)		
Inches.	Inches.	Thickness. Inches.	Pounds.	Inches.	Maximum.	Minimum.	
6 7 8 9 10 12 15	$ \begin{array}{c} 1\frac{1}{2} \\ 1\frac{3}{4} \\ 2 \\ 2 \\ 2 \\ 2\frac{1}{4} \\ 2\frac{1}{2} \end{array} $	1/4/1/4 56 56 56 56 56 56 56 56 56 56 56 56 56	1.28 1.49 2.12 2.12 2.55 2.87 3.19	$1\frac{1}{8}$ $1\frac{1}{8}$ $1\frac{1}{4}$ $1\frac{1}{4}$ $1\frac{1}{4}$ $1\frac{1}{4}$ $1\frac{1}{2}$	$\begin{array}{c} 0'-11\frac{1}{2}''\\ 1'-1\frac{1}{2}''\\ 1'-3''\\ 1'-4\frac{1}{2}''\\ 1'-6\frac{1}{2}''\\ 1'-10\frac{1}{2}''\\ 2'-2\frac{1}{2}''\\ \end{array}$	65 // 75 8 // 81 8 // 91 2 // 101 8 // 13 // 15 5 //	

Based on Gerdon's Formula  $P = \frac{50000}{1 + \frac{(12 L)^2}{36000 r^2}}$ . Safety factor 4.



			Weight of each Channel.	Depth of Channels.				
42	44	46	48	50	52	54	Lbs. per Foot.	Inches.
							13.25 15.00 20.00 25.00	9 "
							15.0 20.0 25.0 30.0 35.0	10
113 135 159 183 206	111 132 155 178 200	108 128 151 173 196					20.5 25.0 30.0 35.0 40.0	12,
202 210 238 265 293 319	199 206 233 260 287 314	195 203 228 255 281 307	192 199 224 250 275 301	188 194 220 245 269 294	184 191 215 239 264 287	181 187 211 234 258 281	33.0 35.0 40.0 45.0 50.0 55.0	15

For detail dimensions see page 204.

# SIZE OF STAY PLATES TO BE USED WITH LATTICED CHANNEL COLUMNS.

Minis Plates b	mum Size of Sat Ends of Col	Stay umns.	Weight of Minimum Stay Plates.	Diameter of Rivets.	0 0 b-	0 1
					101	
Inches.	Inches.	Inches.	Pounds.	Inches.	Oil	
8 <sup>1</sup> / <sub>4</sub> 9 <sup>1</sup> / <sub>4</sub> 10 <sup>1</sup> / <sub>2</sub> 11 <sup>1</sup> / <sub>4</sub> 12 <sup>1</sup> / <sub>4</sub> 14 <sup>1</sup> / <sub>4</sub> 16 <sup>1</sup> / <sub>4</sub>	1/4 1/4 1/6 1/6 1/6 1/6 1/6 3/8 3/8	$7\frac{1}{2}$ $10$ $9$ $12$ $12$ $15$ $15$	4.38 6.55 8.37 11.95 15.62 22.73 25.90	5/8/5/8/4/4/4/4/4/4/4/4/4/4/4/4/4/4/4/4/	6	d

### SAFE LOADS IN THOUSANDS OF POUNDS FOR 6" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 L)^2}{35000 r^2}}$ . Safety factor 4.



#### SERIES A.

Weight of each Channel.	Thickness of Plates.	Weight of Column.	Area of Column Section.	Least Radius of Gyration.	L,e	Length in Feet.					
Lbs. per Foot.	Inches,	Lbs.per Ft.	Sq. Ins.	Inches.	4	6	8	10			
8	1/4 5 6 6 8 7 1 6 7 1 7 6 1 2 9 6 8	29.6 33.0 36.4 39.8 43.2 46.6 50.0	8.76 9.76 10.76 11.76 12.76 13.76 14.76	2.35 2.35 2.34 2.34 2.34 2.34 2.33	108 121 133 145 158 170 182	107 119 131 143 155 167 180	105 117 129 141 152 164 176	102 114 125 137 149 160 172			
10.5	1/4 5 6 8 7 6 12 9 6 8	34.6 38.0 41.4 44.8 48.2 51.6 55.0	10.18 11.18 12.18 13.18 14.18 15.18 16.18	2.27 2.27 2.28 2.28 2.28 2.28 2.28 2.28	126 138 150 163 175 187 200	124 136 148 160 173 185 197	121 133 145 157 169 181 193	118 130 141 153 165 176 188			
13	1/4 5/6 3/8 7/6 11/2 9/6 5/8	39.6 43.0 46.4 49.8 53.2 56.6 60.0	11.64 12.64 13.64 14.64 15.64 16.64 17.64	2.20 2.21 2.22 2.23 2.23 2.24 2.24	144 156 168 181 193 205 218	141 154 166 178 190 202 214	138 150 162 174 186 198 210	135 146 158 169 181 192 204			
15.5	1/4 5/6 3/8 7/6 1/2 1/2 1/6 5/8	44.6 48.0 51.4 54.8 58.2 61.6 65.0	13.12 14.12 15.12 16.12 17.12 18.12 19.12	2.14 2.15 2.16 2.17 2.18 2.19 2.19	162 174 186 199 211 224 236	159 171 183 195 207 220 232	155 167 179 191 203 215 227	151 162 174 186 197 209 220			

### SAFE LOADS IN THOUSANDS OF POUNDS FOR 6" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 L)^2}{36000 r^2}}$ . Safety factor 4.



#### SERIES A.

·			Thickness of Plates.	Weight of each Channel.				
12	14	16	18	20	22	24	Inches.	Lbs. per Foot.
99 111 122 133 144 156 166	96 107 118 128 139 150 161	92 103 114 124 135 145 155	89 99 109 119 129 139 149	85 95 104 114 124 133 142	81 90 99 109 118 127 136	77 86 94 103 112 121 130	1/4 5-6 5-8 7-6 1-6 29-6 5-8	8
114 126 137 148 159 171 182	110 121 133 143 154 165 176	106 117 127 138 148 159 169	102 112 122 132 142 152 162	97 107 116 126 135 144 154	92 102 111 120 130 139 148	88 96 106 114 123 132 140	1/4/5/6/00/7/16/29/6/00	10.5
130 141 153 164 175 186 197	125 136 147 158 169 179 190	120 131 141 152 162 173 183	115 125 135 145 155 166 176	109 119 129 138 148 158 167	104 113 122 131 140 150 159	99 107 116 125 133 143 151	1/4-6-8-8-7-11-1-2-9-8-8-8	13
146 157 170 180 191 202 213	140 151 162 172 184 195 205	134 145 155 165 176 187 197	128 138 148 158 168 178 188	122 131 140 150 160 170 180	115 125 133 143 152 162 171	109 118 127 135 144 153 161	1/4 5/6 5/8 7/6 1/2 9/16 5/8	15.5

### SAFE LOADS IN THOUSANDS OF POUNDS FOR 7" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 L)^2}{36000 r^2}}$ . Safety factor 4.



#### SERIES A.

Weight of each Channel.	Thickness of Plates.	Weight of Column.	Area of Column Section.	Least Radius of Gyration.	L,e	ength	in Fe	eet.
Lbs. per Foot.	Inches.	Lbs.per Ft.	Sq. Ins.	Inches.	4	6	8	10
9.75	1/4/5/68/88/7/61/29/16/5/8	34.8 38.6 42.5 46.3 50.1 53.9 57.8	10.20 11.32 12.45 13.58 14.70 15.82 16.95	2.63 2.63 2.62 2.62 2.62 2.62 2.62 2.62	126 140 154 168 182 196 210	125 139 152 166 180 194 207	123 137 150 163 177 190 204	121 134 147 160 174 187 200
12.25	1/4 56 8/8 7/6 1/2 9/6 5/8	39.8 43.6 47.5 51.3 55.1 58.9 62.8	11.70 12.82 13.95 15.08 16.20 17.32 18.45	2.55 2.56 2.56 2.56 2.57 2.57 2.57	145 159 173 187 200 214 228	143 157 171 185 198 212 225	141 154 168 182 195 208 222	138 151 164 178 191 204 217
14.75	1/4 5/6 5/8 7/6 1/2 9/16 5/8	44.8 48.6 52.5 56.3 60.1 63.9 67.8	13.18 14.30 15.43 16.56 17.68 18.80 19.93	2.49 2.50 2.50 2.51 2.52 2.52 2.53	163 177 191 205 219 233 247	161 175 189 202 216 230 244	158 172 185 199 212 226 239	155 168 181 195 208 221 234
17.25 " " "	1/4 56 3/8 7/6 11/2 9/15/8	49.8 53.6 57.5 61.3 65.1 68.9 72.8	14.64 15.76 16.89 18.02 19.14 20.26 21.39	2.42 2.43 2.45 2.46 2.46 2.47 2.48	181 195 209 223 237 251 265	178 192 206 220 234 248 261	175 189 202 216 229 243 257	171 185 198 211 224 238 251
19.75	1/4 5/6 3/8 7/6 1/2 9/6 5/8	54.8 58.6 62.5 66.3 70.1 73.9 77.8	16.12 17.24 18.37 19.50 20.62 21.74 22.87	2.37 2.38 2.40 2.41 2.42 2.43 2.44	199 213 227 241 255 269 283	197 210 224 238 251 265 279	193 206 220 234 247 260 274	188 201 214 228 242 255 268

### SAFE LOADS IN THOUSANDS OF POUNDS FOR 7" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 L)^2}{36000 r^2}}$ . Safety factor 4.



#### SERIES A.

		1	Lengt	h in I	Feet.			Thickness of Plates.	Weight of each Channel,
12	14	16	18	20	22	24	26	Inches.	Lbs.per Ft.
118 130 143 156 169 182 195	115 127 140 153 165 178 190	111 123 135 148 160 172 184	108 119 131 143 154 166 178	104 1 138 149 161 172	99 1 0 1 1 132 143 154 165	96 106 116 127 137 148 158	92 102 112 122 132 142 152	1/4 568 3/8 716/298 115/8	9.75
134 147 160 173 186 199 212	130 143 156 168 181 194 207	126 139 151 163 176 188 200	122 134 146 158 169 181 193	118 129 140 152 163 174 185	113 124 135 1 5 1 6	108 118 129 39 .50 .61 171	103 113 123 133 144 154 164	1/4/56/87/19/29/29/19/29/29/29/29/29/29/29/29/29/29/29/29/29	12.25
151 164 177 190 202 215 229	146 159 171 184 196 209 222	142 154 166 178 191 203 215	136 148 160 171 184 196 207	131 142 154 165 177 188 199	126 136 147 158 170 180 191	120 131 141 151 162 173 183	115 125 135 144 155 165 175	1/4 5 16 30 8 16 16 16 16 16 16 16 16 16 16	14.75
166 180 193 206 218 231 245	161 174 187 199 212 224 238	156 168 181 193 205 217 229	150 162 174 186 197 209 220	143 155 166 178 190 201 212	137 148 159 171 182 192 203	131 142 153 163 173 184 194	126 135 146 155 165 176 186	1/4 5/6 37/8 7/6 1/22 9/16/8	17.25
183 196 209 222 234 248 261	177 189 202 215 227 240 253	170 183 195 208 220 231 243	164 175 187 199 211 223 235	157 168 180 191 202 214 225	150 161 172 183 194 204 216	143 153 164 174 185 195 207	136 146 157 166 177 186 196	1/4 16 3/8 76/2 15/8	19.75

### SAFE LOADS IN THOUSANDS OF POUNDS FOR 8" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$  Safety factor 4.



#### SERIES A.

Weight of each Channel.	Thickness of Plates.	Weight of Column.	Area of Column Section.	Least Radius of Gyration.	Le	engtl	n in	Fee	t.
Lbs. per Foot.	Inches.	Lbs.per Ft.	Sq. Ins.	Inches.	4	6	8	10	12
11.25	1/4/5/6/8/7/14/2/9/6/8	39.5 43.7 48.0 52.3 56.5 60.8 65.0	11.70 12.95 14.20 15.45 16.70 17.95 19.20	2.98 2.97 2.97 2.96 2.95 2.95 2.95	145 161 176 192 207 223 238	144 159 175 190 205 221 236	142 157 172 188 203 219 233	140 155 170 185 200 214 229	137 152 167 181 196 210 225
13.75	1/45/6/897/6/20/6/89	44.5 48.7 53.0 57.3 61.5 65.8 70.0	13.08 14.33 15.58 16.83 18.08 19.33 20.58	2.92 2.92 2.92 2.91 2.91 2.91 2.91	162 178 193 209 224 240 255	161 176 191 207 222 237 253	159 174 189 204 220 235 250	156 171 186 201 216 231 246	153 168 182 197 212 226 241
16.25	1/4 56/8 711/29/6/8	49.5 53.7 58.0 62.3 66.5 70.8 75.0	14.56 15.81 17.06 18.31 19.56 20.81 22.06	2.86 2.87 2.87 2.87 2.87 2.87 2.87	181 196 212 227 243 258 274	179 194 210 225 240 256 271	176 192 207 222 237 252 267	173 188 203 218 233 248 263	170 185 199 214 228 243 258
18.75	1/4 5 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6	54.5 58.7 63.0 67.3 71.5 75.8 80.0	16.02 17.27 18.52 19.77 21.02 22.27 23.52	2.81 2.81 2.82 2.82 2.83 2.83 2.83	199 214 230 245 261 276 292	197 212 227 243 258 274 289	194 209 224 240 255 270 285	190 205 221 236 250 265 280	186 201 216 230 245 260 275
21.25	1/4-5/6/8 7-6/8 11/2/9/6/8	59.5 63.7 68.0 72.3 76.5 80.8 85.0	17.50 18.75 20.00 21.25 22.50 23.75 25.00	2.76 2.77 2.77 2.78 2.79 2.79 2.80	217 233 248 264 279 295 310	215 230 245 261 276 291 307	212 227 242 257 272 287 302	208 223 238 253 267 282 297	204 218 233 247 262 276 291

### SAFE LOADS IN THOUSANDS OF POUNDS FOR 8" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50\,000}{1 + \frac{(12\,L)^2}{36\,000\,r^2}}$  Safety factor 4.



#### SERIES A.

	,	1		Thickness of Plates,	Weight of each Channel.					
14	16	18	20	30	Inches.	Lbs.per Ft.				
134 149 163 177 192 206 221	131 145 159 173 187 201 215	128 141 154 168 182 195 209	124 137 150 163 176 189 203	120 133 146 158 170 183 196	116 128 141 153 165 178 190	112 124 136 147 159 171 183	108 120 131 142 153 165 177	104 115 126 137 147 158 169	1/4 5 6 8 7 6 1 2 9 1 5 8	11.25
150 164 178 193 207 221 236	146 160 174 188 202 216 229	142 155 169 182 196 209 223	138 151 164 177 190 203 216	133 146 159 171 184 196 209	129 141 153 166 178 190 203	124 136 148 160 172 183 195	119 131 142 153 164 176 187	115 126 137 148 159 170 181	1/4 56 30,8 76 129 15,8	13.75
166 180 195 209 223 237 252	162 176 189 203 217 231 245	157 171 184 198 211 224 238	152 165 178 191 204 217 231	147 160 172 185 198 210 223	142 154 166 178 191 203 215	137 148 160 172 184 195 207	131 143 154 165 177 188 199	126 137 148 159 170 181 191	1/4 5 16 3/8 7/6 1/2 1/6 5/8	16.25
182 196 210 225 240 254 268	177 191 205 219 233 246 260	172 185 199 212 226 239 253	167 180 193 206 219 232 245	161 174 186 199 211 224 236	155 167 180 192 204 216 228	149 160 173 185 196 208 220	143 154 166 178 189 200 211	137 148 160 171 181 192 203	1/4 5 16 3/8 7/6 1/2 1/6 1/2 1/6 5/8	18.75
198 212 226 241 256 270 284	193 207 220 234 249 263 277	187 200 214 227 241 254 268	181 194 207 220 233 246 260	174 187 200 213 225 238 250	168 180 192 205 217 229 241	162 173 185 196 209 221 232	155 166 178 189 201 212 223	148 159 170 181 192 202 214	1/4 5 6 /8 7 6 /2 9 6 /8 15 /8	21.25

### SAFE LOADS IN THOUSANDS OF POUNDS FOR 9" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 L)^2}{36000 r^2}}$ . Safety factor 4.



#### SERIES A.

Weight of each	Thick- ness of	Weight	Area of Column	Least Radius of		I,er	igth	in F	eet.	
Channel.	Plates.	Column.	Section.	Gyration.						
Lbs.perFt.	Inches.	Lbs.per Ft.	Sq. Ins.	Inches.	6	8	10	12	14	16
13.25	1/4 5 16 3/8 76 1/2 9 16 5/8	45.2 49.9 54.6 59.2 63.9 68.5 73.3	13.28 14.66 16.03 17.40 18.78 20.16 21.53	3.34 3.32 3.31 3.30 3.29 3.28 3.28	164 181 198 215 232 249 266	162 179 196 213 229 246 263	160 177 193 210 227 243 260	158 174 191 207 223 239 255	155 171 187 203 219 235 251	152 168 183 199 214 230 246
15	1/4 5 16 3/8 7/6 1/2 9/6 1/5/8	48.7 53.4 58.1 62.7 67.4 72.0 76.8	14.32 15.70 17.07 18.44 19.82 21.20 22.57	3.29 3.28 3.28 3.27 3.26 3.26 3.25	177 194 211 228 245 262 279	175 192 209 225 242 259 275	173 189 206 222 239 255 272	170 186 202 219 235 251 267	167 183 199 215 231 247 263	163 179 195 210 226 242 257
20	1/4 5-6 3/8 7-6 1/2 9-6 1/2 9-6 5/8	58.7 63.4 68.1 72.7 77.4 82.0 86.8	17.26 18.64 20.01 21.38 22.76 24.14 25.51	3.19 3.19 3.19 3.19 3.19 3.19 3.18	213 230 247 263 280 297 314	210 227 244 261 278 294 311	208 224 241 257 274 291 307	204 220 236 253 269 285 301	200 216 232 248 264 280 296	196 212 227 243 259 274 290
25	1/4 5/6 8/7/6/2 1/2 9/6/8	68.7 73.4 78.1 82.7 87.4 92.0 96.8	20.20 21.58 22.95 24.32 25.70 27.08 28.45	3.10 3.11 3.11 3.12 3.12 3.12 3.12	249 266 283 300 317 334 351	246 263 279 296 313 330 346	243 259 276 292 309 325 342	238 254 270 287 304 320 336	234 250 265 281 297 313 329	228 244 260 275 291 307 322

### SAFE LOADS IN THOUSANDS OF POUNDS FOR 9" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 L)^2}{36000 r^2}}$ . Safety factor 4.



#### SERIES A.

		]		Thickness	Weight of each					
									Plates.	Channel.
18	20	22	24	26	28	30	32	34	Inches.	Lbs.per Ft.
149 164 179 194 209 225 240	145 160 175 189 204 219 234	141 156 171 184 199 214 228	137 152 165 179 194 208 222	134 147 160 174 188 202 215	129 143 155 169 182 195 209	125 138 150 163 176 189 202	121 134 146 158 171 182 194	117 129 141 153 165 176 188	1/4 56 87 67 67 96 8	13,25
160 175 190 206 221 236 252	156 171 186 201 216 231 245	152 166 181 195 210 225 238	148 162 176 190 203 217 231	143 157 171 184 197 211 225	139 152 166 178 191 204 218	134 147 160 172 185 198 211	130 142 154 167 179 191 204	126 137 149 161 173 185 196	1/4 56 3/8 76 1/2 9 16 5/8	15
192 207 222 237 253 268 282	186 201 216 231 246 260 275	181 196 210 224 239 253 268	176 190 204 218 232 246 260	170 184 197 211 224 238 251	165 178 191 204 217 230 243	159 172 185 197 210 223 236	154 166 179 191 203 216 226	148 160 172 183 195 207 219	1/4- 	20
223 238 253 268 283 298 313	216 232 246 261 276 291 306	210 224 239 253 267 282 296	204 218 232 246 260 274 287	197 210 224 238 252 265 279	191 204 217 230 243 256 269	183 197 210 222 235 247 260	177 189 201 213 226 238 250	170 183 194 206 218 229 241	1/4 5 16 3/8 76 1/2 96 15/8	25   

### SAFE LOADS IN THOUSANDS OF POUNDS FOR 10" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$ . Safety factor 4.



#### SERIES A.

Weight of each Channel.	Thick- ness of Plates.	Weight of Column.	Area of Column Section.	Least Radius of Gyration.		L,en	gth	in F	eet.	
Lbs.per Ft.	Inches.	Lbs.per Ft.	Sq. Ins.	Inches.	6	8	10	12	14	16
15	1/4 5/6 8/8 7/6 1/2 9/16/8	50.4 55.5 60.6 65.7 70.8 75.9 81.0	14.92 16.42 17.92 19.42 20.92 22.42 23.92	3.62 3.61 3.59 3.58 3.58 3.57 3.56	184 203 221 240 259 277 296	183 201 220 238 257 275 293	181 199 217 235 254 272 290	179 197 215 232 250 268 286	176 193 211 229 247 264 282	173 191 207 225 242 259 277
20	1/4 5 16/8 7 16/2 9 16/8	60.4 65.5 70.6 75.7 80.8 85.9 91.0	17.76 19.26 20.76 22.26 23.76 25.26 26.76	3.52 3.52 3.51 3.51 3.51 3.50 3.50	219 238 257 275 294 312 331	217 236 254 272 291 309 328	215 233 252 270 288 305 324	212 230 248 266 284 302 320	209 226 244 262 279 297 314	205 223 239 257 274 291 308
25	1/4 5 6 8 7 6 1/2 9 1 5/8	70.4 75.5 80.6 85.7 90.8 95.9 101.0	20.70 22.20 23.70 25.20 26.70 28.20 29.70	3.42 3.43 3.43 3.43 3.43 3.44 3.44	255 274 293 311 330 348 367	253 272 290 308 327 345 364	250 268 287 305 323 341 359	247 265 282 300 318 336 355	242 260 278 295 313 330 348	238 255 272 289 307 324 341
30  	1/4 5/6 1/2 9/6 1/2 9/6 8/8	80.4 85.5 90.6 95.7 100.8 105.9 111.0	23.64 25.14 26.64 28.14 29.64 31.14 32.64	3.33 3.34 3.35 3.36 3.36 3.37 3.37	292 310 329 347 366 384 403	289 307 325 344 362 380 399	285 303 321 340 358 376 394	281 299 317 334 352 370 388	276 294 311 329 346 364 381	271 288 305 322 339 358 375
35  	1/4 5 6 8 8 7 6 1/2 9 6 5/8	90.4 95.5 100.6 105.7 110.8 115.9 121.0	26.58 28.08 29.58 31.08 32.58 34.08 35.58	3.26 3.27 3.28 3.29 3.29 3.30 3.31	328 347 365 384 402 421 439	324 343 361 380 398 416 435	320 338 357 375 393 411 429	315 333 351 369 387 405 423	309 327 344 362 379 398 415	303 320 337 354 372 390 407

### SAFE LOADS IN THOUSANDS OF POUNDS FOR 10" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50\,000}{1 + \frac{(12\,L)^2}{36\,000\,r^2}}$ . Safety factor 4.



#### SERIES A.

			Thick- ness of Plates.	Weight of each Channel.							
18	20	22	24	26	28	30	32	34	36	Inches.	Lbs.per Ft.
170 187 204 221 238 255 271	166 183 199 216 232 249 266	162 179 195 211 228 243 259	159 175 190 206 222 238 253	154 170 186 200 216 231 246	151 165 180 195 210 225 239	146 161 175 189 204 219 233	142 156 170 184 199 212 226	138 152 165 178 192 206 218	134 147 160 172 186 199 212	1/4 5/6 3/8 7/6 1/2 9/16 5/8	15
201 218 235 252 269 286 303	196 213 230 246 263 279 296	192 208 224 240 256 272 289	187 203 219 235 251 265 281	182 197 213 228 244 259 274	177 192 207 222 236 251 266	172 187 201 216 230 244 258	167 181 195 209 223 237 251	161 175 189 202 216 229 243	157 170 182 195 209 222 235	1/4 5 16 3/8 76 1/2 9 16/8	20  
233 250 267 284 301 318 335	228 245 261 278 294 311 327	222 238 255 271 287 303 319	216 232 248 263 279 295 310	210 225 241 256 271 286 302	204 219 233 248 263 279 294	198 213 227 242 256 271 285	191 206 220 234 248 262 276	186 199 213 226 240 253 267	180 193 206 219 232 245 258	1/4 5 6 8/8 7 6 1/2 9 16/8	25   
265 281 298 315 332 350 367	258 275 291 307 324 342 358	252 268 284 301 317 333 349	245 260 276 293 308 324 339	238 253 268 284 299 315 330	230 245 260 276 290 305 320	223 237 252 267 281 296 310	216 230 243 258 272 286 300	209 222 237 250 263 276 290	201 214 228 241 254 267 280	1/4 5 6 8 7 6 1/2 9 6 5/8	30 " " " "
296 313 330 347 363 380 398	289 306 322 338 354 371 389	282 298 313 329 345 361 379	273 289 305 320 336 351 367	265 279 296 311 326 341 356	256 271 287 301 316 330 345	248 262 278 292 306 320 334	240 254 267 282 296 310 323	232 245 258 273 286 299 312	224 237 249 263 276 289 301	1/4 5/6/8 7/6/29/6/8	85   

### SAFE LOADS IN THOUSANDS OF POUNDS FOR 12" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 L)^2}{36000 r^2}}$ . Safety factor 4.



#### SERIES A.

Weight of each Channel.	Thick- ness of Plates.	Weight of Column.	Area of Column Section.	Least Radius of Gyration.		L,eı	ngtl	h ii	n IF	'eet		
Lbs.per Ft.	Inches.	Lbs.per Ft.	Sq. Ins.	Inches.	8	10	12	14	16	18	20	22
20.5	1/4 5/6 3/8 7/6 1/2 9/16/8	64.8 70.8 76.7 82.7 88.6 94.6 100.5	19.06 20.81 22.56 24.31 26.06 27.81 29.56	4.41 4.38 4.36 4.34 4.32 4.30 4.28	235 257 278 300 321 343 364	233 255 276 298 319 340 362	232 253 273 295 316 337 358	229 250 271 292 313 333 354	227 247 267 288 309 330 350	223 244 264 285 304 325 345	220 240 260 280 300 319 339	217 236 256 275 295 315 335
25	1/4 5/6 8/8 7/6 1/2 9/16/8	73.8 79.8 85.7 91.7 97.6 103.6 109.5	21.70 23.45 25.20 26.95 28.70 30.45 32.20	4.35 4.32 4.31 4.29 4.27 4.26 4.25	268 289 311 332 354 375 397	266 287 308 330 351 373 393	263 284 305 327 348 369 390	261 282 303 323 344 365 586	257 278 299 319 340 360 381	254 274 294 315 335 356 376	250 270 290 310 330 350 370	246 266 285 305 324 343 363
30	1/4 5 16 3/8 7 16 1/2 9 16/8	83.8 89.8 95.7 101.7 107.6 113.6 119.5	24.64 26.39 28.14 29.89 31.64 33.39 35.14	4.27 4.26 4.25 4.23 4.22 4.21 4.21	304 325 347 368 390 411 433	302 323 344 365 387 408 429	299 320 341 362 383 404 425	295 316 337 358 379 400 421	292 312 333 353 374 395 415	288 308 329 348 368 389 409	283 303 323 343 363 382 402	278 298 317 337 357 377 396
35	1/4 5 16/8 7/6 1/2 9/16/8	93.8 99.8 105.7 111.7 117.6 123.6 129.5	27.58 29.33 31.08 32.83 34.58 36.33 38.08	4.19 4.18 4.18 4.17 4.16 4.16 4.15	340 361 383 405 426 448 469	337 358 380 401 422 444 465	334 355 376 397 418 439 461	330 351 372 392 413 434 455	326 347 367 388 409 429 449	321 341 362 382 402 423 443	316 336 356 376 396 416 436	310 330 349 369 389 408 428
40	1/4 5/6 3/8 7/6 1/2 9/6/8	103.8 109.8 115.7 121.7 127.6 133.6 139.5	30.52 32.27 34.02 35.77 37.52 39.27 41.02	4.13 4.12 4.12 4.12 4.11 4.11 4.11	376 398 419 441 462 484 505	373 394 416 437 458 480 501	369 390 411 433 454 475 496	365 386 406 427 448 469 490	360 380 401 421 442 463 483	354 374 395 415 435 456 476	349 368 388 408 428 448 468	343 363 382 402 420 440 459

### SAFE LOADS IN THOUSANDS OF POUNDS FOR 12" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$ . Safety factor 4.



#### SERIES A.

				L,e1	ıgth	i11 I	Feet.				Thick- ness of Plates.	Weight of each Channel.
24	26	28	30	32	34	36	38	40	42	44	Inches.	Lbs.per Ft.
213 232 252 271 289 309 328	209 228 246 266 285 304 322	206 223 242 260 279 297 316	201 220 237 255 274 291 309	196 214 232 249 267 285 302	193 209 227 244 261 278 296	188 205 221 238 255 271 288	184 200 216 232 249 265 281	179 195 211 227 242 258 274	175 190 206 223 237 251 267	170 186 200 216 230 245 259	1/4 5 16 3/8 7 16 1/2 9 16 5/8	20.5
242 260 280 299 319 338 358	237 256 275 293 312 331 350	233 251 269 288 306 324 343	228 246 263 282 300 318 335	223 240 258 275 293 311 329	218 235 252 270 286 303 320	213 230 246 263 280 295 312	208 224 241 256 272 289 306	203 218 234 250 265 281 297	197 213 229 243 259 273 289	193 207 222 237 252 267 281	1/4 5 16/8/8 7 16/2 9 16/8	25
274 293 313 331 350 369 389	268 287 306 325 343 362 381	262 281 300 318 337 354 372	257 276 293 311 329 347 365	251 269 287 304 321 339 357	245 263 280 297 313 331 348	240 256 273 290 307 322 339	234 250 267 282 299 315 332	228 244 260 275 291 307 323	223 237 253 268 282 298 314	216 232 246 261 276 290 305	1/4 5 16 3/8 7 16 1/2 9 16/8	30  
305 324 344 362 381 400 420	299 318 337 356 375 394 411	292 311 329 348 366 385 404	286 304 322 340 358 376 394	280 296 314 332 349 367 385	273 290 308 323 341 358 375	266 283 300 317 332 349 365	259 275 292 308 325 341 356	253 268 284 300 316 332 348	246 262 277 291 307 323 338	239 254 270 283 298 313 328	1/4 5 16 3/8 7 16 1/2 9 16 5/8	35   
336 356 375 394 413 433 452	329 348 367 386 405 424 442	322 340 359 377 396 412 433	314 333 351 369 387 405 423	308 324 342 360 377 395 412	301 316 333 351 368 385 402	293 310 326 343 358 375 391	285 301 318 334 350 367 383	277 293 309 325 341 357 373	269 285 300 316 331 347 362	262 277 292 307 322 337 352	1/4 56 8/7 16/2 15/8	40

#### SAFE LOADS IN THOUSANDS OF POUNDS FOR 15" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 L)^2}{36000 r^2}}$ . Safety factor 4.



#### SERIES A.

Wainht	mh: ale	W-:-14	Auga of	Tood									
Weight of each	Thick- ness of	Weight	Area of	Least Radius of		T	en	orth	1 11	115	eet		
Channel.	Plates.	Column.	Section.	Gyration.			7011	5.1				•	
Lbs.per Ft.	Inches.	Lbs.per Ft.	Sq. Ins.	Inches.	12	14	16	18	20	22	24	26	28
		Zoot Poz I ti											
33	3/8	109.4	32.55	5.41	399	396	393	390	386	381	378	373	367
66	16	116.6	34.68	5.38	425 451	422 448	418 444	415	411 436	406	401 426	397	391 415
66	3/8/6/29/6/84/6/4	123.8 131.0	$36.80 \\ 38.92$	5.36 5.33	$\frac{451}{476}$	448	470	440 465	460	$\frac{431}{456}$	450	420 444	437
66	5/8	138.2	41.05	5.31	502	500	495	490	485	481	475	468	461
66	116	145.4	43.18	5.29	529	<b>52</b> 3	521	516	510	504	499	492	485
66		152.7	45.30	5.24	555	550	545	541	535	529	522	515	509
35	3/8/6/29/6/8-16/4	113.4	33.33	5.40	409	406	402	399	395	390	387	381	376
66	16	120.6	35.46	5.37 5.35	435	432	428 453	424 449	420 445	415 440	410 435	406 429	400 424
66	72	$127.8 \\ 135.0$	$37.58 \\ 39.70$	$\frac{5.35}{5.32}$	461 486	457 483	479	474	469	465	459	453	4446
66	5/8	142.2	41.83	5.30	512	509	505	500	494	488	484	477	470
"	116	149.4	43.96	5.28	538	534	530	525	520	513	508	501	494
66		156.7	46.08	5.27	564	560	556	551	545	538	531	525	518
40	3/8 76 1/2 9/6/81/6/3/4	123.4	36.27	5.35	445	441	438	433	430	425	419	414	409
66	16	130.6 137.8	38.40 40.52	5.33 5.31	470 496	467 493	463 489	459 484	454 479	$\frac{450}{475}$	444 469	438 462	432 455
6.6	9	145.0	42.64	5.29	522	519	514	509	504	498	493	486	479
66	5/8	152.2	44.77	5.27	548	544	540	535	529	523	516	511	503
66	116	159.4	46.90	5.26	574	570	566	560	554	548	540	535	527
		166.7	49.02	5.24	600	595	590	586	579	572	565	557	551
45	3/8 7-16/1/2 9-16/8-1-16/3/4	133.4	39.23	5.31	480	477 503	473	469	464	459	454	447	441
66	16	140.6 147.8	41.36 43.48	5.29 5.27	506 532	528	499 525	494 519	489 514	483 508	478 501	472 496	465 489
6.6	9	155.0	45.60	5.25	558	554	550	545	539	532	525	518	512
66	5/8	162.2	47.73	5.24	584	580	575	570	564	557	550	542	536
66	116	169.4	49.86	5.23	610	606	600	596	589	582	575	567	558
		176.7	51.98	2.21	636	631	626	619	614	607	599	591	582
50	78	143.4 150.6	42.17 44.30	5.26 5.24	516 542	512 538	509 533	504 529	498 524	492 517	486 511	481 503	474 498
66	1/2	157.8	46.42	5.23	568	564	559	555	549	542	535	528	520
66	9 16	165.0	48.54	5.21	594	590	584	578	574	567	559	552	543
66	5/8	172.2	50.67	5.20	620	615	610	604	599	592	584	576	567
66	3/8 7-6/2 9-6/81/6/4	179.4 186.7	52.80 54.92	5.19 5.18	646 672	$\frac{641}{667}$	636 661	629 654	622 647	616 641	608 633	600 624	591 615
55		4		1	552	548	543			527	520	513	505
3,5	3/876/296/816/4	153.4 160.6	45.11 47.24	5.21 5.19	578	574	569	538 563	533 557	552	544	537	529
66	1/2	167.8	49.36	5.18	604	600	594	588	582	576	569	561	553
66	16	175.0	51.48	5.17	630	625	620	613	607	599	593	585	576
66	18	182.2	53.61	5.16	656	651	645	639	632	624	616	609	600
66	1 8 3/4	189.4 196.7	55.74	5.15 5.14	682	677 703	671 696	664 689	657 682	649 673	640 665	633 655	624 648
	/4	100.1	07.00	0.11	1 100	100	000	000	002	010	1 000	000	010

#### SAFE LOADS IN THOUSANDS OF POUNDS FOR 15" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 L)^2}{36000 r^2}}$ . Safety factor 4.

### SERIES A.

												Thick- ness of Plates.	Weight of each Channel.
30	32	34	36	38	40	42	44	46	48	50	52	Inches.	Lbs.per Ft.
363 385 409 432 456 478 501	357 381 402 425 449 472 493	351 374 397 418 441 464 484	345 368 390 411 433 456 476	340 361 383 405 425 447 467	334 356 376 397 419 438 460	327 349 370 389 411 432 451	322 342 362 381 402 423 442	316 335 355 375 394 414 432	309 329 347 367 388 405 423	304 322 342 359 379 397 416	297 315 334 351 371 390 407	3/8 7-6 1-2 9-1-5 1-6 5/81-6 3/4	33
370 394 417 441 463 486 510	366 387 411 434 457 478 501	360 383 404 426 449 472 493	353 376 398 419 441 464 486	348 369 391 413 433 455 477	342 364 383 405 427 446 468	335 357 376 397 418 437 459	330 349 370 389 410 431 452	323 342 362 383 401 422 442	316 337 355 375 393 413 433	310 329 349 367 386 404 423	304 322 341 359 378 397 414	3/8 76 1/2 9 15/8 16/8 16/8 16/8 16/8 16/8 16/8 16/8 16	35   
403 427 450 472 495 519 542	396 420 443 466 487 510 533	390 412 435 458 479 502 524	384 405 427 450 472 495 515	377 399 420 441 464 486 505	370 392 413 433 455 476 498	363 384 405 427 446 467 488	357 376 397 418 439 457 478	350 370 389 409 430 450 468	342 363 383 400 420 440 458	337 355 374 392 411 431 450	329 347 366 385 402 421 440	3/8 7/6 1/2 9/16 5/81 1/6 3/4	40
436 458 481 504 528 552 573	429 452 473 496 519 542 566	421 444 465 488 510 533 556	414 436 459 479 501 523 546	406 428 450 472 492 514 536	400 420 441 463 485 506 525	392 414 433 454 475 496 515	384 405 426 445 465 486 507	376 397 417 435 456 476 496	370 388 408 428 446 465 485	362 380 399 419 438 455 475	354 374 390 409 429 448 464	3/8 <sup>7</sup> 16/916/8116/4	45
466 490 513 535 558 582 605	459 482 505 528 549 572 595	451 474 496 519 542 562 585	445 465 487 510 532 554 574	437 456 478 500 522 544 566	428 450 471 490 512 533 555	420 441 462 481 502 523 544	411 432 453 473 491 512 533	405 423 443 463 484 501 521	396 414 433 453 473 493 510	387 407 424 443 463 482 499	379 398 417 433 452 471 490	3/8/7/6 1/2/9/6 1/6/8/1/6 1/6/4	50
497 520 544 567 591 614 638	491 512 535 558 581 604 627	482 503 525 548 571 593 616	474 496 516 538 560 582 605	465 487 509 528 550 572 593	456 477 499 520 539 560 582	447 468 489 510 531 549 570	440 458 479 499 520 541 558	431 448 469 489 509 529 549	421 441 458 478 498 518 537	412 431 448 468 487 506 525	403 422 441 457 476 495 514	3/8/7/6/29/6/81/6/4	55

# SAFE LOADS IN THOUSANDS OF POUNDS FOR 6" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 L)^2}{36000 r^2}}$ . Safety factor 4.



#### SERIES B.

Weight of each	Thickness of	Weight	Area of Column	Least Radius of		engtl,	1 in	Feet	
Channel.	Plates.	Column.	Section.	Gyration.		,engti			•
Lbs.perFt.	Inches.	Lbs.per Ft.	Sq. Ins.	Inches.	4	6	8	10	12
8	1/4 5 6 7 6 7 1 1/2 9 8 9 8 9 8 9 8 9 8 9 8 9 8 9 8 9 8 9	31.3 35.1 39.0 42.8 46.6 50.4 54.3	9.26 10.39 11.51 12.64 13.76 14.89 16.01	2.74 2.73 2.71 2.70 2.70 2.69 2.68	115 129 142 156 170 184 198	114 127 141 155 169 183 196	112 126 139 153 166 180 193	110 123 136 150 163 176 190	107 121 134 147 160 172 185
10.5	1/4 5/8/8/7/6/20/6/8	36.3 40.1 44.0 47.8 51.6 55.4 59.3	10.68 11.81 12.93 14.06 15.18 16.31 17.43	2.68 2.67 2.66 2.66 2.65 2.65	132 146 160 174 188 202 216	131 145 158 172 186 200 213	129 142 156 170 183 197 210	126 140 153 166 179 193 206	123 137 150 163 176 189 202
13	1/4 5/8 7/5/8 7/11/29/5/8	41.3 45.1 49.0 52.8 56.6 60.4 64.3	12.14 13.27 14.39 15.52 16.64 17.77 18.89	2.54 2.62 2.62 2.62 2.61 2.61 2.61	150 164 178 192 206 220 234	148 162 176 190 204 218 231	146 160 173 187 200 214 227	143 157 170 183 197 210 223	139 153 164 179 192 205 218
15.5	1/4 56 8 6 8 6 8 6 8 8 8 8 8 8 8 8 8 8 8 8 8	46.3 50.1 54.0 57.8 61.6 65.4 69.3	13.62 14.75 15.87 17.00 18.12 19.25 20.37	2.47 2.54 2.57 2.57 2.57 2.57 2.57	169 183 196 210 224 238 252	166 180 194 208 222 236 249	164 178 191 205 218 232 245	160 174 187 200 214 227 240	155 169 182 195 208 221 234

#### SAFE LOADS IN THOUSANDS OF POUNDS FOR 6" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$ . Safety factor 4.



#### SERIES B.

		1	_engt	h in I	Feet.			Thickness of Plates.	Weight of each Channel.
14	16	18	20	22	24	26	28	Inches.	Lbs.perFt.
105 118 130 143 155 168 181 120 133 145 158 171	102 114 126 139 151 163 175 116 129 141 154 166	99 111 123 134 146 158 170 113 125 136 148 160	95 107 118 130 141 153 163 108 121 132 143 155	92 103 114 125 136 147 158 105 116 127 138 149	88 99 109 120 131 141 151 100 111 122 133 143	85 95 105 115 126 135 145 96 107 117 127 137	82 91 101 110 120 130 140 92 102 112 122 131	1/4-66/9-66/9-66/9-66/9-66/9-66/9-66/9-66	8   10.5
183 196 135 149 162	178 190 131 144 157	172 184 126 139 151	166 178 121 135 146	160 171 116 129 134	153 164 112 124 134	147 157 107 119 129	141 151 102 114 123		13
174 186 199 211	169 181 193 206	163 175 187 198 149	158 168 189 191	151 162 173 184	145 155 166 176	139 149 159 169	133 143 152 162	1/4 5/6/6/8/7/6/29/6/8 1/4	15.5
164 178 190 203 215 228	159 172 184 196 209 221	153 166 178 189 201 213	148 160 171 182 194 205	142 153 164 175 186 196	136 147 158 168 179 189	130 141 151 161 171 181	124 134 144 154 163 173	1/4 5.66 3/8 7.66 1/2 9.166 5/8	66

# SAFE LOADS IN THOUSANDS OF POUNDS FOR 7" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50\,000}{1 + \frac{(12\;\mathrm{L})^2}{36\,000\;\mathrm{r}^2}}$ . Safety factor 4.



#### SERIES B.

Weight of each Channel.	Thick- ness of Plates.	Weight of Column.	Area of Column Section.	Least Radius of Gyration.		Len	gth	in F	eet.	
Lbs.per Ft.	Inches.	Lbs.per Ft.	Sq. Ins,	Inches.	6	8	10	12	14	16
9.75	1/4 15/6/87 16/87 16/8 15/8	38.2 42.9 47.6 52.2 56.9 61.5 66.3	11.20 12.58 13.95 15.32 16.70 18.08 19.45	3.20 3.27 3.33 3.35 3.34 3.33 3.32	138 155 172 189 206 223 240	137 154 170 187 204 221 238	135 151 168 185 202 218 235	132 149 166 182 198 215 231	130 146 163 179 195 211 227	127 143 160 175 191 207 223
12.25	1/4 15/8 17/3 1/2 15/8	43.2 47.9 52.6 57.2 61.9 66.5 71.3	12.70 14.08 15.45 16.82 18.20 19.58 20.95	3.08 3.16 3.22 3.29 3.31 3.30 3.29	156 173 190 208 225 242 259	155 172 188 206 222 239 256	153 169 186 203 220 236 253	150 166 183 200 216 233 249	147 163 180 196 213 229 244	143 159 176 192 208 224 239
14.75	1/4 5 6 9 16 9 16 1/2 9 16 5/8	48.2 52.9 57.6 62.2 66.9 71.5 76.3	14.18 15.56 16.93 18.30 19.68 21.06 22.43	2.99 3.07 3.14 3.20 3.26 3.27 3.27	174 191 209 225 243 260 277	172 189 206 223 240 257 274	170 186 203 220 237 253 270	167 183 200 216 233 250 266	163 179 196 212 229 245 261	159 176 192 208 224 240 256
17.25	1/4 5/6 16/8 7/6 1/2 9/6 5/8	53.2 57.9 62.6 67.2 71.9 76.5 81.3	15.64 17.02 18.39 19.76 21.14 22.52 23.89	2.91 2.99 3.06 3.13 3.19 3.24 3.24	192 209 226 243 260 277 294	190 207 224 240 258 275 291	187 204 220 237 254 271 288	183 200 217 234 250 267 283	179 195 212 228 245 262 278	174 191 207 224 240 257 272
19.75	1/4 5/6 3/8 7/6 1/2 9/6 5/8	58.2 62.9 67.6 72.2 76.9 81.5 86.3	17.12 18.50 19.87 21.24 22.62 24.00 25.37	2.85 2.93 3.00 3.07 3.13 3.19 3.21	210 228 244 261 279 296 313	207 225 241 259 275 293 309	204 221 238 254 272 289 305	200 217 233 250 267 284 301	195 212 228 245 262 278 294	190 206 223 240 256 273 288

#### SAFE LOADS IN THOUSANDS OF POUNDS FOR 7" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$ . Safety factor 4,



#### SERIES B.

Length in Feet.									Thickness of Plates.	Weight of each Channel.
18	20	22	24	26	28	30	32	34	Inches.	Lbs.per Ft.
124 140 156 171 187 202 218	121 137 152 167 182 198 213	118 133 148 163 178 192 207	114 130 144 159 173 187 201	111 125 140 154 168 182 196	107 121 136 149 163 176 190	103 117 132 145 158 171 184	100 114 127 140 153 165 178	97 110 123 136 147 160 172	1/4 6 6 8 7 6 1 2 9 6 8 7 6 1 2 9 6 8 9 6 9 8 9 6 9 8 9 6 9 8	9.75
140 156 172 188 204 218 234	136 152 167 183 199 213 228	132 147 163 178 194 207 222	128 143 158 173 188 202 216	124 139 153 168 182 196 210	119 134 148 163 176 190 203	115 129 143 158 171 184 197	111 125 139 153 165 178 190	107 120 133 148 160 172 184	1/4 <sup>1</sup> 6 <sup>1</sup> 6′00′07 <sup>1</sup> 11′09 <sup>1</sup> 6′0	12.25
155 171 187 203 219 235 250	150 166 182 198 214 229 244	145 161 177 192 209 223 238	141 156 172 187 202 217 231	136 151 166 181 196 210 223	131 146 161 175 190 203 216	127 141 155 169 184 197 209	122 136 149 163 178 190 203	117 130 144 158 172 184 196	1/4- 16 16 16 17 17 17 17 18 18 18 18 18 18 18 18 18 18 18 18 18	14.75
169 186 202 218 235 250 265	164 180 197 212 228 244 259	159 175 190 206 222 238 252	154 169 185 200 216 231 245	148 163 178 194 208 224 238	143 157 172 188 202 217 230	137 152 166 180 195 209 222	132 146 160 174 189 202 215	128 140 154 167 181 195 207	1/4 5 16 38 76 16 12 9 16 58	17.25
185 201 217 233 249 267 282	179 195 211 227 243 259 275	173 189 205 220 236 252 266	167 182 198 214 229 245 259	161 176 191 206 222 236 251	155 169 185 199 215 229 243	149 163 177 192 207 222 236	143 157 170 185 200 214 227	137 150 164 178 192 206 219	1/4 5 16 3/87 7/6 1/2 9 15/8	19.75

#### SAFE LOADS IN THOUSANDS OF POUNDS FOR 8" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$ . Safety factor 4.



#### SERIES B.

Weight of each Channel.	Thick- ness of Plates.	Weight of Column.	Area of Column Section.	Least Radius of Gyration.	Length in Feet.						
Lbs.per Ft.	Inches. Lbs.perFt		Eq. Ins.	Inches.	6	8	10	12	14	16	18
11.25	1/4- 5688876 1/2- 9- 16/8	42.9 48.0 53.1 58.2 63.3 68.4 73.5	12.70 14.20 15.70 17.20 18.70 20.20 21.70	3.62 3.70 3.72 3.70 3.68 3.66 3.65	157 176 194 213 231 250 268	156 174 193 211 229 248 266	154 172 191 209 227 245 264	152 171 189 207 224 242 260	150 168 186 203 221 239 256	147 165 183 200 218 234 252	144 162 180 196 213 230 247
13.75	1/4 5 16 3/8 7 16 1/2 9 16/8	47.9 53.0 58.1 63.2 68.3 73.4 78.5	14.08 15.58 17.08 18.58 20.08 21.58 23.08	3.52 3.60 3.67 3.67 3.66 3.64 3.63	174 193 211 230 248 267 285	172 191 209 228 246 265 283	171 189 207 226 244 262 280	168 187 205 223 241 258 276	165 184 202 220 237 255 272	163 181 198 216 233 250 268	159 177 195 212 229 246 262
16.25	1/4 5 6 8 8 7 7 6 1/2 9 1 6 5/8	52.9 58.0 63.1 68.2 73.3 78.4 83.5	15.56 17.06 18.56 20.06 21.56 23.06 24.56	3.42 3.50 3.58 3.64 3.63 3.62 3.61	192 211 229 248 266 285 303	190 209 228 246 264 283 301	188 206 225 244 261 279 298	185 204 222 240 258 276 294	182 200 219 237 254 272 289	179 197 215 233 250 268 285	175 193 211 229 245 262 279
18.75	1/4 5/6 3/8 7/6 1/2 9/6/8	57.9 63.0 68.1 73.2 78.3 83.4 88.5	17.02 18.52 20.02 21.52 23.02 24.52 26.02	3.34 3.42 3.50 3.57 3.61 3.60 3.59	210 229 247 266 284 303 322	208 227 245 264 282 301 319	205 224 242 261 279 297 315	202 221 239 257 276 294 312	199 217 235 254 271 289 307	195 213 231 249 267 284 301	191 208 227 245 262 279 296
21.25	1/4 56 3/8 17 1/2 96 5/8	62.9 68.0 73.1 78.2 83.3 88.4 93.5	18.50 20.00 21.50 23.00 24.50 26.00 27.50	3.27 3.36 3.43 3.51 3.57 3.57 3.57	228 247 266 284 303 321 340	226 244 263 282 300 319 337	223 241 260 279 297 315 333	219 238 256 275 293 311 329	215 234 252 270 289 306 324	211 229 247 265 283 301 318	206 224 243 260 278 295 313

## SAFE LOADS IN THOUSANDS OF POUNDS FOR 8" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 L)^2}{36000 r^2}}$ . Safety factor 4.



#### SERIES B.

			Le	ngth	in	Feet				Thickness of Plates.	Weight of each Channel.
20	22	24	26	28	30	32	34	36	38	Inches.	Lbs.per Ft.
142 159 176 193 209 225 242	138 156 172 189 204 221 237	135 152 168 184 200 215 231	131 148 164 180 194 210 226	128 144 160 175 190 204 219	124 141 155 170 184 199 214	121 137 151 166 179 194 207	117 133 147 161 175 188 202	114 129 143 156 169 182 195	110 125 139 151 164 176 189	1/4 5 6 8 7 6 2 9 6 8 7 11 2 9 6 8	11.25
156 173 191 208 224 241 257	152 170 187 203 219 236 251	149 165 183 199 214 230 246	144 161 178 193 209 224 239	140 157 173 187 203 218 233	137 153 168 183 198 213 226	132 148 164 178 193 206 220	128 144 159 173 186 200 213	124 139 154 168 181 194 207	120 134 149 162 175 188 200	1/4 15 15 3/8 16 1/2 16 5/8	13.75
171 189 206 224 240 257 274	167 184 202 219 235 251 267	163 179 197 214 230 245 261	158 175 191 209 223 239 254	153 170 187 203 218 233 247	149 165 181 198 211 226 241	144 160 176 191 206 220 233	140 155 170 186 199 213 227	135 150 165 180 194 207 219	130 145 160 175 187 200 213	1/4 5-6 50 7-16 7-16 7-16 7-16 7-16 7-16 7-16 7-16	16.25
186 204 221 239 257 272 289	181 199 216 233 250 267 283	176 194 210 228 245 260 276	171 188 205 222 238 254 269	166 182 199 216 231 247 262	161 177 193 210 226 240 254	155 171 188 203 219 233 247	150 166 182 198 213 226 239	145 161 176 191 206 219 232	140 155 170 186 200 212 224	1/4 5 1/6 3/8 1/6 3/8 1/2 1/2 1/6 5/8	18.75
201 219 237 254 272 289 305	196 214 231 248 265 282 298	191 208 225 243 260 276 291	184 202 218 236 252 268 283	178 196 212 229 246 261 276	173 190 206 223 239 253 268	167 184 200 216 231 245 260	161 178 193 209 225 239 253	156 172 187 202 218 231 244	150 165 180 196 211 224 237	1/4 156 158 1176 176 176 176 176 176 176 176 176 17	21.25

# SAFE LOADS IN THOUSANDS OF POUNDS FOR 9'' CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$ . Safety factor 4.



#### SERIES B.

Weight of each Channel.	Thick- ness of Plates.	Weight of Column.	Area of Column Section.	Least Radius of Gyration.											
Lbs.per Ft.	Inches.	Lbs.per Ft.	Sq. Ins.	Inches.	6	8	10	12	14	16	18	20			
13.25 " " " " 15.0	1/4/5/6/8/7/6/29/5/8 1/4/5/6/8/7/5/7/6/5/8/6/8/6/8/6/8/6/8/6/8/6/8/6/8/6/8/6	48.6 54.1 59.7 65.2 70.7 76.2 81.7 52.1 57.6 63.2 68.7 74.2 79.7 85.2	14.28 15.90 17.56 19.16 20.78 22.40 24.03 15.32 16.94 18.57 20.20 21.82 23.44 25.07	4.05 4.10 4.07 4.04 4.02 4.00 3.99 3.97 4.05 4.05 4.01 3.99 3.97	177 197 217 237 257 277 297 190 210 230 250 270 290 310	176 196 216 236 256 276 296 188 208 228 249 268 288 308	174 194 214 234 253 273 293 187 207 226 246 266 286 306	192 212 231 251 270 290 185 204 224	170 190 209 228 248 267 286 183 202 221 241 260 279 299	168 187 207 225 244 263 282 180 199 218 237 256 275 295	184 203 222 240 259	181			
20.0	1/4 556 876 766 1/2 976 8	62.1 67.6 73.2 78.7 84.2 89.7 95.2	18.26 19.88 21.51 23.14 24.76 26.39 28.01	3.78 3.87 3.95 3.98 3.96 3.95 3.94	226 246 266 286 306 327 347	224 244 264 285 305 325 345	222 242 262 282 302 322 342	219 239 260 279 299 318 338	216 236 256 276 295 314 333	213 233 252 272 291 309 328	209 228 248 268 286 304 323	205 224 244 263 280 299 317			
25.0	1/44 566/87/6/29 1/29/8/15/8	72.1 77.6 83.2 88.7 94.2 99.7 105.2	21.20 22.82 24.45 26.08 27.70 29.32 30.95	3.64 3.73 3.81 3.89 3.92 3.91 3.90	262 282 303 323 343 363 383	260 280 300 320 341 361 380	257 277 298 317 337 357 377	254 274 294 314 333 353 373	251 270 290 310 329 348 368	246 266 285 305 324 343 362	242 261 281 301 319 338 357	236 255 276 295 314 332 350			

# SAFE LOADS IN THOUSANDS OF POUNDS FOR 9" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 L)^2}{36000 r^2}}$ . Safety factor 4.



### SERIES B.

				L,e	ngth	in	Feet		t		Thickness of Plates.	Weight of each Channel.
22	24	26	28	30	32	34	36	38	40	42	Inches.	Lbs.per Ft.
160 178 196 214 232 250 268	157 174 192 210 227 245 263	153 172 188 206 222 240 257	150 168 184 201 217 234 251	146 164 180 196 212 229 245	143 160 175 192 207 223 239	139 156 171 187 202 217 233	136 152 167 182 196 211 227	132 148 163 177 191 206 221	128 144 158 172 186 200 215	125 140 154 167 181 194 208	1/4-56 3/8-76 1/2-96 5/8	13.25
171 190 208 225 243 261 280	167 186 204 221 238 256 274	164 182 199 216 233 251 268	159 178 195 212 228 245 261	156 174 190 207 223 239 255	152 169 186 202 217 233 248	148 165 181 197 212 227 242	144 161 176 192 206 221 235	140 156 172 187 200 215 229	136 152 167 181 195 209 223	132 148 162 176 189 203 216	1/4 5 6 8 7 6 2 6 8 14 5 8	15.0
201 220 239 258 275 293 311	197 215 234 253 269 287 305	192 211 229 247 264 281 298	187 206 224 242 258 274 291	183 200 218 236 251 268 284	177 195 213 230 245 261 277	172 190 207 224 239 255 270	168 185 202 218 232 248 263	162 180 196 213 226 241 256	158 174 191 205 220 234 247	153 168 186 200 214 228 240	1/4 5/6 9/8 7/6 1/2 9/6 5/8	20.0
232 250 269 288 308 326 344	226 245 264 283 301 319 335	221 238 258 276 295 312 328	214 233 252 270 288 304 320	209 227 245 264 280 296 313	202 220 238 257 273 289 309	197 214 232 250 266 281 297	190 207 226 242 259 274 289	185 201 218 236 252 266 281	179 196· 212 229 245 260 273	173 189 206 222 238 251 264	1/4 5/6 6/8 7/6 1/2 1/2 1/6/8	25.0

### SAFE LOADS IN THOUSANDS OF POUNDS FOR 10" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$ . Safety factor 4.



#### SERIES B.

Weight of each Channel.	Thick- ness of Plates.	Weight of Column,		Least Radius of Gyration.		1	Len	gtl	ı ir	F	eet		
Lbs.per Ft.	Inches.	Lbs.per Ft.	Sq. Ins.	Inches.	8	10	12	14	16	18	20	22	24
15	14566 (8) 16 (9) 16 (8)	55.5 61.9 68.3 74.6 81.0 87.4 93.8	16.42 18.30 20.17 22.05 23.92 25.80 27.67	4.49 4.58 4.65 4.70 4.67 4.65 4.63	203 226 249 272 296 319 342	201 224 247 271 294 316 339	199 223 245 268 291 314 337	198 220 243 266 289 311 334	195 218 241 263 286 308 330	193 216 238 261 282 304 326	190 212 235 257 278 300 322	187 209 232 253 275 296 317	185 206 228 250 271 291 312
20	1/5/6, 69, 69, 69, 69, 69, 69, 69, 69, 69, 6	65.5 71.9 78.3 84.6 91.0 97.4 103.8	19.26 21.14 23.01 24.89 26.76 28.64 30.51	4.29 4.39 4.47 4.55 4.62 4.63 4.61	237 261 284 307 331 354 377	236 259 282 305 328 351 374	233 257 279 303 326 349 371	231 254 277 300 323 346 368	228 251 273 297 319 341 364	225 248 270 292 315 337 359	221 244 266 289 311 333 355	218 240 262 285 306 328 349	214 236 258 280 302 323 344
25	1415660	75.5 81.9 88.3 94.6 101.0 107.4 113.8	22.20 24.08 25.95 27.83 29.70 31.58 33.45	4.13 4.23 4.32 4.40 4.48 4.55 4.58	274 297 320 343 367 390 413	271 294 318 341 364 387 410	268 292 315 338 361 384 407	265 288 312 334 357 380 403	262 285 308 331 853 376 399	258 280 303 326 349 371 394	254 277 299 322 343 366 388	249 272 294 316 339 361 383	245 266 288 310 332 355 377
30  	1/4/5/76/00/716/20/15/00 1/20/15/10 1/20/15/10	85.5 91.9 98.3 104.6 111.0 117.4 123.8	25.14 27.02 28.89 30.77 32.64 34.52 36.39	4.01 4.11 4.20 4.28 4.36 4.43 4.50	309 333 356 379 403 426 449	307 330 353 377 400 423 446	303 327 349 373 396 419 442	300 323 346 369 392 415 438	295 318 341 365 387 410 432	291 313 336 359 382 404 428	286 308 331 353 376 399 422	280 302 326 348 371 392 415	275 298 320 342 364 386 469
35	1/45/6/67/6/20/6/8	95.5 101.9 108.3 114.6 121.0 127.4 133.8	28.08 29.96 31.83 33.71 35.58 37.46 39.33	3.90 4.00 4.10 4.18 4.26 4.33 4.40	345 369 392 415 438 462 485	342 365 389 412 436 459 481	338 361 385 408: 431: 454 478	334 357 380 404 426 450 472	329 352 375 398 420 444 467	324 346 369 392 415 437 461	318 340 363 386 409 432 455	312 334 356 379 4/1 424 447	304 327 349 373 395 418 439

# SAFE LOADS IN THOUSANDS OF POUNDS FOR 10" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 L)^2}{36000 r^2}}$ . Safety factor 4.



# SERIES B.

				Le:	ngt	h i	n F	`eet				Thickness of Plates.	Weight of each Channel.
26	28	30	32	34	36	38	40	42	44	46	48	Inches.	Lbs.per Ft.
181 202 224 246 266 287 307	220 241	174 195 216 237 257 276 296	191 212 233 251 271	167 188 208 228 246 266 285	163 183 204 223 242 261 278	159 179 199 218 237 254 273	156 176 195 214 231 249 267	152 171 190 209 226 244 260	148 167 185 204 221 237 254	145 163 181 199 215 232 248	141 159 177 195 210 226 241	1/44-5-6-8-8-8-8-8-8-8-8-8-8-8-8-8-8-8-8-8-8	15
210 232 254 275 297 318 339	206 227 248 270 291 313		197 218 238 260 281 301	193 214 234 254 274 295 313	188 208 228 249 269 288 307	183 203 223 243 264 282 301	179 198 218 238 257 276 293	174 193 213 232 251 269 286	169 189 208 226 246 263 280	165 183 202 221 239 257 272	160 179 197 216 233 250 266	1/4 5/6 1/6 1/6 1/2 9/6 5/8	20
239 262 284 305 327 349 370	256 277 299 322 342	229 250 272 294 315 336 356	224 245 266 287 309 330 350	219 240 260 281 302 322 343	213 234 254 274 296 316 335	207 227 248 268 288 308 328	202 221 241 261 282 301 321	196 216 236 256 274 295 312	190 210 229 248 268 287 305	186 204 223 241 261 280 299	180 199 217 236 255 274 290	1/4-56 80 7-16/29 6/8	25
269 291 313 335 357 379 401	285 306	257 278 300 322 342 364 386	250 272 293 314 336 357 378	244 265 286 308 328 349 370	237 258 279 300 320 342 362	231 252 273 292 313 333 355	224 245 265 286 305 326 345	218 239 258 278 298 317 338	212 232 251 270 290 310 329	205 225 243 264 282 301 321	199 218 238 256 275 294 312	1/4. 5 16 3/8 7 16 1/2 9 16 5/8	30 " " " "
298 320 343 365 387 409 432	313 336 357 379 401	349 372 393	384	269 291 312 334 354 375 397	262 283 304 325 345 367 387	255 275 296 317 338 358 379	248 267 287 309 329 350 369	239 260 281 301 320 340 361	232 252 273 292 312 331 351	225 245 265 284 303 323 341	219 238 257 276 294 314 333	1/4- 166/8- 169/8- 169/8- 169/8- 169/8- 169/8-	35   

### SAFE LOADS IN THOUSANDS OF POUNDS FOR 12" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50\ 000}{1 + \frac{(12\ L)^2}{36\ 000\ r^2}}$ . Safety factor 4.



#### SERIES B.

Weight of each Channel,	Thick- ness of Plates.	Weight of Column.	Area of Column Section.	Least Radius of Gyration.		1	Len	gt1	1 11	1 F	eet		
Lbs.per Ft.	Inches.	Lbs.per Ft.	Sq. Ins.	Inches.	8	10	12	14	16	18	20	22	24
20.5	1/4 5/6 3/8 7/6 1/2 9/6 1/8	68.2 75.0 81.8 88.6 95.4 102.2 109.0	20.06 22.06 24.06 26.06 28.06 30.06 32.06	5.23 5.18 5.14 5.10 5.07 5.04 5.01	248 273 298 322 347 372 397	247 272 296 321 345 370 394	246 270 295 318 343 367 392	244 268 292 317 340 364 389	241 266 290 314 337 361 385	240 263 287 311 333 357 381	237 260 283 307 331 354 377	234 258 280 303 327 349 372	231 254 276 299 322 344 367
25	1/4 5/6 8/8 7/6 1/2 9/6/8	77.2 84.0 90.8 97.6 104.4 111.2 118.0	22.70 24.70 26.70 28.70 30.70 32.70 34.70	5.09 5.14 5.11 5.07 5.05 5.02 5.00	281 306 330 355 380 405 429	279 304 328 353 378 402 427	277 302 326 351 375 400 424	275 300 324 348 372 396 421	273 297 321 345 369 393 417	270 294 318 341 365 389 412	267 291 315 338 361 384 408	264 287 311 334 356 379 403	261 284 307 330 351 374 397
30 " " " "	1/4/5/6/8/7/6/29/6/8	87.2 94.0 100.8 107.6 114.4 121.2 128.0	25.64 27.64 29.64 31.64 33.64 35.64 37.64	4.93 5.04 5.07 5.04 5.02 4.99 4.98	317 342 367 391 416 441 466	315 340 365 389 414 438 463	313 338 362 387 411 435 460	311 335 359 383 408 432 456	308 332 356 380 404 428 452	304 328 352 376 400 424 447	300 326 349 373 395 419 442	296 321 345 367 390 413 437	292 316 340 362 385 408 431
35   	1/4 5/6 3/8 7/6 1/2 9/6/8	97.2 104.0 110.8 117.6 124.4 131.2 138.0	28.58 30.58 32.58 34.58 36.58 38.58 40.58	4.80 4.91 5.01 4.99 4.97 4.95 4.94	353 378 403 428 453 477 502	351 376 401 425 450 475 499	349 374 398 422 447 471 496	346 370 395 419 443 468 492	342 366 391 415 439 463 487	338 362 387 411 435 458 482	334 358 383 406 430 453 477	329 354 378 401 424 448 469	325 349 373 396 419 442 463
40	1/4 516 3/8 716 1/2 916 5/8	107.2 114.0 120.8 127.6 134.4 141.2 148.0	31.52 33.52 35.52 37.52 39.52 41.52 43.52	4.69 4.80 4.90 4.95 4.94 4.92 4.91	389 414 439 464 489 514 538	387 412 437 462 486 511 535	384 409 434 458 483 507 532	380 405 430 455 479 503 526	377 402 425 451 474 497 521	373 396 421 446 470 492 516	367 391 416 441 464 486 510	362 386 411 435 457 480 503	357 381 405 429 451 473 496

# SAFE LOADS IN THOUSANDS OF POUNDS FOR 12" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 L)^2}{36000 r^2}}$ . Safety factor 4.



#### SERIES B.

-				Le	eng	th i	in 1	Feet.	•			Thick- ness of	Weight of each
												Plates.	Channel.
26	28	30	32	34	36	38	40	42	44	46	48	Inches.	Lbs.per Ft.
228 251 272 295 318 339 362	225 247 269 291 313 334 356	222 243 265 286 308 328 350	218 239 261 281 303 324 344	215 235 256 276 297 319 338	211 231 251 271 292 313 332	207 227 247 266 286 307 326	204 223 242 262 281 301 319	200 218 237 257 275 295 313	196 214 232 251 269 288 306	191 209 228 246 263 282 299	187 205 223 241 258 276 293	1/4-5-6-8-8-8-8-8-8-8-8-8-8-8-8-8-8-8-8-8-8	20.5 " " "
257 280 302 325 348 369 391	253 276 298 320 342 363 385	249 272 293 315 337 357 379	245 268 288 310 331 351 373	241 263 283 304 325 345 366	236 258 279 299 319 339 359	232 253 274 293 313 332 352	227 248 268 287 307 325 345	222 243 263 281 301 319 338	219 238 258 275 295 312 331	214 234 252 269 288 305 324	210 229 247 264 282 299 317	1/4 5/8 3/8 7/6 1/2 9/6 5/8	25   
288 312 336 357 379 402 425	284 307 330 351 374 396 418	279 302 325 346 368 389 411	274 298 320 341 361 383 404	269 293 314 335 355 376 397	264 287 308 329 348 369 390	259 282 302 323 342 362 382	254 276 296 316 335 355 375	249 271 290 310 328 347 367	243 265 284 304 321 340 359	238 260 278 297 314 333 351	233 254 272 291 307 326 344	1/4 56 3/8 7/6 1/2 976 5/8	30    
320 344 368 390 413 434 456	315 338 362 384 406 427 449	310 333 356 378 400 420 442	303 327 350 371 393 413 434	297 321 344 365 386 405 426	292 315 337 358 379 398 418	286 309 331 351 371 390 410	280 303 324 344 364 382 402	273 295 318 337 355 374 394	267 289 311 330 347 366 385	261 282 304 323 340 358 377	255 276 298 316 332 350 369	1/4 5 18/8 7/6 1/2 9/6 1/2 9/6 5/8	35 " " "
351 375 399 422 444 466 489	344 369 393 415 437 459 481	339 363 386 408 430 452 473	333 355 380 401 423 444 465	326 349 373 394 415 436 457	318 342 366 387 407 428 448	312 335 357 379 399 420 440	306 328 350 372 391 411 431	298 320 343 364 383 403 420	291 313 335 356 375 394 411	285 306 328 348 367 386 402	278 299 321 341 359 375 393	1/4 56 3/8 76 1/2 96 15/8	40

## SAFE LOADS IN THOUSANDS OF POUNDS FOR 15" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 \text{ L})^2}{36000 \text{ r}^2}}$ . Safety factor 4.



#### SERIES B.

Weight of each Channel.	Thick- ness of Plates.	Weight of Column.	Area of Column Section.	Least Radius of Gyration.		1	Len	ıgtl	1 is	n F	eet		
Lbs.per Ft.	Inches.	Lbs.per Ft.	Sq. Ins.	Inches.	12	14	16	18	20	22	24	26	28
33 " " " "	3/8 7/6 / 29/6 / 8/1/6 / 4	117.0 125.5 134.0 142.5 151.0 159.5 168.0	34.80 37.30 39.80 42.30 44.80 47.30 49.80	6.59 6.57 6.52 6.48 6.44 6.41 6.38	429 460 491 521 552 583 614	427 458 489 519 549 580 611	425 456 485 516 546 577 607	423 453 482 513 543 573 604	420 450 479 509 539 569 599	417 447 476 505 535 565 595	414 442 472 501 531 561 589	410 438 468 497 526 554 583	406 434 463 492 521 549 578
35   	3/8/16/29/6/81/6/4	121.0 129.5 138.0 146.5 155.0 163.5 172.0	35.58 38.08 40.58 43.08 45.58 48.08 50.58	6.55 6.56 6.52 6.48 6.44 6.41 6.38	439 470 501 531 562 592 623	437 468 498 528 559 590 620	435 465 495 525 556 586 617	432 463 492 522 552 583 613	428 459 488 519 549 579 609	425 455 485 515 545 574 604	422 451 481 511 540 570 598	418 447 477 506 535 563 592	414 443 472 501 531 558 587
40	3/8 716 1/2 9 15/8 116 3/4	131.0 139.5 148.0 156.5 165.0 173.5 182.0	38.52 41.02 43.52 46.02 48.52 51.02 53.52	6.41 6.51 6.50 6.47 6.43 6.40 6.37	475 506 537 567 598 629 659	472 503 534 564 595 626 656	470 500 531 561 592 622 653	467 497 527 558 588 618 649	464 494 524 554 584 614 644	460 490 520 550 580 610 638	457 486 516 545 575 603 633	451 482 511 541 570 598 627	447 477 507 536 563 592 621
45	3/88 76 1/22 9 6 8 1 6 8 1 6 1 1 3 1 1 1 3 1 1 1 3 1 1 1 3 1 1 1 3 1 1 1 3 1 1 1 3 1 1 1 3 1 1 1 3 1	141.0 149.5 158.0 166.5 175.0 183.5 192.0	41.48 43.98 46.48 48.98 51.48 53.98 56.48	6.28 6.39 6.48 6.45 6.42 6.39 6.37	511 542 573 604 634 665 696	509 539 570 601 631 662 693	506 536 567 597 628 658 689	502 533 563 594 624 654 685	498 529 559 590 620 650 680	494 525 555 585 615 645 673	490 520 551 580 610 638 667	486 515 546 575 603 632 661	480 510 541 570 597 626 655
50	3/8 7-6 1/2 9-6/81-6/8 1-3/4	151.0 159.5 168.0 176.5 185.0 193.5 202.0	44.42 46.92 49.42 51.92 54.42 56.92 59.42	6.17 6.28 6.37 6.43 6.40 6.37 6.35	547 578 609 640 671 701 732	544 575 606 636 667 698 729	541 572 603 633 664 694 725	537 567 599 629 660 690 720	533 563 595 625 655 685 715	528 559 589 620 650 678 708	523 555 584 615 643 673 702	519 550 579 610 637 667 696	514 543 573 602 631 660 689
55	3/8 7 1 1/2 9 1 5/8 1 1 6/8 1 1 6/4	203.5	47.36 49.86 52.36 54.86 57.36 59.86 62.36	6.07 6.18 6.28 6.37 6.38 6.35 6.33	583 614 645 676 707 738 768	580 610 642 673 703 734 764	576 607 639 669 700 730 760	571 603 633 665 695 726 756	567 599 629 660 690 721 751	563 593 624 654 685 713 743	556 588 619 648 678 707 737	551 582 613 643 672 701 730	546 577 605 636 665 694 724

### SAFE LOADS IN THOUSANDS OF POUNDS FOR 15" CHANNEL AND PLATE COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{50000}{1 + \frac{(12 L)^2}{36000 r^2}}$ . Safety factor 4.



#### SERIES B.

				Le	ng	th:	in ]	Feet	•			Thick- ness of Plates.	Weight of each Channel.
30	32	34	36	38	40	42	44	46	48	50	52	Inches.	Lbs.per Ft.
401 430 459 487 515 543 572	397 425 454 482 509 538 566	393 421 449 477 503 532 560	388 416 444 470 498 525 553	383 411 439 464 492 519 544	379 406 433 458 485 512 537	374 401 427 452 479 504 530	369 395 422 446 473 497 523	364 390 414 440 466 490 516	359 384 408 434 457 483 508	353 379 402 427 450 476 501	348 373 396 421 444 468 491	3/8 7/6 1/2/9/16/5/8 1/6/3/4	33
410 439 468 496 523 552 581	406 434 463 491 518 546 575	401 430 458 486 512 540 568	397 425 452 478 506 534 562	392 420 447 473 500 528 553	387 414 442 467 494 521 546	382 409 436 461 487 512 538	377 404 430 454 481 505 531	372 398 422 448 474 498 524	367 392 416 442 465 491 516	361 387 410 435 458 483 509	356 381 404 429 451 476 498	3/8 7-16/24 9-15/81-16/3/4	35   
442 473 502 530 557 586 615	438 468 496 525 551 580 608	433 463 491 517 545 573 601	428 457 485 511 539 567 592	423 452 480 505 532 560 585	417 446 471 499 526 553 577	410 439 465 492 519 543 570	404 433 459 485 512 536 562	399 427 453 479 502 528 554	393 421 446 472 495 521 546	387 414 440 465 488 513 538	381 408 433 458 480 505 527	3/8 76/1/2 9/5/81/6 15/81/6 3/4	40
475 505 536 563 591 620 649	470 500 530 557 585 613 642	464 494 524 550 578 607 635	459 488 516 544 572 600 625	451 483 510 537 565 592 517	445 474 504 531 558 582 609	440 468 497 524 550 575 601	433 462 490 517 540 567 593	427 455 483 509 533 559 585	421 449 477 502 525 551 576	413 442 470 492 518 543 568	407 435 463 485 510 535 556	3/8 7/6 1/2 9/6 15/8 1/6 1/6 3/4	45  
507 537 568 596 625 654 682	501 531 562 590 618 647 675	495 525 555 583 612 640 665	489 519 547 577 604 630 657	481 510 540 570 597 622 649	475 504 533 563 590 614 641	469 497 526 555 579 606 632	462 493 519 548 571 598 623	453 483 512 538 563 589 615	447 476 504 530 555 581 603	440 467 497 522 547 572 594	433 460 487 514 539 561 585	3/8 7-16 1/2 9-16 5/81-16 3/4	50
540 569 599 630 659 687 716	532 562 593 623 652 680 706	526 556 586 616 645 670 698	520 549 579 607 637 662 690	511 542 570 599 627 654 681	504 533 562 592 619 646 673	497 526 555 584 611 637 664	490 519 547 576 602 628 652	481 511 540 568 594 620 643	474 501 532 560 585 608 633	466 494 521 552 577 599 624	457 486 513 540 565 590 614	3/8 76/2 1/2 9/6/81/6/4	55  

### SAFE LOADS IN THOUSANDS OF POUNDS FOR HOLLOW ROUND CAST IRON COLUMNS. SQUARE ENDS.

Based on Gordon's Formula P=  $1 + \frac{1}{800 \, d^2}$ 

P=safe load in pounds per square inch. l=length of column in inches.

d=outside diameter of column in inches. Ultimate compressive strength=80 000 pounds per square inch. Safety factor 8. Safe loads for other safety factors than that of the tables may be obtained as fol-

lows :-New safe load=Safe load from table × New factor

	New factor													
Diameter in	Thick- ness in		eng	th								Area of Metal in	Weight per Foot in	
Inches.	Inches.	6	8	10	12	14	16	18	20	22	24	Sq. Ins.	Pounds.	
6	3/4 7/8	105 119	94 107	82 94	72 82	62 71	54 62	47 54	41 47	36 41	32 36	12.4 14.1	38.7 44.0	
7	3/4 7/8	130 149	119 136	108 123	96 110	86 98	76 87	67 77	60 68	53 61	47 54	14.7 16.8	$\frac{46.0}{52.6}$	
8	3/4 7/8 1	155 178 200	145 166 186	133 153 172	122 139 158	110 $126$ $142$	99 114 128	89 104 115	80 92 <b>10</b> 3	72 83 93	65 75 84	17.1 19.6 22.0	53.4 61.2 68.7	
9	7/8 1 11/8	207 233 258	196 220 244	183 206 228	169 190 211	159 179 198	142 160 177	130 146 162	118 133 147	108 121 134	98 110 122	22.3 25.1 27.8	69.8 78.5 87.0	
10	7/8 1 11/8 11/4	235 265 294 323	225 254 281 308	212 240 266 291	199 224 249 273	185 209 232 254	172 194 215 235	158 178 198 217	146 164 182 200	134 151 168 184	123 139 154 169	25.1 28.3 31.4 34.4	78.4 88.4 98.0 107.4	
11	1 1 <sup>1</sup> / <sub>8</sub> 1 <sup>1</sup> / <sub>4</sub> 1 <sup>3</sup> / <sub>8</sub>	298 330 363 395	287 317 350 380	273 304 333 361	259 287 315 342	243 270 296 322	227 253 277 301	212 235 258 280	197 219 240 261	183 203 223 242	169 188 206 224	31.4 34.9 38.3 41.6	98.2 109.1 119.7 129.9	
12	$1\frac{1}{8}$ $1\frac{1}{4}$ $1\frac{3}{8}$ $1\frac{1}{2}$	368 404 439 473	356 391 425 458	342 375 408 440	326 358 389 419	309 339 369 397	291 320 348 375	274 300 327 352	256 281 306 330	239 263 287 308	223 245 267 288	38.4 42.2 45.9 49.5	120.1 131.9 143.4 154.6	
13	$1\frac{1}{8}$ $1\frac{1}{4}$ $1\frac{3}{8}$ $1\frac{1}{2}$	404 444 484 522	393 432 470 507	379 417 454 490	364 400 435 470	347 382 415 448	330 363 395 426	312 343 373 403	294 323 352 380	277 304 331 358	260 286 311 336	42.0 46.1 50.2 54.2	131.2 144.2 156.9 169.4	
14	$ \begin{array}{c c} 1^{1}/4 \\ 1^{3}/8 \\ 1^{1}/2 \\ 1^{5}/8 \end{array} $	485 528 570 612	473 515 556 597	459 499 540 579	442 482 520 558	424 462 499 535	405 441 477 511	386 420 454 487	366 399 431 462	347 378 408 437	327 357 385 413	50.1 54.5 58.9 63.2	156.5 170.4 184.1 197.4	
15	$1\frac{3}{8}$ $1\frac{1}{2}$ $1\frac{5}{8}$ $1\frac{3}{4}$	573 618 664 708	560 605 650 694	545 589 632 675	528 570 612 653	509 550 590 630	489 528 567 605	467 505 542 577	446 482 517 552	424 459 492 525	406 439 471 502	58.9 63.6 68.3 72.8	183.9 203.4 213.4 227.6	
16	1½ 15% 13¼ 17%	666 716 764 909	654 702 750 892	638 686 732 871	620 666 711 846	600 645 689 819	579 622 664 790	557 598 638 759	533 573 611 727	510 548 584 695	486 522 558 663	68.3 73.4 78.3 93.2	213.5 229.3 244.8 291.3	

# SAFE LOADS IN THOUSANDS OF POUNDS FOR HOLLOW ROUND CAST IRON COLUMNS. SQUARE ENDS.

Based on Gordon's Formula  $P = \frac{10000}{1000}$  $1 + \frac{1}{800 \, d^2}$ 

P=safe load in pounds per square inch.
l=length of column in inches.

d=outside diameter of column in inches.

Ultimate compressive strength=80 000 pounds per square inch. Safety factor 8. Safe loads for other safety factors than that of the tables may be obtained as follows:

lows:—New safe load=Safe load from table  $\times \frac{\sigma}{\text{New factor}}$ 

Diameter in	Thick- ness in	I.	eng	ŗth	of	Col	lum	ın i	n F	'ee	t.	Area of Metal in	Weight per Foot in
Inches.	Inches.	14	16	18	20	22	24	26	28	30	32	Sq. Ins.	Pounds.
18	15/8 $13/4$ $17/8$ $2$	754 806 857 907	732 782 832 880	708 757 805 852	684 732 777 823	659 704 749 792	633 677 720 762	608 650 691 731	596 637 677 717	557 596 633 670	533 569 605 641	83.6 89.3 95.0 100.5	261.2 279.2 296.8 314.2
20	13/4 17/8 2 21/8	922 981 1039 1097		876 932 987 1041	850 905 958 1011	824 877 929 980	797 848 898 948	769 819 867 915	742 789 836 882	714 760 805 849	687 731 774 817	100.3 106.8 113.1 119.3	313.6 333.6 353.4 372.9
22	17/8 2 21/8 21/4	1239	$1147 \\ 1213$	$\frac{1122}{1186}$	$1094 \\ 1157$	$1065 \\ 1126$	976 1035 1094 1150	$1004 \\ 1062$				118.5 125.7 132.9 139.6	370.5 392.7 415.3 436.3
24	$\begin{array}{c c} 2 \\ 2^{1/8} \\ 2^{1/4} \\ 2^{3/8} \end{array}$	1376 1449	$1352 \\ 1423$	1311 1380	$\frac{1298}{1367}$	$1268 \\ 1335$	1171 1238 1303 1367	$1206 \\ 1269$	$1173 \\ 1235$	$ 1140 \\ 1200$	$\frac{1106}{1165}$	138.2 146.0 153.7 161.4	432.0 456.4 480.4 504.2
26	2 <sup>1</sup> / <sub>8</sub> 2 <sup>1</sup> / <sub>4</sub> 2 <sup>3</sup> / <sub>8</sub> 2 <sup>1</sup> / <sub>2</sub>	$1596 \\ 1675$	1572 1650	$1546 \\ 1623$	$1517 \\ 1593$	$\frac{1487}{1562}$	1382 $1456$ $1528$ $1600$	$1423 \\ 1494$	$1389 \\ 1458$	$1354 \\ 1422$	$1319 \\ 1385$	159.4 167.9 176.3 184.6	498.1 524.6 550.9 576.8
28	2½ 2½ 2½ 25/8	1829 1917	$1806 \\ 1892$	$1780 \\ 1864$	1751 1834	$1721 \\ 1802$	1608 1689 1769 1848	$1655 \\ 1734$	1620 1697	1584 1660	$1548 \\ 1622$	182.0 191.2 200.3 209.3	568.8 597.5 625.9 653.9
30	23/8 21/2 25/8 23/4	$2078 \\ 2172$	$2055 \\ 2148$	$2028 \\ 2119$	$\begin{vmatrix} 2000 \\ 2090 \end{vmatrix}$	$\frac{1969}{2058}$	2024	1903 1989	$\begin{vmatrix} 1867 \\ 1952 \end{vmatrix}$	1830 1913	1711 1793 1874 1954	206.1 216.0 225.8 235.4	644.1 675.0 705.5 735.7
32	2½ 25/8 23/4 27/8	$2341 \\ 2442$		$\frac{2292}{2391}$	$2264 \\ 2361$	$\frac{2233}{2329}$	2104 2200 2295 2389	$2165 \\ 2259$	$\frac{2129}{2221}$	$2092 \\ 2182$	2141	231.7 242.2 252.7 263.1	724.0 757.0 789.7 822.1
34	25/8 23/4 27/8 3	$\begin{vmatrix} 2620 \\ 2728 \end{vmatrix}$	$\frac{2596}{2703}$	$2570 \\ 2676$	2542 2646	$2511 \\ 2614$	2374 2478 2580 2681	2441 2544	$2406 \\ 2505$	$\frac{2370}{2468}$	2329 2425	258.7 270.0 281.1 292.2	808.6 843.7 878.5 913.0
36	23/4 27/8 3	2796 2913	2774 2889	2749 2863	2721 2834	2692 2803	2660	2626 2735	2591 2698	2553 2659	2515 2619	287.3 299.2 311.0	897.7 935.0 971.9

### STRENGTH OF HOLLOW ROUND AND HOLLOW RECTANGULAR CAST IRON COLUMNS.

For various values of  $\frac{L}{d}$  in which:—

L = length of column in feet.

d = least outside diameter in inches.

P = ultimate strength in pounds per square inch.

BASED ON GORDON'S FORMULÆ FOR COLUMNS WITH SQUARE ENDS.

HOLLOW RECTANGULAR. HOLLOW ROUND.

L		Strength er sq. in.	L	Ultimate in lbs. p	Strength er sq. in.
d	Hollow Round.	Hollow Rectangular,	d	Hollow Round.	Hollow Rectangular.
1.0	67800	70487	2.5	37647	43396
1.1	65692	68770	2.6	36088	41834
1.2	63532	66983	2.7	34599	40326
1.3	61340	65142	2.8	33178	38871
1.4	59137	63265	2.9	31817	37471
1.5	56940	61366	3.0	30534	36123
1.6	54766	59458	3.1	29306	34829
1.7	52625	57553	3.2	28137	33586
1.8	50531	55660	3.3	27025	32393
1.9	48491	53792	3.4	25967	31249
2.0	46512	51954	3.5	24961	30152
2.1	44598	50151	3.6	24004	29101
2.2	42753	48391	3.7	23093	28094
2.3	40979	46676	3.8	22227	27130
2.4	39277	45011	3.9	21403	26206

Safe loads for any given hollow round or hollow rectangular columns, corresponding to any suitable factor of safety can be found from the above table as follows:-Find from the table the ultimate strength in pounds per square inch corresponding d. Multiply this by the area of the column in square inches to the given value of and divide the product by the safety factor which will give as a quotient the required safe load in pounds.

Example: - Required the safe load for a hollow round cast iron column 16 feet long, 10 inches external diameter with metal 1 inch thick with safety factor of eight.  $\frac{L}{d}$  in this case is  $\frac{16}{10} = 1.6$  and the corresponding ultimate strength from

the tables is 54 766 pounds per square inch.

From the table of areas of circles it is found that the net area of the column is 28.3 square inches. The safe load is therefore 54.766 imes 28.3approximately 97 net tons, which is the required result.

# EXPLANATIONS OF TABLES OF SAFE LOADS FOR BEAM BOX-GIRDERS AND PLATE GIRDERS, PAGES 282 TO 296 INCLUSIVE.

For cases in which the loads to be carried exceed the capacities of single rolled beams or ordinary beam girders composed of two or more beams with the usual bolts and separators, it is necessary to use built-up sections.

BEAM BOX-GIRDERS .- A useful and economical section of this kind can be composed of two rolled beams with plates riveted to the top and bottom flanges, making a beam box-girder, tables of safe uniformly distributed loads for which are given on pages 282 to 291 inclusive.

The safe loads given in the tables include the weights of the beam box-girders. and are figured from the moment of inertia or section modulus after making the necessary deductions for rivet holes, the fibre stress used in the calculations being 15 000 pounds per square inch of net section.

Beam box-girders are particularly useful for supporting wide walls and in other locations up to the limits of their capacity, but they should not be placed where exposed to moisture, as the section is such that access cannot be had to their interior for inspection and painting.

PLATE GIRDERS.-In cases where the widths of beam box-girders would prohibit their use, and for loads greater than their capacities, plate girders composed of plates and angles may be used.

Tables of safe loads uniformly distributed for plate girders from 24" to 48" deep

are given on pages 292 to 296 inclusive.

The loads given in the tables include the weights of the girders and are calculated from the moment of inertia or section modulus after making a proper deduction for rivet holes, the fibre stress used in the calculations being 15000 pounds per

square inch of net section.

Although the tables do not show the stiffener angles for plate girders, care should be taken that these are provided in all cases where necessary to prevent buckling of the web due to the shearing action therein. The stiffeners should be made of angles riveted to the web, fitted tightly between the top and bottom flange angles, and they should be provided, at the ends of the girders, of such size and number as to be capable of carrying the total reaction at each end to the supports. Stif-

feners should also be provided at intervals along the girder, spaced at suitable distances apart as determined by the formula and explanations on pages 64 and 65.

Care should also be taken in arranging the rivet spacing for connecting the flange angles to the web, so that sufficient rivets are provided to properly transmit the stresses which act between these two portions of the construction. This will require the rivets to be spaced more closely at the ends than at the centre, and the exact spacing at any point along the girder may be obtained by dividing the product of the distance between the centre lines of the rivet holes in the two flanges and the resistance of one rivet by the total vertical shear at the given point, thus:

$$p = \frac{r h}{S}$$
 in which

S = the total vertical shear, in pounds, at the point under consideration.

r = the resistance of one rivet, i. e., the bearing value or shearing value, whichever is the smaller, expressed in pounds.

h = the depth of the girder between the upper and lower centre lines of rivets, expressed in inches.

p = pitch of rivets in the flange angles, expressed in inches.

The formula above will give the theoretical rivet spacing at any point in the flanges due to the total shear, but in practice the pitch for various portions of the length should be stated for the least possible number of spacing panels containing an even number of spaces, the pitch in each of which should preferably be expressed in even inches or even inches and halves or quartets of an inch, and the usual limits of pitch will vary from  $2\frac{1}{2}$ " to 6".

The rivet spacing should also conform to the rules given on page 312, and in

cases where loads are applied directly to the flanges, sufficient rivets must be provided to carry these in addition to the rivets necessary for securing the web and

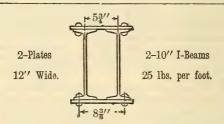
flanges together as explained above.

It should also be noted that the safe loads given in the tables are based on the assumption that the girder is supported laterally, otherwise a proper reduction in the allowable safe load must be made, as explained in connection with beams on

pages 62 and 63.

The weights of beam box-girders and plate-girders in the tables are expressed in pounds per lineal foot, including the rivets necessary to secure the web and flanges together, but the weights do not include any allowance for brackets, stiffeners, connections or other details, as these will vary, dependent upon the conditions of each case.

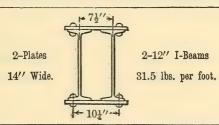
Safe loads below are figured for fibre stress of 15 000 pounds per square inch, with  $\frac{13}{18}$  rivet holes in both flanges deducted, and include weight of girder.



Distance Center to Center of Bearings in				of Pl Greater th					
Feet.	$\frac{1}{2}$	$\frac{9}{16}$	<u>5</u> 8	$\frac{1}{16}$	34	$\frac{\frac{1}{3}}{16}$	7/8	$\frac{15}{16}$	1
10	90	96	102	109	115	121	127	134	140
11	82	87	93	99	104	110	116	121	127
12	75	80	85	90	96	101	106	111	117
13	69	74	79	84	88	93	98	103	108
14	64	69	73	78	82	86	91	95	100
15	60	64	68	72	77	81	85	89	93
16	56	60	64	68	72	76	80	83	87
17	53	57	60	64	68	71	75	79	82
18	50	53	57	60	64	67	71	74	78
19	47	51	54	57	60	64	67	70	74
20	45	48	51	54	57	60	64	67	70
21	43	46	49	52	55	58	61	64	67
22	41	44	47	49	52	55	58	61	64
23	39	42	45	47	50	53	55	58	61
24	38	40	43	45	48	50	53	56	58
25	36	38	41	43	46	48	51	53	56
26	35	37	39	42	44	47	49	51	54
27	33	36	38	40	43	45	47	49	52
28	32	34	37	39	41	43	45	48	50
29	31	33	35	37	40	42	44	46	48
30	30	32	34	36	38	40	42	45	47
31	29	31	33	35	37	39	41	43	45
32	28	30	32	34	36	38	40	42	44
33	27	29	31	33	35	37	39	40	42
34	26	28	30	32	34	36	37	39	41
Weight per Foot in Pounds.	94.6	99.8	104.8	110.0	115.0	120.1	125.2	130.3	135.4
Section Modulus.	90.1	96.3	102.4	108.6	114.8	121.0	127.2	133.5	139.8
Coefficient of Deflection.	0.	00000145		0.0	0000118	3	0.	0000000	98

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings  $=\frac{1}{360}$  span.

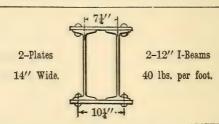
Safe loads below are figured for fibre stress of 15 000 pounds per square inch, with 13" rivet holes in both flanges deducted, and include weight of girder.



Distance Center		Thic	kness	of Pl	ates	in I	nche	es.	
to Center of Bearings in		For T	hicknesses!	Greater th	an 3/4"	Use Tw	o Plates.		
Feet.	$\frac{1}{2}$	9 16	<u>5</u> 8	$\frac{\frac{11}{16}}{16}$	34	13 16	7/8	$\frac{15}{16}$	1
10 11 12 13 14	132 120 110 102 94	141 128 117 108 101	150 136 125 115 107	159 144 132 122 113	167 152 140 129 120	176 160 147 136 126	185 168 154 143 132	194 177 162 149 139	203 185 169 156 145
15 16 17 18 19	88 83 78 73 70	94 88 83 78 74	100 94 88 83 79	106 99 93 88 83	112 105 98 93 88	118 110 104 98 93	123 116 109 103 98	129 121 114 108 102	135 127 120 113 107
20 21 22 23 24	66 63 60 57 55	70 67 64 61 59	75 71 68 65 62	79 76 72 69 66	84 80 76 73 70	88 84 80 77 73	93 88 84 81 77	97 92 88 84 81	102 97 92 88 85
25 26 27	53 51 49	56 54 52	60 58 55	63 61 59	67 64 62	71 68 65	74 71 69	78 75 72	81 78 75
28	47	50	53	57	60	63	66	69	73
29	46	49	52	55	58	61	64	67	70
30	44	47	50	53	56	59	62	65	68
31 32 33 34	43 41 40 39	45 44 43 41	48 47 45 44	51 50 48 47	54 52 51 49	57 55 53 52	60 58 56 54	63 61 59 57	66 64 62 60
Weight per Foot in Pounds,	114.4	120.4	126.3	132.3	138.3	144.2	150.1	156.1	162.0
Section Modulus.	132.1	140.9	149.7	158.5	167.4	176.3	185.3	194.2	203.2
Coefficient of Deflection.	0	.00000084	2	0.0	0000068	8	0.0	0000005	77

For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings  $= \frac{1}{360}$  span.

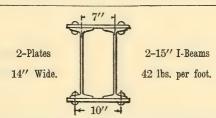
Safe loads below are figured for fibre stress of 15 000 pounds per square inch, with  $\frac{13}{16}$  rivet holes in both flanges deducted, and include weight of girder.



Distance Center to Center of			kness hicknesses						
Bearings in Feet.	$\frac{1}{2}$	$\frac{9}{16}$	<u>5</u> 8	$\frac{11}{16}$	34	13 16	7/8	15/6	1
10	147	155	164	173	181	190	199	208	217
11	133	141	149	157	165	173	181	189	197
12	122	129	137	144	151	158	166	173	181
13	113	119	126	133	140	146	153	160	167
14	105	111	117	123	130	136	142	148	155
15	98	104	109	115	121	127	133	139	144
16	92	97	102	108	113	119	124	130	135
17	86	91	96	102	107	112	117	122	127
18	81	86	91	96	101	106	111	115	120
19	77	82	86	91	95	100	105	109	114
20	73	78	82	86	91	95	99	104	108
21	70	74	78	82	86	91	95	99	103
22	67	71	75	78	82	86	90	94	99
23	64	68	71	75	79	83	87	90	94
24	61	65	68	72	76	79	83	87	90
25	59	62	66	69	73	76	80	83	87
26	56	60	63	66	70	73	77	80	83
27	54	58	61	64	67	70	74	77	80
28	52	55	59	62	65	68	71	74	77
29	51	54	57		63	66	69	72	75
30	49	52	55	58	60	63	66	69	73
31	47	50	53	56	59	61	64	67	70
32	46	49	51	54	57	59	62	65	68
33	44	47	50	52	55	58	60	63	66
34	43	46	48	51	53	56	59	61	64
Weight per Foot in Pounds.	131.4	137.4	143.3	149.3	155.3	161.2	167.1	173.1	179.0
Section Modulus.	146.6	155.3	163.9	172.7	181.4	190.2	199.0	207.8	216.7
Coefficient of Deflection.	0	.00000076	33	0.0	0000063	5	0.0	0000005	39

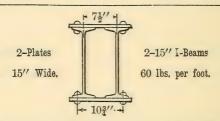
For safe loads below the heavy lines, the deflections will be greater than the allowable limit for plastered ceilings =  $\frac{1}{240}$  span.

Safe loads below are figured for fibre stress of 15 000 pounds per square inch, with 18" rivet holes in both flanges deducted, and include weight of girder.



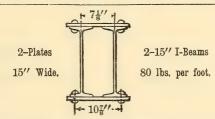
Distance Cen- ter to Center							lates an ¾"				
of Bearings in Feet.	5/8	$\frac{1}{1}\frac{1}{6}$	34	13 16	7/8	$\frac{15}{16}$	1	$1_{\frac{1}{16}}$	11/8	1 3 6	$1\frac{1}{4}$
10	212	223	234	245	256	267	278	289	300	312	323
11	193	203	213	223	233	243	253	263	273	283	293
12	177	186	195	204	213	223	232	241	250	260	269
13	163	172	180	188	197	205	214	223	231	240	248
14	151	159	167	175	183	191	199	207	215	223	231
15	141	149	156	163	171	178	185	193	200	208	215
16	133	139	146	153	160	167	174	181	188	195	202
17	125	131	138	144	151	157	164	170	177	183	190
18	118	124	130	136	142	148	155	161	167	173	179
19	112	117	123	129	135	141	146	152	158	164	170
20	106	112	117	122	128	134	139	145	150	156	161
21	101	106	111	117	122	127	132	138	143	148	154
22	96	101	106	111	116	121	126	131	137	142	147
23	92	97	102	107	111	116	121	126	131	135	140
24	88	93	98	102	107	111	116	121	125	130	135
25	85	89	94	98	102	107	111	116	120	125	129
26	82	86	90	94	98	103	107	111	116	120	124
27	79	83	87	91	95	99	103	107	111	115	120
28	76	80	84	88	91	95	99	103	107	111	115
29	73	77	81	84	88	92	96	100	104	107	111
30	71	74	78	82	85	89	93	96	100	104	108
31	68	72	75	79	83	86	90	93	97	101	104
32	66	70	73	77	80	83	87	90	94	97	101
33	64	68	71	74	78	81	84	88	91	94	98
34	62	66	69	72	75	79	82	85	88	92	95
Weight per Ft. in Pounds.	147.3	153.3	159.3	165.2	171.1	177.1	183.0	189.0	194.9	200.9	206.8
Section Modulus.	212.1	223.0	234.0	245.0	256.0	267.1	278.2	289.3	300.5	311.6	322.8
Coefficient of Deflection.	0.0	00000	426	0.0	0000003	62	0.0	0000003	14	0.0000	00281

Safe loads below are figured for fiber stress of 15 000 pounds per square inch, with  $\frac{15}{15}$ " rivet holes in both flanges deducted, and include weight of girder.



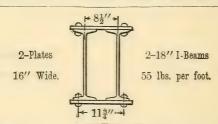
Distance Cen- ter to Center		Thickness of Plates in Inches. For Thicknesses Greater than 34" Use Two Plates.												
of Bearings in Feet.	5/8	$\frac{1}{1}\frac{1}{6}$	34	13 16	7/8	$\frac{15}{16}$	1	$1\frac{1}{16}$	11/8	1 3 1 6	11/4			
10 11 12 13 14	259 236 216 199 185	271 246 226 208 193	282 257 235 217 202	294 267 245 226 210	306 278 255 235 218	318 289 265 244 227	329 299 274 253 235	341 310 284 262 244	353 321 294 272 252	365 332 304 281 261	377 342 314 290 269			
15 16 17 18 19	173 162 152 144 136	181 169 159 150 143	188 177 166 157 149	196 184 173 163 155	204 191 180 170 161	212 198 187 176 167	220 206 194 183 173	227 213 201 190 180	235 221 208 196 186	243 228 215 203 192	251 235 222 209 198			
20 21 22 23 24	130 123 118 113 108	135 129 123 118 113	141 134 128 123 118	147 140 134 128 123	153 146 139 133 127	159 151 144 138 132	165 157 150 143 137	171 162 155 148 142	176 168 160 153 147	182 174 166 159 152	188 179 171 164 157			
25 26 27 28 29	104 100 96 93 89	108 104 100 97 93	113 109 105 101 97	118 113 109 105 101	122 118 113 109 105	127 122 118 113 109	132 127 122 118 114	136 131 126 122 118	141 136 131 126 122	146 140 135 130 126	151 145 140 135 130			
30 31 32 33 34	86 84 81 79 76	90 87 85 82 80	94 91 88 86 86 83	98 95 92 89 87	102 99 96 93 90	106 102 99 96 93	110 106 103 100 97	114 110 107 103 100	118 114 110 107 104	122 118 114 111 107	126 122 118 114 111			
Weight per Ft. in Pounds.	187.6	194.0	200.4	206.7	213.1	219.5	225.8	232.2	238.6	245.0	251.4			
Section Modulus.	259.2	270.8	282.4	294.1	305.8	317.5	329.3	341.1	353.0	364.9	376.8			
Coefficient of Deflection.	0.0	0.000000350									000240			

Safe loads below are figured for fiber stress of 15 000 pounds per square inch, with 18" rivet holes in both flanges deducted, and include weight of girder.



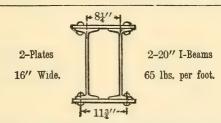
Distance Cen-			Thi	ekne	ess o	f Pla	ates	in Iı	iche	s.			
ter to Center		For Thicknesses Greater than 34" Use Two Plates.											
of Bearings in Feet.	<u>5</u> 8	11 16	3/4	13 16	7/8	15 16	1	116	11/8	1 3 1 6	$1\frac{1}{4}$		
10 11 12 13 14	300 272 250 231 214	311 283 259 239 222	322 293 269 248 230	334 303 278 257 238	345 314 288 265 247	357 324 297 274 255	368 335 307 283 263	380 345 316 292 271	391 356 326 301 279	403 366 336 310 288	414 377 345 319 296		
15 16 17 18 19	200 187 176 167 158	207 194 183 173 164	215 201 190 179 170	222 209 196 185 176	230 216 203 192 182	238 223 210 198 188	245 230 217 204 194	253 237 223 211 200	261 244 230 217 206	269 252 237 224 212	276 259 244 230 218		
20 21 22 23 24	150 143 136 130 125	156 148 141 135 130	161 154 147 140 134	167 159 152 145 139	173 164 157 150 144	178 170 162 155 149	184 175 167 160 153	190 181 173 165 158	196 186 178 170 163	201 192 183 173 168	207 197 188 180 173		
25 26 27 28 29	120 115 111 107 103	124 120 115 111 107	129 124 119 115 111	133 128 124 119 115	138 133 128 123 119	143 137 132 127 123	147 142 136 131 127	152 146 141 136 131	156 150 145 140 135	161 155 149 144 139	166 159 153 148 143		
30 31 32 33 34	100 97 94 91 88	104 100 97 94 91	107 104 101 98 95	111 108 104 101 98	115 111 108 105 102	119 115 111 108 105	123 119 115 112 108	127 122 119 115 112	130 126 122 119 115	134 130 126 122 118	138 134 130 126 122		
Weight per Ft. in Pounds.	227.6	234.0	240.4	246.7	253.1	259.5	265.8	272.2	278.6	285.0	291.4		
Section Modulus.	299.7	311.0	322.4	333.7	345.1	356.6	368.1	379.6	391.2	402.8	414.4		
Coefficient of Deflection.	0.0	00000	305	0.	0000002	269	0.	0000002	239	0.0000	000218		

Safe loads below are figured for fiber stress of 15000 pounds per square inch, with  $\frac{13}{6}$  rivet holes in both flanges deducted, and include weight of girder.



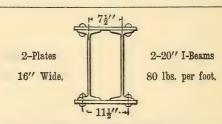
Distance Cen- ter to Center								ita III Use Two			
of Bearings in Feet.	3/4	$\frac{13}{16}$	7 8	15 16	1	116	11/8	1 3 1 6	$1\frac{1}{4}$	15	13/8
15	227	237	247	258	268	278	289	299	309	320	330
16	213	222	232	242	251	261	271	280	290	300	310
17	200	209	218	227	237	246	255	264	273	282	291
18	189	198	206	215	223	232	241	249	258	267	275
19	179	187	195	203	212	220	228	236	244	253	261
20	170	178	186	193	201	209	217	224	232	240	248
21	162	169	177	184	191	199	206	214	221	228	236
22	155	162	169	176	183	190	197	204	211	218	225
23	148	155	161	168	175	182	188	195	202	209	215
24	142	148	155	161	168	174	180	187	193	200	206
25	136	142	148	155	161	167	173	179	186	192	198
26	131	137	143	149	155	161	167	173	179	185	191
27	126	132	137	143	149	155	160	166	172	178	183
28	122	127	133	138	144	149	155	160	166	171	177
29	117	123	128	133	139	144	149	155	160	165	171
30	113	119	124	129	134	139	144	150	155	160	165
31	110	115	120	125	130	135	140	145	150	155	160
32	106	111	116	121	126	130	135	140	145	150	155
33	103	108	112	117	122	127	131	136	141	145	150
34	100	105	109	114	118	123	127	132	137	141	146
35	97	102	106	110	115	119	124	128	133	137	142
36	95	99	103	107	112	116	120	125	129	133	138
37	92	96	100	104	109	113	117	121	125	130	134
38	90	94	98	102	106	110	114	118	122	126	130
39	87	91	95	99	103	107	111	115	119	123	127
Weight per Ft. in Pounds.	195.5	202.2	209.0	215.8	222.6	229.4	236.2	243.1	249.8	256.7	263.4
Section Modulus.	340.5	355.8	371.2	386.6	402.1	417.5	433.0	448.6	464.2	479.8	495.4
Coefficient of Deflection.	0.0	000000	223	0.	0000001	.93	0.	0000001	70	0.000	000154

Safe loads below are figured for fiber stress of 15 000 pounds per square inch, with 18" rivet holes in both flanges deducted, and include weight of girder.



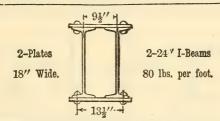
Distance Cen- ter to Center		•		_			ates				
of Bearings in Feet.	3 4	13	7/8	15 16	1	116	11/8	1 3 1 6	11/4	15/16	13/8
15	275	286	297	308	320	331	343	354	365	377	388
16	257	268	279	289	300	310	321	332	343	350	364
17	242	252	262	272	282	292	302	312	322	333	343
18	229	238	248	257	266	276	285	295	305	314	324
19	217	226	235	244	252	261	270	280	288	298	307
20	206	214	223	231	240	248	257	266	274	283	291
21	196	204	212	220	228	237	245	253	261	269	277
22	187	195	203	210	218	226	234	241	249	257	265
23	179	186	194	201	209	216	223	231	238	246	253
24	172	179	186	193	200	207	214	221	228	236	243
25	165	171	178	185	192	199	206	212	219	226	233
26	158	165	171	178	184	191	198	204	211	217	224
27	153	159	165	171	178	184	190	197	203	209	216
28	147	153	159	165	171	177	184	190	196	202	208
29	142	148	154	160	165	171	177	183	189	195	201
30	137	143	149	154	160	166	171	177	183	188	194
31	133	138	144	149	155	160	166	171	177	182	188
32	129	134	139	145	150	155	161	166	171	177	182
33	125	130	135	140	145	151	156	161	166	171	177
34	121	126	131	136	141	146	151	156	161	166	171
35	118	122	127	132	137	142	147	152	157	162	166
36	114	119	124	129	133	138	143	148	152	157	162
37	111	116	120	125	130	134	139	144	148	153	157
38	108	113	117	122	126	131	135	140	144	149	153
39	106	110	114	119	123	127	132	136	141	145	149
Weight per Ft. in Pounds.	215.5	222.2	229.0	235.8	242.6	249.4	256.2	263.1	269.8	276.7	283.4
Section Modulus.	411.8	428.7	445.7	462.7	479.7	496.7	513.8	531.2	548.1	565.3	582.5
Coefficient of Deflection.	0.0	00000	168	0.	0000001	147	0.	0000001	31	0.0000	000119

Safe loads below are figured for fiber stress of 15 000 pounds per square inch, with  $\frac{15}{15}$ " rivet holes in both flanges deducted, and include weight of girder.



Distance Cen- ter to Center								in In Use Two		S.	
of Bearings in Feet.	34	$\frac{13}{16}$	7/8	$\frac{15}{16}$	1	$1\frac{1}{16}$	11/8	$1\frac{3}{16}$	$1\frac{1}{4}$	$1\frac{5}{16}$	13/8
15	309	320	331	343	354	365	376	387	399	410	421
16	290	300	311	321	332	342	353	363	374	384	395
17	273	283	292	302	312	322	332	342	352	362	372
18	258	267	276	285	295	304	313	323	332	342	351
19	244	253	262	270	279	288	297	306	315	324	332
20	232	240	249	257	265	274	282	291	299	307	316
21	221	229	237	245	253	261	269	277	285	293	301
22	211	218	226	234	241	249	256	264	272	279	287
23	202	209	216	223	231	238	245	253	260	267	275
24	193	200	207	214	221	228	235	243	249	256	263
25	186	192	199	206	212	219	226	232	239	246	253
26	178	185	191	198	204	211	217	224	230	236	243
27	172	178	184	190	196	203	209	215	221	228	234
28	166	172	178	184	189	195	201	208	214	220	226
29	160	166	171	177	183	189	195	200	206	212	218
30	155	160	166	171	177	182	188	194	199	205	211
31	150	155	160	166	171	177	182	187	193	198	204
32	145	150	155	161	166	171	176	182	187	192	197
33	141	146	151	156	161	166	171	176	181	186	191
34	136	141	146	151	156	161	166	171	176	181	186
35	133	137	142	147	152	156	161	166	171	176	180
36	129	133	138	143	147	152	157	161	166	171	175
37	125	130	134	139	143	148	152	157	162	166	171
38	122	126	131	135	140	144	148	153	157	162	166
39	119	123	127	132	136	140	145	149	153	158	162
Weight per Ft. in Pounds.	245.5	252.2	259.0	265.8	272.6	279.4	286.2	293.1	299.8	306.7	313.4
Section Modulus	463.8	480.4	497.1	513.8	530.6	547.3	564.1	581.2	597.8	614.7	631.7
Coefficient of Deflection.	0.0	000000	149	0.	000000	133	0.	.0000001	119	0.000	000110

Safe loads below are figured for fiber stress of 15000 pounds per square inch, with 18" rivet holes in both flanges deducted, and include weight of girder.



Distance Cen- ter to Center		-						in X1 Use Two			
of Bearings in Feet.	34	13 16	7/8	15 16	1	$1_{\overline{1}\overline{6}}$	11/8	$1_{rac{3}{16}}$	$1\frac{1}{4}$	$1_{\frac{5}{16}}$	13/8
15	396	411	427	442	458	473	489	505	520	536	551
16	371	386	400	415	429	444	458	473	488	502	517
17	349	363	377	390	404	418	431	445	459	473	487
18	330	343	356	369	381	394	407	421	433	446	460
19	312	325	337	349	361	374	386	398	411	423	435
20	297	308	320	332	343	355	367	379	390	402	414
21	283	294	305	316	327	338	349	361	372	383	394
22	270	280	291	302	312	323	333	344	355	365	376
23	258	268	278	288	299	309	319	329	339	349	360
24	247	257	267	276	286	296	306	315	325	335	345
25	237	247	256	265	275	284	293	303	312	321	331
26	228	237	246	255	264	273	282	291	300	309	318
27	220	228	237	246	254	263	272	280	289	298	306
28	212	220	229	237	245	254	262	270	279	287	295
29	205	213	221	229	237	245	253	261	269	277	285
30	198	206	213	221	229	237	244	252	260	268	276
31	192	199	206	214	222	229	237	244	252	259	267
32	186	193	200	207	215	222	229	237	244	251	258
33	180	187	194	201	208	215	222	229	236	244	251
34	175	181	188	195	202	209	216	223	229	236	243
35	170	176	183	190	196	203	210	216	223	230	236
36	165	171	178	184	191	197	204	210	217	223	230
37	160	167	173	179	186	192	198	205	211	217	224
38	156	162	168	175	181	187	193	199	205	211	218
39	152	158	164	170	176	182	188	194	200	206	212
Weight per Ft. in Pounds.	255.7	263.3	271.0	278.6	286.2	293.9	301.5	309.2	316.8	324.5	332.1
Section Modulus.	593.7	616.9	640.1	663.4	686.7	710.0	733.3	757.1	780.2	803.6	827.1
Coefficient of Deflection.	0.00	000000	983	0.0	0000000	370	0.0	0000007	78	0.0000	0000713

# SAFE UNIFORMLY DISTRIBUTED LOADS FOR PLATE GIRDERS IN THOUSANDS OF POUNDS.

The safe loads below include the weight of the girder and are calculated for a fiber stress of 15 000 pounds per square inch on the net section. The net section is obtained by deducting holes figured at  $\frac{7}{8}$  of an inch in diameter (for  $\frac{3}{4}$ " rivets) from both flanges.

Web : 24" ×			Flange Ang $5^{\prime\prime} imes3^{\prime\prime}$		₩eb Pl 27"×			ge Angles
Distance Center to Center of		kness gles in					of Fl	
Bearings in Feet.	3/8	1/2	5/8	3/4	3/8	1/2	5/8	3/4
25 26 27 28 29	59 57 55 53 51	74 71 68 66 63	87 84 81 78 75	92 89 86	69 67 64 62 60	85 82 79 76 74	101 97 93 90 87	103 99
30 31 32 33 34	50 48 46 45 44	61 59 57 56 54	73 70 68 66 64	83 80 78 75 73	58 56 54 53 51	71 69 67 65 63	84 81 79 76 74	96 93 90 87 85
35 36 37 38 39	42 41 40 39 38	53 51 50 48 47	62 60 59 57 56	71 69 67 66 64	50 48 47 46 44	61 59 58 56 55	72 70 68 66 65	82 80 78 76 74
40 41 42 43 44	37 36 35 35 34	46 45 44 43 42	54 53 52 51 49	62 61 59 58 57	43 42 41 40 39	53 52 51 50 49	63 61 60 59 57	72 70 69 67 65
45 46 47 48 49	33 32 32 31 30	41 40 39 38 38	48 47 46 45 44	55 54 53 52 51	39 38 37 36 35	47 46 45 44 44	56 55 54 53 51	64 63 61 60 59
50 51 52 53 54	30 29 29 28 28 28	37 36 35 35 35 34	44 43 42 41 40	50 49 48 47 46	35 34 33 33 32	43 42 41 40 40	50 49 48 48 47	58 57 55 54 53
Weight per Foot in Pounds.	74.1	86.9	99.7	111.7	78	90.8	103.6	115.6

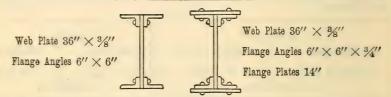
# SAFE UNIFORMLY DISTRIBUTED LOADS FOR PLATE GIRDERS IN THOUSANDS OF POUNDS.

The safe loads below include the weight of the girder and are calculated for a fiber stress of  $15\,000$  pounds per square inch on the net section. The net section is obtained by deducting holes figured at  $\frac{7}{8}$  of an inch in diameter (for  $\frac{3}{4}$ " rivets) from both flanges.

Web	Plate	ماه	Flange An	gles	Web P	late	Flan	ge Angles
30′′ )	× ¾"	<u> </u>	5" × 3½	⁄2''	33"×	³¾"′ 	5"	× 3½"
Distance Center to Center of			of Fl a Incl			kness gles i		
Bearings in Feet	3/8	1/2	5/8	3/4	3/8	1/2	5/8	3/4
30 31 32 33 34	74 71 69 67 65	91 88 86 83 81	108 105 101 98 95	116 113 109	83 81 78 76 74	103 100 97 94 91	122 118 114 111 107	131 127 123
35 36 37 38 39	63 61 60 58 57	78 76 74 72 70	93 90 88 85 83	106 103 101 98 95	72 70 68 66 64	88 86 84 81 79	104 101 99 96 94	119 116 113 110 107
40 41 42 43 44	55 54 53 51 50	69 67 65 64 62	81 79 77 75 74	93 91 89 86 85	63 61 60 58 57	77 75 74 72 70	91 89 87 85 83	104 102 99 97 95
45 46 47 48 49	49 48 47 46 45	61 60 58 57 56	72 71 69 68 66	83 81 79 77 76	56 54 53 52 51	69 67 66 64 63	81 79 78 76 75	93 91 89 87 85
50 51 52 53 54	44 43 43 42 41	55 54 53 52 51	65 64 62 61 60	74 73 72 70 69	50 49 48 47 46	62 61 59 58 57	73 72 70 69 68	84 82 80 79 77
55 56 57 58 59	40 39 39 38 37	50 49 48 47 46	59 58 57 56 55	68 66 65 64 63	46 45 44 43 42	56 55 54 53 52	66 65 64 63 62	76 75 73 72 71
Weight per Foot in Pounds.	86.6	101.4	116.2	129.4	90.4	105.2	120 <b>.0</b>	133.2

#### SAFE UNIFORMLY DISTRIBUTED LOADS FOR PLATE GIRDERS IN THOUSANDS OF POUNDS.

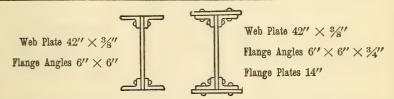
The safe loads below include the weight of the girder and are calculated for a fiber stress of 15 000 pounds per square inch on the net section. The net section is obtained by deducting holes figured at  $\frac{7}{8}$  of an inch in diameter (for  $\frac{3}{4}$ " rivets) from both flanges.



Distance Center to Center of Bearings	Thickness of Flange Angles in Inches.				Thickness of Flange Plate in Inches.				
in Feet.	3/8	1/2	5/8	3/4	1/2	5/8	3/4	7/8	1
30 31 32 33 34	108 104 101 98 95	134 130 125 122 118	159 154 149 144 140	183 177 171 166 161	238 230 223 216 210	255 247 239 232 225	264 256 248 241	264 256	
35	92	115	136	157	204	219	234	249	264
36	90	112	132	152	198	213	227	242	257
37	87	109	129	148	193	207	221	235	250
38	85	106	125	144	188	201	215	229	243
39	83	103	122	141	183	196	210	223	237
40	81	100	119	137	178	191	205	218	231
41	79	98	116	134	174	187	200	213	225
42	77	96	113	131	170	182	195	207	220
43	75	93	111	128	166	178	190	203	215
44	74	91	108	125	162	174	186	198	210
45	72	89	106	122	158	170	182	194	205
46	70	87	104	119	155	166	178	189	201
47	69	85	101	317	152	163	174	185	197
48	67	84	99	114	149	160	171	182	193
49	66	82	97	112	146	156	167	178	189
50	65	80	95	110	143	153	164	174	185
51	63	79	93	108	140	150	160	171	181
52	62	77	92	106	137	147	157	168	178
53	61	76	90	104	135	144	154	164	174
54	60	74	88	102	132	142	152	161	171
55	59	73	87	100	130	139	149	158	168
56	58	72	85	98	127	137	146	156	165
57	57	70	84	96	125	134	144	153	162
58	56	69	82	95	123	132	141	150	159
59	55	68	81	93	121	130	139	148	157
Weight per Foot in Pounds.	107.5	126.3	144.7	162.7	214.1	226	237.9	249.8	261.7

# SAFE UNIFORMLY DISTRIBUTED LOADS FOR PLATE GIRDERS IN THOUSANDS OF POUNDS.

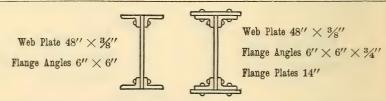
The safe loads below include the weight of the girder and are calculated for a fiber stress of 15 000 pounds per square inch on the net section. The net section is obtained by deducting holes figured at one inch in diameter (for  $\frac{7}{8}$ " rivets) from both flanges.



Distance Center to Center of	Thickness of Flange Angles in Inches.			lenter to lenter to lenter of learnings  Flange Angles in Inches.					late
in Feet.	1/2	5/8	3/4	1/2	5/8	3/4	7/8	1	11/4
35	139	164	189	240	257	275	292	309	309
36	135	160	184	234	250	267	284	301	
37	131	155	179	227	244	260	276	293	
38	128	151	174	221	237	253	269	285	
39	125	148	169	216	231	247	260	278	
40	122	144	165	210	225	240	256	271	301
41	119	140	161	205	220	235	249	264	294
42	116	137	157	200	215	229	243	258	287
43	113	134	154	195	210	224	238	252	280
44	111	131	150	191	205	219	232	246	274
45	108	128	147	187	200	214	227	241	268
46	106	125	144	183	196	209	222	235	262
47	103	122	141	179	192	205	217	230	256
48	101	120	138	175	188	200	213	226	251
49	99	117	135	172	184	196	209	221	246
50	97	115	132	168	180	192	204	217	241
51	95	113	130	165	177	189	200	212	236
52	94	111	127	162	173	185	197	208	232
53	92	109	125	159	170	181	193	204	227
54	90	107	122	156	167	178	189	201	223
55	88	105	120	153	164	175	186	197	219
56	87	103	118	150	161	172	183	193	215
57	85	101	116	147	158	169	179	190	211
58	84	99	114	145	155	166	176	187	208
59	82	98	112	142	153	163	173	184	204
60	81	96	110	140	150	160	170	180	201
61	80	94	108	138	148	158	168	178	197
62	78	93	107	136	145	155	165	175	194
63	77	91	105	133	143	153	162	172	191
64	76	90	103	131	141	150	160	169	188
Weight per Foot in Pounds.	134.9	153.3	171.3	224.7	236.6	248.5	260.4	272.3	296.1

# SAFE UNIFORMLY DISTRIBUTED LOADS FOR PLATE GIRDERS IN THOUSANDS OF POUNDS.

The safe loads below include the weight of the girder and are calculated for a fiber stress of  $15\,000$  pounds per square inch on the net section. The net section is obtained by deducting holes figured at one inch in diameter (for  $\frac{7}{8}$ " rivets) from both flanges.



Distance Center to Center of Bearings  Thickness of Flange Angles in Inches.				Thickness of Flange Plate in Inches.					
in Feet.	1/2	5/8	3/4	1/2	5/8	3/4	7/8	1	11/4
35	166	195	224	283	303	322	342	362	361
36	161	190	218	275	294	313	333	352	
37	157	185	212	267	286	305	324	342	
38	153	180	206	260	279	297	315	333	
39	149	175	201	254	272	289	307	325	
40	145	171	196	247	265	282	299	317	352
41	141	167	191	241	258	275	292	309	343
42	138	163	187	236	252	269	285	302	335
43	135	159	182	230	246	263	279	295	327
44	132	155	178	225	241	256	272	288	320
45	129	152	174	220	235	251	266	282	312
46	126	149	170	215	230	245	260	275	306
47	123	145	167	211	225	240	255	270	299
48	121	142	163	206	221	235	249	264	293
49	118	140	160	202	216	230	244	259	287
50	116	137	157	198	212	226	240	253	281
51	114	134	154	194	208	221	235	248	276
52	112	131	151	190	204	217	230	244	270
53	109	129	148	187	200	213	226	239	265
54	107	127	145	183	196	209	222	235	260
55	105	124	142	180	193	205	218	230	256
56	104	122	140	177	189	201	214	226	251
57	102	120	137	174	186	198	210	222	247
58	100	118	135	171	183	195	206	218	242
59	98	116	133	168	179	191	203	215	238
60	97	114	131	165	176	188	200	211	234
61	95	112	128	162	174	185	196	208	231
62	94	110	126	160	171	182	193	204	227
63	92	109	124	157	168	179	190	201	223
64	91	107	122	155	165	176	187	198	220
Weight per Foot in Pounds,	142.5	160.9	178.9	232.3	244.2	256.2	268	279.9	303.7

#### GRILLAGE BEAMS FOR FOUNDATIONS.

In designing foundations for walls or columns carrying heavy loads resting upon the soil, it is necessary to distribute the weight over a suitable area, and this is readily accomplished, in a small depth, by using a grillage composed of steel beams imbedded in concrete, thus obviating the necessity of large masses of masonry and deep excavations. For heavy loads on soil of small bearing power three tiers of beams may be necessary, while for lighter loads and soil of greater bearing power two tiers of beams will ordinarily suffice.

The grillage beams which are to be surrounded by concrete should be spaced not less than 3" apart in the clear between the flanges, so that the concrete may be thoroughly rammed between them and gas-pipe, or standard cast-iron separators should

be used to maintain the beams in proper position.

Knowing the total weight to be carried and the allowable intensity of loading per square foot of the supporting soil, the area of the footing required can be readily found, which taken into consideration with any other conditions limiting the form or proportions of the footing, will determine the external dimensions of the foundation. The beams may be considered as subjected to a uniform load extending over a portion of their upper surfaces, the centre of which is at the centre of length of the beams, and as being uniformly supported from below throughout their length.

Under these circumstances, the maximum bending moment will occur at the centre of the beam and, using the notation given for the upper tier in the sketch

below, this bending moment for one beam will be as follows:

Bending moment in inch pounds =  $\frac{W}{8}$  (c – b)

in which c and b are expressed in inches and W is the total weight in pounds on one beam, obtained by dividing the total load by the number of beams composing

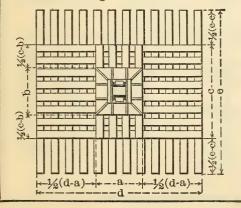
the tier in question.

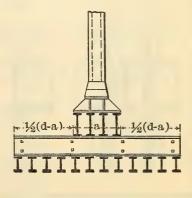
This formula for the bending moment is the same as that for a beam of the length (c-b) supported at the ends and uniformly loaded with the total weight W, so that the proper sizes of beams, bending considered, may be obtained directly from the tables of safe loads uniformly distributed for Cambria I-beams, on pages 76 to 86 inclusive, or for cases in which the lengths are shorter than those given in these tables, the sizes may be calculated from the coefficients of strength or the section moduli given in the tables of properties of I-beams, pages 156 to 159 inclusive, taking care, however, to use as the length, the distance (c-b), for the upper tier, and the corresponding figures for the other tiers.

After determining the size of beam required based upon bending, as stated above, an examination should also be made of the capacity of the beam web to resist buckling. This may be done by considering the web as a column of height equal to the clear distance between the fillets and calculating the safe load therefor by the use of the tables of strength for steel columns or struts, on pages 190 to 193, using the

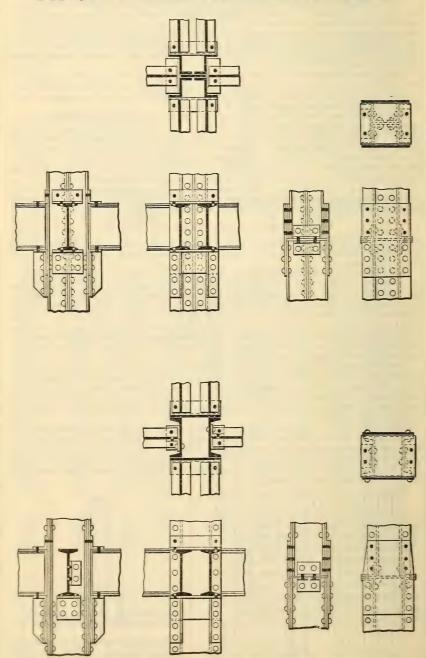
proper safety factor.

If the beam web is found insufficient as a column when calculated in this manner, a beam with a web of greater thickness should be tried until one is found that will meet this requirement and the conditions for bending; or it might be more economical, in some cases, to use the beam with the thinner web and provide it with sufficient separators, fitting between the beam flanges, or stiffeners secured to the web to assist it in resisting as a column.

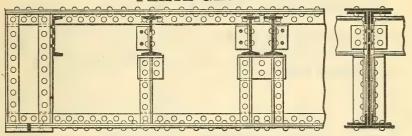


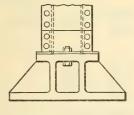


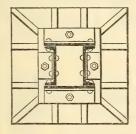
# TYPICAL DETAILS FOR STEEL COLUMNS.

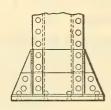


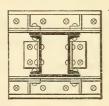
# TYPICAL DETAILS OF COLUMN BASES AND PLATE GIRDERS.

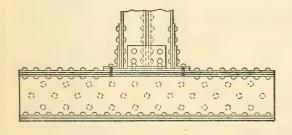


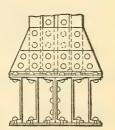


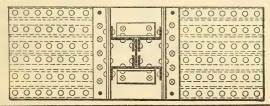












Allowable Unit Stresses for Steel and Iron.	New York. 1902.	Chicago. 1902.	Philadelphia, 1902.	Boston. 1902.			
Steel and Iron.	Pounds per Square Inch.						
COMPRESSION: Rolled Steel Rolled Steel	16,000		14 500‡ 16 250∥				
Wrought Iron	16 000 12 000 16 000		12 500 17 500	8 000			
Steel Pins and Rivets (Bearing) Wrought Iron Pins and Rivets (Bearing)	20 000 15 000	20 000 15 000		18 000 15 000			
TENSION: Rolled Steel	16 000 16 000	15,000	14500† $16250$	15 000			
Wrought Iron	12 000 3 000	12 000	12 500	12 000			
EXTREME FIBER STRESS—BENDING Rolled Steel Beams	16 000	16 000		16 000			
" Pins, Rivets and Bolts	20 000	22 500 15 000		22 500			
Riveted "Beams (Net Flange Section) Rolled Wrought Iron Beams	14 000 12 000	12 000	• • •	12 000			
" " Pins,Rivets & Bolts Riveted " Beams (Net Flange	15 000	18 000		18 000			
Section)	12 000 16 000	10 000		8 000			
" Tension "	3 000	2 500	3 750	2 500			
Compression in Flanges of Built Beams, Steel				12 000			
Wrought Iron				10 000			
SHEAR: Steel Web Plates	9 000		8 750‡ 10 000∥	10 000			
" Shop Rivets and Pins	10,000	10 000	8 750‡ 10 000∥	66			
" Field " " "	8,000	66	8 750‡ 10 000	66			
" Bolts	7 000		8 750‡ 10 000	66			
Wrought Iron Web Plates	6 000	7.500	7 500	9 000			
" Shop Rivets and Pins	7 500 6 000	7 500	ee	"			
Cast Iron	5 500 3 000		"	66			
	_		14 500				
COLUMNS: Mild Steel	$15200-58\frac{L}{R}$	15 000*	$1 + \frac{L^2}{13500R^2}$	12 000*			
			16 250				
Medium Steel	66	66	$1 + \frac{L^2}{11000R^2}$	66			
	T.		12 500				
Wrought Iron	$14000-80\frac{L}{R}$	12 000*	$1 + \frac{L^2}{15000D^2}$	10 000*			
	Т.		17 000	See Section 19 of Bos-			
Cast Iron	$11300-30\frac{L}{R}$	10 000†	$1 + \frac{L^2}{400D^2}$	ton Build- ing Laws			
* Reduced by approved modern formulæ. † Mild.    Medium. † Reduced by Gordon's formula. Reduced for eccentric loads.							

Live Loads for Floors in Different	Man W	( nr:	Dhilad-lati	Dont	
Live Loads for Floors in Different Classes of Buildings, Exclusive of the Weight of the Materials	New York, 1902.	Chicago. 1902.	Philadelphia. 1902.	Boston. 1902.	
of Construction.	Pounds per Square Foot.				
Dwellings, Apartment Houses, Hotels,		1			
Tenement Houses or Lodging Houses	60	40	70	50	
Office Buildings—First Floor	150	100	100	100	
" above First Floor	<b>7</b> 5	100	100	100	
Schools or Places of Instruction	75	C 40%		80	
Stables or Carriage Houses	75	{ 40* 100†	• • •	• • •	
Buildings for Public Assembly "Ordinary Stores, Light Manu-	90	100	120	150	
facturing and Light Storage	120	100	120		
facturing and Light Storage Stores for Heavy Materials, Warehouses					
and Factories	150		150	250	
Roofs—Pitch less than 20°	50	25	30	25‡	
more 20	30	25	30	25‡	
Sidewalks Public Buildings, except Schools	300			150	
Allowable Unit Stresses for Ma-					
sonry and Building Materials.		1	1		
COMPRESSION.	Pounds per Square Inch.				
Concrete (Portland) Cement, 1; Sand, 2;			1		
Stone, 4	230	55	208		
Concrete (Portland) Cement, 1; Sand, 2;	208	66	66		
Stone, 5	208				
Sand, 2; Stone, 4	125	66	66		
Concrete (Rosendale or equal) Cement, 1;					
Sand, 2; Stone, 5	111	66	"		
Rubble Stonework, Portland Cement Mortar	140		139		
" Rosendale " "	111		66		
Lime and	97		111		
Brickwork in Portland Cement Mortar;	70		69½		
Cement, 1; Sand, 3	250		208		
Brickwork in Rosendale, or equal, Cement	208		66		
Mortar; Cement, 1; Sand, 3 Brickwork in Lime and Cement Mortar;	208				
Cement, 1; Lime, 1; Sand, 6	160		167		
Brickwork in Lime Mortar; Lime, 1; Sand, 4.	111		111		
Dimension Stones in Cement Mortar		70			
Beds		97			
Granites (according to Test)	1000 to 2400				
Greenwich Stone Gneiss (New York City)	1200				
Gneiss (New York City)	1300				
Limestone (according to Test)	700 to 2300				
)	600 to 1200				
	400 to 1600				
Bluestone (North River) Brick (Haverstraw, Flatwise)	$\frac{2000}{300}$		• • •		
Slate	1000				
	2000				

<sup>\*</sup>Stables less than 500 Square Feet in Area.

<sup>† &</sup>quot; over 500 " ... Wind at 30 lbs. per Square Foot Horizontal.

Allowable Unit Stresses for Masonry.	New York. 1902.	Chicago. 1902.	Philadelphia. 1902.	Boston. 1902.
EXTREME FIBRE STRESS-BENDING	Transmission of the Contract and Contract an	Pounds pe	r Square Inch.	
Granite Greenwich Stone Gneiss (New York City) Limestone Slate Marble Sandstone Bluestone—North River Concrete (Portland) Cement, 1; Sand, 2; Stone, 4 Concrete (Portland) Cement, 1; Sand, 2; Stone, 5 Concrete (Rosendale or equal) Cement, 1; Sand, 2; Stone, 4 Concrete (Rosendale or equal) Cement, 1; Sand, 2; Stone, 5 Brick (Common) Brickwork (in Cement)  Allowable Unit Stresses for Timber.	30			
Oak, with Grain	900 800 1000 600 800 400 800 400 1200 1000 500 500 500		750 91 <sup>2</sup> / <sub>3</sub> 500 50 50 41 <sup>2</sup> / <sub>3</sub>	250 250 150 150
Yellow Pine White " Spruce Oak Hemlock	1200 800 800 1000 600		1800 1250 1000	• • •

	1 1		
New York. 1902.	Chicago 1902.	Philadelphia. 1902.	Boston. 1902.
Poun	ds Per	Square Inch.	
1200 800 800 1000	1250 750 750 1000	1600	1250 750 750 1000
1200 600 800	• • •	900	• • •
1000-18 <sup>L</sup> / <sub>P</sub>		$\frac{\mathrm{U}}{6} \times \frac{\mathrm{L}^*}{600\mathrm{D}}$	
$800-15\frac{L}{D}$		66	
900-17 <sup>L</sup> <sub>D</sub>		66	
$\frac{5}{8}(800-15\frac{L}{D})$		66	
1½(")		66	
70 500	100 250	66 <sup>2</sup> / <sub>3</sub>	100
250	150	50	80
320	150	500	
600	250		150
720		/12/	
275 150		41623	
	$\begin{array}{c c} & 1902. \\ \hline & & & \\ \hline &$	$\begin{array}{ c c c c }\hline 1902. & 1902. \\ \hline & 1902. & 1902. \\ \hline & Pounds Per & 3 \\ \hline & 1200 & 1250 \\ 800 & 750 \\ 1000 & 1000 \\ 1200 & 600 & \\ \hline & & & & & \\ \hline & 1000-18\frac{L}{D} & \\ \hline & & & & & \\ \hline & & & & & \\ \hline & & & &$	$\begin{array}{ c c c c c c c c c }\hline & 1902. & 1902. & 1902. \\ \hline \hline & Pounds Per Square Inch. \\ \hline & 1200 & 1250 & 1600 \\ 800 & 750 & 1100 \\ 1000 & 1000 & . & . & . \\ 1200 & 600 & . & . & . & . \\ 600 & 800 & . & . & . & . \\ \hline & & & & & & & \\ \hline & & & & & & \\ \hline & & & &$

 $*\frac{U}{6}$  = Allowable Compression in Lbs. per Sq. Inch and  $\frac{L}{D}$  = Ratio of Length to Diameter in Inches.

Allowable Unit Stresses for Timber Columns in Accordance with the Building Laws of Boston and Chicago.

#### For Posts with Flat Ends.

The Stresses given in the following table, in which L = Length of Post, D = Least Diameter of Post, and S = Stress per Square Inch.

White Pine and Spruce.		Long-Leaf Y	White Oak.	
$\frac{\mathbf{L}}{\mathbf{D}}$	S	L D	S	S
0 to 10 10 " 35 35 " 45 45 " 50	625 500 375 250	0 to 15 15 " 30 30 " 40 40 " 45 45 " 50	1000 875 750 625 500	750 650 560 470 375

For information not given in these tables, see Complete Building Laws of the Various Cities.

# EXPLANATION OF TABLES OF RIVETS AND PINS.

#### Rivets.

In the design of riveted joints the total stress transmitted is assumed to be taken up by the rivets, no allowance being made for the friction between the plates riveted together, and the manner of failure of the joint will be by shearing of the rivet or crushing of the plate. This assumes that the rules given on page 312 are followed and failure by tearing off the plate caused by the rivets being too near the edge is thus prevented.

In the table of "Shearing Value of Rivets and Bearing Value of Riveted Plates," pages 306 and 307, these values are given for all customary sizes and thicknesses corresponding to various usual allowable unit stresses.

For any given size of rivet or thickness of plate to be used, an inspection of the table will show at once if the bearing value of the plate or the shearing value of the rivet is to govern the design and the amount of stress that can be transmitted by each rivet.

#### Pins.

In designing pin-connected joints the points which govern the design are the bending moments produced in the pin by the bars or plates connected, and the bearing value of the plates themselves. The bearing value in the case of eye-bars of proper proportions is sufficiently ample and need not be computed. Shear in pins need not ordinarily be considered, as the bending and bearing stresses usually determine the size.

In the table of "Maximum Bending Moments on Pins," pages 308 and 309, is given the allowable bending moments on pins of various diameters for the usual allowable fibre stresses.

In the table of "Bearing Values of Pin Plates for One-Inch Thickness of Plate," on page 313, is given the allowable bearing values of plates against pins of various usual diameters, corresponding to the customary unit stresses of this character.

If the bearing value exceeds the allowable limit in any given case pin-plates must be added, thus increasing the bearing value until it is reduced to a safe limit as shown by the tables.

#### CONVENTIONAL SIGNS FOR RIVETING.

FIELD. **S**нор. Two Full Heads. Countersunk Inside (Farside) and Chipped. Countersunk Outside (Nearside) and Chipped. Countersunk both Sides and Chipped. OUTSIDE. INSIDE. (NEARSIDE.) BOTH SIDES. (FARSIDE.) Flattened to 1/8" high or Countersunk and not Chipped. Flattened to 1/4" high. Flattened to 3/4" high.

This system, designed by F. C. Osborn, C.E., has for foundation the diagonal cross to represent a countersink, the blackened circle for a field rivet and the diagonal stroke to indicate a flattened head. The position of the cross, with respect to the circle (inside, outside or both sides), indicates the location of the countersink and similarly the number and position of the diagonal strokes indicate the height and position of the flattened heads.

Any combination of field, countersunk and flattened head rivets liable to occur may be readily indicated by the proper combination of above signs.

## SHEARING VALUE OF RIVETS AND BEARING VALUE OF RIVETED PLATES.

ALL DIMENSIONS IN INCHES.
Shearing Value = Area of Rivet × Allowable Shearing Stress per Square Inch.

Diameter	Area	Single	Double	Bearin	for Di	Different		
of Rivet.	Square Inches.	Shear at 6 000 lbs.	Shear at 12 000 lbs.	$\frac{1}{4}$	<u>5</u> 16	38	7 16	
3/8	.1105	663	1325	1125		1688		
1/2	.1964	1178	2356	1500		2250		
5/8	.3068	1841	3682	1875		2813	3281	
3/4	.4418	2651	5301	2250		3375		
7/8	.6013	3608	7216	2625	3281	3938		
1	.7854	4712	9425	3000	3750	4500	5250	
Diameter	Area	Single	Double	Bearin	g Value	for Di	fferent	
of Rivet.	in Square Inches.	Shear at 6 750 lbs.	Shear at 13 500 lbs.	$\frac{1}{4}$	$\frac{5}{16}$	38	<b>7</b> 16	
3/8	.1105	746	1491	1266	1582	1898		
1/2	.1964	1325	2651	1688	2109	2531	2953	
5/8	.3068	2071	4142	2109	-	3164		
3/4	.4418	2982	5964	2531		3797	4430	
7/8	.6013	4059	8118	2953	3691	-	5168	
1	.7854	5301	10603	3375	4219	5063	5906	
Diameter	Area	Single	Double	Bearin	g Value	for Di	fferent	
of	in	Shear at	Shear at					
Rivet.	Square Inches.	7 500 lbs.	15 000 lbs.	$\frac{1}{4}$	$\frac{5}{16}$	8	$\frac{7}{16}$	
9/	1105	000	1058	1400	1850	0100		

	1			1	10		10
3/8	.1105	828	1657	1406	1758	2109	
1/2	.1964	1473	2945	1875	2344	2813	3281
5/8	.3068	2301	4602	2344	2930	3516	4102
3/4	.4418	3313	6627	2813	3516	4219	4922
7/8	.6013	4510	9020	3281	4102	4922	5742
1	.7854	5891	11781	3750	4688	5625	6563
Diameter	Area	Single	Double	Bearin	g Value	for Di	ferent

Diameter	Area	Single	Double	Bearing Value for Differe					
of Rivet.	in Square Inches.	Shear at 10 000 lbs.	Shear at 20 000 lbs.	$\frac{1}{4}$	$\frac{5}{16}$	<u>3</u>	$\frac{7}{16}$		
3/8	.1105	1105	2209	1875					
1/2	.1964	1964	3927	2500	3125	3750	4375		
5/8	.3068	3068	6136	3125	3906	4688	5469		
3/4	.4418	4418	8836	3750	4688	5625	6563		
7/8	.6013	6013	12026	4375	5469	6563	7656		
1	.7854	7854	15708	5000	6250	7500	8750		

In the above tables the bearing values between the lower and upper zigzag black lines are greater than single and less than double shear for the corresponding dimensions, so that in case of single shear the single shearing value governs, and in case of double shear, the bearing value governs the design.

## SHEARING VALUE OF RIVETS AND BEARING VALUE OF RIVETED PLATES.

ALL DIMENSIONS IN INCHES.

Bearing Value = Diameter of Rivet × Thickness of Plate × Allowable Bearing Stress per Square Inch	
Thicknesses of Plate in Inches at 12 000 Pounds per Square Inch	

1/2	9 16	<u>5</u> 8	$\frac{1}{1}\frac{1}{6}$	$\frac{3}{4}$	$\frac{13}{16}$	78	$\frac{15}{16}$	1
2000								
3000								
3750	4219	4688						
4500	5063	5625	6188	6750				
5250	5906	6563	7219	7875	8531	9188	9844	
6000	6750	7500	8250	9000	9750	10500	11250	12000
· ·								

#### 

		-						
3375								
4219	4746	5273						
5063		6328						
5906	6645	7383	8121	8859	9598	10336	11074	
6750	7594	8438	9281	10125	10969	11213	12656	13500

## Thicknesses of Plate in Inches at 15 000 Pounds per Square Inch.

0
)

## Thicknesses of Plate in Inches at 20 000 Pounds per Square Inch.

$\frac{1}{2}$	$\frac{9}{16}$	<u>5</u>	$\frac{1}{1}\frac{1}{6}$	$\frac{3}{4}$	$\frac{13}{16}$	78	$\frac{15}{16}$	1
5000								
6250	7031	7813						
7500	8438	9375	10313	11250				
8750	9844	10938	12031	13125	14219	15313	16406	
10000	11250	12500	13750	15000	16250	17500	18750	20000

The bearing values above and to the right of the upper zigzag black lines are greater than double shear for the corresponding dimensions, so that in these cases the shearing values govern the design.

The bearing values below and to the left of the lower zigzag black lines are less than single shear, so that in these cases the bearing values govern the design.

# MAXIMUM BENDING MOMENTS ON PINS WITH EXTREME FIBRE STRESSES

VARYING FROM 15 000 TO 25 000 POUNDS PER SQUARE INCH.

Diameter of	Area of Pin	Mom	ents in I	nch-Pot tresses		Fibre
Pin in Inches.	in Square Inches.	15 000 Lbs. per Square Inch.	18 000 Lbs. per Square Inch.	20 000 Lbs. per Square Inch.	22 500 Lbs. per Square Inch.	25 000 Lbs. per Square Inch.
1 1½ 1½ 1¾ 13/8	.785 .994 1.227 1.485	1470 2100 2900 3830	1770 2520 3450 4590	1960 2800 3830 5100	2210 3150 4310 5740	2450 3490 4790 6380
$1\frac{1}{2}$ $1\frac{5}{8}$ $1\frac{3}{4}$ $1\frac{7}{8}$	1.767	4970	5960	6630	7460	8280
	2.074	6320	7580	8430	9480	10530
	2.405	7890	9470	10520	11840	13150
	2.761	9710	11650	12940	14560	16180
2	3.142	11780	14140	15710	17670	19630
2 <sup>1</sup> / <sub>8</sub>	3.547	14130	16960	18840	21200	23550
2 <sup>1</sup> / <sub>4</sub>	3.976	16770	20130	22370	25160	27960
2 <sup>3</sup> / <sub>8</sub>	4.430	19730	23670	26300	29590	32880
21/2	4.909	23010	27610	30680	34510	38350
25/8	5.412	26640	31960	35520	39960	44400
23/4	5.940	30630	36750	40830	45940	51040
27/8	6.492	34990	41990	46660	52490	58320
3 <sup>1</sup> / <sub>8</sub> 3 <sup>1</sup> / <sub>4</sub> 3 <sup>3</sup> / <sub>8</sub>	7.069 7.670 8.296 8.946	39730 44940 50550 56610	47680 53930 60660 67940	52970 59920 67400 75480	59600 67410 75830 84920	66220 74900 84250 94350
31/2	9.621	63140	75770	84180	94710	105230
35/8	10.321	70150	84180	93530	105220	116910
33/4	11.045	77660	93190	103540	116490	129430
37/8	11.793	85690	102820	114250	128530	142810
4	12.566	94250	113100	125660	141370	157080
4 <sup>1</sup> / <sub>8</sub>	13.364	103360	124040	137820	155040	172270
4 <sup>1</sup> / <sub>4</sub>	14.186	113050	135660	150730	169570	188410
4 <sup>3</sup> / <sub>8</sub>	15.033	123320	147980	164420	184980	205530
4½	15.904	134190	161030	178920	201290	223650
45/8	16.800	145690	174830	194250	218510	242810
43/4	17.721	157820	189390	210430	236740	263040
47/8	18.665	170580	204740	227490	255920	284360
5	19.635	184080	220890	245440	276120	306800
5 <sup>1</sup> / <sub>8</sub>	20.629	198230	237880	264310	297350	330390
5 <sup>1</sup> / <sub>4</sub>	21.648	213090	255710	284120	319640	355160
5 <sup>3</sup> / <sub>8</sub>	22.691	228680	274420	304910	343020	381130
5 <sup>1</sup> / <sub>2</sub>	23.758	245010	294010	326680	367510	408350
5 <sup>5</sup> / <sub>8</sub>	24.850	262100	314510	349460	393140	436830
5 <sup>3</sup> / <sub>4</sub>	25.967	279960	335950	373280	419940	466600
5 <sup>7</sup> / <sub>8</sub>	27.109	298620	358340	398160	447930	497700

# MAXIMUM BENDING MOMENTS ON PINS WITH EXTREME FIBRE STRESSES

VARYING FROM 15 000 TO 25 000 POUNDS PER SQUARE INCH.

Diameter of	Area of Pin	Mom		nch-Pou tresses c		Fibre
Pin in Inches.	in Square Inches.	15 000 Lbs. per Square Inch.	18 000 Lbs. per Square Inch.	20 000 Lbs. per Square Inch.	22 500 Lbs. per Square Inch.	25 000 Lbs. per Square Inch.
$ \begin{array}{c} 6 \\ 6^{1/8} \\ 6^{1/4} \\ 6^{3/8} \end{array} $	28.274	318090	381700	424120	477130	530140
	29.465	338380	406060	451180	507580	563970
	30.680	359530	431430	479370	539290	599210
	31.919	381530	457840	508710	572300	635890
$6\frac{1}{2}$ $6\frac{5}{8}$ $6\frac{3}{4}$ $6\frac{7}{8}$	33.183	404420	485400	539230	606630	674030
	34.472	428200	513840	570940	642300	713670
	35.785	452900	543480	603870	679350	754830
	37.122	478530	574240	638040	717800	797550
7 7½ 7½ 7¾ 7³/ <sub>8</sub>	38.485 39.871 41.282 42.718	505110 532650 561180 590710	606130 639190 673420 708860	673480 710210 748250 787620	757660 798980 841780 886070	841850 887760 935310 984520
7 <sup>1</sup> / <sub>2</sub>	44.179	621260	745510	828350	931890	1035440
7 <sup>5</sup> / <sub>8</sub>	45.664	652850	783410	870460	979270	1088080
7 <sup>3</sup> / <sub>4</sub>	47.173	685480	822580	913980	1028220	1142470
7 <sup>7</sup> / <sub>8</sub>	48.707	719190	863030	958920	1078780	1198650
8	50.265	753980	904780	1005310	1130970	1256640
8 <sup>1</sup> / <sub>8</sub>	51.849	789880	947860	1053170	1184820	1316470
8 <sup>1</sup> / <sub>4</sub>	53.456	826900	992280	1102530	1240350	1378170
8 <sup>3</sup> / <sub>8</sub>	55.088	865060	1038070	1153410	1297590	1441760
8 <sup>1</sup> / <sub>2</sub>	56.745	904370	1085250	1205830	1356560	1507290
8 <sup>5</sup> / <sub>8</sub>	58.426	944860	1133830	1259820	1417290	1574770
8 <sup>3</sup> / <sub>4</sub>	60.132	986540	1183850	1315390	1479810	1644240
8 <sup>7</sup> / <sub>8</sub>	61.862	1029430	1235310	1372570	1544140	1715710
9	63.617	1073540	1288250	1431390	1610310	1789240
91/8	65.397	1118900	1342680	1491860	1678340	1864830
91/4	67.201	1165510	1398610	1554010	1748270	1942520
98/8	69.029	1213400	1456080	1617870	1820100	2022340
91/2	70.882	1262590	1515110	1683450	1893880	2104310
95/8	72.760	1313090	1575700	1750780	1969630	2188480
93/4	74.662	1364910	1637900	1819880	2047370	2274850
97/8	76.590	1418090	1701700	1890780	2127130	2363480
$   \begin{array}{c}     10 \\     10^{1} 4 \\     10^{1} 2 \\     10^{3} 4   \end{array} $	78.540 82.516 86.590 90.763	$\begin{array}{c} 1472620 \\ 1585850 \\ 1704740 \\ 1829430 \end{array}$	1767150 1903020 2045690 2195320	1963500 2114470 2272990 2439250	2208930 2378780 2557120 2744150	2454370 2643090 2841240 3049060
$   \begin{array}{c}     11 \\     11\frac{1}{4} \\     11\frac{1}{2} \\     12   \end{array} $	95.033	1960060	2352070	2613410	2940090	3266770
	99.402	2096760	2516110	2795680	3145140	3494600
	103.869	2239670	2687610	2986230	3359510	3732790
	113.098	2544690	3053630	3392920	3817040	4241150

#### RIVETS.

## TABLES OF AREAS IN SQUARE INCHES, TO BE DEDUCTED FROM RIVETED PLATES OR SHAPES TO OBTAIN NET AREAS.

Thick- ness Plates		_			SIZ		)F I	HOI	Æ.					
in Inches.	1/4	5 16	3/8	7 16	1/2	9 16	5/8	11 16	3/4	13 16	7/8	15 16	1	110
1/4 16 3/8 7 16	.06 .08 .09	.08 .10 .12 .14	.09 .12 .14 .16	.11 .14 .16 .19	.13 .16 .19 .22	.18	.20	.21	.19 .23 .28 .33	.20 .25 .30	.22 .27 .33	.23 .29 .35 .41	.31	
$\frac{1}{2}$ $\frac{9}{16}$ $\frac{5}{8}$ $\frac{11}{16}$	.13 .14 .16 .17	.16 .18 .20 .21	.19 .21 .23 .26	.22 .25 .27 .30	.25 .28 .31 .34	.28 .32 .35 .39	.35	.39	.38 .42 .47 .52	.41 .46 .51	.44 .49 .55	.47 .53 .59 .64	.50 .56 .63	
3/4 136 7/8 156 156	.19 .20 .22 .23	.23 .25 .27 .29	.28 .30 .33 .35	.33 .36 .38 .41	.38 .41 .44 .47	.42 .46 .49 .53	.47 .51 .55	.52 .56 .60 .64	.56 .61 .66 .70	.61 .66 .71 .76	.66 .71 .77 .82	.70 .76 .82 .88	.75 .81 .88 .94	.80 .86 .93 1.00
$1 \\ 1\frac{1}{16} \\ 1\frac{1}{8} \\ 1\frac{3}{16}$	.25 .27 .28 .30	.31 .33 .35 .37	.38 .40 .42 .45	.44 .46 .49 .52	.50 .53 .56	.56 .60 .63 .67	.63 .66 .70 .74	.69 .73 .77 .82	.75 .80 .84 .89	.81 .86 .91 .96	.88 .93 .98 1.04	.94 1.00 1.05 1.11	1.06	1.13 1.20
$ \begin{array}{c} 1\frac{1}{4} \\ 1\frac{5}{16} \\ 1\frac{3}{4} \\ 1\frac{7}{16} \end{array} $	.31 .33 .34 .36	.39 .41 .43 .45	.47 .49 .52 .54	.55 .57 .60 .63	.63 .66 .69	.70 .74 .77 .81	.78 .82 .86 .90	.86 .90 .95	.94 .98 1.03 1.08	1.02 1.07 1.12 1.17	1.09 1.15 1.20 1.26	1.17 1.23 1.29 1.35	1.25 1.31 1.38 1.44	
$\begin{array}{c} 1\frac{1}{2} \\ 1\frac{9}{16} \\ 1\frac{5}{8} \\ 1\frac{11}{16} \end{array}$	.38 .39 .41 .42	.47 .49 .51 .53	.56 .59 .61 .63	.66 .68 .71 .74	.75 .78 .81 .84	.84 .88 .91 .95	.94 .98 1.02 1.05	1.03 1.07 1.12 1.16	1.13 1.17 1.22 1.27	1.22 1.27 1.32 1.37	1.31 1.37 1.42 1.47	1.41 1.46 1.52 1.58	1.50 1.56 1.63 1.69	1.66 1.73
$ \begin{array}{c} 1\frac{3}{4} \\ 1\frac{13}{16} \\ 1\frac{1}{8} \\ 1\frac{15}{16} \\ 2 \end{array} $	.44 .45 .47 .48 .50	.55 .57 .59 .61 .63	.66 .68 .70 .73	.77 .79 .82 .85	.88 .91 .94 .97 1.00	.98 1.02 1.05 1.09 1.13	1.09 1.13 1.17 1.21 1.25	1.20 1.25 1.29 1.33 1.38	1.31 1.36 1.41 1.45 1.50	1.42 1.47 1.52 1.57 1.63	1.53 1.59 1.64 1.70 1.75	1.64 1.70 1.76 1.82 1.88	1.75 1.81 1.88 1.94 2.00	1.93 1.99 2.06

#### MAXIMUM SIZE OF RIVETS IN BEAMS, CHANNELS AND ANGLES.

I-BEAMS.						CH	CHANNELS. ANGLES.					
of Beam. 1 Inch's Po 3 4 5 6 7 7 8 9 10 12	Veight per Foot. ounds. 5.5 7.5 9.75 12.25 15.0 18.00 21.0 25.0 31.5 40.0	of Rivet.	Depth of Beam Inchs 15 15 18 20 20 24	Weight per Foot, Pounds.  42.0 60.0 80.0 55.0 65.0 80.0 80.0	Size of Rivet, Inches.	Depth of Channel Inches.  3 4 5 6 77 8 9 10 12 15	Weight per Foot. Pounds. 4.0 5.25 6.50 8.0 9.75 11.25 13.25 15.0 20.50 33.0	of Rivet.	Len'th of Leg. Inches 3/4 1 1 1/4 1 1/5 1 3/4 2 2 1/4 2 2 1/6 1 5/16	of Rivet.	Len'th of Leg. Inches 21/2 23/4 3 31/2 4 41/2 5 6 7	Size of Rivet. Inch's 3/4 3/4 1 1 1 1 1 1

#### RIVETS.

## TABLES OF AREAS IN SQUARE INCHES, TO BE DEDUCTED FROM RIVETED PLATES OR SHAPES TO OBTAIN NET AREAS.

	SIZE OF MULE.												Thick- ness Plates. in		
11/8	136	11/4	1 1 5 1 6	13/8	1 7 16	11/2	1 9 16	15/8	<b>1</b> <sup>1</sup> / <sub>16</sub>	13/4	113	17/8	$1\frac{15}{16}$	2	inches.
.28 .35 .42 .49	.30 .37 .45 .52	.31 .39 .47 .55	.33 .41 .49 .57	.34 .43 .52 .60	.36 .45 .54 .63	.38 .47 .56	.49	.51	.42 .53 .63 .74	.44 .55 .66 .77	.45 .57 .68 .79	.47 .59 .70 .82	.48 .61 .73 .85	.50 .63 .75	1/4 5 16 3/8 7 16
.56 .63 .70 .77	.59 .67 .74 .82	.63 .70 .78 .86	.66 .74 .82 .90	.69 .77 .86 .95	.72 .81 .90 .99	.75 .84 .94 1.03	.88	.81 .91 1.02 1.12	.84 .95 1.05 1.16	.88 .98 1.09 1.20	.91 1.02 1.13 1.25	.94 1.05 1.17 1.29	.97 1.09 1.21 1.33	1.00 1.13 1.25 1.38	$\frac{1}{2}$ $\frac{9}{16}$ $\frac{5}{8}$ $\frac{11}{16}$
.84 .91 .98 1.05		.94 1.02 1.09 1.17		$\frac{1.12}{1.20}$	$\frac{1.17}{1.26}$	$\frac{1.22}{1.31}$	1.37	$\frac{1.32}{1.42}$	1.27 1.37 1.48 1.58	1.31 1.42 1.53 1.64	1.36 1.47 1.59 1.70	1.41 1.52 1.64 1.76	1.45 1.57 1.70 1.82	1.50 1.63 1.75 1.88	3/4 136 7/85 16
1.13 1.20 1.27 1.34	$1.26 \\ 1.34$	1,25 1,33 1,41 1,48	1.39 1.48	1.46 1.55	$1.53 \\ 1.62$	1.59 1.69	1.56 1.66 1.76 1.86	1.73 1.83	1.69 1.79 1.90 2.00	1.75 1.86 1.97 2.08	1.81 1.93 2.04 2.15	1.88 1.99 2.11 2.23	1.94 2.06 2.18 2.30	2.00 2.13 2.25 2.38	$1 \\ 1\frac{1}{16} \\ 1\frac{1}{8} \\ 1\frac{3}{16}$
1.41 1.48 1.55 1.62	1.56 1.63	1.56 1.64 1.72 1.80		1.80	1.80 1.89 1.98 2.07			2.13	2.11 2.21 2.32 2.43	2.19 2.30 2.41 2.52	2.27 2.38 2.49 2.61	2.34 2.46 2.58 2.70	2.42 $2.54$ $2.66$ $2.79$	2.50 2.63 2.75 2.88	$1\frac{1}{4}$ $1\frac{5}{16}$ $1\frac{3}{8}$ $1\frac{7}{16}$
$\frac{1.76}{1.83}$	1.86	1.88 1.95 2.03 2.11	1.97 2.05 2.13 2.21	2.06 2.15 2.23 2.32	2.16 2.25 2.34 2.43	2.25 2.34 2.44 2.53	$\frac{2.44}{2.54}$	2.54	2.53 2.64 2.74 2.85	2.63 2.73 2.84 2.95	2.72 2.83 2.95 3.06	2.81 2.93 3.05 3.16	2.91 3.03 3.15 3.27	3.00 3.13 3.25 3.38	$\begin{array}{c} 1\frac{1}{2} \\ 1\frac{9}{16} \\ 1\frac{5}{8} \\ 1\frac{11}{16} \end{array}$
$\frac{2.11}{2.18}$	2.08 2.15 2.23 2.30 2.38	2.19 2.27 2.34 2.42 2.50	2.30 2.38 2.46 2.54 2.63	2.49 $2.58$ $2.66$	2.61 $2.70$ $2.79$	2.91	2.83	2.84 2.95 3.05 3.15 3.25	2.95 3.06 3.16 3.27 3.38	3.06 3.17 3.28 3.39 3.50	3.17 3.29 3.40 3.51 3.63	3.28 3.40 3.52 3.63 3.75	3.39 3.51 3.63 3.75 3.88	3.50 3.63 3.75 3.88 4.00	

## RIVET SPACING. ALL DIMENSIONS IN INCHES.

Size of	Minimum	Maximum Pitch at Ends of	Minimum Pitch in Flanges of		om Edge of Piece to of Rivet Hole.		
Rivet.	Pitch. Compression Members.		Chords and Gird's.	Minimum.	Usual.		
1/4 5/8 1/2 5/8 3/4 7/8 1	3/4 $11/8$ $11/8$ $17/8$ $21/4$ $25/8$ $3$	2 <sup>1</sup> / <sub>2</sub> 3 3 <sup>1</sup> / <sub>2</sub> 4	4 4 4	$egin{array}{cccccccccccccccccccccccccccccccccccc$	11/4 11/2 15/4 2		

For General Rules for Rivet Spacing see next page.

## GENERAL RULES FOR RIVET SPACING FOR BRIDGE AND STRUCTURAL WORK.

The pitch or distance from center to center of rivets should not be less than 3 diameters of the rivet. In bridge work the pitch should not exceed 6 inches or 16 times the thickness of the thinnest outside plates except in special cases hereafter noted. In the flanges of beams and girders where plates more than 12 inches wide are used, an extra line of rivets with a pitch not greater than 9 inches should be driven along each edge to draw the plates together.

At the ends of compression members the pitch should not exceed 4 diameters of the rivet for a length equal to twice the width or diameter of the member.

In the flanges of girders and chords carrying floors, the pitch should not exceed 4 inches.

For plates in compression the pitch in the direction of the line of stress should not exceed 16 times the thickness of the plate, and the pitch in a direction at right angles to the line of stress should not exceed 32 times the thickness, except for cover plates of top chords and end posts in which the pitch should not exceed 40 times their thickness.

The distance between the edge of any piece and the center of the rivet hole should not be less than  $1\frac{1}{4}$  inches for  $\frac{3}{4}$  inch and  $\frac{7}{8}$  inch rivets except in bars less than  $2\frac{1}{2}$  inches wide; when practicable it should, for all sizes, be at least 2 diameters of the rivet and should not exceed 8 times the thickness of the plate.

Minimum spacing is generally used in pin plates, at ends of columns, girders, etc., etc.

In figuring clearance of rivets for special cases, allow  $\frac{3}{8}$  inch in addition to diameter of head.

## BEARING VALUES OF PIN PLATES. FOR ONE INCH THICKNESS OF PLATE.

Bearing value = Diameter of Pin  $\times 1'' \times$  Stress per Square Inch.

Diameter of Pin.	Area of Pin.	Bearing Value at 12 000 Pounds per Square Inch.	Bearing Value at 13 500 Pounds per Square Inch.	Bearing Value at 15 000 Pounds per Square Inch.	Diam- eter of Pin.	Area of Pin,	Bearing Value at 12 000 Pounds per Square Inch.	Bearing Value at 13 500 Pounds per Square Inch.	Bearing Value at 15 000 Pounds per Square Inch.
Inches.	Sq. Ins.	Pounds.	Pounds.	Pounds.	Inches.	Sq. Ins.	Pounds.	Pounds.	Pounds.
$1\\1^{1}_{8}\\1^{1}_{4}\\1^{3}_{8}$	.785	12000	13500	15000	4 <sup>1</sup> / <sub>2</sub>	15.90	54000	60750	67500
	.994	13500	15190	16880	4 <sup>5</sup> / <sub>8</sub>	16.80	55500	62440	69380
	1.227	15000	16880	18750	4 <sup>3</sup> / <sub>4</sub>	17.72	57000	64130	71250
	1.485	16500	18560	20630	4 <sup>7</sup> / <sub>8</sub>	18.67	58500	65810	73130
$1\frac{1}{2}$ $1\frac{5}{8}$ $1\frac{3}{4}$ $1\frac{7}{8}$	1.767 2.074 2.405 2.761	18000 19500 21000 22500	20250 21940 23630 25310	22500 24380 26250 28130	5 5½ 5½ 5½ 53/8	19.64 20.63 21.65 22.69	60000 61500 63000 64500	67500 69190 70880 72560	75000 76880 78750 80630
$\begin{array}{c} 2 \\ 2^{1}/8 \\ 2^{1}/4 \\ 2^{3}/8 \end{array}$	3.142	24000	27000	30000	5 <sup>1</sup> / <sub>2</sub>	23.76	66000	74250	82500
	3.547	25500	28690	31880	5 <sup>5</sup> / <sub>8</sub>	24.85	67500	75940	84380
	3 976	27000	30380	33750	5 <sup>3</sup> / <sub>4</sub>	25.97	69000	77630	86250
	4.430	28500	32060	35630	5 <sup>7</sup> / <sub>8</sub>	27.11	70500	79310	88130
$2\frac{1}{2}$ $2\frac{5}{8}$ $2\frac{3}{4}$ $2\frac{7}{8}$	4.909	30000	33750	37500	6	28.27	72000	81000	90000
	5.412	31500	35440	39380	6 <sup>1</sup> / <sub>8</sub>	29.46	73500	82690	91880
	5.940	33000	37130	41250	6 <sup>1</sup> / <sub>4</sub>	30.68	75000	84380	93750
	6.492	34500	38810	43130	6 <sup>3</sup> / <sub>8</sub>	31.92	76500	86060	95630
$     \begin{array}{c}       3 \\       3 \\       4 \\       3 \\       3 \\       8     \end{array} $	7.069	36000	40500	45000	6½	33.18	78000	87750	97500
	7.670	37500	42190	46880	65%	34.47	79500	89440	99380
	8.296	39000	43880	48750	63/4	35.79	81000	91130	101250
	8.946	40500	45560	50630	67/8	37.12	82500	92810	103130
31/2	9.621	42000	47250	52500	7	38.48	84000	94500	105000
35/8	10.32	43500	48940	54380	7½	44.18	90000	101250	112500
33/4	11.05	45000	50630	56250	8	50.27	96000	108000	120000
37/8	11.79	46500	52310	58130	8½	56.75	102000	114750	127500
$\frac{4}{4^{1}/8}$ $\frac{4^{1}/8}{4^{3}/8}$	12.57	48000	54000	60000	9	63.62	108000	121500	135000
	13.36	49500	55690	61880	10	78.54	120000	135000	150000
	14.19	51000	57380	63750	11	95.03	132000	148500	165000
	15.03	52500	59060	65630	12	113.10	144000	162000	180000

Example.—The stress in the end post of a bridge is  $250\,000$  pounds and the diameter of the pin is 55%". Required the total thickness of steel pin plates for a bearing value of  $15\,000$  pounds per square inch.

From the table the bearing value of a 55%" pin in a 1" plate for  $15\,000$  pounds unit stress is  $84\,380$  pounds. Therefore the total thickness of metal required is

 $\frac{250\,000}{84\,380} = 2.96^{\prime\prime}.$ 

The nearest commercial size would therefore be 11/2" on each side, including web and necessary reinforcing plates.

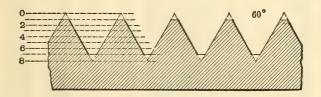
### DIMENSIONS OF BOLTS AND NUTS.

FRANKLIN INSTITUTE STANDARD.

		Bolts a	nd Thr	eads.		Rou	gh Nut	s and I	Iead	ls.
Diameter of Bolt,	Threads per Inch.	Diameter at Root of Thread.	Width of Flat.	Area of Bolt Body.	Area of Bolt at Root of Thread.	Short Diameter of Square and Hexagon,	Long Diameter of Square,	Long Diameter of Hexagon,	Thickness of Nuts.	Thickness of Heads.
Ins.	No.	Ins.	Ins.	Sq. Ins.	Sq. Ins.	Ins.	Ins.	Ins.	Ins.	Ins.
- 네슈타이 이 기타이 이 1 대한 이 네슈타이 이 1 대한 기타이 이 1 대한 기타이 이 1 대한 기타이 이 1 대한 기타이 기타이 이 1 대한 기타이	20 16 14 13 2 11 10 9 8 7 7 6 6 5 5 5 4 4 4 4 3 3 3 3 3 3 2 2 2 2 2 2 2 2 2 2	.185 .240 .294 .344 .400 .454 .507 .620 .731 .837 .940 1.065 1.160 1.284 1.389 1.490 1.615 1.712 1.962 2.175 2.425 2.629 2.879 3.100 3.317 3.567 3.798 4.028 4.255 4.480 4.730 4.953 5.203 5.423	.0062 .0070 .0078 .0089 .0096 .0104 .0113 .0125 .0140 .0156 .0180 .0210 .0210 .0227 .0250 .0280 .0280 .0310 .0357 .0357 .0357 .0357 .0410 .0410 .0410 .0435 .0460 .0500 .0500 .0526 .0526 .0526 .0555	.049 .077 .110 .150 .196 .249 .307 .442 .601 .785 .994 1.227 1.485 1.767 2.074 2.405 2.761 3.142 3.976 4.909 5.940 7.069 8.296 9.621 11.045 12.566 14.186 15.904 17.721 19.635 21.648 23.758 25.967 28.274	.027 .045 .068 .093 .126 .162 .202 .302 .420 .550 .694 .893 1.057 1.295 1.515 1.744 2.302 3.023 3.715 4.619 5.428 6.510 7.548 8.641 9.993 11.329 12.743 14.220 15.763 17.572 19.267 21.262 23.098	982146562 162 66 67 7 8 8 8 9 9 162146562 162 66 66 7 7 8 8 8 9 9 162146562 162 66 66 7 7 8 8 8 8 9 16214656 16214666 16214666 16214666 1621466 1	.707 .840 .972 1.105 1.238 1.370 1.503 1.768 2.033 2.298 2.563 2.829 3.094 3.359 3.624 3.889 4.154 4.420 4.950 5.480 6.011 7.071 7.602 8.132 8.662 9.193 9.723 10.253 10.253 10.784 11.844 12.375 12.905	.577 .686 .794 .902 1.010 1.119 1.227 1.443 1.660 1.876 2.093 2.309 2.526 2.742 2.959 3.175 3.392 3.608 4.042 4.475 4.908 5.341 5.774 6.207 6.640 7.073 7.506 7.939 8.372 8.805 9.238 9.671 10.104 10.537	1 1 1 1 1 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2	14161626 Theiches 200 200 in 1216 in 1

# RULES FOR PROPORTIONS OF BOLTS AND NUTS.

#### FRANKLIN INSTITUTE STANDARD.



The dimensions of nuts and bolts are determined by the following rules, which apply to both square and hexagon.

Short diameter of rough nut  $= 1\frac{1}{2} \times \text{diameter of bolt} + \frac{1}{8} \text{ in.}$ 

Short diameter of finished nut  $= 1\frac{1}{2} \times \text{diameter of bolt} + \frac{1}{16} \text{ in.}$ 

Thickness of rough nut = diameter of bolt.

Thickness of finished nut = diameter of bolt  $-\frac{1}{16}$  in.

Short diameter of rough head  $= 1\frac{1}{2} \times \text{diameter of bolt } + \frac{1}{8} \text{ in.}$ 

Short diameter of finished head  $=1\frac{1}{2} \times \text{diameter of bolt} + \frac{1}{16} \text{ in.}$ 

Thickness of rough head  $=\frac{1}{2}$  of short diameter of head.

Thickness of finished head = diameter of bolt  $-\frac{1}{16}$  in.

In 1864, a committee of the Franklin Institute recommended the above system of screw threads and bolts which was devised by Mr. William Sellers, of Philadelphia. This system as far as it relates to screw threads is generally used in the United States, but the proportions of bolt heads and nuts are not adhered to because the sizes of bar required to make the nuts are special and extra work is necessary to make the bolt heads. Sizes of nuts and bolt heads in accordance with the *Manufacturers' Standard* are given on following pages, Nos. 321, 322 and 323.

# WEIGHTS OF 100 MACHINE BOLTS WITH SQUARE HEADS AND HEXAGON NUTS.

## $\begin{array}{c} \textbf{FRANKLIN INSTITUTE STANDARD SIZES.} \\ \textbf{Basis} - 1 \text{ cubic foot Iron} = 480 \text{ pounds.} \end{array}$

Length under Head to Point.	Dia	mete	er of	Bol	ts in	Inc	hes.
Inches,	1/4	5 16	3 8	7 16	1/2	9 16	<u>5</u> 8
1½ 1¾ 1¾	4.9 5.3	8.2 8.7	12.2 13.0				
2 21/4 21/4 22/2 28/4	5.6	9.2 9.8	14.5	20.6	28.1	37.0	47.5
2½ 2¾ 4	6.3		16.1	22.7	30.8	40.4	51.7
3 3½ 3½ 3½ 38⁄4	7.0 7.3 7.7 8.0	11.4 11.9 12.4 13.0	16.8 17.6 18.4 19.1	24.8	33.5 34.9	43.9 45.6	56.0 58.1
$\frac{4}{4^{1/2}}$	8.3 9.0	13.5 14.6	19.9 21.4	27.9 30.0	37.6 40.3	49.0 52.5	62.4 66.6
5´2 5½ 6	9.7 10.4 11.1	15.6 16.7 17.8	23.0 24.5 26.0	32.1 34.2 36.2	45.8	59.4	75.2
$\begin{array}{c} 61_2 \\ 7 \\ 71_2 \end{array}$	11.7 12.4 13.1	18.8 19.9 21.0	27.6 29.1	38.3 40.4	51.2 53.9	66.3 69.7	83.7 87.9
8 8½ 9 9½	13.8 14.5 15.1 15.8	22.0 23.1 24.2 25.2	32.2 33.7 35.3 36.8	44.6 46.7 48.8 50.8	62.1 64.8	80.1 83.5	100.7 105.0
$10 \\ 101/2 \\ 11$	16.5 17.2 17.9	26.3 27.4 28.4	38.3 39.9 41.4	52.9 55.0 57.1	70.3 73.0 75.7	90.4 93.9 97.3	113.5 117.8 122.0
$11\frac{1}{2}$ $12$ $12\frac{12\frac{1}{2}}{13}$	18.5	29.5 30.5 31.6 32.7	42.9 44.5 46.0 47.5	59.2 61.3 63.2 65.4	81.2 83.9	104.2 107.7	130.5
$13\frac{1}{2}$ $14$ $14\frac{1}{2}$		33.7	49.1 50.6 52.1	67.5 69.6 71.7	92.1 94.8	118.0 121.5	147.6 151.8
15 15½ 16	,		53.7 55.2	73.8 75.9	97.5 100.3 103.0	124.9 128.4 131.8	160.4
161 <sub>2</sub> 17 17 <sup>1</sup> / <sub>2</sub>				77.9 80.0 82.1 84.2	105.7 108.4 111.2	135.3 138.7 142.2	164.6 168.9 173.1 177.4
18 18½ 19					113.9 116.6 119.3	145.6 149.1 152.5	
19½ 20				• • •	122.1 124.8	156.0 159.4	194.4
One inch in length of 100 Bolts.  To obtain Weights with Square Nuts per 100: Add.	1.36 .23	2.13	3.07	.99	$\frac{5.45}{1.42}$	$\frac{6.90}{1.96}$	$\frac{8.52}{2.62}$
Weight of one Hexagon Nut. Weight of one Hexagon Head.	.0116	.020	.031	.046	.065	.088	.117
Weight of one Square Nut. Weight of one Square Head.	.0139	.024	.038	.056	.079	.108	.143
All weig							

## WEIGHTS OF 100 MACHINE BOLTS WITH SQUARE HEADS AND HEXAGON NUTS.

## FRANKLIN INSTITUTE STANDARD SIZES.

Basis — 1 cubic foot Iron = 480 pounds.										
Length under Head to Point.	Dia	met	er of	Bol	ts in	Inc	hes.			
Inches.	34	7/8	1	11/8	11/4	$1\frac{3}{8}$	$1\frac{1}{2}$			
$\frac{1\frac{1}{2}}{1\frac{3}{4}}$	64.5	95.2	134	182	240	309	390			
$\frac{1}{4}$	67.6	99.4 103.5	140 145	189 196	248 257	319 329	402 414			
21/4	73.7	103.3	150	203	265	340	426			
21/ <sub>4</sub> 21/ <sub>2</sub> 23/ <sub>4</sub>	76.8	111.9		210	274	350	439			
3	79.8 82.9	116.1 120.2	161 167	216 223	282 291	360 371	451 463			
31/4	86.0	124.4	172	230	300	381	475			
31/4 31/2 38/4	89.1 92.1	128.6 132.8		$237 \\ 244$	308 317	391 402	488 500			
4	95.2	136.9		251	325	412	512			
$\begin{array}{c} 4\\ \frac{4^{1}}{2} \end{array}$	101.3	145.3	199	265	342	432	537			
5 <sup>1</sup> / <sub>2</sub>	107.4 113.6	153.6 162.0		279 292	359 376	453 474	561 586			
6	119.7	170.3	232	306	393	494	610			
$\frac{61}{2}$	125.9 132.0	178.7 187.0	$   \begin{array}{c c}     243 \\     254   \end{array} $	320 334	410 427	515 536	635 659			
7½	138.1	195.4		348	444	556	684			
8	144 3	203.7	276	361	461	577	709			
8 <sup>1</sup> / <sub>2</sub>	150.4 156.5	212.1 $220.4$	287 298	375 389	478 495	597 618	733 758			
$9\frac{1}{2}$	162.7	228.8		402	513	639	782			
$\frac{10}{10\frac{1}{2}}$	168.8 174.9	$237.1 \\ 245.5$	319 330	417 430	530 547	659 680	807 831			
11	181.1	253.8		444	564	701	856			
$11\frac{1}{2}$	187.2	262.2	352	458	581	721	880			
$\frac{12}{12\frac{1}{2}}$	193.3 199.5	270.5 $278.9$	363 374	472 486	598 615	742 762	905 929			
13	205.6	287.2	385	499	632	783	954			
13½	211.7	295.6 303.9		513	649	804 824	978			
$\frac{14}{14\frac{1}{2}}$	224.0	312.3	407	527 541	666	845	1003 1027			
15	230.1 236.3	320.6		555	700	866 886	1052			
15½ 16	242.4	329.0 337.3		568 582	717 734	907	1077 1101			
$16\frac{1}{2}$	248.5	345.7	461	596	751	927	1126			
17 17½	254.7 260.8	$354.0 \\ 362.4$	472 483	610 624	768 785	948 969	1150 1175			
18	266.9	370.7	494	637	802	989	1199			
$\frac{18\frac{1}{2}}{19}$	273.1 279.2	379.1 387.4	505 516	651	819 836	1010	1224			
191/2	279.2	395.8	526	665 679	853	1031 1051	$1248 \\ 1273$			
20	291.5	404.1	537	693	870	1072	1297			
One inch in length of 100 Bolts.	12.27	16.70	21.82	27.61	34.09	$\frac{41.25}{}$	49.09			
To obtain Weights with Square Nuts per 100: Add.	4.35	6.72	9.81	13.73	18.57	24.42	31.42			
Weight of one Hexagon Nut. Weight of one Hexagon Head.	.190 .235	.289	.417 .516	.579 .616	.777 .962	1.016 1.259	1.299 1.611			
Weight of one Square Nut Weight of one Square Head .	.234 .271	.356 .412	.515 .596	.716 .827	.963 1.111	1.260 1.453	1.614 1.860			

All weights are approximate.

# WEIGHTS OF 100 MACHINE BOLTS WITH SQUARE HEADS AND NUTS.

#### WROUGHT IRON.

#### MANUFACTURERS' STANDARD SIZES.

Basis - Hoopes & Townsend's List.

Length under Head	I	)iam	eter	of H	olt i	n In	ches	6.
to Point. Inches,	1/4	5 16	3 8	7 16	$\frac{1}{2}$	9 16	5/8	3/4
1½	3.9	6.2	9.7	14.7	20.4	26.0	37.0	58.0
$\begin{array}{c} 2 \\ 2 \frac{1}{2} \end{array}$	4.6 5.4	7.2 8.2	11.3 12.9	16.5 18.5	$\frac{22.4}{25.0}$	29.0 32.2	39.9 44.1	63.2 69.0
$\frac{3}{31/2}$	6.2 6.9	9.3 10.4	14.5 16.1	20.5 22.6	27.8 30.6	35.4 38.7	48.3 52.5	75.2 81.4
$\begin{array}{c} 4\\ 4\frac{1}{2} \end{array}$	7.6 8.3	11.5 12.6	17.7 19.2	24.7 26.8	33.4 36.2	42.0 45.3	56.7 60.9	87.6 93.8
$5\\5\frac{1}{2}$	9.0 9.7	13.7 14.8	20.7 22.2	28.9 31.0	39.0 41.8		65.1 69.2	100.0 106.1
6 6½	10.4 11.1	15.9 17.0	23.7 25.2	33.1 35.2	44.6 47.4	55.2 58.5	73.4 77.6	112.2 118.3
7 71/ <sub>2</sub>	11.8 12.5	18.1 19.2	26.7 28.2	37.3 39.4	50.2 53.1	61.8 65.1	81.8 86.0	124.4 130.5
8	13.2 14.6	20.3 22.5	29.7 33.1	41.5 45.7	56.0 61.5	68.5 75.2	90.0 98.0	136.6 148.8
10 11			36.5 40.0	49.9 54.1	$67.0 \\ 72.5$	81.9 88.7	106.3 114.6	161.0 173.2
12 13			43.5 47.0	58.3 61.5	78.0 83.5	95.5 102.3	122.9 131.2	184.4 196.6
14 15					89.0 94.5	109.1 116.0	139.5 148.0	208.8 221.0
16 17					100.0 105.5	123.0 130.0	156.5 165.0	233.2 245.4
18 19					111.0 116.5	137.0 144.0	173.5 182.0	257.6 269.8
20 21					$122.0 \\ 127.5$	151.0 158.0	190.5 198.0	282.0 294.0
22 23							206.0 215.0	306.0 318.0
24 25			:::				224.0 233.0	330.0 342.0

# WEIGHTS OF 100 MACHINE BOLTS WITH SQUARE HEADS AND NUTS.

#### WROUGHT IRON.

#### MANUFACTURERS' STANDARD SIZES.

Basis — Hoopes & Townsend's List.

Length under Head	Diameter of Bolt in Inches.									
to Point. Inches.	7/8	1	11/8	11/4	13/8	$1_{2}^{1}$	13/4	2		
2 2½	98 106	145 153								
$\frac{3}{3^{1/2}}$	114 122	163 174	240 253	309 3 <i>2</i> 5	350 370	480 500				
$\begin{array}{c} 4\\4^{1}\!/_{2}\end{array}$	130 138	185 196	267 281	342 359	390 410	520 545	800 833	• • •		
5	147	207	295	376	$\frac{430}{450}$	570	866	1370		
5½	155	218	309	394		595	900	1414		
6 61/2	163	229	323	412	470	620	934	1458		
	172	240	337	430	490	645	968	1502		
7	180	251	351	448	510	670	1002	1546		
7½	187	262	365	466	530	695	1036	1590		
8	195	273	379	484	550	725	1070	1634		
9	212	295	407	518	590	775	1138	1722		
10	229	317	435	552	630	825	1206	1810		
11	246	339	463	586	670	875	1274	1898		
12	263	361	491	620	710	925	1342	1986		
13	280	383	519	655	751	975	1410	2074		
14	297	405	547	690	793	1025	1478	2162		
15	314	427	575	725	835	1075	1548	2250		
16	331	449	603	760	877	1125	1616	2338		
17	348	471	631	795	919	1175	1684	2426		
18	365	493	659	830	961	1225	1752	2514		
19	382	515	687	865	1003	1275	1820	2602		
20	399	537	715	900	1045	1325	1888	2690		
21	416	559	743	935	1087	1375	1956	2778		
22	437	581	771	970	1129	1425	2024	2866		
23	454	603	799	1005	1171	1475	2092	2954		
24	470	625	827	1040	1213	1525	2160	3042		
25	487	647	855	1075	1255	1575	2228	3130		

Bolts from 11/8 inches to 2 inches, inclusive, are fitted with nuts made to U.S. Standard.

## WEIGHTS OF 100 ROUND-HEADED RIVETS OR ROUND-HEADED BOLTS WITHOUT NUTS.

#### WROUGHT IRON.

Basis — 1 cubic foot Iron = 480 pounds.

Length under Head to Point.	Dia	mete	er of	Rive	et in	Inc	hes.
Inches.	3/8	$\frac{1}{2}$	5 8	3 4	7 8	1	$1\frac{1}{8}$
1	4.7	9.3	16.0	25.2	37.2	52.6	71.3
11/4	5.5	10.7	18.1	28.3	41.3	58.0	78.2
11/2	6.2	12.1	20.2	31.3	45.5	63.5	85.1
13/4	7.0	13.4	22.4	34.4	49.7	68.9	92.0
2 21/4 21/4 22/4 23/4	7.8 8.5 9.3 10.1	14.8 16.2 17.5 18.9	24.5 26.6 28.8 30.9	37.5 40.5 43.6 46.7	53.9 58.0 62.2 66.4	74.4 79.8 85.3 90.7	98.9 105.8 112.7 119.6
3	10.8	20.3	33.0	49.8	70.6	96.2	126.5
31/4	11.6	21.6	35.1	52.8	74.7	101.6	133.4
31/2	12.4	23.0	37.3	55.9	78.9	107.1	140.3
33/4	13.1	24.3	39.4	59.0	83.1	112.6	147.2
4	13.9	25.7	41.5	62.0	87.3	118.0	154.1
41/4	14.7	27.1	43.7	65.1	91.4	123.5	161.0
41/2	15.4	28.4	45.8	68.2	95.6	128.9	167.9
43/4	16.2	29.8	47.9	71.2	99.8	134.4	174.8
5	17.0	31.2	50.1	74.3	104.0	139.8	181.7
51/4	17.7	32.5	52.2	77.4	108.2	145.3	188.6
51/2	18.5	33.9	54.3	80.4	112.3	150.7	195.6
55/4	19.3	35.3	56.4	83.5	116.5	156.2	202.5
6	20.0	36.6	58.6	86.6	120.7	161.6	209.4
614	20.8	38.0	60.7	89.6	124.8	167.1	216.3
613	21.6	39.3	62.8	92.7	129.0	172.5	223.2
654	22.3	40.7	65.0	95.8	133.2	178.0	230.1
7	23.1	42.1	67.1	98.8	137.4	183.5	237.0
71/4	23.9	43.4	69.2	101.9	141.6	188.9	243.9
71/2	24.6	44.8	71.4	105.0	145.7	194.4	250.8
78/2	25.4	46.2	73.5	108.0	149.9	199.8	257.7
8	26.2	47.5	75.6	111.1	154.1	205.3	264.6
8½	27.7	50.2	79.9	117.2	162.4	216.2	278.4
9	29.2	53.0	84.1	123.4	170.8	227.1	292.2
9½	30.8	55.7	88.4	129.5	179.1	238.0	306.0
$ \begin{array}{c} 10 \\ 10 \frac{1}{2} \\ 11 \\ 11 \frac{1}{2} \\ 12 \end{array} $	32.3	58.4	92.7	135.6	187.5	248.8	319.8
	33.8	61.2	96.9	141.8	195.8	259.8	333.6
	35.4	63.9	101.2	147.9	204.2	270.7	347.4
	36.9	66.6	105.4	154.1	212.5	281.6	361.2
	38.4	69.3	109.7	160.2	220.9	292.5	375.0
One inch in length of 100 Rivets		5.45	8.52	12.27	16.70	21.82	27.61
Weight of 100 Rivet Heads		4.82	9.95	16.12	24.29	34.77	47.67

# WEIGHTS AND DIMENSIONS OF BOLT HEADS. MANUFACTURERS' STANDARD SIZES.

Basis—Hoopes & Townsend's List.

Diameter		Squ	are.			Hexa	agon.	
of Bolt,	Short Diameter.	Long Diameter.	Thickness.	Weight per 100.	Short Diameter.	Long Diameter.	Thickness.	Weight per 100.
Inches.	Inches.	Inches.	Inches.	Pounds.	Inches.	Inches.	Inches.	Pounds.
$\frac{1}{4}$	7 16	.619	3 16	1.0	7 16	.505	3 16	.9
$\frac{5}{16}$	$\frac{1}{2}$	.707	$\frac{1}{4}$	1.7	$\frac{1}{2}$	.578	$\frac{1}{4}$	1.5
38	$\frac{1}{3}\frac{9}{2}$	.840	$\frac{9}{32}$	2.8	$\frac{19}{32}$	.686	$\frac{9}{32}$	2.4
$\frac{7}{16}$	$\frac{1}{1}\frac{1}{6}$	.972	38	4.9	$\frac{1}{1}\frac{1}{6}$	.794	38	4.3
$\frac{1}{2}$	$\frac{3}{4}$	1.061	$\frac{7}{16}$	6.8	$\frac{3}{4}$	.866	$\frac{7}{16}$	5.9
$\frac{9}{16}$	$\frac{2}{3}\frac{7}{2}$	1.193	$\frac{1}{2}$	9.9	$\frac{27}{32}$	.974	$\frac{1}{2}$	8.6
<u>5</u> 8	$\tfrac{15}{16}$	1.326	$\frac{1}{3}\frac{7}{2}$	13.0	$\frac{1}{1}\frac{5}{6}$	1.083	$\frac{1}{3}\frac{7}{2}$	11.2
34	1 <u>1</u> 8	1.591	<u>5</u>	22.0	1 <del>1</del> /8	1.299	<u>5</u>	19.0
<del>7</del> 8	$1\frac{5}{16}$	1.856	34	34.8	$1\frac{5}{16}$	1.516	34	33.1
1	$1\frac{1}{2}$	2.122	<u>7</u> 8	54.7	$1\frac{1}{2}$	1.733	<u>7</u> 8	47.4
11/8	15/8	2.298	1	73.3	15/8	1.877	1	63.5
$1\frac{1}{4}$	13/4	2.475	1 <u>1</u> 8	95.7	13/4	2.021	1 <u>1</u> 8	82.9
13/8	$2\frac{1}{8}$	3.006	$1\frac{1}{4}$	156.8	2	2.309	13/8	132.3
$1\frac{1}{2}$	$2\frac{3}{8}$	3.359	13/8	215.4	$2\frac{3}{8}$	2.743	$1\frac{1}{2}$	203.5
15/8	$2\frac{1}{2}$	3.536	$1\frac{1}{2}$	260.3	$2\frac{1}{2}$	2.888	18	244.4
13/4	$2\frac{3}{4}$	3.889	15/8	341.3	$2\frac{3}{4}$	3.176	13/4	318.4
17/8	3	4.243	13/4	437.4	3	3.464	17/8	408.2
2	3 <u>1</u>	4.420	17/8	508.5	31/8	3.610	2	469.9

# WEIGHTS AND DIMENSIONS OF HEXAGON NUTS.

#### MANUFACTURERS' STANDARD SIZES.

BASIS—HOOPES & TOWNSEND'S LIST.

Diameter				Diameter	Pla	in.	Cup	ped.
of Bolt.	Short Diameter.	Long Diameter.	Thickness.	of Rough Hole.	Weight per 100.	Number in 100.	Weight per 100.	Number in 100.
Inches.	Inches.	Inches.	Inches.	Inches.	Pounds.	Pounds.	Pounds.	Pounds.
기속5 [1 전 1 전 1 전 1 전 1 전 1 전 1 전 1 전 1 전 1	- 1621-1621-162-162-162-162-162-1621-1621	.578 .722 .866 1.011 1.011 1.155 1.155 1.299 1.299 1.299 1.444 1.444 1.588 1.733 1.733 1.733 1.733 1.733 1.733 1.733 1.733 1.877 2.021 2.021 2.309 2.599 2.888 3.176 3.464 4.043 4.043 4.043	기록 5 H 2 J 1	7 60 0 10 10 10 7 10 7 10 7 10 10 10 10 10 10 10 10 10 10 10 10 10	1.3 2.3 4.3 7.0 7.5 9.9 10.8 13.7 15.9 17.9 19.5 23.0 22.2 26.6 30.3 34.5 40.0 37.7 45.9 45.3 50.8 57.5 63.7 100.0 138.9 138.2 243.9 333.3 408.2 493.8 487.8 512.8	7800 4440 2330 1430 1330 1010 930 730 630 560 514 435 450 376 330 290 250 265 218 221 197 174 157 100 72 54 41 30 24 ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½	1.2 2.1 4.0 6.3 6.9 9.2 10.2 12.5 15.2 17.0 18.5 21.7 20.6 25.4 28.8 32.3 37.6 35.3 43.5 42.6 47.6 53.8 59.5 90.9 126.6 169.5 222.2 303.0 370.4 459.8 454.5 487.8	8500 4790 2510 1580 1440 1090 980 800 660 588 541 460 485 394 347 310 266 283 230 235 210 186 168 110 79 59 45 33 27 21 <sup>3</sup> / <sub>4</sub> 22 <sup>4</sup> / <sub>2</sub> 20 <sup>1</sup> / <sub>2</sub>

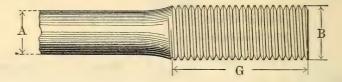
# WEIGHTS AND DIMENSIONS OF SQUARE NUTS.

#### MANUFACTURERS' STANDARD SIZES.

Basis—Hoopes & Townsend's List.

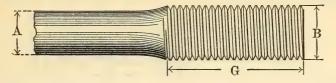
Diameter		_		Diameter	Plain.		Cup	ped.
of Boit.	Short Diameter.	Long Diameter.	Thickness.	of Rough Hole,	Weight per 100.	Number in 100	Weight per 100.	Number
Inches.	Inches.	Inches.	Inches.	Inches	Pounds.	Pounds.	Pounds.	Pounds.
$\frac{1}{4}$	$\frac{1}{2}$	.707	$\frac{1}{4}$	$\frac{7}{32}$	1.5	6750	1.4	7200
$\frac{5}{16}$	<u>5</u> 8	.884	$\frac{5}{16}$	$\frac{9}{32}$	2.8	3540	2.5	4000
3/8	$\frac{3}{4}$	1.061	38	$\frac{1}{3}\frac{1}{2}$	4.8	2100	4.2	2380
$\frac{7}{16}$	58 34 78 78	1.237	$\frac{7}{16}$	$\frac{1}{3}\frac{3}{2}$	7.5	1330	6.8	1460
	7/8	1.237		$\frac{7}{16}$	8.9	1120	8.1	1230
$\frac{1}{2}$ $\frac{1}{2}$	1	1.414	$\frac{1}{2}$	$\frac{7}{16}$	11.9	840	10.8	930
$\frac{9}{16}$	1 <del>1</del> /8	1.591	$\frac{9}{16}$	$\frac{1}{2}$	15.4	650	14.3	700
<u>5</u> 8	11/8	1.591	<u>5</u> 8	$\frac{9}{16}$	17.3	575	16.1	620
চাত তাত হাৰ হাৰ হাৰ বাহু বাহু চাহু	$1\frac{1}{4}$	1.768	500 500 504 504 504 706 708 708	9 16	23.0	435	21.1	475
$\frac{3}{4}$	$1\frac{1}{4}$	1.768	$\frac{3}{4}$	$\frac{2}{3}\frac{1}{2}$	27.8	360	25.0	400
$\frac{3}{4}$	13/8	1.945	34	$\frac{2}{3}\frac{1}{2}$	31.7	315	29.0	345
$\frac{3}{4}$	$1\frac{1}{2}$	2.122	34	$\frac{2}{3}\frac{1}{2}$	41.0	244	37.0	270
$\frac{7}{8}$	$1\frac{1}{2}$	2.122	7/8	$\frac{25}{32}$	46.5	215	41.7	240
$\frac{7}{8}$	15/8	2.298	7/8	$\frac{2}{3}\frac{5}{2}$	55.6	180	48.8	205
$\frac{7}{8}$	$1\frac{3}{4}$	2.475	7/8	$\frac{25}{32}$	61.3	163	54.6	183
1	$1\frac{3}{4}$	2.475	1	7/8	70.9	141	64.1	156
1	2	2.828	1	$\begin{array}{c} \frac{25}{32} \\ \frac{7}{8} \\ \frac{7}{8} \\ \frac{15}{16} \end{array}$	95.2	105	87.0	115
$1\frac{1}{8}$	2	2.828	11/8	$\frac{15}{16}$	102.0	98	94.3	106
$1\frac{1}{8}$	$2\frac{1}{4}$	3.182	11/8	$\frac{1}{1}\frac{5}{6}$	135.1	74	123.5	81
$1\frac{1}{4}$	$2\frac{1}{4}$	3.182	11/4	$1\frac{1}{16}$	156.3	64	142.9	70
$1\frac{1}{4}$	$2\frac{1}{2}$	3.536	$1\frac{1}{4}$	$1\frac{1}{16}$	192.3	52	175.4	57
13/8	$2\frac{3}{4}$	3.889	13/8	$1\frac{3}{16}$	250.0	40	227.3	44
$1\frac{1}{2}$	3	4.243	$1\frac{1}{2}$	$1\frac{5}{16}$	317.5	$31\frac{1}{2}$	285.7	35
15/8	$3\frac{1}{4}$	4.597	15/8	$1\frac{7}{16}$	454.5	22	400.0	25
$1\frac{3}{4}$	$3\frac{1}{2}$	4.950	13/4	$1\frac{9}{16}$	555.6	18	500.0	20
$1\frac{7}{8}$	$3\frac{3}{4}$	5.303	17/8	$1\frac{1}{1}\frac{1}{6}$	666.7	15	625.0	16
2	4	5.657	2	$1\frac{1}{1}\frac{3}{6}$	816.3	$12\frac{1}{4}$	784.3	123
				10				4

#### UPSET SCREW ENDS FOR ROUND BARS.



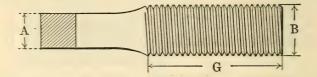
Diameter of Bar.	Area of Body of Bar.	Diameter of Screw.	Length of Upset.	Area at Root of Thread.	Number of Threads per Inch.	Weight per Foot of Bar.	Add for Upset.	Excess of Area at Root of Thread Over that of Body of Bar.
Inches.	Sq. Ins.	Inches.	Inches.	Sq. Ins.		Pounds.	Inches.	Per Cent,
12 12 15 8 116	.196 .249 .307 .371		$4\frac{1}{4}$ $4\frac{1}{4}$ $4\frac{1}{2}$ $4\frac{1}{2}$	.302 .302 .420 .550	10 10 9 8	.668 .845 1.043 1.262	$6\frac{1}{2}$ $4\frac{1}{4}$ $5\frac{1}{2}$ $6\frac{1}{4}$	54 21 37 48
3 1 3 7 7 8 1 5 1 6	.442 .519 .601 .690	$1\frac{1}{4}$	4½ 43 43 43 43	.550 .694 .893 .893	7	1.502 1.763 2.044 2.347	4½ 5½ 6¼ 4½	25 34 49 29
$1 \\ 1_{\frac{1}{1}6} \\ 1_{\frac{1}{8}} \\ 1_{\frac{3}{6}}$	.785 .887 .994 1.108	$1\frac{3}{8}$ $1\frac{1}{5}$	5 5 5 5	1.057 1.057 1.295 1.295	6 6 6	2.670 3.014 3.379 3.766	5 14 4 44 4 37 3 34	35 19 30 17
$\begin{array}{c} 1\frac{1}{4} \\ 1\frac{5}{16} \\ 1\frac{3}{8} \\ 1\frac{7}{16} \end{array}$	1.227 1.353 1.485 1.623	13	5 1/4 1/4 1/4 1/2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	1.515 1.744 1.744 2.048	5	4.173 4.600 5.049 5.518	$4\frac{1}{2}$ $5$ $4$ $4\frac{3}{4}$	23 29 18 26
$\begin{array}{c} 1\frac{1}{2} \\ 1\frac{9}{16} \\ 1\frac{5}{8} \\ 1\frac{1}{1}\frac{1}{6} \end{array}$	1.767 1.918 2.074 2.237	2	51212314314 555555555555555555555555555555555	2.302 2.302 2.650 2.650	41/2	6.008 6.520 7.051 7.604	5 \frac{1}{4} \\ 4 \frac{1}{2} \\ 5 \\ 4 \\ 4 \\ 4 \\ 4 \\ 4 \\ 4 \\ 4	30 20 28 18
$\begin{array}{c} 1\frac{3}{4} \\ 1\frac{1}{16} \\ 1\frac{7}{8} \\ 1\frac{1}{16} \end{array}$	2.405 2.580 2.761 2.948	$\begin{array}{c} 2\frac{1}{4} \\ 2\frac{3}{8} \end{array}$	5 <sup>3</sup> / <sub>4</sub> 5 <sup>3</sup> / <sub>4</sub> 6 6	3.023 3.023 3.419 3.715	$\begin{array}{c} 4\frac{1}{2} \\ 4\frac{1}{2} \end{array}$	8.178 8.773 9.388 10.020	$\frac{4\frac{3}{4}}{4}$ $4\frac{1}{2}$ $5$	26 17 24 26

### UPSET SCREW ENDS FOR ROUND BARS.



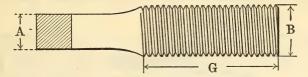
Diameter of Bar.	Area of Body of Bar.	Diameter of Screw.	Length of Upset,	Area at Root of Thread.	Number of Threads per Inch.	Weight per Foot of Bar.	Add for Upset.	Excess of Area at Root of Thread Over that of Body of Bar.
A	0.7	В	G					
Inches.	Sq. Ins.	Inches.	Inches.	Sq. Ins.		Pounds.	Inches.	Per Cent.
$egin{array}{c} 2 \ 2_{16}^{1} \ 2_{8}^{3} \ 2_{16}^{3} \ \end{array}$	3.142 3.341	22 22 22 22 22 22 22 22 22 22 22 22 22	$\begin{array}{c} 6 \\ 6\frac{1}{4} \end{array}$	3.715 4.155	4	10.68 11. <b>3</b> 6	$\frac{4\frac{1}{4}}{4\frac{3}{4}}$	18 24
$2\frac{1}{8}$ $2\frac{3}{16}$	3.547 3.758	25834 24	$egin{array}{c} 6 \\ 6 rac{1}{4} \\ 6 rac{1}{4} \\ 6 rac{1}{4} \end{array}$	4.155 4.619	4	12.06 12.78	$4$ $4\frac{1}{2}$	17 23
$2\frac{1}{4} \ 2\frac{5}{5}$	3.976 4.200	$2\frac{7}{8}$ $2\frac{7}{9}$	$6\frac{1}{2}$ $6\frac{1}{3}$	5.108 5.108	4	13.52 14.28	$\frac{5\frac{1}{4}}{4\frac{1}{5}}$	28 22
$2\frac{1}{4}$ $2\frac{5}{16}$ $2\frac{3}{8}$ $2\frac{7}{16}$	<b>4.4</b> 30 <b>4.</b> 666	27/8 27/8 3 31/8	$6\frac{1}{2}$ $6\frac{1}{2}$ $6\frac{1}{2}$ $6\frac{1}{2}$	5.428 5.957	$rac{3rac{1}{2}}{3rac{1}{2}}$	15.07 15.86	5 \frac{1}{4} \\ 4 \frac{1}{2} \\ 4 \frac{3}{4} \\ 5 \frac{1}{2}	22 23 28
$2\frac{1}{2}$	4.909 5.157	$\frac{3\frac{1}{8}}{3\frac{1}{4}}$	$\frac{6\frac{3}{4}}{6\frac{3}{4}}$	5.957 6.510	$\frac{3\frac{1}{2}}{3\frac{1}{3}}$	16.69 17.53	$\frac{4\frac{3}{4}}{5\frac{1}{4}}$	21 26
$2^{\frac{1}{2}}_{1\overline{6}}$ $2^{\frac{5}{8}}_{1\overline{6}}$	5.412 5.673	3014143 303 308	$\frac{6\frac{3}{4}}{6\frac{3}{4}}$ $\frac{6\frac{3}{4}}{7}$	6.510 7.087	चेत्र   चेत्र   चेत्र   चेत्र   चेत्र   चेत्र   चेत्र   चेत्र   चेत्र   चेत्र	18.40 19.29	434 544 42 5	20 25
	5.940 6.213	338	7	7.087 7.548	$\frac{3\frac{1}{2}}{3\frac{1}{2}}$	20.20 21.12	$\frac{4\frac{1}{2}}{4\frac{3}{2}}$	19
$egin{array}{c} 2rac{3}{4} \ 2rac{1}{1}rac{3}{16} \ 2rac{7}{1}rac{5}{16} \ \end{array}$	6.492 6.777	ମ୍ବାରକୁକ୍ଷ୍ୟୋଗ୍ରରମ୍ବର ପର ପର ପର ସେ	7 7 7 1 7 1 4	8.171 8.171	31/4 31/4 31/4 31/4 31/4	22.07 23.04	4½ 4¾ 5¼ 4¾ 4¾	19 22 26 21
	7.069 7.670	$\frac{3\frac{3}{4}}{3\frac{7}{4}}$	$7\frac{1}{4}$	8.641 9.305	3	24.03 26.08	5 51	22 21
<del>ဂ</del> ဂ္ဂ ဂ္ဂ ဂ္ဂ ဂ္ဂ ဂ္ဂ ဂ္ဂ ဂ္ဂ ဂ္ဂ ဂ္ဂ ဂ	8.296 8.946	$egin{array}{c} 3rac{3}{4} \\ 3rac{7}{8} \\ 4 \\ 4rac{1}{8} \end{array}$	$7\frac{1}{4}$ $7\frac{1}{2}$ $7\frac{1}{2}$ $7\frac{1}{2}$	9.993 10.706	3 3 3	28.20 30.42	5 5 <u>1</u> 4 <u>3</u> 4 <u>3</u> 4 <u>3</u>	20 20
$\frac{31}{2}$	9.621 10.321	41/4	8	11.329 12.743	$2\frac{7}{8}$	32.71 35.09	$\frac{4\frac{1}{2}}{51}$	18
ମ୍ବର୍ଷ ପ୍ରଥମ୍ବର ପ୍ରସ୍ଥ ପ୍ରଥମ୍ବର ପ୍ରସ୍ଥ	11.045 11.793	$4\frac{1}{4}$ $4\frac{1}{2}$ $4\frac{5}{8}$ $4\frac{3}{4}$	8 8 8 1 8 1 8	13.544 14.220	27 22 22 22 22 22 22	37.56 40.10	$egin{array}{c} 4rac{1}{2} \ 5rac{1}{4} \ 5 \end{array} \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \$	23 23 21
4	12.566	5	81/2	15.763	$2\frac{1}{2}$	42.73	$5\frac{1}{4}$	25

### UPSET SCREW ENDS FOR SQUARE BARS.



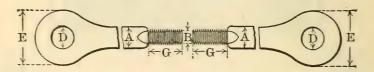
Side of Square Bar.	Area of Body of Bar.	Diameter of Screw.	Length of Upset.	Area at Root of Thread.	Number of Threads per Inch.	Weight per Foot of Bar.	Add for Upset.	Excess of Area at Root of Thread Over that of Body
A		В	G					of Bar.
Inches.	Sq. Ins.	Inches.	Inches.	Sq. Ins.		Pounds.	Inches.	Per Cent.
12 9 15 8 1 16	.250 .316 .391 .473	1	41/41/2 42/2 42/2 42/2	.302 .420 .550 .550	10 9 8 8	.850 1.076 1.328 1.607	4 5 5 3 3 4 3	21 33 41 17
34.5 11.7 8 1.5 6	.563 .660 .766 .879	1 1 4 1 3 3 4 1 3 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	43/4 43/4 5 5	.694 .893 1.057 1.057	7 7 6 6	1.913 2.245 2.603 2.989	$4\frac{1}{2}$ $5\frac{3}{4}$ $4\frac{1}{4}$	23 35 38 20
$\begin{array}{c} 1 \\ 1\frac{1}{16} \\ 1\frac{1}{8} \\ 1\frac{3}{16} \end{array}$	1.000 1.129 1.266 1.410	1 5	5 5 1 4 5 4 5 4	1.295 1.515 1.515 1.744	$ \begin{array}{c c} 6 \\ 5\frac{1}{2} \\ 5\frac{1}{2} \\ 5 \end{array} $	3.400 3.838 4.303 4.795	$4\frac{3}{4}$ $5\frac{1}{2}$ $4\frac{1}{4}$ $4\frac{3}{4}$	29 34 20 24
$\begin{array}{c} 1\frac{1}{4} \\ 1\frac{5}{16} \\ 1\frac{3}{8} \\ 1\frac{7}{16} \end{array}$	1.563 1.723 1.891 2.066	$\frac{1^{\frac{7}{8}}}{2}$	5 5 1 2 1 2 3 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	2.048 2.048 2.302 2.650	5	5.312 5.851 6.428 7.026	$5\frac{1}{4}$ $4\frac{1}{4}$ $4\frac{1}{2}$ $5\frac{1}{4}$	31 19 22 28
$\begin{array}{c} 1\frac{1}{2} \\ 1\frac{9}{16} \\ 1\frac{5}{8} \\ 1\frac{1}{1}\frac{1}{6} \end{array}$	2.250 2.441 2.641 2.848	2 1/8 -1/4 3/8 3/8 2 2 2 2 2	534 534 6	2.650 3.023 3.419 3.419	41/2 41/2 41/2 41/2 41/2	7.650 8.300 8.978 9.682	$4\frac{1}{4}$ $4\frac{1}{2}$ $5$ $4\frac{1}{4}$	18 24 30 20
$\begin{array}{c} 1\frac{3}{4} \\ 1\frac{1}{1}\frac{3}{6} \\ 1\frac{7}{8} \\ 1\frac{1}{1}\frac{5}{6} \end{array}$	3.063 3.285 3.516 3.754	25	$\begin{array}{c c} 6 \\ 6\frac{1}{4} \\ 6\frac{1}{4} \\ 6\frac{1}{4} \end{array}$	3.715 4.155 4.155 4.619	4 4 4 4	10.410 11.170 11.950 12.760	$4\frac{1}{2}$ $5$ $4\frac{1}{4}$ $4\frac{1}{2}$	21 26 18 23

### UPSET SCREW ENDS FOR SQUARE BARS.



Side of Square Bar.	Area of Body of Bar.	Diameter of Screw.	Length of Upset.	Area at Root of Thread.	Number of Threads per Inch.	Weight per Foot of Bar.	Add for Upset.	Excess of Area at Root of Thread Over that of Body of Bar.
A		В	G					
Inches.	Sq. Ins.	Inches.	Inches.	Sq. Ins.		Pounds.	Inches.	Per Cent.
$egin{array}{c} 2 \ 2 rac{1}{16} \ 2 rac{1}{8} \ 2 rac{3}{16} \end{array}$	4.000 4.254 4.516 4.785	27/8 27/8 3 3	$6\frac{1}{2}$ $6\frac{1}{2}$ $6\frac{1}{2}$ $6\frac{1}{2}$ $6\frac{3}{4}$	5.108 5.108 5.428 5.957	4 4 3 2 1 2 2 2	13.60 14.46 15.35 16.27	5 4 <sup>1</sup> / <sub>4</sub> 4 <sup>1</sup> / <sub>2</sub> 5	28 20 20 24
$rac{2rac{1}{4}}{2rac{5}{1}6}$ $2rac{3}{8}$ $2rac{7}{1}6$	5.063 5.348 5.641 5.941	୍ର ପ୍ରକ୍ରାଷ୍ଟ୍ର କ୍ରମ୍ବର	$\frac{6\frac{3}{4}}{6\frac{3}{4}}$	5.957 6.510 7.087 7.087	121212 901212 901212	17.22 18.19 19.18 20.20	4143445 412	18 22 26 19
$egin{array}{c} 2rac{1}{2} \ 2rac{9}{16} \ 2rac{5}{8} \ 2rac{1}{1}rac{1}{6} \end{array}$	6.250 6.566 6.891 7.223	୍ର ପ୍ରକ୍ରମ୍ବର	7 7 1 7 1 7 1 4	7.548 8.171 8.171 8.641	314 3414 36 36 37 37	21.25 22.33 23.43 24.56	$4\frac{3}{4}$ $5\frac{1}{4}$ $4\frac{1}{2}$ $4\frac{3}{4}$	21 24 19 20
$egin{array}{c} 2rac{3}{4} & 3 \ 2rac{1}{1}rac{3}{6} & 2rac{5}{1}rac{5}{6} & 2 \end{array}$	7.563 7.910 8.266 8.629	$egin{array}{c} 3rac{7}{8} \ 3rac{7}{8} \ 4 \ 4rac{1}{8} \end{array}$	$7\frac{1}{2}$ $7\frac{1}{2}$ $7\frac{1}{2}$ $7\frac{1}{2}$	9.305 9.305 9.993 10.706	න න න න	25.71 26.90 28.10 29.34	5 4 1 2 3 4 4 3 5 5	23 18 21 24
3 1 2 2 1 4 3 8	9.000 9.766 10.563 11.391	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	$7\frac{3}{4}$ 8 8 8 8 1	10.706 12.087 12.743 13.544	3 2 <sup>7</sup>   <sub>0</sub> 33  <sub>4:5</sub>   <sub>4:5</sub>   <sub>4</sub> 2  <sub>4</sub> 2  <sub>4</sub> 2  <sub>4</sub> 3   30.60 33.20 35.92 38.73	$egin{array}{c} 4rac{1}{2} \ 5rac{1}{4} \ 5 \ 5 \ \end{array}$	19 24 21 19	
25/83/47/8	12.250 13.141 14.063 15.016	4 <sup>7</sup> / <sub>8</sub> 5 5 5 5 4	0122 0212234334 00434	15.068 15.763 16.658 17.572	$2^{\frac{5}{2}}$ $2^{\frac{1}{2}}$ $2^{\frac{1}{2}}$	41.65 44.68 47.82 51.05	$5\frac{1}{2}$ $5\frac{1}{4}$ $5\frac{3}{4}$	23 20 18 17
4	16.000	$5\frac{1}{2}$	9	19.267	$2\frac{3}{8}$	54.40	$5\frac{1}{4}$	20

### UPSET SCREW ENDS FOR FLAT BARS.



$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Width of Bar. A	Thickness of Bar. Truches	Diameter of Upset of Bar.  B	Area of Bar.	Area at Root of Thread.	Length of Upset of Bar.	Add for Upset of Bar.
6 43 095 000	4 4 4 4 4 4	7-100 1-100-1-44-5100-1-64-514-1-10 1-1-45-5105-1-64-5105-1-45-5105-1-64-5105-1-64-5105-1-64-5105-1-64-5105-1-45-5105-1-64	Inches.   1 4+1015  05  4+1  0	2.63 3.0 3.38 3.75 4.13 4.50 3.50 4.00 4.50 5.50 6.50 7.00 3.75 4.38 5.63 6.25 6.88 7.50 8.13 8.75 6.75	3,023 3,719 4,159 4,62 4,92 5,43 3,719 4,62 5,43 6,51 7,54 7,54 4,62 5,43 6,51 7,55 8,64 9,99 9,99 8,64	Inches. 5 12 12 12 12 12 12 12 12 12 12 12 12 12	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$

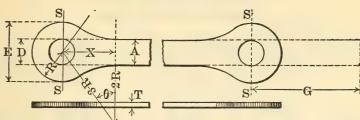
For dimensions of heads corresponding to different-sized pins, see table of Eye Bars on page 329.

Shortest length of bar permissible on account of method of manufacture is 6'0"

center to end.

The above length is used only for bars having heads  $12\frac{1}{2}''$  diameter or less. When possible lengths of 7' 0" are preferred.

#### STEEL EYE BARS.



As = Area of Excess to form one Head = Plane Area of Head — AX. 
$$A_{\rm E} = \frac{(180 + 2\theta)}{360} \pi R^2 + \left(4 R^2 - \frac{A^2}{4}\right) {\rm Tan.} \theta - .0698 R^2 \theta.$$

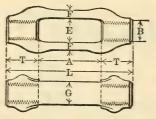
$$\cos \theta = \frac{2R + \frac{A}{2}}{3R} \cdot G = \frac{5A_{\rm E}}{4A} \cdot \frac{{\rm Log.} \frac{\pi}{360} = 7.940848 - 10.}{.0698 = 8.843855 - 10.}$$

377: 341 6	w:	Dismoden	Diameter of		Additional Length of
Width of Body of	Minimum Thickness.	Diameter of Head of	Diameter of Largest	Sectional Area of	Bar Beyond Center
Bar.	of Bar.	Bar.	Pin Hole.	the Head on Line S—S in Excess of	of Eye Required to Form One Head.
				that in Body of	
A	T	E	D	Bar.	G
Inches.	Inches.	Inches.	Inches.		Inches.
2		41/2	17/8	33 %	$7\frac{1}{2}$
2		$5\frac{1}{2}$	27	"	$12\frac{1}{2}$
$2\frac{1}{2}$		$5\frac{1}{2}$	$2\frac{2}{8}$	66	$9\frac{1}{2}$
$2\frac{7}{2}$		$6\frac{5}{2}$	$3\frac{2}{8}$	66	13 -
3	3	$6\frac{7}{5}$	$2\frac{2}{3}$	66	$10\frac{1}{2}$
3	3	8	4	66	17 1
3	3	9	5	"	$\begin{array}{c} 12\frac{1}{2} \\ 9\frac{1}{2} \\ 13\frac{1}{2} \\ 10\frac{1}{2} \\ 17\frac{1}{2} \\ 22\frac{1}{2} \\ 17\frac{1}{2} \\ 21 \\ 27\frac{1}{2} \end{array}$
4	3	91	41	66	171
Ā	3	101	51	66	212
Ā	3	111	61	"	271
5	3	111	45	37 %	202
5	ত ৰত ৰত ৰত ৰত ৰত ৰত ৰত ৰ	121	172757575 2324 5456767676767676767676767676767676767676	37 %	20 24 27½ 32 21½ 27 31½
5	14	13	61	"	971
5	1	14	78 78	"	392
6	17	121	$5\frac{18}{4}$	"	911
o c	7 8 7 8	102		66	21 <u>2</u>
O C	18	145	0 <del>1</del>	66	911
0	1.5	107	( <del>4</del>		012
(	$\frac{15}{16}$	102	98 71	40%	26 <sup>2</sup> 32
(	16	17	( de	66	3% 951
8	1	16	$0\frac{9}{4}$	"	201
8	1	18	04		302
2 2 2 2 3 3 3 4 4 4 5 5 5 5 6 6 6 7 7 8 8 8 9 9 9	1	4	7.57.5687	"	$\begin{array}{c} 35\frac{1}{2} \\ 30\frac{1}{2} \\ 35 \\ 32\frac{1}{2} \end{array}$
9	18	192	7	66	32½
9	1 1 8	$21\frac{1}{2}$	9	66	$36\frac{\tilde{1}}{2}$
9	$1\frac{1}{4}$	$22\frac{1}{2}$	10		• •
. 10	18 18 14 14 18	$24\frac{1}{2}$	105		• •
(TO)	C 1 1 .	1	·		1 1 112

The size of head given is the size of die. The size of finished head will overrun this about \(\frac{1}{2}\)'. Eye Bars are Hydraulic Forged without the addition of extraneous metal and without buckles or welds. The heads on Eye Bars are finished of the same thickness "T" as body of bar.

## TURNBUCKLES.

PRESSED WROUGHT IRON.







THE CLEVELAND CITY FORGE AND IRON CO.

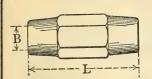
Dir	nensions o	f Bar.							
Diameter of Screw.	Diameter of Bar.	Side of Square Bar.	L	TE	A	Œ	<b>I</b> F	н	G
Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
9\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	1/2 and 9/6 5/8 3/4 3/6 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5 1.5	1/2 9	71/8 71/8 71/9 71/9 71/9 85/8 9 93/4 101/9 111/9 111/9 123/4 131/9 131/9 131/9 141/4 145/8 15 153/4 141/9 171/4 18 1211/9 18 18 19 19 19 19 19 19 19 19 19 19 19 19 19	9 12 12 14 15 15 15 15 15 15 15 15 15 15 15 15 15	6666666666666666666999999	26 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	# # 1	113/8   19/8   113/8	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1

Standard Lengths, 6, 9, 12, 15, 18, 24, 36, 48 and 72 inches between heads (A) for all sizes.

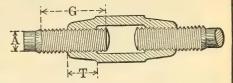
Lengths of Upset Ends shown on pages 324 to 327 are those best adapted for use with Turnbuckles of Standard Lengths as above.

Dimensions E, F, G and H depend upon the specifications of the Bars with which the Turnbuckles are to be used.

#### RIGHT AND LEFT NUTS.





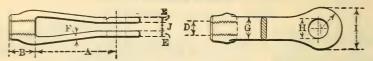


							-	
Diam-	Length	Diameter	Side of	Length	Length	Diam- eter	Weig	ght of
of	of	of Bar.	Square Bar.	of Nut.	of Thread.	of Hex.		One Nut and Two Screw
Screw.	Upset.						One Nut.	Screw
В	G	A	A	L	T	W		Ends.
Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Pounds.	Pounds.
781 118143	4½ 4½ 4¾ 434	$\begin{array}{c} \frac{58}{88} \\ \frac{1}{1}\frac{1}{16} \text{ and } \frac{3}{4} \\ \frac{1}{1}\frac{3}{16} \\ \frac{7}{16} \\ \frac{1}{1}\frac{1}{16} \\ \frac{7}{1} \\ \frac{1}{1}\frac{1}{16} \\ \frac{1}{1}\frac{1}{16} \\ \frac{1}{1}\frac{1}{16} \\ \frac{1}{1}\frac{1}{1}\frac{1}{16} \\ \frac{1}{1}\frac{1}\frac$	$\begin{array}{c} \frac{9}{16} \\ \frac{5}{8} \text{ and } \frac{11}{16} \\ \frac{3}{4} \\ \frac{13}{16} \\ \frac{7}{8} \end{array} \text{ "} \frac{15}{16} \end{array}$	Ordinary Lengths. $6$ $6$ $6\frac{1}{2}$ $6\frac{1}{2}$	$ \begin{array}{c} 1\frac{7}{16} \\ 1\frac{7}{6} \\ 1\frac{5}{8} \\ 187 \end{array} $	15/005/00 12 20	134 134 9	41/4 41/4 71/2 71/2
162-143162-1245162 142-125 143162-1245162 143-12514 1 1 1 1 1 1 1 1 1 2 2 2 2 2 2 2 2 2 2	4 4 4 4 5 5 5 5 5 5 5 6 6	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	\frac{1}{8}	6 6 6 7 7 7 7 8 8 8 8 9 9 9 9 9 9 9 9 9 9 9 9	7 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	5/20-5/20 5/20-3/20-3/20-4/20-4/20-3/20-3/20-3/20-3/20-3/20-3/20-3/20-3	4 4 6 6 9 9 12 16 6 6 11 1 1 1 6 6 6 2 2 8 5 5 5 5 5	414 771 1128 1128 1128 1138 114 1158 1168 1168 1168 1168 1168 1168 1168
14518-125183147  222222222	6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	9 9 9 10	$egin{array}{cccccccccccccccccccccccccccccccccccc$	3 3 3 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	$12\frac{1}{5}$ $16\frac{34}{4}$ $21\frac{1}{5}$ $21\frac{1}{5}$ $26\frac{1}{5}$	31 ½ 4134 4134 534 534 664
3 144-12334 4 4	$\begin{array}{c} 6\frac{1}{2} \\ 6\frac{3}{4} \\ 7 \\ 7\frac{1}{4} \\ 7\frac{1}{2} \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	10 10 10 10½ 11 11½ 12 Extra	$egin{array}{c} 3_{136}^{136} \ 3_{858}^{136} \ 3_{116}^{136} \ 4_{16}^{116} \ \end{array}$	4 5 5 5 6	$26\frac{1}{2}$ $32$ $38\frac{1}{4}$ $45$ $53\frac{1}{2}$	$ \begin{array}{c c} 66\frac{1}{4} \\ 81 \\ 97\frac{3}{4} \\ 116 \\ 138 \end{array} $
1440c-44000-0400004400 111111111112	43434 445 55555 5555 5	$\begin{array}{c} \frac{7}{8} & \text{``} & \frac{15}{16} \\ \frac{1}{7} & \text{``} & \frac{1}{16} \\ 1 & \text{``} & \frac{1}{16} \\ 1\frac{1}{8} & \text{``} & \frac{1}{16} \\ 1\frac{1}{16} & \text{``} & \frac{1}{3} \\ 1\frac{1}{16} & \text{``} & \frac{1}{3} \\ 1\frac{7}{16} & \text{``} & \frac{1}{2} \\ 1\frac{1}{2} & \text{``} & \frac{1}{9} \end{array}$	$\begin{bmatrix} \frac{3}{4} \\ \frac{1}{18} \\ \frac{7}{8} \end{bmatrix} & \text{``} & \frac{15}{16} \\ 1 \\ 1 \\ \frac{1}{16} \\ 1 \\ \frac{3}{16} \\ 1 \\ \frac{1}{4} \end{bmatrix} & \text{``} & 1 \\ \frac{5}{16} \\ 1 \\ \frac{1}{16} \\ \text{``} & 1 \\ 1$	Lengths. 12 $8\frac{1}{2}$ $8\frac{1}{2}$ $9$ $9\frac{1}{2}$ $10$ $10$	$\begin{array}{c} 2\frac{1}{805005007827827827821656} \\ 1\frac{1}{11}\frac{1}$	02 02 02 02 02 02 02 03 03 03 03 03 03 03 03 03 03 03 03 03	$\begin{array}{c} 4 \\ 4 \\ 6_{\frac{1}{4}} \\ 6_{\frac{1}{4}} \\ 8_{\frac{3}{4}} \\ 12_{\frac{1}{4}} \\ 12_{\frac{1}{4}} \end{array}$	954-54-1 954-54-1 154-1 21-55-4 21-55-4 29-4 29-4 29-4 29-4

For Details of Upset Ends, see pages 324 to 327.

Length of Upset Ends for use with Right and Left Nuts may be made one inch shorter than the dimensions given in column "G" above.

#### CLEVISES.

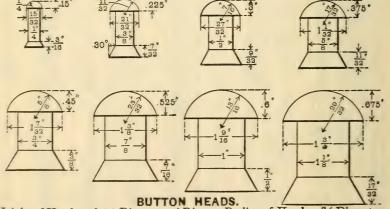


THE CLEVELAND CITY FORGE AND IRON CO.

Diameter of Screw.	Length of Fork.	Length of Thread.	1	Dia	ım	ete	er	of	P	in	in	X1	ıcl	hes	<b>5.</b>	USe	l with	ons to Speci ters I	fied
D	A	В	1	11/4	$1\frac{1}{2}$	13/4	2	21/4	21/2	23/4	3	31/4	31/2	33/4	4	I	G	F	E
Ins.	Ins.	Ins.			Di	an	et	er	I	in	In	ch	es	,		Ins.	Ins.	Ins.	Ins.
3/4	$5\frac{1}{2}$	11/8	23/4	$ 2^{3}/4 $	23/4	3							٠.			23/4	11/2	1/2	17
1/8	6 6	13/8	$\frac{2^{9}/4}{2^{3}/4}$	23/4	3	31/4	31/6		::	• •	::		: :	: :		3	15/8	1/2	$\frac{17}{32}$
11/8	6 61/6	13/4		23/4	3	31/4	31/2	33/4								31/4	13/4	16	19 32
13/	61/2	21/8		3	31/	33/	4	3%4 43%	43/						: :	31/2	$1\frac{7}{8}$	9 16	19 32
11/2	7 2	21/4			33/4	4	43/8	43/8	43/4							33/4	2	5/8	21 32
13/4	8	$\frac{2\frac{1}{2}}{25}$	::		::	43/8	43/8	4 <sup>3</sup> / <sub>4</sub> 5 <sup>1</sup> / <sub>4</sub>	51/4	51/			. :	• •		4	21/8	8/8	$\frac{21}{32}$
17/8	8	27/8				-/8	51/4	514	514	534						43/8	21/4	116	23 32
21/2	9	31/4			::		51/4	53/4	53/4	63/4	63/	• •		: :	• •	43/4	$2\frac{1}{2}$	23	3/4
21/4	10	31/4						53/4	63/4	63/4	63/4	$6\frac{3}{4}$				51/4	$2^{3}/_{4}$	13	7/8
23/8 21/2	10	33/2		1::	::		: :		63/4	63/4	8	8	8		• •	$5\frac{3}{4}$	3	2 7 3 2	15 18
25/8	10	4								8	8	8	8	8		$6\frac{3}{4}$	31/4	15	116
23/4	$\frac{12}{12}$	41/4		1::				::			8	8	8	8	9	8	4	116	11/4
3	12	41/2									8	8	9	9	9	9	41/2	15	11/2

Dimension H is usually  $\frac{1}{32}$  larger than diameter of pin and J is made to suit the thickness of the pin plate. The above Clevises are designed for use with medium steel rods of 60 000 to 68 000 pounds tensile strength per square inch, having standard upsets as shown on pages 324 to 327.

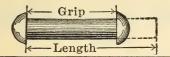
## DIMENSIONS OF RIVET HEADS AFTER DRIVING

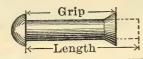


Height of Head =  $\frac{6}{10}$  × Diameter of Rivet. Radius of Head =  $\frac{3}{4}$  Diameter of Rivet +  $\frac{1}{16}$ ".

Diameter of Countersunk Head same as Button Head. Angle of Countersink = 30°. In figuring Clearances for Rivet Heads allow for Heights as follows: 5%" for 34" rivets, 34" for 7%" rivets. All dimensions in inches.

### LENGTH OF RIVETS REQUIRED FOR VARIOUS GRIPS INCLUDING AMOUNT NECESSARY TO FORM ONE HEAD.





Grip of		Dia	metei	of Ri	ivet in	Inch	es.	
Grip of Rivet in Inches.	1//	3'/	$\frac{1}{2}$ //	<u>5</u> //	3//	. $\frac{7}{8}$ //	1′′	1\frac{1}{8}''
1 Inches.  1	1 11/8 11/4/8 11	11/3/9/2/8 /4/8 /8/4/8/8 /8/4/8/8/4/8 /8/4/8/9/4/8 /8/4/8/8/4/8/9/8/9	12 1158448 1178 12144848 12148 121448 12148 12148 121448 121448 121448 121448 121448 121448 121448 121448 121448 121448 121448 121448 121448 121448 121448 121448 121448 121448 1	13/4/8 17/8 2 1/8/8/4/8 2 2 1/2/8/4/8 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	17/8 21/4/4 21/4/8 21/4/8 21/4/8 21/4/8 21/4/8 31/4/8 31/4/8 31/4/8 31/4/8 41/4/8 41/4/8 51/4/8 55/4/8 55/4/8 55/4/8	78 21448 221448 221448 221448 221448 331333 3377 44448 221448 33155 3317 4448 445 55145 555 556 666 6634	1// 21/8/4/8/22/8/4/8 /8/4/8 /8/4/8/27/8 /4/8 /4/8 /4/8 /4/8 /4/8 /4/8 /4/8 /	118 21/4 22/3/8/22/8/4/8 21/4/8/22/8 21/4/8/8/22/8 21/4/8/8/22/8 21/4/8/8/22/8 21/4/8/8/22/8 21/4/8/8 21/4/8/8 21/4/8
434 47/8	51/8 51/4 53/8	55/8 53/4	61/8	6 <sup>1</sup> / <sub>8</sub> 6 <sup>1</sup> / <sub>4</sub> 6 <sup>1</sup> / <sub>2</sub>	6 <sup>1</sup> / <sub>8</sub> 6 <sup>1</sup> / <sub>4</sub> 6 <sup>1</sup> / <sub>2</sub> 6 <sup>5</sup> / <sub>8</sub>	65/8 63/4	6 <sup>3</sup> / <sub>4</sub> 6 <sup>7</sup> / <sub>8</sub>	6 <sup>3</sup> / <sub>4</sub> 6 <sup>7</sup> / <sub>8</sub>
5 51/8 51/4 53/8 55/8 55/8 57/8	51/2 55/8 53/4 57/8 6 61/8 61/4 63/8	57/8 6 61/8 61/4 63/8 61/2 63/4 67/8	61/4 63/8 61/2 65/8 63/4 67/8 71/8 71/4	65/8 63/4 67/8 71/8 71/8 71/4 75/8	63/4 67/8 71/8 71/4 73/8/6/4 73/8 77/8	67/8 7 71/8 71/4 73/8 71/2 75/8 73/4 77/8	7 71/8 71/4 73/8 71/2 75/8 73/4 77/8	7 71/8 71/4 73/8 71/2 75/8 73/4 77/8 81/8

Amount in Inches to be subtracted from above lengths for Countersunk Heads.

 ½
 ½
 ½
 ½
 %
 ¾
 ½
 ½

### BRIDGE PINS, NUTS AND PILOT NUTS.

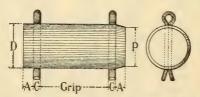


All Threads 8 per inch.

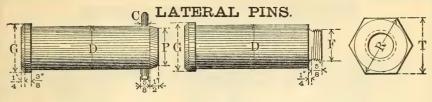
		Till Illica	ds o per me.		
Nominal Diameter of Pin.	Turned Diameter of Pin. D	Diameter of Thread.	Short Diameter of Nut.  A	Long Diameter of Nut.  G	Diameter of Holes in Eye Bars,
Inches.	Inches.	Inches.	Inches.	Inches.	
11374 211472 211472 31474 41472 41472 41472 41472 61472 61472 61472 6172 6172 6172 6172 6172 6172 6172 61	111122223 333 44 44 15 55 6 6 6 6 6 6 6 6	11/4 11/2 11/2 11/2 2 2 21/2 21/2 21/2 2	$\begin{array}{c} 2\\ 2^{1/2}\\ 2^{1/2}\\ 3\\ 3\\ 3^{1/2}\\ 4\\ 4\\ 4^{1/2}\\ 5\\ 5\\ 5^{1/2}\\ 6\\ 6\\ 6^{1/2}\\ 7\\ 7\\ 7^{1/2}\\ 7^{1/2}\\ \end{array}$	22.27.27.27.67.67.67.67.67.67.67.67.67.67.67.67.67	D + 100 " + 10

Allow 16' excess for each eye bar packed on the pin.

### COLD ROLLED STEEL COTTER PINS.

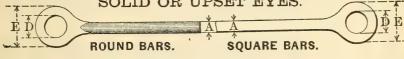


Dimensions of Pin in Inches.														
Diameter of Pin.	D	1	11/4	1½	13/4	2	21/4	21/2	23/4	3	31/4	31/2	33/4	4
Diameter of Reduced Point.	P	7/8	11/8	11/4	11/2	13/4	2	21/4	21/2	23/4	3	31/4	31/2	33/4
Lengths of Ends.	A	5 16	16	9 16	9 76	1/2	1/2	1/2	1/2	7/8	7/8	7/8	7/8	7/8
Diameter of Cotter.	C	5 16	5 16	5 16	5 16	3/8	3/8	3/8	3/8	1/2	1/2	1/2	1/2	1/2
Diameter of Pin Hole.	more design	116	15	1 9 16	113	$2\frac{1}{16}$	25	2 9 16	213	316	3516	3 9	313	416



Rough Diameter of Pin.	Nominal Diameter of Pin.	Finished Diameter of Pin.	Reduced Point.	Short Diameter of Nut.	Long Diameter of Nut.	Diameter of Thread.	Diameter of Cotter Pin.					
G	N	D	P	T	R	F	C					
Inches.	Inches.	Inches.	Inches.	Inches.	Inches,	Inches.	Inches.					
$1\frac{1}{2}$	11/4	$1_{\frac{3}{1}6}$	1	15/8	17/8	1	16					
$\frac{13}{4}$	$\frac{11}{13}$	$\frac{17}{111}$	11/4	2 91/	276	11/4	66					
21/4	2	116 115	13/4	$\frac{21_{2}^{2}}{2}$	$\frac{278}{278}$	11/2	6.6					
21/2	21/4	$2^{\frac{13}{16}}_{16}$	2	$\frac{217}{212}$	$\frac{27}{8}$	$\frac{1}{2}$	3/8					
3 23/4	2½	$\frac{2_{16}}{211}$	21/4	31/2	$\frac{416}{41}$	$\frac{2}{2}$	66					
31/4	3	$2^{\frac{16}{15}}_{16}$	$\frac{23}{4}$	$3\frac{1}{2}$	$4\frac{16}{16}$	$\frac{1}{2}$	"					
31/2	31/4	3.3	31/4	41/2	$\frac{5.3}{1.6}$	$\frac{2^{1}/2}{2^{1}}$	66					
3% 4	31/2	316 311	31/2	41/2	$5\frac{3}{16}$	$\frac{2\frac{1}{2}}{2\frac{1}{2}}$	"					
	$D = G - \frac{5}{18}''. \qquad P = N - \frac{1}{4}''.$											

COUNTER AND LATERAL RODS. SOLID OR UPSET EYES.

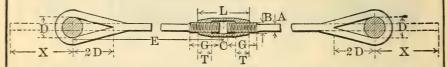


Bar.	Head.	of Largest Pin.	for One Head.	Square Bar.	of Largest Head.	Diameter of Largest Pin.	Add for One Head.
A	E	<u>D</u>	<b>-</b>	A	E	<b>D</b>	
Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.	Inches.
7/8 1 11/8 11/4 13/8 11/2 15/8 11/8 2 15/8 21/8 21/8 21/8 22/8 22/8 22/8 23/8 22/8 23/8 24/8 28/8 21/8 28/8 21/8 28/8 21/8 21/8 28/8 21/8 28/8 21/8 28/8 21/8 28/8 21/8 28/8 21/8 28/8 21/8 28/8 21/8 28/8 21/8 28/8 21/8 28/8 21/8 28/8 21/8 28/8 21/8 28/8 21/8 28/8 21/8 28/8 21/8 28/8 21/8 28/8 21/8 28/8 21/8 28/8 21/8 21	21/4 41/4 41/4 55 51/2 66 67/2 77/2 8 8 8	11/4 21/2 21/2 23/4 3 3 31/4 31/4 31/4 4 4 4 4	9 18 16 20½ 18½ 20 18½ 21 19½ 21 21 22 20 24½ 223¼ 223¼ 224 22½ 24	1 1/8 11/4 13/8 11/4 15/8 13/4 17/8 2 1/8 21/2 25/8 21/4 11/4 13/8 11/2 13/8 11/4 13/8 11/2 13/8 11/4 11/4 11/4 11/4 11/4 11/4 11/4 11	41/4 41/4 5 5 5 5 5 6 6 6 1/2/2/2 8 8 8 5 5 3 4 1/2/2/4 6 3 1/2/2/4	2 2 2 3 3 5 5 5 5 5 4 4 4 4 4 5 5 5 5 5 5 5 5	16 14 1814 1614 1814 1614 1814 17 2114 1934 2214 2114 2194 23 20 20 18

For details of upset screw ends for round and square bars see pages 324 to 327.

## COUNTER AND LATERAL RODS.

#### LOOP WELDED EYES.



Additional length of bar beyond center of pin required to make eye for square or round bars.

Diameter or Side of Bar.			Dia	ame	ter o	f Piı	n in	Inch	es.		
of Bar. Inches.	3/4	1	11/4	1½	13/4	2	21/4	21/2	23/4	3	31/4
<b>1</b> (245)@60]47- @	534 64 634	$\begin{array}{c} 6_{\frac{3}{4}} \\ 7_{\frac{1}{4}} \\ 7_{\frac{9}{2}} \\ 8 \end{array}$	$7\frac{1}{2}$ $8$ $8\frac{1}{2}$ $9$	8½ 9 9½ 10	$\begin{array}{c} 9\frac{1}{2} \\ 10 \\ 10\frac{1}{4} \\ 10\frac{3}{4} \end{array}$	$   \begin{array}{c}     10\frac{1}{4} \\     10\frac{3}{4} \\     11\frac{1}{4} \\     11\frac{3}{4}   \end{array} $	$ \begin{array}{c} 11\frac{1}{4} \\ 11\frac{3}{4} \\ 12\frac{1}{4} \\ 12\frac{3}{4} \end{array} $	$12\frac{1}{4}$ $12\frac{1}{4}$ $13\frac{1}{4}$ $13\frac{1}{2}$	$13\frac{1}{4} \\ 13\frac{1}{2} \\ 14 \\ 14\frac{1}{2}$	14 14½ 15 15½	$   \begin{array}{c}     15 \\     15\frac{1}{2} \\     16 \\     16\frac{1}{2}   \end{array} $
1 1 1 1 1 3 8		8½	$ \begin{array}{c c} 9\frac{1}{2} \\ 10 \\ 10\frac{1}{4} \\ \dots \end{array} $	$\begin{array}{c} 10\frac{1}{4} \\ 10\frac{3}{4} \\ 11\frac{1}{4} \\ 11\frac{3}{4} \end{array}$	$ \begin{array}{c} 11\frac{1}{4} \\ 11\frac{3}{4} \\ 12\frac{1}{4} \\ 12\frac{3}{4} \end{array} $	$12\frac{1}{4}$ $12\frac{3}{4}$ $13\frac{1}{4}$ $13\frac{1}{2}$	$13\frac{1}{4} \\ 13\frac{1}{2} \\ 14 \\ 14\frac{1}{2}$	$14$ $14\frac{1}{2}$ $15$ $15\frac{1}{2}$	$15$ $15\frac{1}{2}$ $16$ $16\frac{1}{2}$	$ \begin{array}{c} 16 \\ 16\frac{1}{2} \\ 16\frac{3}{4} \\ 17\frac{1}{4} \end{array} $	$16\frac{3}{4}$ $17\frac{1}{4}$ $17\frac{3}{4}$ $18\frac{1}{4}$
1½ 158347 178				121/4	$13\frac{1}{4}$ $13\frac{1}{2}$ $14$	$ \begin{array}{c c} 14 \\ 14\frac{1}{2} \\ 15 \\ 15\frac{1}{2} \end{array} $	$ \begin{array}{c c} 15 \\ 15\frac{1}{2} \\ 16 \\ 16\frac{1}{2} \end{array} $	$   \begin{array}{c}     16 \\     16\frac{1}{2} \\     16\frac{3}{4} \\     17\frac{1}{4}   \end{array} $	$   \begin{array}{c}     16\frac{3}{4} \\     17\frac{1}{4} \\     17\frac{3}{4} \\     18\frac{1}{4}   \end{array} $	$   \begin{array}{c}     17\frac{3}{4} \\     18\frac{1}{4} \\     18\frac{3}{4} \\     19\frac{1}{4}   \end{array} $	$   \begin{array}{r}     18\frac{3}{4} \\     19\frac{1}{4} \\     19\frac{1}{2} \\     20   \end{array} $
$2rac{1}{2}$ $2rac{1}{4}$ $2$ $2$						16	$ \begin{array}{c c} 16\frac{3}{4} \\ 17\frac{1}{4} \\ 18 \\ \dots \end{array} $	$   \begin{array}{r}     17\frac{3}{4} \\     18\frac{1}{4} \\     18\frac{3}{4} \\     19\frac{1}{4}   \end{array} $	$   \begin{array}{r}     18\frac{3}{4} \\     19\frac{1}{4} \\     19\frac{3}{4} \\     20\frac{1}{4}   \end{array} $	$   \begin{array}{c}     19\frac{1}{2} \\     20\frac{1}{4} \\     20\frac{3}{4} \\     21\frac{1}{4}   \end{array} $	$20\frac{1}{2}$ $21$ $21\frac{1}{2}$ $22$
2 1/21-5/08/3/47/08 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2								193	$20\frac{3}{4}$ $21\frac{1}{4}$ $21\frac{3}{4}$	$ \begin{array}{c} 21\frac{3}{4} \\ 22\frac{1}{4} \\ 22\frac{3}{4} \\ 23\frac{1}{4} \end{array} $	$\begin{array}{c} 22\frac{3}{4} \\ 23\frac{1}{4} \\ 23\frac{3}{4} \\ 24\frac{1}{4} \end{array}$
3 3 3 4 3										23\frac{3}{4}	$   \begin{array}{r}     24\frac{3}{4} \\     25\frac{1}{4} \\     25\frac{3}{4}   \end{array} $

Length in inches beyond center of pin required to form one eye = X. FORMULÆ: When  $\frac{A}{2} = \text{or} < 1$ 

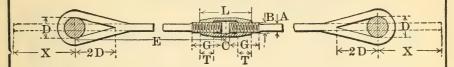
X = 3.7 [D + A] + 1

When  $\frac{A}{2} > 1$   $X = 3.7 [D + A] + \frac{A}{2}$ 

A = Side or Diameter of Bar.

D = Diameter of Pin. Length of bar including amount required to form one eye =  $E - \frac{1}{2}C + X$ .

## COUNTER AND LATERAL RODS. LOOP WELDED EYES.



Additional length of bar beyond center of pin required to make eye for square or round bars.

Diameter or Side		Diameter of Pin in Inches.												
of Bar. Inches.	3½	3¾	4	41/4	4½	<b>4</b> <sup>3</sup> / <sub>4</sub>	5	51/4	5½	53/4	6			
H(245)@8)47- 00	$16 \\ 16\frac{1}{2} \\ 16\frac{3}{4} \\ 17\frac{1}{4}$	$   \begin{array}{c}     16\frac{3}{4} \\     17\frac{1}{4} \\     17\frac{3}{4} \\     18\frac{1}{4}   \end{array} $	17 <sup>3</sup> / <sub>4</sub> 18 <sup>1</sup> / <sub>4</sub> 18 <sup>3</sup> / <sub>4</sub> 19 <sup>1</sup> / <sub>4</sub>	$   \begin{array}{c}     18\frac{3}{4} \\     19\frac{1}{4} \\     19\frac{1}{2} \\     20   \end{array} $	$   \begin{array}{c}     19\frac{1}{2} \\     20 \\     20\frac{1}{2} \\     21   \end{array} $	$20\frac{1}{2}$ $21$ $21\frac{1}{2}$ $22$	$\begin{array}{c} 21\frac{1}{2} \\ 22 \\ 22\frac{1}{2} \\ 22\frac{3}{4} \end{array}$	$\begin{array}{c} 22\frac{1}{2} \\ 22\frac{3}{4} \\ 23\frac{1}{4} \\ 23\frac{3}{4} \end{array}$	$\begin{array}{c} 23\frac{1}{4} \\ 23\frac{3}{4} \\ 24\frac{1}{4} \\ 24\frac{3}{4} \end{array}$	$\begin{array}{c} 24\frac{1}{4} \\ 24\frac{3}{4} \\ 25\frac{1}{4} \\ 25\frac{3}{4} \end{array}$	$25\frac{1}{4}$ $25\frac{3}{4}$ $26$ $26\frac{1}{2}$			
1 10-14:00 1 1 1	$   \begin{array}{c}     17\frac{3}{4} \\     18\frac{1}{4} \\     18\frac{3}{4} \\     19\frac{1}{4}   \end{array} $	$   \begin{array}{r}     18\frac{3}{4} \\     19\frac{1}{4} \\     19\frac{1}{2} \\     20   \end{array} $	$   \begin{array}{c}     19\frac{1}{2} \\     20 \\     20\frac{1}{2} \\     21   \end{array} $	$20\frac{1}{2}$ $21$ $21\frac{1}{2}$ $22$	$ \begin{array}{c} 21\frac{1}{2} \\ 22 \\ 22\frac{1}{2} \\ 22\frac{3}{4} \end{array} $	$\begin{array}{c} 22\frac{1}{2} \\ 22\frac{3}{4} \\ 23\frac{1}{4} \\ 23\frac{3}{4} \end{array}$	$\begin{array}{c} 23\frac{1}{4} \\ 23\frac{3}{4} \\ 24\frac{1}{4} \\ 24\frac{3}{4} \end{array}$	$\begin{array}{c} 24\frac{1}{4} \\ 24\frac{3}{4} \\ 25\frac{1}{4} \\ 25\frac{3}{4} \end{array}$	$\begin{array}{c} 25\frac{1}{4} \\ 25\frac{3}{4} \\ 26 \\ 26\frac{1}{2} \end{array}$	$26$ $26\frac{1}{2}$ $27$ $27\frac{1}{2}$	$   \begin{array}{c}     27 \\     27\frac{1}{2} \\     28 \\     28\frac{1}{2}   \end{array} $			
1½ 1½ 1½ 1½ 1½ 1½	$ \begin{array}{c c} 19\frac{1}{2} \\ 20 \\ 20\frac{1}{2} \\ 21 \end{array} $	$20\frac{1}{2}$ $21$ $21\frac{1}{2}$ $22$	$\begin{array}{c} 21\frac{1}{2} \\ 22 \\ 22\frac{1}{2} \\ 22\frac{3}{4} \end{array}$	$\begin{array}{c} 22\frac{1}{2} \\ 22\frac{3}{4} \\ 23\frac{1}{4} \\ 23\frac{3}{4} \end{array}$	$\begin{array}{c} 23\frac{1}{4} \\ 23\frac{3}{4} \\ 24\frac{1}{4} \\ 24\frac{3}{4} \end{array}$	$\begin{array}{c} 24\frac{1}{4} \\ 24\frac{3}{4} \\ 25\frac{1}{4} \\ 25\frac{3}{4} \end{array}$	$\begin{array}{c} 25\frac{1}{4} \\ 25\frac{3}{4} \\ 26 \\ 26\frac{1}{2} \end{array}$	$26$ $26\frac{1}{2}$ $27$ $27\frac{1}{2}$	$27$ $27\frac{1}{2}$ $28$ $28\frac{1}{2}$	$\begin{array}{c} 28 \\ 28\frac{1}{2} \\ 28\frac{3}{4} \\ 29\frac{1}{4} \end{array}$	$\begin{array}{c} 28\frac{3}{4} \\ 29\frac{1}{4} \\ 29\frac{3}{4} \\ 30\frac{1}{4} \end{array}$			
2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	$\begin{array}{c} 21\frac{1}{2} \\ 22 \\ 22\frac{1}{2} \\ 23 \end{array}$	$\begin{array}{c} 22\frac{1}{2} \\ 23 \\ 23\frac{1}{2} \\ 24 \end{array}$	$\begin{array}{c} 23\frac{1}{4} \\ 23\frac{3}{4} \\ 24\frac{1}{4} \\ 25 \end{array}$	$\begin{array}{c} 24\frac{1}{4} \\ 24\frac{3}{4} \\ 25\frac{1}{4} \\ 25\frac{3}{4} \end{array}$	$\begin{array}{c} 25\frac{1}{4} \\ 25\frac{3}{4} \\ 26\frac{1}{4} \\ 26\frac{3}{4} \end{array}$	$\begin{array}{c} 26 \\ 26\frac{1}{2} \\ 27\frac{1}{4} \\ 27\frac{3}{4} \end{array}$	$   \begin{array}{c}     27 \\     27\frac{1}{2} \\     28 \\     28\frac{1}{2}   \end{array} $	$28$ $28\frac{1}{2}$ $29$ $29\frac{1}{2}$	$\begin{array}{c} 28\frac{3}{4} \\ 29\frac{1}{2} \\ 30 \\ 30\frac{1}{2} \end{array}$	$29\frac{3}{4}$ $30\frac{1}{4}$ $30\frac{3}{4}$ $31\frac{1}{4}$	$\begin{array}{c} 30\frac{3}{4} \\ 31\frac{1}{4} \\ 31\frac{3}{4} \\ 32\frac{1}{4} \end{array}$			
21 <u>22</u> 5 <u>883</u> 47 <u>8</u>	$ \begin{array}{c} 23\frac{1}{2} \\ 24 \\ 24\frac{1}{2} \\ 25\frac{1}{4} \end{array} $	$24\frac{1}{2}$ $25$ $25\frac{1}{2}$ $26$	$\begin{array}{c} 25\frac{1}{2} \\ 26 \\ 26\frac{1}{2} \\ 27 \end{array}$	$\begin{array}{c} 26\frac{1}{4} \\ 26\frac{3}{4} \\ 27\frac{1}{2} \\ 28 \end{array}$	$   \begin{array}{c}     27\frac{1}{4} \\     27\frac{3}{4} \\     28\frac{1}{4} \\     28\frac{3}{4}   \end{array} $	$\begin{array}{c} 28\frac{1}{4} \\ 28\frac{3}{4} \\ 29\frac{1}{4} \\ 29\frac{3}{4} \end{array}$	$\begin{array}{c} 29 \\ 29\frac{3}{4} \\ 30\frac{1}{4} \\ 30\frac{3}{4} \end{array}$	$30 \\ 30\frac{1}{2} \\ 31 \\ 31\frac{1}{2}$	$\begin{array}{c} 31 \\ 31\frac{1}{2} \\ 32 \\ 32\frac{1}{2} \end{array}$	$32\frac{1}{2}$ $33\frac{1}{2}$	$\begin{array}{c} 32\frac{3}{4} \\ 33\frac{1}{4} \\ 33\frac{3}{4} \\ 34\frac{1}{2} \end{array}$			
9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	$\begin{array}{c} 25\frac{3}{4} \\ 26\frac{1}{4} \\ 26\frac{3}{4} \\ 27\frac{1}{4} \\ 27\frac{3}{4} \end{array}$	$\begin{array}{c c} 26\frac{1}{2} \\ 27 \\ 27\frac{3}{4} \\ 28\frac{1}{4} \\ 28\frac{3}{4} \end{array}$	$\begin{array}{c c} 27\frac{1}{2} \\ 28 \\ 28\frac{1}{2} \\ 29 \\ 29\frac{1}{2} \end{array}$	$\begin{array}{c c} 28\frac{1}{2} \\ 29 \\ 29\frac{1}{2} \\ 30 \\ 30\frac{1}{2} \end{array}$	$\begin{array}{c c} 29\frac{1}{4} \\ 30 \\ 30\frac{1}{2} \\ 31 \\ 31\frac{1}{2} \end{array}$	$\begin{array}{c} 30\frac{1}{4} \\ 30\frac{3}{4} \\ 31\frac{1}{4} \\ 31\frac{3}{4} \\ 32\frac{1}{2} \end{array}$	$\begin{array}{c} 31\frac{1}{4} \\ 31\frac{3}{4} \\ 32\frac{1}{4} \\ 32\frac{3}{4} \\ 33\frac{1}{4} \end{array}$	$\begin{array}{c} 32\frac{1}{4} \\ 32\frac{3}{4} \\ 33\frac{1}{4} \\ 33\frac{3}{4} \\ 34\frac{1}{4} \end{array}$	$33\frac{1}{2}$ $34$ $34\frac{3}{4}$ $35\frac{1}{4}$	$ \begin{array}{c c} 34 \\ 34\frac{1}{2} \\ 35 \\ 35\frac{1}{2} \\ 36 \end{array} $	$35$ $35\frac{1}{2}$ $36$ $36\frac{1}{2}$ $37$			

For additional length required to form upset end and details of same see tables of Upset Ends, pages 324 to 327.
For details of Turnbuckles, see page 330.
For details of Right and Left Nuts, see page 331.

### STANDARD STEEL WIRE NAILS AND SPIKES.

Sizes, Lengths and Approximate Number per Pound.

	COMMON					1		1	1 60				N.
Sizes.	Length.	Diam B. W. G.	Inches.	No. per Pound.	Barbed Common,	Clinch.	Fence.	Finishing.	Barbed Finishing.	Fine.	Barrel.	Casing.	Smooth Box.
2d 3d Fine. 3d Com. 4d	3/4 7/8 1 11/4 13/3 11/2 13/4 2 1/4 21/4 21/4 31/4 31/4 31/4 31/4 31/4 6	15 121/2 121/2 111/2 111/2 101/4 101/4 9 9 8 6 5 4 3 2		900 615 322 250 200 154 106 85 74 57 46 29 23 17 13½ 10½	\$600 594 339 2300 205 135 96 92 63 52 30 23 17 13½ 10½	267 230 156 110 98 86 66 57 46	2	359 317 214 3 195 2 134 5 120	884 767 491 359 317 214 195 134	550	940 804 620 590 542 365 3222	675 5675 396 2600 239 1600 148 108 99 69 50 45 35	550 366 250 236 157 145 107 98 65 45
Sizes.	Length.	Barbed Box.	Ova Car Light	arbed l Head Nails.	Slating.	Barbed Roofing.	Shingle.	Tobacco.	Lining.		neter.		No. per ound.
2d 3d Fine. 3d Com	3/4 11/8 11/4 11/4 11/4 11/4 11/4 11/4 11	236 1 157 145 107 98 65	260 134 51 119 85 988 75 866 55 866 55 43 40 39 27 21 188 15	51 45 38	385 230 198 125 112 	648 413 384 339 231  154 185 90 	380 256 226 200 130 115 79	1	930 660 4410	6.54322111	.20 .22 .23 .25 .28 .30 .30 .5 .5 .8 .8 .8 .8	0 2 8 2 9 1 4 1 0 1	29 23 18 18 18 19 71 71 71 71 71 71 71 71 71 71 71 71 71

#### MISCELLANEOUS STEEL WIRE NAILS.

	Approximate Number per Pound.															
wire Wee.	eter ches.					Le	eng	ths	— <b>I</b> 1	ıch	es	•				
Birming- ham Wire Gauge.	Diameter in Inches.	3 16		$\frac{1}{4}$	3/8		$\frac{1}{2}$	<u>5</u>	34		7/8	1		11/8	$1\frac{1}{4}$	$1\frac{1}{2}$
00 3/8 0 1/6 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22	.380 .375 .340 .313 .284 .259 .238 .220 .203 .180 .165 .148 .134 .120 .109 .095 .085 .072 .065 .049 .042 .035 .032	2000 2370 3047	0 18 0 18 2 1	2840 3504 4571 2233 32276 6668 50000 7777 2856	666 83 109 142 233 304 415 551 1000 1185 1523	3 7 6 9 1 3 1 6 6 1 8 8 2 6 6 3 7 4 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	211 2247 2299 345 414 496 628 822 072 420 752 280 1138 334 500 888 428	169 197 239 275 331 397 502 658 857 1136 402 1402 1828 3310 6000 7111 9143	100 122 144 166 200 222 277 33 411 544 1166 1552 2007 761	20 14 164 169 163 188 177 188 187 188 188 188 188 188 188	87 104 121 141 171 197 236 283 359 469 613 811 (001 (001 (305) (781 2364 2933 4400 6079	10 11 12 12 12 12 12 12 13 14 15 15 20 26 37 44 15 20 26 37 44 44	23 149 772 177 148 14 11 11 1366 10 776 143 14 1558 1 1559 1 250 350 350 350 350 350 350 350 350 350 3	385 839 370	33 34 45 52 60 72 85 99 120 137 165 198 429 429 568 701 913 1246 52133 3000	27 27 29 38 44 50 60 71 82 100 115 138 165 209 274 357 473 584 761 1038 1379 1778
Birming- ham Wire Gauge.	Diameter in Inches.	13/4	2	$2\frac{1}{4}$	$2\frac{1}{2}$	23/4	3	$3\frac{1}{2}$	4	$4\frac{1}{2}$	es 5	6	7	8	9	10
						<u></u>	-	$-\frac{\sigma_{\overline{2}}}{2}$			-	-			-	-
00 0 3/8 0 5/16 2 3 4 5 6 7 7 8 9 10	.380 .375 .340 .313 .284 .259 .238 .220 .203 .180 .165 .148	23 23 25 32 37 43 51 60 71 85 98 118	20 20 21 28 32 38 45 53 62 75 86 103	18 18 19 25 29 34 40 47 55 67 76 92	16 16 17 23 26 30 36 42 50 60 69 82	15 16 21 24 28 33 39 45 54 62 75	14 14 15 19 22 25 30 35 41 50 69	12 13 16 19 22 26 30 35 43 49 59	10 10 11 14 16 19 23 26 31 37 43 52	9 10 13 14 17 20 24 28 33 39 46	11 13 15 18 21 25 30 35 41	7 7 8 10 11 13 15 18 21 25 29	6 6 7 8 9 11 13 15 18	11	41/2 41/2 5 6 7 8 10	4 4 4 5 5 6 6 7 7 9
10 11 12 13 14 15 16 17 18	.134 .120 .109 .095 .083 .072 .065 .058	142 179 235 306 406 500 653 890 1182	124 157 204 268 350 438 571 779	110 139 182 238 315 389 508	99 125 164 214 284 350	90 114 149 195 258	83 105 137 178 236	71 90 117	62 79 103	55 70	50	Wingau  00 0	ge.	33/2 33/2 4 5 6	- -	

These approximate numbers are an average only, and the figures given may be varied either way, by changes in the dimensions of heads or points. Brads and no-head nails will run more to the pound than table shows, and large or thick-headed nails will run less.

### CUT STEEL NAILS AND SPIKES.

Sizes, Lengths and Approximate Number per Pound.

-	Sizes.	Length.	Common,	. Clin	Clinch.		ishing.	Casing and Box.		Fencing.	Spikes.
	2d 3d 4d 5d 6d 7d 8d 9d 10d 12d 16d	1 1 <sup>1</sup> / <sub>4</sub> 1 <sup>1</sup> / <sub>2</sub> 1 <sup>3</sup> / <sub>4</sub> 2 2 <sup>1</sup> / <sub>4</sub> 2 <sup>1</sup> / <sub>2</sub> 2 <sup>3</sup> / <sub>4</sub> 3 3 <sup>1</sup> / <sub>4</sub> 3 <sup>1</sup> / <sub>2</sub>	740 460 280 210 160 120 88 73 60 46	460 2 280 1 210 1 160 1 120 88 73 60 46 33			100 880 530 350 300 210 168 130 104 96 86	420 300 210 180 130 107 88 70 52		100 80 60 52 38 26 20 18	17
	20d 25d 30d 40d 50d 60d	4 4 <sup>1</sup> / <sub>4</sub> 4 <sup>1</sup> / <sub>2</sub> 5 5 <sup>1</sup> / <sub>2</sub> 6 6 <sup>1</sup> / <sub>2</sub> 7	23 20 16½ 12 10 8		24		76	38 30 26 20 16	•	16	14 11 9 7½ 6 5½ 5
	Sizes.	Length. Inches.	Barrel.	Light Barrel.	Slat	ing.	Sizes.	Length. Inches.		t Grip.	Edge Grip. Fine.
	2d 3d	5/8 3/4 7/8 1 11/8 11/4	750 600 500 450 310 280	400		40	2d 3d 4d	3/4 7/8 1 11/8 13/8	]	1462 1300 1100 800 650	960 750 600
	4d 5d 6d 7d	$1\frac{3}{8}$ $1\frac{1}{2}$ $1\frac{3}{4}$ $2$ $2\frac{1}{4}$	210 190	224	2	 220 .80		130 97 85	В	120 94	Shingle.
	9d 10d 12d 16d	2½ 2½ 2¾ 3 3½ 3½						68 58 48		74 62 50 40 27	90 72 60

# SQUARE BOAT SPIKES.

Approximate Number in a Keg of 200 Pounds.

Size.		Length of Spike-Inches.										
Inches.	3	4	5	6	7	8	9	10	11	12	14	16
1/4	3000	2375	2050	1825								
5 16	1660	1360	1230	1175	990	880						
3/8	1326	1140	940	800	650	600	525	475				
76				600	590	510	400	360	320	230		
1/2				450	375	335	300	275	260	240		
5/8					• •	260	240	220	205	190	175	160

# RAILROAD SPIKES.

Size Measured Under Head,	Average Number per Keg	Quantity of Spi Single Track. 4 Spikes per T	Rail Used, Weight per Yard, Pounds,		
Inches.	of 200 Pounds.	Pounds. Kegs.			
$5\frac{1}{2} \times \frac{5}{8}$	300	7040	35 <del>1</del>	75 to 100	
$5\frac{1}{2} \times \frac{9}{16}$	375	5870	291/3	45 " 75	
$5 \times \frac{9}{16}$	400	5170	26	40 " 56	
5 ×½	450	4660	231/3	35 '' 40	
$4\frac{1}{2} \times \frac{1}{2}$	530	3960	20	30 " 35	
$4 \times \frac{1}{2}$	600	3520	$17\frac{2}{3}$	25 " 35	
$4\frac{1}{2} \times \frac{7}{16}$	680	3110	15½	20 " 30	
$4 \times \frac{7}{16}$	720	2910	143/4	20 3 30	
$3\frac{1}{2}  imes \frac{7}{16}$	900	2350	11	16 " 25	
4 × 3/8	1000	2090	101/2	16 " 25	
$3\frac{1}{2}  imes \frac{3}{8}$	1190	1780	9	16 " 20	
$3 \times \frac{3}{8}$	1240	1710	8½	16 " 20	
$2\frac{1}{2} \times \frac{3}{8}$	1342	1575	77/8	8 " 16	

# WROUGHT-IRON WELDED STEAM, GAS AND WATER PIPE.

TABLE	of Stani	DARD SIZ	ES AND I	JIM EN	510	NS BY	AN	IERICAN	TUBE AND	Iron Co.
Nominal Inside	Actual Inside	Actual Outside	Thickness	Nomin Weig	nal ht			FERENCE.	LENGTH P	ER SQUARE SURFACE.
Diameter.	Diameter.	Diameter.	1	per Fo	ot.	Intern		External.	Inside.	Outside.
Inches.	Inches.	Inches.	Inches.		Pounds.		S.	Inches.	Feet.	Feet.
1/8	.27	.405	.07	.2	4	.84		1.27	14.15	9.44
3/2	.36 .49	.54 .675	.09	.5	6	1.5		1.69 2.12	10.50 7.67	7.07 5.65
1/8 1/4 3/8 1/2 3/4	.62	.84	.10	8.	4	1.9	5	2.65	6.13	4.50
/4	.82	1.05	.11	1.1		$\frac{2.5}{3.2}$	8	3.29	4.63	3.63
11/4	1.04 1.38	1.315 1.66	.13	1.6	4	4.3	3	4.13 5.21	3.67 2.76	2.90 2.30
1/2	1.61	1.9	.14	2.6	8	5.0	6	5.96	2.37	2.01
2.	2.06	2.375	.15 .20	3.6		6.4		7.46	1.84	1.61
2½ 3	2.46 3.06	$\frac{2.875}{3.5}$	.21	5.7 7.5		7.7 9.6		9.03 10.96	1.54 1.24	1.32 1.09
31/2	3.56	4.	,22	9.0	0	11.1	4	12.56	1.07	.95
4	4.02	4.5	.23	10.6		12.6		14.13	.94	.81
$\frac{41}{2}$	4.50 5.04	5. 5.56	.25	12.3 14.5		14.1 15.8		15.70 17.47	.84	.76 .62
6 7	6.06	6.625	.28	18.7	6	19.0	5	20.81	.63	.57
7	7.02	7.625	.30	23.2	7	22.0	6	23.95	.54	.50
8 9	7.98 9.00	8.625 9.625	.32 .34	28.1 33.7		25.0 $28.2$		27.09 30.43	.47	.44
10	10.01	10.75	.36	40.0		31.4		33.77	.38	.35
11	11.	11.75	.37	45.		34.5	5	36.91	.34	.32
12 13	12. 13.25	12.75 14.	.37 .37	49.0 54.0		37.7 41.6		40.05 43.98	.32	.30
14	14.25	15.	.37	58.0		44.7		47.12	.27	.25
15	15.40	16.	.28	66.0		48.4	8	50.26	.25	.24
16	16.40	17.	.30					53.41	.23	.23
		18	34	75.0	n	54.4	1	56 55	99	91
17	17.30	18.	.34	75.0	1	54.4	,	56.55	SOCKETS	ON PIPE
Nominal	Internal	Extern	nal Le	ngth	1	To. of	Co	ntents of	SOCKETS	ON PIPE.
-		1	nal Le		Th	lo. of reads	Co			
Nominal Inside	Internal	Extern Area	nal Cont	ngth	Th	To. of	Co	ntents of one Foot	SOCKETS Outside	ON PIPE.
Nominal Inside Diameter. Inches.	Internal Area.  Sq. Inches	Extern Area	nal Condition of C	ength aining ic Foot.	The per	No. of areads r Inch.	Co	ntents of one Foot Length. dallons.	SOCKETS Outside Diameter. Inches.	ON PIPE.  Length.  Inches.
Nominal Inside Diameter. Inches.	Internal Area.  Sq. Inches  .06 .10	Extern Area	nal Cont 1 Cub Hes. H	ength aining ic Foot. eet. 00. 85.	The per	No. of areads r Inch.	Co	ntents of the Foot Length. Hallons.	SOCKETS Outside Diameter. Inches60 .78	Length. Inches. 81 1.00
Nominal Inside Diameter.	Internal Area.  Sq. Inches	Extern Area	nal Cont 1 Cub 1 C	ength aining ic Foot.	The per	No. of areads r Inch.	Co	ntents of one Foot Length. dallons.	SOCKETS Outside Diameter. Inches.	ON PIPE.  Length.  Inches.
Nominal Inside Diameter. Inches.	Internal Area.  Sq. Inches  .06 .10 .19 .30 .53	Extern Area	hes. L6 Com/1 Ouk thes. H12 25 222 13 35 7 555 44 86 22	ength aining ic Foot. Peet. 00. 85. 51.5 72.4 70.	The per	No. of areads r Inch.	Co	ntents of the Foot Length. Gallons	SOCKETS Outside Diameter. Inches60 .78 .91 1.10 1.34	ON PIPE.  Length.  Inches.  81  1.00  1.10  1.31  1.56
Nominal Inside Diameter. Inches.	Internal Area.  Sq. Inches  .06 .10 .19 .30 .53 .86	Extern Area	hes. L6 Com/1 Ouk thes. H12 25 222 13 35 7 555 44 86 22	ength aining ic Foot. Peet. 00. 85. 51.5 72.4 70.	The per	No. of areads r Inch.  27 18 18 14 14	Co	ntents of the Foot Length. Gallons.  .002 .002 .005 .010 .023 .040	SOCKETS  Outside Diameter, Inches, .60 .78 .91 1.10 1.34 1.66	ON PIPE.  Length.  Inches.  .81 1.00 1.10 1.31 1.56 1.75
Nominal Inside Diameter. Inches.	Internal Area.  Sq. Inches  .06 .10 .19 .30 .53	Extern Area	nal Cont Cont Cont Cont Cont Cont Cont Cont	ngth aining ic Foot. leet. 00. 85. 51.5 72.4	The period of th	No. of areads of Inch.  27 18 18 14 11 12 11 12 11 12	Co	ntents of the Foot Length. Gallons	SOCKETS  Outside Diameter.  Inches.  .60 .78 .91 1.10 1.34 1.66 2.00 2.28	ON PIPE.  Length.  Inches.  81  1.00  1.10  1.31  1.56
Nominal Inside Diameter, Inches.  1/8 1/4 1/4 1/4 1/2 2	Internal Area.  Sq. Inches  .06 .10 .19 .30 .53 .86 1.49 2.03 3.35	Extern Area  Sq. Inc  1 3 2 4	Land   Local   Conf.   1 (0uh   1 (0uh   1   1   1   2   1   1   1   1   1   1	ongth aining in Foot. Peet. 100. 100. 100. 100. 100. 100. 100. 10	The period of th	No. of areads of Inch.  27 18 18 14 11 12 11 12 11 12 11 12	Co	ntents of the Foot Length. Sallons	SOCKETS Outside Diameter. Inches60 .78 .91 1.10 1.34 1.66 2.00 2.28 2.81	ON PIPE.  Length. Inches81 1.00 1.10 1.31 1.56 1.75 1.94 2.19 2.31
Nominal Inside Diameter, Inches, 14 34 34 11 114 117 2 2 214	Internal Area.  Sq. Inches  .06 .10 .19 .30 .53 .86 1.49 2.03 3.35 4.78	Extern Area  Sq. Inc  1. 3. 2. 4. 6.	help land land land land land land land land	ngth aining ic Foot. leet. 00. 85. 51.5 72.4 70. 666.9 96.25 70.65 42.36 30.11	The period of th	No. of areads of Inch.  27 18 18 14 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 12	Co	ntents of the Foot Length. Sallons	SOCKETS Outside Diameter. Inches60 .78 .91 1.10 1.34 1.66 2.00 2.28 2.81 3.28	ON PIPE.  Length.  Inches.  .81 1.00 1.10 1.31 1.56 1.75 1.94 2.19 2.31 2.70
Nominal Inside Diameter, Inches, 1/8 1/4 11/4 11/4 22 21/2 3	Internal Area.  Sq. Inches  .06 .10 .19 .30 .53 .86 1.49 2.03 3.35 4.78 7.38 9.83	Extern Area  Sq. Inc  1 3 2 4	nal Comit Out Out Out Out Out Out Out Out Out Ou	ngth aining ic Foot. leet. 000. 85. 51.5 72.4 70. 66.9 96.25 70.65 42.36 30.11 19.49 14.56	The period of th	No. of areads of Inch.  27 18 18 14 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 12	Co	ntents of ine Foot Length. Length. Rallons	SOCKETS  Outside Diameter.  Inches.  .60 .78 .91 1.10 1.34 1.66 2.00 2.28 2.81 3.28 4.02 4.50	ON PIPE.  Length.  Inches.
Nominal Inside Diameter. Inches. 1/8 1/8 1/8 1/9 1/9 1/9 1/9 1/9 1/9 1/9 1/9 1/9 1/9	Internal Area.  Sq. Inches  .06 .10 .19 .30 .53 .86 1.49 2.03 3.35 4.78 7.38 9.83 12.73	Extern Area  Sq. Inc  1. 3. 2. 4. 6. 9. 12.	nal Com 1 Ouk 1 Ou	mgth aining ic Foot. leet. 00. 85. 51.5 72.4 70. 666.9 96.25 70.65 42.36 30.11 19.49 14.56 11.31	The period of th	No. of areads of Inch.  27 18 18 14 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 12	Co	ntents of ine Foot Length. Co22 .002 .005 .010 .023 .040 .063 .255 .367 .500 .652	SOCKETS  Outside Diameter.  Inches,  .60 .78 .91 1.10 1.34 1.66 2.00 2.28 2.81 3.28 4.02 4.50 5.10	ON PIPE.  Length.  Inches.  .81 1.00 1.10 1.31 1.56 1.75 1.94 2.19 2.31 2.70 3.00 3.12 3.12
Nominal Inside Diameter.  Inches.  1/8 1/8 1/8 1/8 1/8 1/8 1/1 1/4 1/2 2 2 2 3 3 3/2 4 4 4/2	Internal Area.  Sq. Inches  .06 .10 .19 .30 .53 .86 1.49 2.03 3.35 4.78 7.38 9.83 12.73 15.93	Extern Area Sq. Inc	Inal Com 1 Out 1 O	mgth aining ic Foot. leet. 00. 85. 51.5 72.4 70. 66.9 96.25 42.36 30.11 19.49 14.56 11.31 9.03	The period of th	No. of areads of Inch.  27 18 18 14 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 12	Co	ntents of me Foot Length. Length. Sallons,	SOOKETS Outside Diameter. Inches60 .78 .91 1.10 1.34 1.66 2.00 2.28 2.81 3.28 4.02 4.50 5.10 5.53	ON PIPE.  Length.  Inches.  .81 1.00 1.10 1.31 1.56 1.75 1.94 2.19 2.31 2.70 3.00 3.12 3.12 3.12
Nominal Inside Diameter, Inches, 1/8 1/4 1/4 1/4 2 2 2 1/2 3 3 1/2 4 4 1/2 5 6	Internal Area.  Sq. Inches  .06 .10 .19 .30 .53 .86 1.49 2.03 3.35 4.78 7.38 9.83 12.73	Extern Area  Sq. Inc  1. 3. 2. 4. 6. 9. 12. 15. 19. 24. 34.	nal   Le Comi   1 Cuk    mgth aining ic Foot. leet. 00. 85. 72.4 70. 66.9 96.25 70.65 42.36 80.11 19.49 14.56 11.31 9.03 4.98	The period of th	No. of areads of Inch.  27 18 18 14 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 12	Co	ntents of ine Foot Length. Length. Rallons. Respectively 1002 and 1003 and	SOOKETS  Outside Diameter.  Inches.  .60 .78 .91 1.10 1.34 1.66 2.00 2.28 2.81 3.28 4.02 4.50 5.10 5.53 6.25 7.34	ON PIPE.  Length. Inches.	
Nominal Inside Diameter. Inches.    1/8 1/4 1/4 11/4 11/2 2 22/2 3 3/2 4 41/2 5 6 6 7	Internal Area.  Sq. Inches  .06 .10 .19 .50 .53 .86 1.49 2.03 3.35 4.78 7.38 9.83 12.73 15.93 19.99 28.88 38.73	Extern Area  Sq. Inc  1. 3. 2. 4. 6. 9. 12. 15. 19. 24. 34. 34. 34.	Le   Com   1 Ouk   1	mgth aining ic Foot, leet, 00. 85. 72.4 70. 66.9 96.25 70.65 42.36 30.11 19.49 14.56 11.31 9.03 7.20 4.98 3.72	The period of th	No. of areads of Inch.  27 18 18 14 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 12	Co	ntents of ine Foot Length, Gallons.  -002 .005 .010 .023 .040 .063 .255 .367 .500 .652 .826 1.02 1.046 2.00	800KETS Outside Diameter. Inches, .60 .78 .91 1.10 1.34 1.66 2.00 2.28 2.81 3.28 4.02 4.50 5.10 5.53 6.25 7.34 8.34	ON PIPE.  Length.  Inches.  .81  1.00  1.31  1.56  1.75  1.94  2.19  2.81  2.70  3.00  3.12  3.12  3.12  3.70  4.31
Nominal Inside Diameter, Inches.  1/8 1/4 1/2 2 21/2 3 31/2 4 41/2 5 6 7 8	Internal Area.  Sq. Inches  .06 .10 .19 .30 .53 .86 1.49 2.03 3.35 4.78 7.38 9.83 12.73 15.93 19.99 28.88 38.73 50.03	Extern Area  Sq. Inc  1. 3. 2. 4. 6. 9. 12. 15. 19. 24. 45. 58.	nal   Le Comi   1 Cuk    mgth aining ic Foot. leet. 00. 851.5 72.4 70. 65 42.36 89.11 19.49 14.56 11.31 9.03 7.20 4.98 3.72 2.88 2.26	The period of th	No. of areads of Inch.  27 18 18 14 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 12	Co	ntents of ine Foot Length. Length. Rallons. Respectively 1002 and 1003 and	SOOKETS  Outside Diameter.  Inches.  .60 .78 .91 1.10 1.34 1.66 2.00 2.28 2.81 3.28 4.02 4.50 5.10 5.53 6.25 7.34	ON PIPE.  Length. Inches.	
Nominal Inside Diameter, Inches, 18 14 14 114 114 114 114 114 114 114 11	Internal Area.  Sq. Inches  .06 .10 .19 .30 .53 .86 1.49 2.03 3.35 4.78 7.38 9.83 12.73 15.93 19.99 28.88 38.73 50.03 63.63 78.83	Extern Area  Sq. Inc  1. 3. 2. 4. 6. 9. 12. 15. 19. 24. 34. 45. 58. 73. 90.	nal   Le Comi	mgth aining ic Foot. Peet. 000. 855. 572.4 70. 666.9 966.25 70.65 42.36 30.11 19.49 14.56 11.31 9.03 7.20 2.88 3.72 2.88 2.26 1.80	The period of th	No. of areads of Inch.  27 18 18 14 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 12	Co	ntents of ine Foot Length. dallons.	SOCKETS Outside Diameter. Inches, .60 .78 .91 1.10 1.34 1.66 2.00 2.28 2.81 3.28 4.02 4.50 5.10 5.53 6.25 7.34 8.34 9.44	ON PIPE.  Length.  Inches.  .81 1.00 1.10 1.31 1.56 1.75 1.94 2.19 2.81 2.70 3.00 3.12 3.12 3.70 3.70 4.31 4.56
Nominal Inside Diameter. Inches.    1/8 1/4 1/4 1/4 1/4 1/2 2 2/2 3 3/2 4 4/2 5 6 6 7 8 9 10 11	Internal Area,  Sq. Inches  .06 .10 .19 .30 .53 .86 1.49 2.03 3.35 4.78 7.38 9.83 12.73 15.93 19.99 28.88 38.73 50.03 63.63 78.83 95.03	Extern Area  Sq. Inc  1. 3. 2. 4. 6. 9. 12. 15. 19. 24. 45. 58. 73. 90. 108.	Le   Com   1 Ouk   1	mgth aining ic Foot. leet. 00. 85. 72.4 70. 66.9 96.25 42.36 80.11 19.49 14.56 11.31 9.03 7.20 2.88 2.26 1.80 1.50	The period of th	No. of areads of Inch.  27 18 18 14 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 12	Co	ntents of ine Foot Length. dallons	800KETS Outside Diameter. Inches, .60 .78 .91 1.10 1.34 1.66 2.00 2.28 2.81 3.28 4.02 4.50 5.10 5.53 6.25 7.34 8.34 9.44 10.47 11.50	ON PIPE.  Length.  Inches.  .81 1.00 1.10 1.31 1.56 1.75 1.94 2.19 2.81 2.70 3.00 3.12 3.12 3.12 3.70 3.70 4.31 4.56 5.75 6.25
Nominal Inside Diameter, Inches, 18 14 14 114 114 114 114 114 114 114 11	Internal Area.  Sq. Inches  .06 .10 .19 .30 .53 .86 1.49 2.03 3.35 4.78 7.38 9.83 12.73 15.93 19.99 28.88 38.73 50.03 63.63 78.83	Extern Area  Sq. Inc  1. 3. 2. 4. 6. 9. 12. 15. 19. 24. 45. 58. 73. 90. 108. 127. 153.	nal   Le Comi	mgth aining ic Foot. leet. 00. 851.5 72.4 70. 65 42.36 80.1 19.49 14.56 11.31 9.03 7.20 4.98 3.72 2.88 2.266 1.80 1.50 1.27 1.04	The period of th	No. of areads of Inch.  27 18 18 14 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 12	Co	ntents of ine Foot Length. Len	800KETS Outside Diameter. Inches, .60 .78 .91 1.10 1.34 1.66 2.00 2.28 2.81 3.28 4.02 4.50 5.10 5.53 6.25 7.34 8.34 9.44 10.47	ON PIPE.  Length, Inches.
Nominal Inside Diameter, Inches, 18 14 14 14 14 14 15 16 6 77 8 9 10 11 12 13 14	Internal Area.  Sq. Inches  .06 .10 .19 .30 .53 .86 1.49 2.03 3.35 4.78 7.38 9.83 12.73 15.93 19.99 28.88 38.73 50.03 63.63 78.83 95.03 113.09 137.88	Extern Area  Sq. Inc  1. 3. 2. 4. 6. 9. 12. 15. 19. 24. 45. 58. 73. 90. 108. 127. 153.	nal   Le Comi   1 Ouk   1	mgth aining ic Foot. Peet. 00. 85. 72.4 70. 66.9 96.25 42.36 30.11 19.49 14.56 11.31 9.03 7.20 2.88 2.26 1.50 1.27 1.04 90	The period of th	No. of areads of Inch.  27 18 18 14 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 12	Co	ntents of ine Foot Length. dallons.	800KETS Outside Diameter. Inches, .60 .78 .91 1.10 1.34 1.66 2.00 2.28 2.81 3.28 4.02 4.50 5.10 5.53 6.25 7.34 8.34 9.44 10.47 11.50	ON PIPE.  Length.  Inches.  .81 1.00 1.10 1.31 1.56 1.75 1.94 2.19 2.81 2.70 3.00 3.12 3.12 3.12 3.70 3.70 4.31 4.56 5.75 6.25
Nominal Inside Diameter. Inches.    1/8	Internal Area.  Sq. Inches  .06 .10 .19 .30 .53 .86 1.49 2.03 3.35 4.78 7.38 9.83 12.73 15.93 19.99 28.88 38.73 50.03 63.63 78.83 95.03 113.09 137.88 159.48 187.04	Extern Area  Sq. Inc  1. 3. 2. 4. 6. 9. 12. 15. 19. 24. 34. 34. 35. 90. 108. 127. 153. 176. 201.	Le   Com   1 Ouk   1	mgth aining ic Foot. Peet. 100. 100. 100. 100. 100. 100. 100. 10	The period of th	No. of areads of Inch.  27 18 18 14 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 11 12 12	Coo	ntents of ine Foot Length. dallons	800KETS Outside Diameter. Inches60 .78 .91 1.10 1.34 1.66 2.00 2.28 2.81 3.28 4.02 4.50 5.10 5.53 6.25 7.34 8.34 9.44 10.47 11.50 13.78	ON PIPE.  Length.  Inches.  .81 1.00 1.10 1.31 1.56 1.75 1.94 2.19 2.81 2.70 3.00 3.12 3.12 3.12 3.70 3.70 4.31 4.56 5.75 6.25
Nominal Inside Diameter, Inches, 18 14 14 14 14 14 15 16 6 77 8 9 10 11 12 13 14	Internal Area.  Sq. Inches  .06 .10 .19 .30 .53 .86 1.49 2.03 3.35 4.78 7.38 9.83 12.73 15.93 19.99 28.88 38.73 50.03 63.63 78.83 95.03 113.09 137.88	Extern Area  Sq. Inc  1. 3. 2. 4. 6. 9. 12. 15. 19. 24. 45. 58. 73. 90. 108. 127. 153.	Le   Com   1 Ouk   1	mgth aining ic Foot. Peet. 00. 85. 72.4 70. 66.9 96.25 42.36 30.11 19.49 14.56 11.31 9.03 7.20 2.88 2.26 1.50 1.27 1.04 90	The period of th	No. of areads of Inch.  27 18 18 14 11 12 11 12 11 12 11 12	Co	ntents of ine Foot Length. dallons.	800KETS Outside Diameter. Inches, .60 .78 .91 1.10 1.34 1.66 2.00 2.28 2.81 3.28 4.02 4.50 5.10 5.53 6.25 7.34 8.34 9.44 10.47 11.50	ON PIPE.  Length.  Inches.  .81 1.00 1.10 1.31 1.56 1.75 1.94 2.19 2.81 2.70 3.00 3.12 3.12 3.12 3.70 3.70 4.31 4.56 5.75 6.25

# MANUFACTURERS' STANDARD SPECIFICATIONS.

REVISED TO FEBRUARY 6, 1903.

## STRUCTURAL STEEL.

#### PROCESS OF MANUFACTURE.

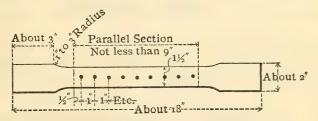
1. Steel may be made by either the Open-hearth or Bessemer process.

## TESTING AND INSPECTION.

2. All tests and inspections shall be made at the place of manufacture prior to shipment.

#### TEST PIECES.

3. The tensile strength, limit of elasticity and ductility, shall be determined from a standard test piece cut from the finished material. The standard shape of the tes piece for sheared plates shall be as shown by the following sketch:



Piece to be the same thickness as the plate.

On tests cut from other material the test piece may be either the same as for sheared plates, or it may be planed or turned parallel throughout its entire length, and in all cases where possible, two opposite sides of the test piece shall be the rolled surfaces. The elongation shall be measured on an original length of 8 inches, except as modified in section 12 paragraph c. Rivet rounds and small bars shall be tested of full size as rolled.

Two test pieces shall be taken from each melt or blow of finished material, one for tension and one for bending; but in case either test develops flaws, or the tensile test piece breaks outside of the middle third of its gauged length, it may be discarded and another test piece substituted therefor.

## ANNEALED TEST PIECES.

4. Material which is to be used without annealing or further treatment shall be tested in the condition in which it comes from the rolls. When material is to be annealed or otherwise treated before use, the specimen representing such material shall be similarly treated before testing.

#### MARKING.

5. Every finished piece of steel shall be stamped with the blow or melt number, and steel for pins shall have the blow or melt number stamped on the ends. Rivet and lacing steel, and small pieces for pin plates and stiffeners, may be shipped in bundles securely wired together, with the blow or melt number on a metal tag attached.

#### FINISH.

6. Finished bars shall be free from injurious seams, flaws or cracks, and have a workmanlike finish.

## CHEMICAL PROPERTIES.

7a. Steel for Buildings, Train Sheds, Highway Bridges and similar structures.

Maximum Phosphorus .10 per cent.

Steel for 76. Railway Bridges.

Maximum Phosphorus .08 per cent.

#### PHYSICAL PROPERTIES.

8. Structural Steel shall be of three grades, RIVET, RAILWAY BRIDGE and MEDIUM.

#### RIVET STEEL.

9. Ultimate strength, 48,000 to 58,000 pounds per square inch. Elastic limit, not less than one-half the ultimate strength.

1,400,000

Percentage of elongation, Ultimate strength

Bending test, 180 degrees flat on itself, without fracture on outside of bent portion.

#### STEEL FOR RAILWAY BRIDGES.

10. Ultimate strength, 55,000 to 65,000 pounds per square inch.

Elastic limit, not less than one-half the ultimate strength.

1,400,000

Percentage of elongation, Ultimate strength

Bending test, 180 degrees to a diameter equal to thickness of piece tested, without fracture on outside of bent portion.

## MEDIUM STEEL.

11. Ultimate strength, 60,000 to 70,000 pounds per square inch. Elastic limit, not less than one-half the ultimate strength.

1,400,000

Percentage of elongation, Ultimate strength

Bending test, 180 degrees to a diameter equal to thickness of piece tested, without fracture on outside of bent portion.

## MODIFICATIONS IN ELONGATION FOR THIN AND THICK MATERIAL.

- 12. For material less than  $\frac{5}{1.5}$  inch and more than  $\frac{3}{4}$  inch in thickness, the following modifications shall be made in the requirements for elongation:
- a. For each increase of  $\frac{1}{6}$  inch in thickness above  $\frac{3}{4}$  inch, a deduction of 1 per cent. shall be made from the specified elongation, except that the minimum elongation shall be 20 per cent. for eye-bar material and 18 per cent. for other structural material.
- b. For each decrease of  $\frac{1}{16}$  inch in thickness below  $\frac{5}{16}$  inch, a deduction of  $2\frac{1}{2}$  per cent. shall be made from the specified elongation.
- c. In rounds of 5 inch or less in diameter, the elongation shall be measured in a length equal to eight times the diameter of section tested.
- d. For pins made from any of the before-mentioned grades of steel, the required elongation shall be 5 per cent. less than that specified for each grade, as determined on a test piece, the center of which shall be one inch from the surface of the bar.

## VARIATION IN WEIGHT.

13. The variation in cross-section or weight of more than  $2\frac{1}{2}$  per cent. from that specified will be sufficient cause for rejection, except in the case of sheared plates which will be covered by the following permissible variations:

- a. Plates  $12\frac{1}{2}$  pounds per square foot or heavier, up to 100 inches wide, when ordered to weight, shall not average more than  $2\frac{1}{2}$  per cent. variation above or  $2\frac{1}{2}$  per cent. below the theoretical weight. When 100 inches wide and over, 5 per cent. above or 5 per cent. below the theoretical weight.
- b. Plates under  $12\frac{1}{2}$  pounds per square foot when ordered to weight, shall not average a greater variation than the following:

Up to 75 inches wide,  $2\frac{1}{2}$  per cent. above or  $2\frac{1}{2}$  per cent. below the theoretical weight. 75 inches wide up to 100 inches wide, 5 per cent. above or 3 per cent. below the theoretical weight. When 100 inches wide and over, 10 per cent. above or 3 per cent. below the theoretical weight.

c. For all plates ordered to gauge, there will be permitted an average excess of weight over that corresponding to the dimensions on the order equal in amount to that specified in the following table:

# TABLE OF ALLOWANCES FOR OVERWEIGHT FOR RECTANGULAR PLATES WHEN ORDERED TO GAUGE.

PLATES WILL BE CONSIDERED UP TO GAUGE IF MEASURING NOT OVER  $_{1\bar{3}\sigma}$  INCH LESS THAN THE ORDERED GAUGE. THE WEIGHT OF 1 CUBIC INCH OF ROLLED STEEL IS ASSUMED TO BE 0.2833 POUND.

PLATES 1/1 AND OVER IN THICKNESS.

	- 4								
THICKNESS OF	WIDTH OF PLATE.								
PLATE. Inch.	Up to 75 Inches. Per Cent.	75 to 100 Inches. Per Cent.	Over 100 to 115 Ins. Per Cent.	Over 115 Inches. Per Cent.					
$\frac{1}{4}$	10	14	18	• •					
4 13 13 7 16	8	12	16						
3/8	7	10	13	17					
$\frac{\overline{7}}{16}$	6	8	10	13					
$\frac{1}{2}$	5	7	9	12					
Over 5 8	$4\frac{1}{2}$	$6\frac{1}{2}$	$8\frac{1}{2}$	11					
<u>5</u>	4	6	8	10					
Over $\frac{5}{8}$	$3\frac{1}{2}$	5	$6\frac{1}{2}$	9					

# Plates Under $\frac{1}{4}$ " in Thickness.

THICKNESS OF PLATE.	WIDTH OF PLATE.					
Inch.	Up to 50 Inches. Per Cent.	50 to 70 Inches. Per Cent.	Over 70 Inches. Per Cent.			
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\frac{10}{8\frac{1}{2}}$	15 12½ 10	20 17 15			

## STRUCTURAL CAST IRON.

1. Except when chilled iron is specified, all castings shall be tough gray iron, free from injurious cold-shuts or blow-holes, true to pattern, and of a workmanlike finish. Sample pieces, one inch square, cast from the same heat of metal in sand moulds, shall be capable of sustaining on a clear span of 4 feet 8 inches, a central load of 500 pounds when tested in the rough bar.

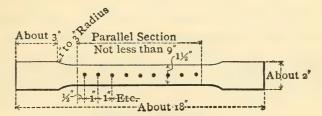
# SPECIAL OPEN-HEARTH PLATE AND RIVET STEEL.

### TESTING AND INSPECTION.

1. All tests and inspections shall be made at the place of manufacture prior to shipment.

#### TEST PIECES.

2. The tensile strength, limit of elasticity and ductility, shall be determined from a standard test piece cut from the finished material. The standard shape of the test piece for sheared plates shall be as shown by the following sketch:



Piece to be the same thickness as the plate.

On tests cut from other material the test piece may be either the same as for sheared plates, or it may be planed or turned parallel throughout its entire length, and in all cases where possible, two opposite sides of the test piece shall be the rolled surfaces. The elongation shall be measured on an original length of 8 inches, except as modified in section 12 paragraph c. Rivet rounds and small bars shall be tested of full size as rolled.

Four test pieces shall be taken from each melt of finished material, two for tension and two for bending; but in case either test develops flaws, or the tensile test piece breaks outside of the middle third of its gauged length, it may be discarded and another test piece substituted therefor.

## ANNEALED TEST PIECES.

3. Material which is to be used without annealing or further treatment shall be tested in the condition in which it comes from the rolls. When material is to be annealed or otherwise treated before use, the specimen representing such material shall be similarly treated before testing.

#### MARKING.

4. Every finished piece of steel shall be stamped with the melt number. Rivet steel may be shipped in bundles securely wired together, with the melt number on a metal tag attached.

#### FINISH.

5. All plates shall be free from injurious surface defects and have a workmanlike finish.

## CHEMICAL PROPERTIES.

6a.	Flange or Boiler	1	Maximum	Phosphorus	.06	per cent.
	Steel.	5	66	Sulphur	.04	"
<i>6b.</i>	Extra Soft and	1	. "	Phosphorus	.04	66
	Fire Box Steel.	5	66	Sulphur	.04	66

### PHYSICAL PROPERTIES.

7. Special Open-hearth Plate and Rivet Steel shall be of three grades, EXTRA SOFT, FIRE BOX and FLANGE or BOILER STEEL.

#### EXTRA SOFT STEEL.

8. Ultimate strength, 45,000 to 55,000 pounds per square inch.

Elastic limit, not less than one-half the ultimate strength.

Elongation, 28 per cent.

Cold and quench bends, 180 degrees flat on itself, without fracture on outside of bent portion.

### FIRE BOX STEEL.

9. Ultimate strength, 52,000 to 62,000 pounds per square inch.

Elastic limit, not less than one-half the ultimate strength.

Elongation, 26 per cent.

Cold and quench bends, 180 degrees flat on itself, without fracture on outside of bent portion.

#### FLANGE OR BOILER STEEL.

10. Ultimate strength, 55,000 to 65,000 pounds per square inch.

Elastic limit, not less than one-half the ultimate strength.

Elongation, 25 per cent.

Cold and quench bends, 180 degrees flat on itself, without fracture on outside of bent portion.

#### BOILER RIVET STEEL.

11. Steel for boiler rivets shall be made of the extra soft grade specified in paragraph No. 8.

# MODIFICATIONS IN ELONGATION FOR THIN AND THICK MATERIAL.

- 12. For material less than  $\frac{5}{16}$  inch and more than  $\frac{3}{4}$  inch in thickness, the following modifications shall be made in the requirements for elongation:
- a. For each increase of  $\frac{1}{8}$  inch in thickness above  $\frac{3}{4}$  inch, a deduction of 1 per cent. shall be made from the specified elongation.
- b. For each decrease of  $\frac{1}{16}$  inch in thickness below  $\frac{5}{16}$  inch, a deduction of  $2\frac{1}{2}$  per cent. shall be made from the specified elongation.
- c. In rounds of  $\frac{5}{8}$  inch or less in diameter, the elongation shall be measured in a length equal to eight times the diameter of section tested.

## VARIATION IN WEIGHT.

- 13. The variation in cross-section or weight of more than  $2\frac{1}{2}$  per cent. from that specified will be sufficient cause for rejection, except in the case of sheared plates which will be covered by the following permissible variations:
- a. Plates  $12\frac{1}{2}$  pounds per square foot or heavier, up to 100 inches wide, when ordered to weight, shall not average more than  $2\frac{1}{2}$  per cent. variation above or  $2\frac{1}{2}$  per cent. below the theoretical weight. When 100 inches wide and over, 5 per cent. above or 5 per cent. below the theoretical weight.

b. Plates under  $12\frac{1}{2}$  pounds per square foot when ordered to weight, shall not average a greater variation than the following:

Up to 75 inches wide,  $2\frac{1}{2}$  per cent. above or  $2\frac{1}{2}$  per cent. below the theoretical weight. 75 inches wide up to 100 inches wide, 5 per cent. above or 3 per cent. below the theoretical weight. When 100 inches wide and over, 10 per cent. above or 3 per cent. below the theoretical weight.

c. For all plates ordered to gauge, there will be permitted an average excess of weight over that corresponding to the dimensions on the order equal in amount to that specified in the following table:

# TABLE OF ALLOWANCES FOR OVERWEIGHT FOR RECTANGULAR PLATES WHEN ORDERED TO GAUGE.

PLATES WILL BE CONSIDERED UP TO GAUGE IF MEASURING NOT OVER  $\frac{1}{100}$  INCH LESS THAN THE ORDERED GAUGE.

THE WEIGHT OF ONE CUBIC INCH OF ROLLED STEEL IS ASSUMED TO BE 0.2833 POUND.

PLATES 1/4 AND OVER IN THICKNESS.

THICKNESS OF	WIDTH OF PLATE,								
PLATE. Inch.	Up to 75 Inches. Per Cent.	75 to 100 Inches. Per Cent.	Over 100 to 115 Ins. Per Cent.	Over 115 Inches. Per Cent.					
1 4 5	10	14 12	18						
45. 13. 87. 16.	7	10	13	17					
1	5	8 7	9	13 12					
2 9 16 5 8 5 8 5 8 5 8 5 8 8 1 8 1 1 1 1 1 1 1	$\frac{4\frac{1}{2}}{4}$	$6\frac{1}{2}$	$8\frac{1}{2}$	11 10					
Over $\frac{5}{8}$	$3\frac{1}{2}$	5	$6\frac{1}{2}$	9					

# PLATES UNDER $\frac{1}{4}$ IN THICKNESS.

THICKNESS OF PLATE,	WIDTH OF PLATE.					
Inch.	Up to 50 Inches. Per Cent.	50 to 70 Inches. Per Cent.	Over 70 Inches. Per Cent.			
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\frac{10}{8\frac{1}{2}}$	15 12½ 10	20 17 15			

## WOODEN BEAMS AND COLUMNS.

The results of a series of studies of wooden beams and columns of various kinds of American timber are contained in the Proceedings of the Fifth Annual Convention of the Association of Railway Superintendents of Bridges and Buildings, October, 1895, at which the Committee on Strength of Bridge and Trestle Timbers presented a report, portions of which have been used in preparing certain of the tables on the following pages, but as noted thereon the arrangement and values in many cases have been modified by later information from various sources.

The publications of the Forestry Division of the United States Department of Agriculture, Bulletins Nos. 8 and 12, and Circular No. 15, contain reports of tests of American woods, and deductions drawn therefrom. Extracts and tables from these reports are given on the following pages.

The tables of safe loads for wooden beams and tables of strength of wooden columns given on the following pages have been specially calculated for this book, using the information regarding the properties of the various species contained in the reports above referred to, as modified in some cases by later data.

EXPLANATION OF THE TABLES OF SAFE LOADS IN POUNDS, UNI-FORMLY DISTRIBUTED FOR RECTANGULAR WOODEN BEAMS ONE INCH THICK, PAGES 360 TO 365 INCLUSIVE.

## General.

For convenience in use, three of these tables have been prepared, from which the safe loads of the various species can be obtained, either directly or by proportion as stated in the footnotes.

The values given in the tables are the safe loads in pounds uniformly distributed, including the weight of the beam itself, for rectangular beams one inch thick for spans from four to forty feet and for depths from four to twenty-four inches. The safe load for a beam of any thickness may be found by multiplying the values given in the tables by the thickness of the beam in inches.

The last column of each of the three Tables of Safe Loads for Rectangular Wooden Beams gives a coefficient of deflection, by means of which the deflection for any beam may be obtained, corresponding to the given span and safe load, by dividing the coefficient by the depth of the beam in inches, which will give approximately the deflection in inches under the given conditions.

In each table the deflection coefficient is given for one species of wood only as shown, but the deflections for other species may be obtained from these by proportion as explained hereafter.

For the reason that wood has no well-defined limit or modulus of elasticity the deflections obtained by the use of the coefficients are only approximate and will vary, dependent upon the moisture content of the wood and the character of the loading. The deflections thus obtained are therefore only useful as a general indication of the amount of bending to be expected under the given conditions and are not exact as in the case of materials like steel, which has a well-defined limit and modulus of elasticity.\*

The safe loads for other species of woods than those stated in the headings of the tables may be obtained from those given, by direct proportion, dependent upon the ratio of their allowable unit stress as compared with that for which the table is figured, as stated in the footnotes at the bottom of the tables.

\*Note.—"A series of tests, undertaken at the College of Forestry at Cornell University, seems to demonstrate that at least in coniferous wood, a definite elastic limit for any particular piece can be easily shown, and that it coincides with the theoretically calculated elastic limit upon the bases of compression tests and their application, according to Neely's formula."

# EXPLANATION OF THE TABLE OF SAFE LOADS FOR RECTANGULAR BEAMS OF WHITE PINE, CEDAR, SPRUCE AND EASTERN FIR.

The various species of woods the values for which are included in this table are calculated for an allowable fibre stress, for flexure, of 700 pounds per square inch.

The deflection coefficients are given for white pine, and are based upon a modulus of elasticity of 1 000 000 pounds per square inch.

The lower dotted line crossing the table indicates the limits of spans for which the deflection will exceed  $\frac{1}{360}$  of the span for the kind of wood for which the deflection coefficient is given. For spans below the line the safe loads given in the tables will produce a deflection greater than  $\frac{1}{360}$  of the span, while those above the line will produce less than this, which is the usual limit of deflection in order to prevent cracking of plastered ceilings. Similarly the upper dotted line indicates the limit of deflection for the kind of wood for which the deflection coefficient is given, corresponding to a modulus of elasticity of

500 000 pounds per square inch which should be considered in cases where the deflection should be more closely limited.

The coefficients of deflection for Cedar corresponding to moduli of 700 000 and 350 000 may be obtained by multiplying those of the table by  $\frac{10}{7}$  and  $\frac{20}{17}$  respectively, and for Spruce and Eastern Fir corresponding to moduli of 1 200 000 and 600 000 by multiplying those of the table by  $\frac{5}{6}$  and  $\frac{5}{3}$  respectively.

The upper full zig-zag line in the table gives the limits of the safe loads corresponding to the allowable shearing stress along the neutral axis of the beam. The safe loads above the line, which are based upon the extreme fibre strains, will produce shearing stresses along the axis or with the grain in excess of that allowable, which in the case of White Pine and the other woods of this table is 100 pounds per square inch.

The position of this line which indicates the limit of safe loads for shearing along the neutral axis was determined by the aid of the following formula:

$$W = \frac{4bds}{3}$$

in which

W = safe load in pounds uniformly distributed.

d = depth of beam in inches.

b = breadth of beam in inches.

s = allowable shear in the direction of the grain in pounds per square inch.

# EXPLANATION OF THE TABLE OF SAFE LOADS FOR RECTANGULAR BEAMS OF SHORT-LEAF YELLOW PINE.

The table is calculated for an allowable fibre stress, for flexure, of 1000 pounds per square inch.

The deflection coefficients are figured for a modulus of elasticity of 1 200 000 pounds per square inch, but may be used for other moduli, after obtaining the corresponding coefficients by proportion as heretofore explained.

The lower dotted line across the table indicates the limits of spans for which the safe load will produce deflections greater than  $\frac{1}{360}$  of the length of the beam. Values above the line will give less deflection than this, and those below will give greater, based on a modulus

of 1 200 000 pounds per square inch. Similarly the upper dotted line indicates the limit of deflection corresponding to a modulus of elasticity of 600 000 pounds per square inch.

The lower full zig-zag line across the table indicates the limiting spans and loads based on the allowable intensity of shearing stress along the neutral axis of the beam. The values above the lower full zig-zag line correspond to shearing stresses greater than the allowable stress in the direction of the grain for Short-leaf Yellow Pine, while those below the line correspond to shearing stresses less than that allowable, which in this case is assumed to be 100 pounds per square inch.

# EXPLANATION OF TABLES OF SAFE LOADS FOR RECTANGULAR BEAMS OF WHITE OAK AND LONG-LEAF YELLOW PINE.

This table is computed for an allowable fibre stress of 1 200 pounds per square inch, for flexure, and the deflection coefficients are calculated for a modulus of elasticity of 1 500 000 pounds per square inch.

The limit for a deflection of  $\frac{1}{3\,6\,0}$  of the span is indicated by the lower dotted zig-zag line on the tables, the values below which correspond to deflections greater than, and those above to deflections less than, the limiting deflections. The upper dotted zig-zag line similarly indicates the limits of deflection for a modulus of elasticity of 750 000 pounds per square inch.

The lower full zig-zag line indicates the limit of allowable shearing stress along the axis corresponding to the allowable intensity, for Yellow Pine, of 150 pounds per square inch.

Similarly the upper full zig-zag line indicates the limits for shearing along the axis for White Oak based on an allowable intensity of 200 pounds per square inch.

# BEARING AT POINTS OF SUPPORT.

Care should be taken in designing to provide sufficient bearing at the points of support so that the allowable intensity of compression across the grain as given in the tables on pages 357 and 359 is not exceeded.

This may be obtained where necessary by the use of corbels or bearing plates of harder wood so arranged as to give a large bearing area against the softer beam. The following statements are made in Bulletin No. 12, U. S. Department of Agriculture, Division of Forestry:

## RECOMMENDED PRACTICE.

"Since the strength of timber varies very greatly with the moisture contents (see Bulletin 8 of the Forestry Division), the economical designing of such structures will necessitate their being separated into groups according to the maximum moisture contents in use.

## MOISTURE CLASSIFICATION.

"Class A (moisture contents, 18 per cent.)—Structures freely exposed

to the weather, such as railway trestles, uncovered bridges, etc.

"Class B (moisture contents, 15 per cent.)—Structures under roof but without side shelter, freely exposed to outside air, but protected from rain, such as roof trusses of open shops and sheds, covered bridges over streams, etc.

"Class C (moisture contents, 12 per cent.)—Structures in buildings unheated, but more or less protected from outside air, such as roof

trusses of barns, enclosed shops and sheds, etc.

"Class D (moisture contents, 10 per cent.)—Structures in buildings at all times protected from the outside air, heated in the winter, such

as roof trusses in houses, halls, churches, etc.

"For long-leaf pine add to all the values given in the tables, except those for moduli of elasticity, tension and shearing, for Class B, 15 per cent.; for Class C, 40 per cent.; and for Class D, 55 per cent. For the other species add to these values, for Class B, 8 per cent.; for Class C, 18 per cent., and for Class D, 25 per cent."

Based upon the above classification of structures, the two following tables have been figured to facilitate calculations of allowable loads for wooden beams and columns.

PROPORTION OF THE VALUES GIVEN IN THE "TABLES OF SAFE LOADS FOR WOODEN BEAMS," PAGES 360
TO 365 INCLUSIVE, TO BE USED IN ORDER TO OBTAIN THE SAFE LOADS FOR THE VARIOUS CLASSES OF STRUCTURES REFERRED TO ABOVE.

Classes,	Yellow Pine.	All Others.
Class A Class B Class C Class D	1.15 1.40	1.00 1.08 1.18 1.25

SAFETY FACTORS TO BE APPLIED TO THE VALUES GIVEN IN THE TABLE OF "STRENGTH OF SOLID WOODEN COLUMNS," PAGES 366 AND 367, IN ORDER TO OBTAIN THE SAFE LOADS FOR THE VARIOUS CLASSES OF STRUCTURES REFERRED TO ABOVE.

Classes.	Yellow Pine.	All Others.
Class A Class B Class C Class D	0.23 0.28	0.20 0.22 0.24 0.25

# SPECIFIC GRAVITY AND WEIGHT PER FOOT FOR VARIOUS KINDS OF TIMBER.

Name of Wood.	Specific Gravity.	Weight per Cubic Foot.	Weight per Foot, Board Measure.
White Oak	0.80	49.94	4.16
	0.38	23.72	1.98
Pine  Douglas Fir Short-leaf Yellow Pine	0.61	38.08	3 17
	0.51	31.84	2.65
	0.51	31.84	2.65
Red Pine (Norway Pine) Spruce and Eastern Fir Hemlock	0.50	31.21	2.60
	0.40	24.97	2.08
	0.40	24.97	2.08
Cypress	0.46	28.72	2.39
	0.37	23.10	1.93
	0.66	41.20	3.43
California Redwood	0.39	24.16 24.97	2.01 2.08

The specific gravities and weights given above are the averages of a large number of determinations by various authorities, for woods containing less than 15 per cent. of moisture or such as are commercially known as dry timber. The weights of green or unseasoned woods will be from 20 to 40 per cent. greater than those given in the above table.

## SAFE UNIT STRESSES FOR TIMBER.

RECOMMENDED IN BULLETIN No. 12, U. S. DEPARTMENT OF AGRICULTURE.

## Division of Forestry.

Safe Unit Stresses at 18% Moisture.

Species.	Modulus of Strength at Rupture per Square Inch.	Modulus of Blasticity per Square Inch.	Elastic Resilience per Cubic Inch.	Grushing Strength End- wise per Square Inch.	Crushing Strength Across the Grain per Square Inch.	Tensile Strength per Square Inch.	Square Inch.
T : 1 C D: (D:		2000					
Long-leaf Pine (Pinus palustris) D Short-leaf Pine (Pinus	1550	720000	1.30	1000	215	12000	125
echinata) D	1300	600000	1.30	840	215	9000	100
White Pine (Pinus strobus)	880	435000	1.00	700	147	7000	75
Norway Pine (Pinus resinosa)	1090	566000		760	143		
Colorado Pine (Pinus ponderosa)	980	444000		630	180		
Douglas Fir (Pseudotsuga douglasii)	1320	690000		880	167		
Redwood (Sequoia sempervirens)	*1440			650	115		
Red Cedar (Juniperus virginiana)	1000	335000		700	250		
Bald Cypress (Taxodium	1000	999000		100	200		
distichum) D	1000	450000	1.10	675	120	6000	60
White Oak (Quercus alba) D	1200	550000	1.25	800	400	10000	200
Factor of Safety		2	1	5	3	1	4

The values marked "D" were obtained from experiments made by the Forestry Division. The other values were obtained from various sources, chiefly the 10th Census Report, but so modified as to give results comparable with Forestry Division values. To arrive at true average values of strength multiply safe loads by factor of safety given in each column. The values for resilience and tensile strength are the ultimate values. The former is practically never used in designing. The latter is a factor impossible to develop in practice, since the piece will always fail in some other way, usually by shearing.

The crushing strength across the grain in above is based upon a crushing of 3 per cent. of the cross sectional height of the piece.

<sup>\*</sup> This value is certainly too large.

<sup>† &</sup>quot; " small.—ED.

## AVERAGE ULTIMATE BREAKING UNIT

	Ten	sion.
Kind of Timber.	With Grain,	Across Grain.
White Oak . White Pine . Southern Long-leaf or Georgia Yellow Pine . Douglas Fir Short-leaf Yellow Pine . Red Pine (Norway Pine) . Spruce and Eastern Fir . Hemlock . Cypress . Cedar . Chestnut . California Redwood . California Spruce .	12000 7000 12000 8000 8000 8000 6000 6000 7000 8500 7000	2000 500 600 500 500 500

# AVERAGE SAFE ALLOWABLE WORKING UNIT

	Ten	sion.
Kind of Timber.	With Grain.	Across Grain,
Factor of Safety.	Ten.	Ten.
White Oak White Pine Southern Long-leaf or Georgia Yellow Pine Douglas Fir. Short-leaf Yellow Pine Red Pine (Norway Pine) Spruce and Eastern Fir Hemlock Cypress. Cedar Chestnut California Redwood. California Spruce	1200 700 1200 800 900 800 800 600 600 700 850 700	200 50 60 50 50 50

The above tables are based on those recommended by the committee on intendents of Bridges and Buildings at their Fifth Annual Convention in October, from various sources.

# STRESSES, IN POUNDS PER SQUARE INCH.

Co	mpression		Tran	sverse.	Shearing.	
With Grain.						
End Bearing.	Columns Under 15 Diams.	AcrossGrain.	Extreme Fibre Stress.	Modulus of Elasticity.	With Grain	Across Grain.
7000 5500 7000 5700 6000 5000 6000	5000 3500 5000 4500 4500 4000 4000 4000	2000 700 1400 800 1000 800 700 700 700 900 600	7000 4000 7000 5000 6000 5000 4000 5000 4000 5000 4500 5000	1500000 1000000 1500000 1400000 1200000 1200000 900000 700000 1000000 700000 1200000	800 400 600 500 400 400 350 400 600 400	4000 2000 5000 4000 3000 2500 1500 2000

# STRESSES, IN POUNDS PER SQUARE INCH.

Co	ompression	ı.	Tran	sverse.	Shearing.	
With Grain.		Across Grain.	Extreme Fibre	Modulus of	With	Across
End Bearing.	Columns Under 15 Diams.		Stress.	Elasticity.	Grain.	Grain.
Five.	Five.	Four.	Six.	Two.	Four.	Four.
1400 1100 1400 1100 1200 1000 1200	1000 700 1000 900 900 800 800 800 800 800 800 800	500 200 350 250 250 200 200 200 200 250 250 150	1200 700 1200 800 1000 800 700 600 800 700 800 750 800	750000 500000 750000 600000 565000 450000 450000 350000 350000 600000	200 100 150 130 100 100 100 100	1000 500 1250 1000 750 600 400 500

<sup>&</sup>quot;Strength of Bridge and Trestle Timbers" of the Association of Railway Super-1895, but the arrangement and values in many cases are now modified by later data

# SAFE LOAD IN POUNDS FOR RECTANGULAR OF WHITE PINE, CEDAR

Allowable fibre stress 700 pounds per square inch safety factor 6. Safe loads for other factors of safety may be obtained as follows:

Span			D	ept	h o	f Be	am	in In	iche	s.		Deflection Coefficient for White Pine.
Feet.	4	5	6	7	8	9	10	11	12	13	14	V
4	311	486			1244	1575	1944	2352	2800	3286	3811	.34
5	249	389	560		996		1556	1882	2240	2629	3049	.53
6	207	324	467		830	1050	1296	1569	1867	2191	2541	.76
7	178		400	544	711		1111	1344	1600	1878	2178	1.03
8	156			476	622	788	972		1400	1643	1906	1.34
9	138	216	311	423	553	700	864	1046	1244	1460	1694	1.70
10	124	194	280	381	498	630	778	941	1120	1314	1524	2.10
11	113	177	255	346	453	573	707	856	1018	1195	1386	2.54
12	103	162	233	318	415	525	648	784	933	1095	1270	3.02
13	96	150	215	293	383	485	598	724	862	1011	1173	3.55
14	89	139	200	272	356	450	556	672	800	939	1089	4.12
15	83	130	187	254	332	420	519	627	747	876	1016	4.73
16	78	122	175	238	311	394	486	588	700	821	953	5.38
17	73	114	165	224	293	371	458	554	659	773	897	6.07
18	69	108	156	212	277	350	432	523	622	730	847	6.80
19	65	102	147	201	262	332	409	495	589	692	802	7.58
20		97	140	191	249	315	389	471	560	657	762	8.40
21		93	133	182	237	300	370	448	533	626	726	9.26
22		88	127	173	226	286	354	428	509	597	693	10.16
23		85	122	166	216	274	338	409	487	572	663	11.11
24			117	159	207	263	324	392	467	548	635	12.10
25			112	152	199	252	311	376	448	526	610	13.13
26			108	147	191	242	299	362	431	506	586	14.20
27			104	141	184	233	288	349	415	487	565	15.31
28			100	136	178	225	278	336	400	469	544	16.46
29			97	131	172	217	268	325	386	453	526	17.66
30			93	127	166	210	259	314	373	438	508	18.90
31			90	123	161	203	251	304	361	424	492	20.18
32			88	119	156	197	243	294	350	411	476	21.50
33			85	115	151	191	236	285	339	398	462	22.87
34				112	146	185	229	277	329	387	448	24.28
35				109	142	180	222	269	320	376	436	25.73

# UNIFORMLY DISTRIBUTED BEAMS ONE INCH THICK AND SPRUCE OR EASTERN FIR.

Modulus of rupture 4 200 pounds per square inch.

New safe load = Safe load from table  $\times \frac{6}{\text{New factor}}$ 

9 19 10 17 11 16 12 14 13 13	750 601 458	2212 1991 1810 1659 1531	2498 2248   2044 1873 1729	2800 2520 2291 2100	3120 2808	<b>20</b> 3457	21	22	23	24	White Pine.
10 17 11 16 12 14 13 13	750 601 458 346	1991 1810 1659 1531	2248 2044 1873	2520 2291	2808						
11 16 12 14 13 13	601 458 346	1810 1659 1531	2044 1873	2291			3811	4183	4571	4978	1.70
11 16 12 14 13 13	601 458 346	1810 1659 1531	1873			3111	3430	3764	4114	4480	2.10
13 13	346	1531		2100	2552	2828	3118	3422	3740	4073	2.54
	- 1		1729	2100	2340	2593	2858	3137	3428	3733	3.02
14 12	250	1/00	- 1 4d U	1938	2160	2393	2638	2896	3165	3446	3.55
		1424	1606	1800	2056	2222	2450	2689	2939	3200	4.12
15 11	167	1328	1499	1680	1872	2074	2287	2510	2743	2987	4.73
16 10	094	1244	1405	1575	1755	1944	2144	2353	2571	2800	5.38
17 10	029	1171	1322	1482	1652	1830	2018	2214	2420	2635	6.07
18 9	972	1106	1249	1400	1560	1728	1906	2091	2286	2489	6.80
19 9	921	1048	1183	1326	1478	1637	1805	1981	2165	2358	7.58
20 8	875	996	1124	1260	1404	1556	1715	1882	2057	2240	8.40
21 8	833	948	1070	1200	1337	1481	1633	1793	1959	2133	9.26
22 7	795	905	1022	1145	1276	1414	1559	1711	1870	2036	10.16
	761	866	977	1096	1221	1353	1491	1637	1789	1948	11.11
24	729	830	937	1050	1170	1296	1429	1569	1714	1867	12.10
25 7	700		899	1008	1123	1244	1372	1506	1645	1792	13.13
26	673	766	865	969	1080	1197	1319	1448	1582	1723	14.20
27 6	648	737	833	933	1040	1152	1270	1394	1524	1659	15.31
28 6	625	711	803	900	1003	1111	1225	1344	1469	1600	16.46
29 6	603	687	775	869	968	1073	1183	1298	1419	1545	17.66
30   5	583	664	749	840	936	1037	1143	1255	1371	1493	18.90
31 5	565	642	725	813	906		1106	1214	1327	1445	20.18
32 5	547	622	703	787	877	972	1072	1176	1286	1400	21 50
33	534	603	681	764	850	943	1039	1141	1247	1358	22.87
34 5	515	586	661	741	826	915	1009	1107	1210	1318	24.28
35 5	500	569	642	720	802	889	980	1076	'	1280	25.73
	486	553	624	700	780	864	953	1046	1143		27.22
	473	538	608	681	759	841	927	1017	1112	1211	28.75
38 4	460	524	592	663	739	819	903	991	1083	1179	30.32
	449	511	576	646	720	798	880	965	1055	1149	31.94
40   4	438	498	562	630	702	778	858	941	1029	1120	33.60

# SAFE LOADS IN POUNDS FOR RECTANGULAR OF SHORT-LEAF

Allowable fibre stress 1000 pounds per square inch. Safety factor 6.

Safe loads for other safety factors may be obtained as follows:

Span			D	ept	h o	f Be	am	in Ir	che	s.		Deflection
in Feet.	4	5	6	7	8	9	10	11	12	13	14	Coefficient.
4	441	694	1000	1361	1778	2250	2778	3361	4000	4694	5444	.40
5	356	556	800	1089	1422	1800	2222	2689	3200	3756	4356	.63
6	296	463	667	907	1185	1500	1852	2241	2667	3130	3630	.90 .
7	254	397	571	778	1016	1286	1587	1921	2286	2683	3111	1.23
8	222	347	500	681	889	1125	1389	1681	2000	2347	2722	1.60
9	198	309	444	605	790	1000	1235	1494	1778	2086	2420	2.03
10	178	278	400	541	711	900	1111	1344	1600	1878	2178	2.50
11	162	253	364	495	646	818	1010	1222	1455	1707	1980	3.03
12	148	231	333	454	593	750		1120	1333	1565	1815	3.60
13	137	214	308	419	547	692	855	1034	1231	1444	1675	4.23
14	127	198	286	389	508	643	794	960	1143	1341	1556	4.90
15	119	185	267	363	474	600	741	896		1252	1452	5.63
16	111	174	250	340	411	563	694	840	1000	1174	1361	6.40
17	105	163	235	320	418	529	654	791	941	1105	1281	7.23
18	99	154	222	302	395	500	617	747	889	1043	1210	8.10
19	94	146	211	287	374	474	585	708	842	988	1146	9.03
20	89	139	200	272	356	450	556	672	800	939	1089	10.00
21	85	132	190	259	339	429	529	640	762	894	1037	11.03
22	81	126	182	247	323	409	505	611	727	854	990	12.10
23	77	121	174	237	309	391	483	585	696	816	947	13.23
24		116	162	227	296	375	463	. 560	667	782	907	14.40
25		111	160	218	284	360	411	538	640	751	871	15.63
26		107	154	209	274	346	427	517	615	722	838	16.90
27		103	148	202	263	333	412	498	593	695	807	18.23
28		99	143	194	254	321	397	480	571	671	778	19.60
29			138	188	245	310	383	464	552	648	751	21.03
30			133	181	237	300	370	448	533	626	726	22.50
31			129	176	229	290	358	434	516	606	703	24.03
32			125	170	222	281	347	420	500	587	681	25.60
33			121	165	215	273	337	407	485	569	660	27.23
34			118	160	209	265	327	395	471	552	641	28.90
35			114	156	203	257	317	384	457	537	602	30.63

Safe loads for any fibre stress may be readily obtained from this table by proportion.

# UNIFORMLY DISTRIBUTED, BEAMS ONE INCH THICK, YELLOW PINE.

Modulus of rupture 6 000 pounds per square inch. New safe load = Safe load from table  $\times \frac{6}{\text{New factor}}$ .

Span			Dep	th o	f Be	am i	n In	ches			Deflection
in Feet.	15	16	17	18	19	20	21	22	23	24	Coefficient.
9	2778	3160	3568	4000	4457	4938	5444	5975	6531	7111	2.03
10	2500	2844	3211	3600	4011	4444	4900	5378	5878	6400	2 50
11	2273	2586	2919	3273	3646	4040	4455	4889	5343	5818	3.03
12	2083	2370	2676	3000	3343	3704	4083	4481	4898	5333	3.60
13	1923	2188	2470	2769	3085	3419	3769	4137	4521	4923	4.23
14	1786	2032	2294	2571	2865	3175	3500	3841	4198	4571	4.90
15	1667	1896	2141	2400	2674	2963	3267	3585	3919	4267	5.63
16	1563	1778	2007	2250	2507	2778	3062	3361	3674	4000	6.40
17	1471	1673	1889	2118	2359	2614	2882	3163	3458	<b>3</b> 765	7.23
18	1389	1580	1789	200 <b>0</b>	2228	2469	2722	2988	3265	3556	8.10
19	1316	1497	1690	1895	2111	2339	2579	2830	3094	3368	9.03
20	1250	1422	1606	1800	2006	2222	2450	2689	2939	3200	10.00
21	1190	1354	1529	1714	1910	2116	2333	2561	2799	3048	11.03
22	1136	1293	1460	1636	1823	2020	2227	2444	2672	2909	12.10
23	1087	1237	1396	1565	1744	1932	2130	2338	2556	2783	13.23
24	1042	1185	1338	1500	1671	1852	2042	2241	2449	2667	14.40
25	1000	1138	1284	1440	1604	1778	1960	2131	2351	2560	15.63
26	962	1094	1235	1385	1543	1709	1885	2068	2261	2462	16.90
27	926	1053	1189	1333	1486	1646	1815	1992	2177	2370	18.23
28	893	1016	1147	1286	1433	1587	1750	1921	2099	2286	19.60
29	862	981	1107	1241	1383	1533	1690	1854	2027	2207	21.03
30	833	948	1070	1200	1337	1481	1633	1793	1959	2133	22.50
31	806	918	1036	1161	1294	1434	1581	1735	1896	2065	24.03
32	781	889	1003	1125	1253	1389	1531	1681	1837	2000	25.60
33	758	862	973	1091	1215	1347	1485	1630	1781	1939	27.23
34	735	837	944	1059	1180	1307	1441	1582	1728	1882	28.90
35	714	813	917	1029	1146	1270	1400	1537	1677	1829	30.63
36	694	780	894	1000	1114	1235	<b>1</b> 361	1494	1633	1778	32.40
37	676	769	868	973	1084	1201	1324	1453	1589	1730	34.23
38	658	749	845	947	1056	1169	1289	1415	1547	1684	36.10
39	641	729	823	923	1028	1140	1256	1379	1507	1641	38.03
40	625	711	803	900	1003	1111	1225	1344	1469	1600	40.00

Safe loads for beams of California Redwood, 3/4 of above.

# SAFE LOADS IN POUNDS FOR RECTANGULAR OF WHITE OAK AND

Allowable fibre stress 1 200 pounds per square inch. Safety factor 6.

Safe loads for other Safety factors may be obtained as follows:

Safe loads for beams of Douglas Fir, Red Pine (Norway Pine), Cypress, Chestnut and California Spruce, 3/3 of above.

# UNIFORMLY DISTRIBUTED, BEAMS ONE INCH THICK, LONG-LEAF YELLOW PINE.

Modulus of rupture 7 200 pounds per square inch.

New safe load = Safe load from table  $\times \frac{6}{\text{New factor}}$ 

Span in			Der	oth o	of Be	am i	n In	ches	֥		Deflection Coefficient.
Feet.	15	16	17	18	19	20	21	22	23	24	V
9	3333	3793	4281	4800	5348	5926	6533	7170	7837	8533	1.94
10	3000	3413	3853	4320	4813	5333	5880	6453	7053	7680	2.40
11	2727	3103	3503	3927	4376	4848	5355	5867	6412	6982	2.90
12	2500	2844	3211	3600	4011	4444	4900	5378	5878	6400	3.46
13	2308	2626	2964	3323	3703	4103	4523	4964	5426	5908	4.06
14	2143	2438	2752	3086	3438	3810	4200	4610	5038	5486	4.70
15	2000	2276	2569	2880	3209	3556	3920	4302	4702	5120	5.40
16	1875	2133	2408	2700	3008	3333	3675	4033	4433	4800	6.14
17	1765	2008	2267	2541	2831	3137	3459	3796	4149	4518	6.94
18	1667	1896	2141	2400	2674	2963	3267	3585	3819	4267	7.78
19	1579	1796	2027	2274	2533	2807	3095	3396	3712	4042	8.66
20	1500	1707	1927	2160	2407	2667	2940	3227	3527	3840	9.60
21	1429	<b>1</b> 625	1835	2057	2292	2540	2800	3073	<b>33</b> 59	3657	10.58
22	1364	1552	1752	1964	2188	2424	2678	2933	3206	3491	11.62
23	1304	1484	1675	1878	2093	2319	2557	2806	3067	3339	12.70
24	1250	1422	1606	1800	2006	2222	2450	2689	2939	3200	13.82
25	1200	1365	1541	1728	1925	2133	2352	2581	2821	3072	15.00
26	1154	1313	1482	1662	1851	2051	2262	2482	2713	2954	16.22
27	1111	1264	1427	1600	1783		2178	2390	2612	2844	17.50
28	1071	<b>1</b> 219	1376	1543	1719	1905		2305	2519	2743	18.82
29	1034	1177	1329	1490	1660	1839	2028	2225	2432	2648	20.18
30	1000	1138	1284	1440	1604	1778	1960	2151	2351	2560	21.60
31	968	1101	1243	1394	1553	1720	1897	2082		2477	23.06
32	938	1067	1204	1350	1504	1667	1838	2017	2217	2400	24.58
33	909	1034	1168	1309	1459	1616	1785	1956	2137	2327	26.14
34	882	1004	1133	1271	1416	1569	1729	1898	2075	2259	27.74
35	857	975	1101	1234	1375	1524	1680	1844	2013	2194	29.40
36	833	948	1070	1200	1337	1481	1633	1793	1909	2133	31.10
37	811	923	1041	1168	1301	1441	1589	1744	1906	2076	32.86
38	789	1	1014	1137	1267	1404	1547	1698	1856	2021	34.66
39	769		988	1108	1234	1368	1508	1655	1809	1969	36.50
40	750	853	963	1080	1203	1333	1470	1613	1763	1920	38.40

Safe loads for beams of Hemlock, 1/2 of above.

# STRENGTH OF SOLID WOODEN COLUMNS OF DIFFERENT KINDS OF TIMBER.

For various values of  $\frac{1}{d}$ .

l = length of column in inches. d = least diameter in inches.

BASED ON THE FORMULA OF THE U. S. DEPARTMENT OF AGRICULTURE, DIVISION OF FORESTRY.

$$P = F \times \frac{700 + 15c}{700 + 15c + c^2}.$$

P = ultimate strength in pounds per square inch.

F = ultimate crushing strength of timber.  $c = \frac{1}{d}$ .

Values of F are those given in table on pages 358 and 359 herein.

	Ultimate Strength in Pounds per Square Inch.								
	White Oak and Southern Long-leaf or Georgia Yellow Pine.	Douglas Fir and Short-leaf Yellow Pine.	Red Pine (Norway Pine), Spruce and Eastern Fir, Hemlock, Cy- press, Chestnut, Cal- ifornia Redwood and California Spruce.	White Pine and Cedar.					
F	5000	4500	4000	3500					
$\frac{1}{d}$									
2	4973	4475	3978	3481					
$egin{array}{c} 2 \ 3 \ 4 \end{array}$	4940	4446	3952	3458					
4	4897	4407	3918	3428					
5	4844	4359	3875	3391					
5 6	4782	4304	3826	3347					
7	4713	4242	3770	3299					
8	4638	4174	3710	3247					
9	4558	4102	3646	3190					
10	4474	4026	3579	3132					
11	4386	3948	3509	3070					
12	4297	3867	3438	3008					
13 14	4206 4114	3785	3365 3291	2944 2880					
14	4114	3703	9291	2000					
15	4022	3620	3217	2815					
16	3930	3537	3144	2751					
17	3838	3455	3071	2687					
18	3748	3373	2998	2624					
19	3659	3293	2927	2561					

For safety factors for various classes of structures to be used in connection with the above table, see p. 356.

# STRENGTH OF SOLID WOODEN COLUMNS OF DIFFERENT KINDS OF TIMBER.

For various values of  $\frac{1}{d}$ .

l = length of column in inches. d = least diameter in inches.

BASED ON THE FORMULA OF THE U. S. DEPARTMENT OF AGRICULTURE, DIVISION OF FORESTRY.

$$P = F \times \frac{700 + 15c}{700 + 15c + c^2}$$

P = ultimate strength in pounds per square inch.

F = ultimate crushing strength of timber.  $c = \frac{1}{d}$ 

Values of F are those given in table on pages 358 and 359 herein.

	Ultimate S	trength in P	ounds per Square	Inch.
	White Oak and Southern Long-leaf or Georgia Yellow Pine.	Douglas Fir and Short-leaf Yellow Pine.	Red Pine (Norway Pine), Spruce and Eastern Fir, Hemlock, Cy- press, Chestnut, Cal- ifornia Redwood and Galifornia Spruce.	White Pine and Cedar.
F	5000	4500	4000	3500
$\frac{1}{d}$				
20	3571	3214	2857	2500
21	3486	3137	2788	2440
22	3402	3061	2721	2381
23	3320	2988	2656	2324
24	3240	2916	2592	2268
25	3162	2846	2529	2213
26	3086	2777	2469	2160
27	3013	2711	2410	2109
28	2941	2647	2353	2059
29	2872	2585	2298	2010
30	2805	2524	2244	1963
32	2677	2409	2142	1874
34	2557	2301	2046	1790
36	2445	2200	1956	1711
38	2340	2106	1872	1638
40	2241	2017	1793	1569
42	2149	1934	1719	1505
44	2063	1857	1650	1444
46	1982	1784	1586	1388
48	1907	1716	1525	1335
50	1835	1652	1468	1285

For safety factors for various classes of structures to be used in connection with the above table, see p. 356.

The Basis for Specific Gravities is Pure Water at 62 Degrees Fah., Barometer 30 Inches. Weight of One Cubic Foot, 62.355 Pounds.	Average Specific Gravity. Water = 1.	Average Weight of One Cubic Foot. Pounds.
Air, atmospheric at 60 degrees F., under pressure of one atmosphere, or 14.7 pounds per square inch, weighs \$\frac{1}{815}\$th as much as water Aluminum.  Anthracite, 1.3 to 1.84; of Penna., 1.3 to 1.7.  broken, of any size, loose  moderately shaken  heaped bushel, loose, 77  to 83 pounds	.00123 2.6 1.5	.0765 162 93.5 52 to 56 56 to 60
" a ton loose occupies 40 to 43 cubic feet  Antimony, cast. " native.  Ash, perfectly dry (see note p. 371). " American White, dry (see note p. 371). Ashes of soft coal, solidly packed Asphaltum, 1 to 1.8  Brass (copper and zinc), cast, 7.8 to 8.4. " rolled  Brick, best pressed " common and hard. " soft inferior  Brickwork, pressed brick, fine joints. " medium quality. " coarse, inferior, soft. " at 125 pounds per cubic foot, 1 cubic yard equals 1.507 tons, and	6.70 6.67 .752 .61 1.4 8.1 8.4	418 416 47 38 40 to 45 87.3 504 524 150 125 100 140 125 100
17.92 cubic feet equal 1 ton  Bronze, copper 8, tin 1 (gun metal)  Cement, hydraulic. American, Rosendale, ground and loose  "hydraulic. American, Rosendale, U. S. struck bush., 70 pounds  hydraulic. American, Rosendale, Louisville bushel, 62 pounds  hydraulic. American, Cumberland, ground, loose  "hydraulic. American, Cumberland, ground, thoroughly shaken  hydraulic. English Portland (U.S. struck bushel, 100 to 128)	8.5	529 56 65 85 81 to 102

The Basis for Specific Gravities is Pure Water at 62 Degrees Fah., Barometer 30 Inches. Weight of One Cubic Foot, 62.355 Pounds.	Average Specific Gravity. Water = 1.	Average Weight of One Cubic Foot. Pounds.
Cement, hydraulic. English Portland, a barrel 400 to 430 pounds  "hydraulic. American Portland, loose "hydraulic. American Portland, thoroughly shaken  Charcoal of pines and oaks Chalk Cherry, perfectly dry (see note p. 371) Clay, potters', dry, 1.8 to 2.1  "dry in lump, loose.  Coal, bituminous, solid, 1.2 to 1.5.  "bituminous, solid, Cambria Co., Pa., 1.27-1.34  "bituminous, broken, of any size, loose "bituminous, moderately shaken "bituminous, a heaped bushel, loose, 70	2.5 .672 1.9 1.35	88  110 15 to 30 156 42 119 63 84  79 to 84 47 to 52 51 to 56
to 78	••••••	00.4.00
Coke, loose, good quality  "loose, a heaped bushel, 35 to 42  "1 ton occupies 80 to 97 cubic feet  Corundum, pure, 3.8 to 4  Copper, cast, 8.6 to 8.8  "rolled, 8.8 to 9  Corledge of the dry (see pate of 271)	3.9 8.7 8.9	23 to 32 
Cork, dry (see note p. 371)	.24	15
Earth, common loam, perfectly dry, loose		72 to 80
" perfectly dry, shaken		82 to 92
" perfectly dry, rammed.		90 to 100
" " slightly moist, loose		70 to 76
" more moist, loose		66 to 68
" " more moist, shaken		75 to 90
" more moist, packed		90 to 100
" as soft flowing mud		104 to 112
" as soft flowing mud		
well pressed  Elm, perfectly dry (see note p. 371)  Flint  Glass, 2.5 to 3.45	.56 2.6 2.98	110 to 120 35 162 186
" common window	2.52	157
Gneiss, common, 2.62 to 2.76	2.69	168

The Basis for Specific Gravities is Pure Water at 62 Degrees Fah., Barometer 30 Inches. Weight of One Cubic Foot, 62.355 Pounds.	Average Specific Gravity. Water = 1.	Average Weight of One Cubic Foot, Pounds.
Gneiss, in loose piles Gold, cast, pure or 24 karat.  "pure, hammered Granite, 2.56 to 2.88. Greenstone, trap, 2.8 to 3.22 Gypsum, plaster of Paris, 2.24 to 2.30 Hickory, perfectly dry (see note p. 371) Ice, .917 to .922 Iron, cast, 6.9 to 7.4  "grey foundry, cold. "molten  "wrought Lead, commercial Lignumvitæ (dry).	19.258 19.5 2.72 3.00 2.27 .85 .92 7.15 7.21 6.94 7.69 11.38 .65–1.33	96 1204 1217 170 187 141.6 53 57.4 446 450 433 480 709.6 41 to 83
Limestone and marbles Lime, quick  " quick, ground, well shaken, per struck	2.6 1.5	164.4 95
bushel 80 pounds	.71 .85 .56	75 44 53 35
Maple, dry (see note p. 371)	.79	49 165
ble, about $\frac{1}{5}$ of mass will be mortar of granite, well-scabbled dry rubble of granite, roughly scabbled mortar rubble, about $\frac{1}{4}$ to $\frac{1}{3}$ of mass		154 138
will be mortar  of granite, scabbled dry rubble  f sandstone, ½ less than granite		150 125
Masonry of brickwork (see Brickwork).  Mercury, at 32 degrees Fah  Mica, 2.75 to 3.1  Mortar, hardened, 1.4 to 1.9  Mud, dry, close  wet, moderately pressed  fluid		849 183 103 80 to 110 110 to 130 104 to 120

The Basis for Specific Gravities is Pure Water at 62 Degrees Fah., Barometer 30 Inches, Weight of One Cubic Foot, 62,355 Pounds,	Average Specific Gravity, Water = 1.	Average Weight of One Cubic Foot. Pounds.
Oak, live, perfectly dry, .88–1.02 (see note p. 371)  "Red, Black, perfectly dry Petroleum Pitch Poplar, dry (see note below) Platinum Quartz Rosin Salt, coarse, (per struck bushel, Syracuse,	.95 .878 1.15 .47 21.5 2.65 1.10	59.3 32 to 45 54.8 71.7 29 1342 165 68.6
N. Y., 56 pounds)		45 90 to 106 118 to 129
Sandstone, 2.1 to 2.73, 131 to 171	2.41	117 151
solid makes 13/4 (about) piled.  Snow, fresh fallen  "moistened, compacted by rain.  Sycamore, perfectly dry (see note below).  Shales, red or black, 2.4 to 2.8.  Silver.  Slate, 2.7 to 2.9.  Soapstone, 2.65 to 2.8.  Steel  Sulphur  Tallow.  Tar.  Tin, cast, 7.2 to 7.5.  Walnut, Black, perfectly dry (see note below).  Water, pure rain, distilled, at 32 degrees F.,	.59 2.6 10.5 2.8 2.73 7.85 2.00 .94 1 7.35 .61	86 5 to 12 15 to 50 37 162 655 175 170 490 125 58.6 62.355 459 38
Bar. 30 inches. " " at 62 degrees F.,		62.417
Bar. 30 inches. at 212 degrees F.,	1	62.355
Bar. 30 inches  sea, 1.026 to 1.030  Zinc or spelter, 6.8 to 7.2	1.028	59.7 64.08 437.5

Note.—Green timbers usually weigh from one-fifth to nearly one-half more than dry; ordinary building timbers, tolerably seasoned, one-sixth more.

For Specific Gravities of woods not given in this table, see page 356.

## STANDARD DECIMAL GAUGE.

			Weight	Carrons Toot	
Standard	Thickness in	Approximate	Weight per Square Foot in Pounds, Avoirdupois.		
Decimal Gauge	Fractions	Thickness	IRON.	STEEL.	
in Inches.	of an Inch.	in Millimetres.	Basis—480	Basis—489.6	
III THOROS,	of all thon.	III MITTINO (1 OS)	Pounds per Cubic Foot.	Pounds per Cubic Foot.	
000	1 500	05080010	00	0016	
.002	1-500 1-250	.05080010 .10160020	.08	.0816 .1632	
.004	3-500	.15240030	.24	.2448	
.008	1-125	.20320041	.32	.3264	
.010	1-100	.25400051	.40	.4080	
.012	3-250	.30480061	.48	.4896	
.014	7-500	.35560071	.56	.5712	
.016	$2-125(\frac{1}{64}+)$	.40640081	.64	.6528	
.018	9-500	.45720091	.72	.7344	
.020	1-50	.50800102	.80	.8160	
.022	11-500	.55880112	.88	.8976	
.025	1-40	.63500127	1.00	1.0200	
.028	7-250	.71120142	1.12	1.1424	
.032	$4-125(\frac{1}{32}+)$	.81280163	1.28	1.3056	
.036	9-250	.91440183	1.44	1.4688	
.040	1-25	1.01600203	1.60	1.6320	
.045	9-200	1.14300229	1.80	1.8360	
.050	1-20	1.27000254	2.00	2.0400	
.055	11-200	1.39700280	2.20	2.2440	
.060	3-50 (16-)	1.52400305 1.65100330	2.40	2.4480	
.065	13-200	1.77800356	2.60 2.80	2.6520 2.8560	
.070	7-100 3-40	1.90500381	3.00	3.0600	
.075	2-25	2.03200406	3.20	3.2640	
.085	17-200	2.15900432	3.40	3.4680	
.090	9-100	2.28600457	3.60	3.6720	
.095	19-200	2.41300483	3.80	3.8760	
.100	1-10	2.54000508	4.00	4.0800	
.110	11-100	2.79400559	4.40	4.4880	
.125	1-8	3.17500630	5.00	5.1000	
.135	27-200	3.42900686	5.40	5.5080	
.150	3-20	3.81000762	6.00	6.1200	
.165	33-200	4.19100838	6.60	6.7320	
.180	9-50	4.57200914	7.20	7.3440	
.200	1-5	5.08001016	8.00	8.1600	
.220	11-50	5.58801118	8.80	8.9760	
.240	6-25	6.09601219	9.60	9.7920	
.250	1-4	6.35001270	10.00	10.2000	

The Standard Decimal Gauge has been recently adopted by the Association of American Steel Manufacturers, the American Railway Master Mechanics' Association and by about seventy-two of the principal railroads of the United States, Canada and Mexico. The decimal system of gauging was recommended by the American Institute of Mining Engineers in 1877 and by the American Society of Mechanical Engineers in 1895.

# WIRE AND SHEET METAL GAUGES. In Decimals of an Inch.

		A12 27	CCIMICIA OI				
Number of Gauge.	Birm- ingham or Stubs Iron Wire Gauge.	American or Brown & Sharpe Wire Gauge.	United States Standard Gauge for Sheet and Plate Iron and Steel.	Washburn & Moen Manu- facturing Co. and John A. Roebling's Sons Co. Wire Gauge.	Trenton fron Co. Wire Gauge.	American Screw Co. Screw Wire Gauge.	British Imperial or English Legal Standard Wire Gauge.
0000000 000000 00000 0000 0000 000 000	258 22303 1655 1209 1658 1209 1658 1209 1658 1209 1658 1209 1658 1209 1658 1658 1658 1658 1658 1658 1658 1658		.5 .46875 .4375 .40625 .375 .34375 .3125 .28125 .265625 .234375 .21875 .203125 .1875 .171875 .171875 .171875 .171875 .170625 .109375 .078125 .078125 .05625 .05625 .05625 .05125 .021875 .0171875 .0171875 .0171875 .0171875 .0171875 .0171875 .0171875 .0171875 .0171875 .01875 .0193				.500 .464 .432 .400 .372 .348 .300 .276 .252 .212 .176 .144 .128 .116 .080 .072 .040 .040 .040 .022 .022 .0164 .0146 .0146 .0146 .0124 .0166 .01

The United States Standard Gauge was legalized by Act of Congress March 3, 1893, as a standard gauge for sheet and plate iron and steel and is used by the Custom House Department and by about forty-five sheet and tin-plate manufacturers.

# WEIGHTS OF SHEETS AND PLATES OF STEEL, WROUGHT IRON, COPPER AND BRASS.

AMERICAN OR BROWNE & SHARPE GAUGE.

No.	Thickness		Weight per Square Foot.					
of	in	041	D					
Gauge.	Inches.	Steel.	Iron.	Copper.	Brass.			
0000	.460000	18.7680	18.4000	20.8380	19.6880			
	.409642	16.7134	16.3857	18.5568	17.5327			
	.364796	14.8837	14.5918	16.5253	15.6133			
0	.324861	13.2543	12.9944	14.7162	13.9041			
1	.289297	11.8033	11.5719	13.1052	12.3819			
2	.257627	10.5112	10.3051	11.6705	11.0264			
3	.229423	9.3605	9.1769	10.3929	9.8193			
4	.204307	8.3357	8.1723	9.2551	8.7443			
5	.181940	7.4232	7.2776	8.2419	7.7870			
6	.162023	6.6105	6.4809	7.3396	6.9346			
7	.144285	5.8868	5.7714	6.5361	6.1754			
8	.128490	5.2424	5.1396	5.8206	5.4994			
9	.114423	4.6685	4.5769	5.1834	4.8973			
10	.101897	4.1574	4.0759	4.6159	4.3612			
11	.090742	3.7023	3.6297	4.1106	3.8838			
12	.080808	3.2970	3.2323	3.6606	3.4586			
13	.071962	2.9360	2.8785	3.2599	3.0800			
14	.064084	2.6146	2.5634	2.9030	2.7428			
15	.057068	2.3284	2.2827	2.5852	2.4425			
16	.050821	2.0735	2.0328	2.3022	2.1751			
17	.045257	1.8465	1.8103	2.0501	1.9370			
18	.040303	1.6444	1.6121	1.8257	1.7250			
19	.035890	1.4643	1.4356	1.6258	1.5361			
20	.031961	1.3040	1.2784	1.4478	1.3679			
21	.028462	1.1612	1.1385	1.2893	1.2182			
22	.025346	1.0341	1.0138	1.1482	1.0848			
23	.022572	.92094	.90288	1.0225	.96608			
24	.020101	.82012	.80404	.91058	.86032			
25	.017900	.73032	.71600	.81087	.76612			
26	.015941	.65039	.63764	.72213	.68227			
27	.014195	.57916	.56780	.64303	.60755			
28	.012641	.51575	.50564	.57264	.54103			
29	.011257	.45929	.45028	.50994	.48180			
30	.010025	.40902	.40100	.45413	.42907			
31	.008928	.36426	.35712	.40444	.38212			
32	.007950	.32436	.31800	.36014	.34026			
33	.007080	.28886	.28320	.32072	.30302			
34	.006305	.25724	.25220	.28562	.26985			
35	.005615	.22909	.22460	.25436	.24032			
36	.005000	.20400	.20000	.22650	.21400			
37	.004453	.18168	.17812	.20172	.19059			
38	.003965	.16177	.15860	.17961	.16970			
39	.003531	.14406	.14124	.15995	.15113			
40	.003144	12828	.12576	.14242	.13456			

For weights of steel plates  $\frac{1}{18}''$  and over in thickness, see " Table of Weights of Flat Rolled Bars," pages 395 to 404.

# WEIGHTS OF SHEETS AND PLATES OF STEEL, WROUGHT IRON, COPPER AND BRASS.

BIRMINGHAM GAUGE.

No		Thickness	Weight per Square Foot.					
of Gaug	1	in Inches.	Steel.	Iron.	Copper.	Brass.		
000		.454 .425 .380	18.5232 17.3400 15.5040	18.16 17.00 15.20	20.5662 19.2525 17.2140	19.4312 18.1900 16.2640		
	0	.340	13.8720	13.60	15.4020	14.5520		
	1	.300	12.2400	12.00	13.5900	12.8400		
	2	.284	11.5872	11.36	12.8652	12.1552		
	3	.259	10.5672	10.36	11.7327	11.0852		
	4	.238	9.7104	9.52	10.7814	10.1864		
	5	.220	8.9760	8.80	9.966	9.4160		
	6	.203	8.2824	8.12	9.1959	8.6884		
	7	.180	7.3440	7.20	8.1540	7.7040		
	8	.165	6.7320	6.60	7.4745	7.0620		
	9	.148	6.0384	5.92	6.7044	6.3344		
1	0 1 2 3 4	.134 .120 .109 .095 .083	5.4672 4.8960 4.4472 3.8760 3.3864	5.36 4.80 4.36 3.80 3.32	6.0702 5.4360 4.9377 4.3035 3.7599	5.7352 5.1360 4.6652 4.0660 3.5524		
1 1 1	56789	.072 .065 .058 .049 .042	2.9376 2.6520 2.3664 1.9992 1.7136	2.88 2.60 2.32 1.96 1.68	3.2616 2.9445 2.6274 2.2197 1.9026	3.0816 2.7820 2.4824 2.0972 1.7976		
2,02,02	20 22 23 24	.035 .032 .028 .025 .022	1.4280 1.3056 1.1424 1.0200 .8976	1.40 1.28 1.12 1.00 .88	1.5855 1.4496 1.2684 1.1325 .9966	1.4980 1.3696 1.1984 1.0700 .9416		
2	25	.020	.8160	.80	.9060	.8560		
	26	.018	.7344	.72	.8154	.7704		
	27	.016	.6528	.64	.7248	.6848		
	28	.014	.5712	.56	.6342	.5992		
	29	.013	.5304	.52	.5889	.5564		
8	30	.012	.4896	.48	.5436	.5136		
	31	.010	.4080	.40	.4530	.4280		
	32	.009	.3672	.36	.4077	.3852		
	33	.008	.3264	32	.3624	.3424		
	34	.007	.2856	.28	.3171	.2996		
	35	.005	.2040	.20	.2265	.2140		
	36	.004	.1632	.16	.1812	.1712		
Specific Gravities		7.85	7.70	8.72	8.24			
		489.6	480.0	543.6	513.6			
		.2833	.2778	.3146	.2972			

# DECIMALS OF A FOOT FOR EACH 1 OF AN INCH.

Inch.	0"	1"	2"	3"	4′′	5"
0	0	.0833	.1667	.2500	.3333	.4167
1 64 3 2 3 64 11	.0013 .0026 .0039 .0052	.0846 .0859 .0872 .0885	.1680 .1693 .1706 .1719	.2513 .2526 .2539 .2552	.3346 .3359 .3372 .3385	.4180 .4193 .4206 .4219
$\begin{array}{c} \frac{5}{64} \\ \frac{3}{32} \\ \frac{7}{64} \\ \frac{1}{8} \end{array}$	.0065 .0078 .0091 .0104	.0898 .0911 .0924 .0937	.1732 .1745 .1758 .1771	.2565 .2578 .2591 .2604	.3398 .3411 .3424 .3437	.4232 .4245 .4258 .4271
$ \begin{array}{r} 9 \\ 64 \\ 5 \\ 32 \\ 114 \\ 63 \\ 16 \end{array} $	.0117 .0130 .0143 .0156	.0951 .0964 .0977 .0990	.1784 .1797 .1810 .1823	.2617 .2630 .2643 .2656	.3451 .3464 .3477 .3490	.4284 .4297 .4310 .4323
$\begin{array}{c} \frac{1}{6}\frac{3}{4} \\ \frac{7}{3}\frac{2}{1}\frac{5}{6}\frac{4}{1} \\ \frac{1}{4} \end{array}$	.0169 .0182 .0195 .0208	.1003 .1016 .1029 .1042	.1836 .1849 .1862 .1875	.2669 .2682 .2695 .2708	.3503 .3516 .3529 .3542	.4336 .4349 .4362 .4375
164 9 3194 65 16	.0221 .0234 .0247 .0260	.1055 .1068 .1081 .1094	.1888 .1901 .1914 .1927	.2721 .2734 .2747 .2760	.3555 .3568 .3581 .3594	.4388 .4401 .4414 .4427
2.6 ± 1.23.0 4 3 80	.0273 .0286 .0299 .0312	.1107 .1120 .1133 .1146	.1940 .1953 .1966 .1979	.2773 .2786 .2799 .2812	.3607 .3620 .3633 .3646	.4440 .4453 .4466 .4479
25/43/227/4 1/3 24/5 7/1	.0326 .0339 .0352 .0365	.1159 .1172 .1185 .1198	.1992 .2005 .2018 .2031	.2826 .2839 .2852 .2865	.3659 .3672 .3685 .3698	.4492 .4505 .4518 .4531
26133614 12	.0378 .0391 .0404 .0417	.1211 .1224 .1237 .1250	.2044 .2057 .2070 .2083	.2878 .2891 .2904 .2917	.3711 .3724 .3737 .3750	.4544 .4557 .4570 .4583

## DECIMALS OF A FOOT FOR EACH <sup>1</sup>/<sub>64</sub> OF AN INCH.

Inch.	6"	ייקי	8"	9"	10"	11"
0	.5000	.5833	.6667	.7500	.8333	.9167
$\begin{array}{c} \frac{1}{64} \\ \frac{1}{32} \end{array}$	.5013 .5026	.5846 .5859	.6680 .6693	.7513 .7526	.8346 .8359	.9180 .9193
$ \begin{array}{r} 3^{2} \\ \overline{64} \\ \underline{1} \\ \overline{16} \end{array} $	.5039 .5052	.5872 .5885	.6706 .6719	.7539 .7552	.8372 .8385	.9206 .9219
$   \begin{array}{r}     5 \\     \hline     6 4 \\     \hline     3 2 \\     \hline     7 \\     \hline     6 4   \end{array} $	.5065 .5078	.5898 .5911	.6732 .6745	.7565 .7578	.8398 .8411	.9232 .9245
64 1 8	.5091 .5104	.5924 .5937	.6758 .6771	.7591 .7604	.8424 .8437	.9258 .9271
$\frac{9}{64}$ $\frac{5}{32}$	.5117 .5130	.5951 .5964	.6784 .6797	.7617 .7630	.8451 .8464	.9284 .9297
5 3 1 1 6 3 1 6	.5143 .5156	.5977 .5990	.6810 .6823	.7643 .7656	.8477 .8490	.9310 .9323
134 72 154 61	.5169 .5182	.6003 .6016	.6836 .6849	.7669 .7682	.8503 .8516	.9336 .9349
64 1 4	.5195 .5208	.6029 .6042	.6862 .6875	.7695 .7708	.8529 .8542	.9362 .9375
174 929 3165 165	.5221 .5234	.6055 .6068	.6888 .6901	.7721 .7734	.8555 .8568	.9388 .9401
$\begin{array}{c} \frac{1}{6}\frac{3}{4} \\ \frac{5}{16} \end{array}$	.5247 .5260	.6081 .6094	.6914 .6927	.7747 .7760	.8581 .8594	.9414 .9427
21 141 13234 263 38	.5273 .5286	.6107 .6120	.6940 .6953	.7773 .7786	.8607 .8620	.9440 .9453
	.5299 .5312	.6133 .6146	.6966 .6979	.7799 .7812	.8633 .8646	.9466 .9479
25 643 1327 7 6 7 16	.5326	.6159 .6172	.6992 .7005	.7826 .7839	.8659 .8672	.9492 .9505
	.5352 .5365	.6185 .6198	.7018 .7031	.7852 .7865	.8685 .8698	.9518 .9531
294 135 231 314	.5378	.6211	.7044	.7878 .7891	.8711 .8724	.9544 .9557
$\frac{\vec{6}\cdot\vec{4}}{2}$	.5404 .5417	.6237 .6250	.7070 .7083	.7904 .7917	.8737 .8750	.9570 .9583

## DECIMALS OF A FOOT FOR EACH 1 OF AN INCH.

Inch.	0"	1"	2′′	3′′	4′′	5"
3/47/245/44 3/61/33/69/16	.0430 .0443 .0456 .0469	.1263 .1276 .1289 .1302	.2096 .2109 .2122 .2135	.2930 .2943 .2956 .2969	.3763 .3776 .3789 .3802	.4596 .4609 .4622 .4635
36192944 193865	.0482 .0495 .0508 .0521	.1315 .1328 .1341 .1354	.2148 .2161 .2174 .2188	.2982 .2995 .3008 .3021	.3815 .3828 .3841 .3854	.4648 .4661 .4674 .4688
4\6\1\2\3\4\1\6 2\3\4\6\1\1	.0534 .0547 .0560 .0573	.1367 .1380 .1393 .1406	.2201 .2214 .2227 .2240	.3034 .3047 .3060 .3073	.3867 .3880 .3893 .3906	.4701 .4714 .4727 .4740
4623274 34634634	.0586 .0599 .0612 .0625	.1419 .1432 .1445 .1458	.2253 .2266 .2279 .2292	.3086 .3099 .3112 .3125	.3919 .3932 .3945 .3958	.4753 .4766 .4779 .4792
4623561436	.0638 .0651 .0664 .0677	.1471 .1484 .1497 .1510	.2305 .2318 .2331 .2344	.3138 .3151 .3164 .3177	.3971 .3984 .3997 .4010	.4805 .4818 .4831 .4844
562356 <sup>7</sup> 8	.0690 .0703 .0716 .0729	.1523 .1536 .1549 .1562	.2357 .2370 .2383 .2396	.3190 .3203 .3216 .3229	.4023 .4036 .4049 .4062	.4857 .4870 .4883 .4896
5/62/95/64/5/6	.0742 .0755 .0768 .0781	.1576 .1589 .1602 .1615	.2409 .2422 .2435 .2448	.3242 .3255 .3268 .3281	.4076 .4089 .4102 .4115	.4909 .4922 .4935 .4948
614 123 234 1	.0794 .0807 .0820	.1628 .1641 .1654	.2461 .2474 .2487	.3294 .3307 .3320	.4128 .4141 .4154	.4961 .4974 .4987

## DECIMALS OF A FOOT FOR EACH 1/64 OF AN INCH.

Inch.	6"	7"	8"	9″	10"	11"
33447 15554 9 16	.5430 .5443 .5456 .5469	.6263 .6276 .6289 .6302	.7096 .7109 .7122 .7135	.7930 .7943 .7956 .7969	.8763 .8776 .8789 .8802	.9596 .9609 .9622 .9635
가(45)임조(4'5)80 양61 838(6'5)80	.5482 .5495 .5508 .5521	.6315 .6328 .6341 .6354	.7148 .7161 .7174 .7188	.7982 .7995 .8008 .8021	.8815 .8828 .8841 .8854	.9648 .9661 .9674 .9688
1.4-1-24-3.4-1-6 2-3-4-6-1-1-6	.5534 .5547 .5560 .5573	.6367 .6380 .6393 .6406	.7201 .7214 .7227 .7240	.8034 .8047 .8060 .8073	.8867 .8880 .8893 .8906	.9701 .9714 .9727 .9740
45432474 22346 34	.5586 .5599 .5612 .5625	.6419 .6432 .6445 .6458	.7253 .7266 .7279 .7292	.8086 .8099 .8112 .8125	.8919 .8932 .8945 .8958	.9753 .9766 .9779 .9792
99455214436 2555611436	.5638 .5651 .5664 .5677	.6471 .6484 .6497 .6510	.7305 .7318 .7331 .7344	.8138 .8151 .8164 .8177	.8971 .8984 .8997 .9010	.9805 .9818 .9831 .9844
5]47;215]47 5(6 2)35(6 7.8	.5690 .5703 .5716 .5729	.6523 .6536 .6549 .6562	.7357 .7370 .7383 .7396	.8190 .8203 .8216 .8229	.9023 .9036 .9049 .9062	.9857 .9870 .9883 .9896
5 62 329 45 6  5 62 35 61 1	.5742 .5755 .5768 .5781	.6576 .6589 .6602 .6615	.7409 .7422 .7435 .7448	.8242 .8255 .8268 .8281	.9076 .9089 .9102 .9115	.9909 .9922 .9935 .9948
663333666 1	.5794 .5807 .5820	.6628 .6641 .6654	.7461 .7474 .7487	.8294 .8307 .8320	.9128 .9141 .9154	.9961 .9974 .9987 1.0000

### DECIMALS OF AN INCH FOR EACH $^1_{64}$ th.

$\frac{1}{32}$ ds.	$\frac{1}{64}$ ths.	Decimal.	Frac-	$\frac{1}{32}$ ds.	$\frac{1}{64}$ ths.	Decimal.	Frac-
1	1 2 3	.015625 .03125 .046875		17	33 34 35	.515625 .53125 .546875	
2	4	.0625	1-16	18	36	.5625	9-16
3	5 6 7	.078125 .09375 .109375		19	37 38 39	.578125 .59375 .609375	
4	8	.125	1-8	20	40	.625	5-8
5	9 10 11	.140625 .15625 .171875		21	41 42 43	.640625 .65625 .671875	
6	12	.1875	3–16	22	44	.6875	11-16
7	13 14 15	.203125 .21875 .234375		23	45 46 47	.703125 .71875 .734375	
8	16	.25	1-4	24	48	.75	3-4
9	17 18 19 20	.265625 .28125 .296875 .3125	5-16	25 26	49 50 51 52	.765625 .78125 .796875 .8125	13-16
	91	000105	- 0			000105	
11	21 22 23	.328125 .34375 .359375		27	53 54 55	.828125 .84375 .859375	
12	24	.375	3-8	28	56	.875	7-8
13	25 26 27	.390625 .40625 .421875		29	57 58 59	.890625 .90625 .921875	
14	28	.4375	7-16	30	60	.9375	15-16
15	29 30 31	.453125 .46875 .484375		31	61 62 63	.953125 .96875 .984375	
16	32	.5	1-2	32	64	1.	1

### WEIGHTS AND AREAS OF SQUARE AND ROUND BARS AND CIRCUMFER-ENCES OF ROUND BARS.

One cubic foot of steel weighs 489.6 lbs.

Thickness	Weight of	Weight of	Area of	Area of	Circumference
or Diameter	□ Bar	O Bar	☐ Bar	O Bar	of O Bar
in Inches.	One Foot Long.	One Foot Long.	in Sq. Inches.	in Sq. Inches.	in Inches.
	020 2000 2005.	020 2000 2029.			
$\begin{array}{c} \frac{1}{16} \\ \frac{5}{64} \\ \frac{3}{22} \\ \frac{7}{64} \end{array}$	.013	.010	.0039	.0031	.1963
64	.021	.016	.0061	.0048	.2454
$3\frac{3}{7}$	.030	.023	.0088	.0069	.2945
6'4	.041	.032	.0120	.0094	.3436
1	.053	.042	.0156	.0123	.3927
8	.067	.053	.0198	.0155	.4418
6 4 5	.083	.065	.0244	.0192	.4909
$\begin{array}{c} \frac{1}{8} \\ 9 \\ 64 \\ 5 \\ 32 \\ \frac{1}{64} \end{array}$	.100	.079	.0295	.0232	.5400
0.1					
3 1634 72 254	.120	.094	.0352	.0276	.5890
$\frac{1}{6}\frac{3}{4}$	.140	.110	.0413	.0324	.6381
3/2	.163	.128	.0479	.0376	.6872
$\frac{1}{6}\frac{3}{4}$	.187	.147	.0549	.0431	.7363
1	.213	.167	.0625	.0491	.7854
4 17	.240	.188	.0706	.0554	.8345
6 4 9 3 3	.269	.211	.0791	.0621	.8836
$     \begin{array}{r}             \frac{1}{4} \\             1 \\             7 \\           $	.300	.235	.0881	.0692	.9327
5 1244 2614 1223 2634	.332	.261	.0977	.0767	.9817
$\frac{21}{64}$	.366	.288	.1077	.0846	1.0308
$\frac{1}{3}\frac{1}{2}$	.402	.316	.1182	.0928	1.0799
64	.439	.345	.1292	.1014	1.1290
<u>3</u>	.478	.376	.1406	.1104	1.1781
2 <sup>8</sup> 5	.519	.407	.1526	.1198	1.2272
$\frac{1}{2}\frac{3}{2}$	.561	.441	.1650	.1296	1.2763
3) 2 61 3 217 4 3 216 4 3 217 4	.605	.475	.1780	.1398	1.3254
$\begin{array}{c} 7 \\ 16 \\ 29 \\ 44 \\ 15 \\ \hline 32 \\ 36 \\ 4 \end{array}$	.651	.511	.1914	.1503	1.3744
<u>29</u> 64	.698	.548	.2053	.1613	1.4235
3 2 3 1	.747	.587	.2197	.1726	1.4726
64	.798	.627	.2346	.1843	1.5217
1 3	.850	.668	.2500	.1963	1.5708
3 3 6 4	.904	.710	.2659	.2088	1.6199
1 2 3 6 1 3 6 1 3 6 1	.960	.754	.2822	.2217	1.6690
$\frac{35}{64}$	1.017	.799	.2991	.2349	1.7181

Thickness	Weight of	Weight of	Area of	Area of	Circumference
or Diameter	□ Bar	○ Bar	□ Bar	O Bar	of O Bar
in Inches.	One Foot Long.	One Foot Long.	in Sq. Inches.	in Sq. Inches.	in Inches.
9 607-1400019-014 9 1-000-1-0009-0-1-0009-0-1-00-1-00-1-00	1.076 1.136 1.199 1.263	.845 .893 .941 .992	.3164 .3342 .3525 .3713	.2485 .2625 .2769 .2916	1.7671 1.8162 1.8653 1.9144
5/8 1/4 1/23/8/4 6 0/93/4/6	1.328 1.395 1.464 1.535	1.043 1.106 1.150 1.205	.3906 .4104 .4307 .4514	.3068 .3252 .3382 .3545	1.9635 2.0126 2.0617 2.1108
1-1-4-6-0-4-0-0-2-7-1-4-1-6-0-2-1-1-4-6-0-2-1-1-4-6-0-2-1-1-4-6-0-2-1-1-4-6-0-2-1-1-4-6-0-2-1-1-4-6-0-2-1-1-4-6-0-2-1-1-4-6-0-2-1-1-4-6-0-2-1-1-4-6-0-2-1-1-4-6-0-2-1-1-4-6-0-2-1-1-4-6-0-2-1-4-6-0-2-1-4-6-0-2-1-1-4-6-0-2-1-1-4-6-0-2-1-1-4-6-0-2-1-1-4-6-0-2-1-1-4-6-0-2-1-1-4-6-0-2-1-1-4-6-0-2-1-1-4-6-0-2-1-4-6-0-2-1-1-4-6-0-2-1-1-4-6-0-2-1-1-4-6-0-2-1-1-4-6-0-2-1-1-4-6-0-2-1-1-4-6-0-2-1-1-4-6-0-2-1-1-4-6-0-2-0-2-1-4-6-0-2-0-2-1-4-6-0-2-0-2-1-4-6-0-2-0-2-1-4-6-0-2-0-	1.607 1.681 1.756 1.834	1.262 1.320 1.379 1.440	.4727 .4944 .5166 .5393	.3712 .3883 .4057 .4236	2.1598 2.2089 2.2580 2.3071
34 34 5 1 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	1.913 2.245 2.603 2.989	1.502 1.763 2.044 2.347	.5625 .6602 .7656 .8789	.4418 .5185 .6013 .6903	2.3562 2.5525 2.7489 2.9452
$rac{1}{16}$	3.400 3.838 4.303 4.795	2.670 3.014 3.379 3.766	1.0000 1.1289 1.2656 1.4102	.7854 .8866 .9940 1.1075	3.1416 3.3379 3.5343 3.7306
1 4 5 1 6 8 7 7	5.312 5.857 6.428 7.026	5.049	1.5625 1.7227 1.8906 2.0664	1.2272 1.3530 1.4849 1.6230	3.9270 4.1233 4.3197 4.5160
$\begin{array}{c} \frac{1}{2} \\ \frac{9}{15} \\ \frac{5}{8} \\ \frac{1}{1} \\ \frac{1}{6} \end{array}$	7.650 8.301 8.978 9.682	6.520 7.051	2.2500 2.4414 2.6406 2.8477	1.7671 1.9175 2.0739 2.2365	4.7124 4.9087 5.1051 5.3014
3 4 3 1 3 6 7 7 8 1 5 6	10.41 11.17 11.95 12.76	8.773 9.388	3.0625 3.2852 3.5156 3.7539	2.4053 2.5802 2.7612 2.9483	5.4978 5.6941 5.8905 6.0868

Thickness	Weight of	Weight of	Area of	Area of	Circumference
or Diameter	□ Bar	O Bar	☐ Bar	O Bar	of O Bar
in Inches.	One Foot Long.	One Foot Long.	in Sq. Inches.	in Sq. Inches.	in Inches.
2 1 16 18 18 136	13.60 14.46 15.35 16.27	10.68 11.36 12.06 12.78	4.0000 4.2539 4.5156 4.7852	3.1416 3.3410 3.5466 3.7583	6.2832 6.4795 6.6759 6.8722
1455 166 38607 16	17.22 18.19 19.18 20.20	13.52 14.28 15.07 15.86	5.0625 5.3477 5.6406 5.9414	3.9761 4.2000 4.4301 4.6664	7.0686 7.2649 7.4613 7.6576
1 2 3 5 5 8 1 1 6	21.25 22.33 23.43 24.56	16.69 17.53 18.40 19.29	6.2500 6.5664 6.8906 7.2227	4.9087 5.1572 5.4119 5.6727	7.8540 8.0503 8.2467 8.4430
34366 7.855 1.166	25.71 26.90 28.10 29.34	20.20 21.12 22.07 23.04	7.5625 7.9102 8.2656 8.6289	5.9396 6.2126 6.4918 6.7771	8.6394 8.8357 9.0321 9.2284
$\frac{3}{16}$	30.60 31.89 33.20 34.55	24.03 25.04 26.08 27.13	9.0000 9.3789 9.7656 10.160	7.0686 7.3662 7.6699 7.9798	9.4248 9.6211 9.8175 10.014
14 5 16 3 8 7 16	35.92 37.31 38.73 40.18	28.20 29.30 30.42 31.56	10.563 10.973 11.391 11.816	8.2958 8.6179 8.9462 9.2806	10.210 10.407 10.603 10.799
1 9 5 5 1 1 6	41.65 43.14 44.68 46.24	32.71 33.90 35.09 36.31	12.250 12.691 13.141 13.598	9.6211 9.9678 10.321 10.680	10.996 11.192 11.388 11.585
3/4-5/6 1/16 1/18 1/16	47.82 49.42 51.05 52.71	37.56 38.81 40.10 41.40	14.063 14.535 15.016 15.504	11.045 11.416 11.793 12.177	11.781 11.977 12.174 12.370

	1				1
Thickness	Weight of	Weight of	Area of	Area of	Circumference
or Diameter	□ Bar	O Bar	□ Bar	O Bar	of O Bar
in Inches.	One Foot Long.	One Foot Long.	in Sq. Inches.	in Sq. Inches.	in Inches.
4	54.40	42.73	16.000	12.566	12.566
	56.11	44.07	16.504	12.962	12.763
10	57.85	45.44	17.016	13.364	12.959
$\begin{array}{c} \frac{1}{16} \\ \frac{1}{8} \\ \frac{3}{16} \end{array}$	59.62	46.83	17.535	13.772	13.155
	01 41	40.04	18.063	14.186	10.050
14 5 16 3 8 7 16	61,41 63,23	48.24 49.66	18.598	14.186	13.352 13.548
$\frac{\overline{1}}{3}$	65.08	51.11	19.141	15.033	13.744
7 16	66.95	52.58	19.691	15.466	13.941
1 2 9 16 5 8 11	68.85	54.07	20.250	15.904	14.137
18 5	70.78 72.73	55.59 57.12	20.816 21.391	16.349 16.800	14.334 14.530
<u>₹</u> 1	74.70	58.67	21.973	17.257	14.726
1 6	7 1.70	00.07		11,201	11.720
3/4	76.71	60.25	22.563	17.721	14.923
$\frac{1}{1}\frac{3}{6}$	78.74	61.84	23.160	18.190	15.119
$\frac{3}{4}$ $\frac{1}{13}$ $\frac{1}{6}$ $\frac{7}{8}$ $\frac{1}{16}$	80.81 82.89	63.46 65.10	23.766 $24.379$	18.665 19.147	15.315 15.512
16	04.09	05.10	44.018	19.147	15.514
5	85.00	66.76	25.000	19.635	15.708
1 1 6	87.14	68.44	25.629	20.129	15.904
$\begin{array}{c} \frac{1}{16} \\ \frac{1}{8} \\ \frac{3}{16} \end{array}$	89.30	70.14	26.266	20.629	16.101
$\frac{3}{16}$	91.49	71.86	26.910	21.135	16.297
1	93.72	73.60	27.563	21.648	16.493
$\frac{\frac{1}{4}}{\frac{5}{5}}$ $\frac{1}{16}$ $\frac{3}{8}$ $\frac{7}{16}$	95.96	75.37	28.223	22.166	16.690
38	98.23	77.15	28.891	22.691	16.886
$\frac{7}{16}$	100.5	78.95	29.566	23.221	17.082
1	102.8	80.77	30.250	23.758	17.279
29	102.8	82.62	30.230	24.301	17.475
16	107.6	84.49	31.641	24.850	17.671
$     \begin{array}{r}       \frac{1}{2} \\       9 \\       \hline       1.6 \\       5 \\       \hline       8 \\       \frac{1}{1} \frac{1}{1} \\     \end{array} $	110.0	86.38	32.348	25.406	17.868
	7104	00.00	20.000	05 005	10,004
4 1 3	112.4 114.9	88.29 90.22	33.063 33.785	25.967 26.535	18.064 18.261
7 6	117.4	92.17	34.516	27.109	18.457
$\frac{3}{4}$ $\frac{1}{1}$ $\frac{3}{6}$ $\frac{7}{8}$ $\frac{1}{1}$ $\frac{5}{6}$	119.9	94.14	35.254	27.688	18.653
10					

Thickness	Weight of	Weight of	Area of	Area of	Circumference
or Diameter	□ Bar	O Bar	□ Bar	O Bar	of O Bar
in Inches.	One Foot Long.	One Foot Long.	in Sq. Inches.	in Sq. Inches.	in Inches.
6	122.4	96.14	36.000	28.274	18.850
1 16 8 8 3 16	125.0	98.14	36.754	28.866	19.046
8 3	127.6 130.2	100.2 102.2	37.516 38.285	29.465	19.242
16	130.2	102.2	38.289	30.069	19.439
1	132.8	104.3	39.063	30.680	19.635
4 5 -5	135.5	106.4	39.848	31.296	19.831
3	138.2	108.5	40.641	31.919	20.028
$\frac{\frac{1}{4}}{\frac{5}{16}}$	140.9	110.7	41.441	32.548	20.224
			40.000		
$     \begin{array}{c}       \frac{1}{2} \\       9 \\       \hline       16 \\       5 \\       8 \\       \hline       11 \\       \hline       16 \\     \end{array} $	143.6	112.8	42.250	33.183	20.420
$\frac{9}{1_{5}6}$	146.5	114.9	43.066	33.824	20.617
ğ 11	149.2 152.1	$117.2 \\ 119.4$	43.891 44.723	34.472	20.813
1ं है	152.1	119.4	44.725	35.125	21.009
<u>3</u>	154.9	121.7	45.563	35.785	21.206
13 13	157.8	123.9	46.410	36.450	21.402
7	160.8	126.2	47.266	37.122	21.598
3 4 13 16 7 8 15 16	163.6	128.5	48.129	37.800	21.795
7	166.6	130.9	49.000	38.485	21.991
$\frac{1}{1,6}$	169.6	133.2	49.879	39.175	22.187
1 8 3 16	172.6 175.6	135.6 137.9	50.766	39.871	22.384
Te	175.6	137.9	51.660	40.574	22.580
1	178.7	140.4	52.563	41.282	22.777
4 5	181.8	142.8	53.473	41.997	22.973
3	184.9	145.3	54.391	42.718	23.169
$\frac{\frac{1}{4}}{\frac{1}{6}}$ $\frac{3}{8}$ $\frac{7}{16}$	188.1	147.7	55.316	43.445	23.366
1296 1698 116	191.3	150.2	56.250	44.179	23.562
15	194.4	152.7	57.191	44.918	23.758
8 11	197.7 200.9	155.2 157.8	58.141	45.664	23.955
16	200.9	107.0	59.098	46.415	24.151
3	204.2	160.3	60.063	47.173	24.347
$\frac{4}{\frac{1}{1}\frac{3}{6}}$	207.6	163.0	61.035	47.937	24.544
3 4 136 7 7 8 155 166	210.8	165.6	62.016	48.707	24.740
$\frac{15}{16}$	214.2	168.2	63.004	49.483	24.936

	1				1
Thickness	Weight of	Weight of	Area of	Area of	Circumference
or Diameter	□ Bar	O Bar	☐ Bar	O Bar	of O Bar
in Inches.	One Foot Long.	One Foot Long.	in Sq. Inches.	in Sq. Inches.	in Inches.
8	217.6	171.0	64.000	50.265	25.133
	221.0	173.6	65.004	51.054	25.329
16	224.5	176.3	66.016	51.849	25.525
1 16 16 16	228.0	179.0	67.035	52.649	25.722
	007.4		00.000	<b>*</b> 0.4 <b>*</b> 0	
145 158 238 276	231.4	181.8	68.063	53.456	25.918
136 3	234.9 238.5	184.5 187.3	69.098 70.141	54.269 55.088	26.114 26.311
87	242.0	190.1	71.191	55.914	26.507
16	212.0	100.1	71.101	33.011	20.007
1/2	245.6	193.0	72.250	56.745	26.704
1.6	249.3	195.7	73.316	57.583	26.900
8	252.9	198.7	74.391	58.426	27.096
$\frac{1}{1}\frac{1}{6}$	256.6	201.6	75.473	59.276	27.293
3	260.3	204.4	76.563	60.132	27.489
3 13 16	264.1	207.4	77.660	60.994	27.685
7/2	267.9	210.3	78.766	61.862	27.882
7 8 15 16	271.6	213.3	79.879	62.737	28.078
0	275.4	216.3	81.000	63.617	28.274
9	279.3	219.3	82.129	64.504	28.471
16	283.2	222.4	83.266	65.397	28.667
1 6 8 3 T 6	287.0	225.4	84.410	66.296	28.863
	0000	990 =	05 500	05 001	00.000
$\frac{1}{4}$	290.9 294.9	228.5 231.5	85.563 86.723	67.201 68.112	29.060 29.256
$\frac{\frac{1}{4}}{\frac{5}{16}}$ $\frac{3}{8}$ $\frac{7}{16}$	294.9	231.5	87.891	69.029	29.452
87	302.8	237.9	89.066	69.953	29.649
16					
1/2	306.8	241.0	90.250	70.882	29.845
<u> </u>	310.9	244.2	91.441	71.818	30.041
1 2 7 6 5 8 1 1 7 6	315.0 319.1	247.4 250.6	92.641 93.848	72.760 73.708	30.238 30.434
16	919.1	200.0	99,040	10.100	90.494
3	323.2	253.9	95.063	74.662	30.631
13	327.4	257.1	96.285	75.622	30.827
$\frac{3}{4}$ $\frac{1}{3}$ $\frac{3}{16}$ $\frac{7}{8}$ $\frac{1}{15}$	331.6	260.4	97.516	76.589	31.023
$\frac{15}{16}$	335.8	263.7	98.754	77.561	31.220

(CONCLUDED.)

Thickness	Weight of	Weight of	Area of	Area of	Circumference
or Diameter	□ Bar	O Bar	□ Bar	O Bar	of O Bar
in Inches.	One Foot Long.	One Foot Long.	in Sq. Inches.	in Sq. Inches.	in Inches.
in indues.	one root hong.	one root hong.	in by, inches.	in bq. inches.	in inches.
10	340.0	267.0	100.00	78.540	31.416
	344.3	270.4	101.25	79.525	31.612
16 16	348.5 352.9	$273.8 \\ 277.1$	102.52 103.79	80.516 81.513	31.809 32.005
16	992.9	211.1	103.78	01.010	52.005
1	357.2	280.6	105.06	82.516	32.201
$\frac{5}{16}$	361.6	284.0	106.35	83.525	32.398
1 4 5 1 6 3 8 7 1 6	366.0	287.4	107.64	84.541	32.594
16	370.4	290.9	108.94	85.562	32.790
1	374.9	294.4	110.25	86.590	32.987
2 9	379.4	297.9	111.57	87.624	33.183
5 8	383.8	301.4	112.89	88.664	33.379
1 9 16 5 8 11 16	388.3	305.0	114.22	89.710	33.576
	222.2	2000			~~ == ~
344360 178556	392.9	308.6	115.56	90.763	33.772
18	397.5 402.1	$312.2 \\ 315.8$	116.91 118.27	91.821 92.886	33.968 34.165
8 15	406.8	319.5	119.63	93.956	34,361
16	100.0	010.0	110.00	00.000	94,001
11	411.4	323.1	121.00	95.033	34.558
1.6	416.1	326.8	122.38	96.116	34.754
$\begin{array}{c} \frac{1}{8} \\ \frac{3}{16} \end{array}$	420.9	330.5	123.77	97.205	34.950
$\frac{3}{16}$	425.5	334.3	125.16	98.301	35.147
1	430.3	337.9	126.56	99.402	35.343
5	435.1	341.7	127.97	100.51	35.539
$\frac{1}{3}$	439.9	345.5	129.39	101.62	35.736
145 166 388 7 166	444.8	349.4	130.82	102.74	35.932
	440.0	0.0.7	700 02		00100
2	449.6	353.1	132.25	103.87	36.128
16	454.5 459.5	357.0 360.9	133.69 135.14	105.00 106.14	36.325 36.521
1.249 1.66 5.88 1.16	464.4	364.8	136.60	107.28	36.717
16	202,2				00.7.2.7
3 4	469.4	368.6	138.06	108.43	36.914
$\frac{13}{16}$	474.4	372.6	139.54	109.59	37.110
34 136 78 156 156	479.5	376.6 380.6	141.02 $142.50$	110.75	37.306
16	484.5	00.00	142.50	111.92	37.503

For Thicknesses from 1 in. to 2 in. and Widths from 1 in. to 123 in.

Thickness in Inches.	1''	$1\frac{1}{4}$	11/2"	13//	2"	21/1	$2^{rac{1}{2}''}$	23/11	12"
1 16 8 3 16 4	.063 .125 .188 .250	.156	.188		.250	.141 .281 .422 .563	.156 .313 .469 .625	.172 .344 .516 .688	.750 1.50 2.25 3.00
5-6 1-3-6 1-2	.313 .375 .438 .500	.391 .469 .547 .625	.469 .563 .656 .750	.547 .656 .766 .875	.750 .875	.703 .844 .984 1.13	.781 .938 1.09 1.25	.859 1.03 1.20 1.38	3.75 4.50 5.25 6.00
9 16 5 8 11 16 34	.563 .625 .688 .750	.703 .781 .859 .938	.844 .938 1.03 1.13	.984 1.09 1.20 1.31	1.13 1.25 1.38 1.50	1.27 1.41 1.55 1.69	1.41 1.56 1.72 1.88	1.55 1.72 1.89 2.06	6.75 7.50 8.25 9.00
$ \begin{array}{c} \frac{13}{16} \\ \frac{7}{8} \\ \frac{15}{16} \end{array} $	.813	1.02	1.22	1.42	1.63	1.83	2.03	2.23	9.75
	.875	1.09	1.31	1.53	1.75	1.97	2.19	2.41	10.50
	.938	1.17	1.41	1.64	1.88	2.11	2.34	2.58	11.25
	1.00	1.25	1.50	1.75	2.00	2.25	2.50	2.75	12.00
$ \begin{array}{c} 1\frac{1}{16} \\ 1\frac{1}{8} \\ 1\frac{3}{16} \\ 1\frac{1}{4} \end{array} $	1.06	1.33	1.59	1.86	2.13	2.39	2.66	2.92	12.75
	1.13	1.41	1.69	1.97	2.25	2.53	2.81	3.09	13.50
	1.19	1.48	1.78	2.08	2.38	2.67	2.97	3.27	14.25
	1.25	1.56	1.88	2.19	2.50	2.81	3.13	3.44	15.00
1 5 6 1 3 8 1 1 7 6 1 1 1 2	1.31	1.64	1.97	2.30	2.63	2.95	3.28	3.61	15.75
	1.38	1.72	2.06	2.41	2.75	3.09	3.44	3.78	16.50
	1.44	1.80	2.16	2.52	2.88	3.23	3.59	3.95	17.25
	1.50	1.88	2.25	2.63	3.00	3.38	3.75	4.13	18.00
1 ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½ ½	1.56	1.95	2.34	2.73	3.13	3.52	3.91	4.30	18.75
	1.63	2.03	2.44	2.84	3.25	3.66	4.06	4.47	19.50
	1.69	2.11	2.53	2.95	3.38	3.80	4.22	4.64	20.25
	1.75	2.19	2.63	3.06	3.50	3.94	4.38	4.81	21.00
$\begin{array}{c} 1\frac{1}{1}\frac{3}{16} \\ 1\frac{7}{18} \\ 1\frac{1}{1}\frac{5}{6} \\ 2 \end{array}$	1.81	2.27	2.72	3.17	3.63	4.08	4.53	4.98	21.75
	1.88	2.34	2.81	3.28	3,75	4.22	4.69	5.16	22.50
	1.94	2.42	2.91	3.39	3.88	4.36	4.84	5.33	23.25
	2.00	2.50	3.00	3.50	4.00	4.50	5.00	5.50	24.00

	1	) (							
Thickness in Inches.	3"	31/1	3½"	33//	4′′	$4\frac{1}{4}''$	41/1	43//	12′′
$\begin{array}{c} \frac{1}{16} \\ \frac{1}{8} \\ \frac{3}{16} \\ \frac{1}{4} \end{array}$	.188	.203	.219	.234	.250	.266	.281	.297	.750
	.375	.406	.438	.469	.500	.531	.563	.594	1.50
	.563	.609	.656	.703	.750	.797	.844	.891	2.25
	.750	.813	.875	.938	1.00	1.06	1.13	1.19	3.00
$\begin{array}{c} \frac{5}{16} \\ \frac{3}{8} \\ \frac{7}{16} \\ \frac{1}{2} \end{array}$	.938	1.02	1.09	1.17	1.25	1.33	1.41	1.48	3.75
	1.13	1.22	1.31	1.41	1.50	1.59	1.69	1.78	4.50
	1.31	1.42	1.53	1.64	1.75	1.86	1.97	2.08	5.25
	1.50	1.63	1.75	1.88	2.00	2.13	2.25	2.38	6.00
9 15 8 11 6 34	1.69 1.88 2.06 2.25	1.83 2.03 2.23 2.44	1.97 2.19 2.41 2.63	2.11 2.34 2.58 2.81	2.25 2.50 2.75 3.00	2.39 2.66 2.92 3.19	2.53 2.81 3.09 3.38	2.67 2.97 3.27 3.56	6.75 7.50 8.25 9.00
$ \begin{array}{c} \frac{13}{16} \\ \frac{7}{8} \\ \frac{15}{16} \end{array} $	2.44	2.64	2.84	3.05	3.25	3.45	3.66	3.86	9.75
	2.63	2.84	3.06	3.28	3.50	3.72	3.94	4.16	10.50
	2.81	3.05	3.28	3.52	3.75	3.98	4.22	4.45	11.25
	3.00	3.25	3.50	3.75	4.00	4.25	4.50	4.75	12.00
$ \begin{array}{c} 1\frac{1}{16} \\ 1\frac{1}{8} \\ 1\frac{3}{16} \\ 1\frac{1}{4} \end{array} $	3.19	3.45	3.72	3.98	4.25	4.52	4.78	5.05	12.75
	3.38	3.66	3.94	4.22	4.50	4.78	5.06	5.34	13.50
	3.56	3.86	4.16	4.45	4.75	5.05	5.34	5.64	14.25
	3.75	4.06	4.38	4.69	5.00	5.31	5.63	5.94	15.00
$\begin{array}{c} 1 \frac{5}{16} \\ 1 \frac{3}{38} \\ 1 \frac{7}{16} \\ 1 \frac{1}{2} \end{array}$	3.94	4.27	4.59	4.92	5.25	5.58	5.91	6.23	15.75
	4.13	4.47	4.81	5.16	5.50	5.84	6.19	6.53	16.50
	4.31	4.67	5.03	5.39	5.75	6.11	6.47	6.83	17.25
	4.50	4.88	5.25	5.63	6.00	6.38	6.75	7.13	18.00
$1\frac{9}{16}$ $1\frac{5}{8}$ $1\frac{1}{16}$ $1\frac{3}{4}$	4.69	5.08	5.47	5.86	6.25	6.64	7.03	7.42	18.75
	4.88	5.28	5.69	6.09	6.50	6.91	7.31	7.72	19.50
	5.06	5.48	5.91	6.33	6.75	7.17	7.59	8.02	20.25
	5.25	5.69	6.13	6.56	7.00	7.44	7.88	8.31	21.00
$\begin{array}{c} 1 \frac{1}{1} \frac{3}{6} \\ 1 \frac{7}{8} \\ 1 \frac{1}{1} \frac{5}{6} \\ 2 \end{array}$	5.44	5.89	6.34	6.80	7.25	7.70	8.16	8.61	21.75
	5.63	6.09	6.56	7.03	7.50	7.97	8.44	8.91	22.50
	5.81	6.30	6.78	7.27	7.75	8.23	8.72	9.20	23.25
	6.00	6.50	7.00	<b>7.50</b>	8.00	8.50	9.00	9.50	24.00
				•					

Thickness in Inches.	5"	51111	5½''	53//	6"	61111	6½"	63/1	12"
$\begin{array}{c} \frac{1}{16} \\ \frac{1}{8} \\ \frac{3}{16} \\ \frac{1}{4} \end{array}$	.313 .625 .938 1.25	.328 .656 .984 1.31	.344 .688 1.03 1.38	.359 .719 1.08 1.44	.375 .750 1.13 1.50	.391 .781 1.17 1.56	.406 .813 1.22 1.63	.422 .844 1.27 1.69	.750 1.50 2.25 3.00
5 1 6 2 1 6 1 6	1.56 1.88 2.19 2.50	1.64 1.97 2.30 2.63	1.72 2.06 2.41 2.75	1.80 2.16 2.52 2.88	1.88 2.25 2.63 3.00	1.95 2.34 2.73 3.13	2.03 2.44 2.84 3.25	2.11 2.53 2.95 3.38	3.75 4.50 5.25 6.00
9 16 5 8 11 16 3	2.81 3.13 3.44 3.75	2.95 3.28 3.61 3.94	3.09 3.44 3.78 4.13	3.23 3.59 3.95 4.31	3.38 3.75 4.13 4.50	3.52 3.91 4.30 4.69	3.66 4.06 4.47 4.88	3.80 4.22 4.64 5.06	6.75 7.50 8.25 9.00
$1 \frac{\frac{1}{1} \frac{3}{6}}{\frac{7}{8}} \\ \frac{\frac{1}{1} \frac{5}{6}}{1}$	4.06 4.38 4.69 5.00	4.27 4.59 4.92 5.25	4.47 4.81 5.16 5.50	4.67 5.03 5.39 5.75	4.88 5.25 5.63 6.00	5.08 5.47 5.86 6.25	5.28 5.69 6.09 6.50	5.48 5.91 6.33 6.75	9.75 10.50 11.25 12.00
$ \begin{array}{c} 1\frac{1}{16} \\ 18 \\ 1\frac{3}{16} \\ 1\frac{1}{4} \end{array} $	5.31 5.63 5.94 6.25	5.58 5.91 6.23 6.56	5.84 6.19 6.53 6.88	6.11 6.47 6.83 7.19	6.38 6.75 7.13 7.50	6.64 7.03 7.42 7.81	6.91 7.31 7.72 8.13	7.17 7.59 8.02 8.44	12.75 13.50 14.25 15.00
$ \begin{array}{c} 1\frac{5}{166} \\ 1\frac{3}{8} \\ 1\frac{7}{16} \\ 1\frac{1}{2} \end{array} $	6.56 6.88 7.19 7.50	6.89 7.22 7.55 7.88	7.22 7.56 7.91 8.25	7.55 7.91 8.27 8.63	7.88 8.25 8.63 9.00	8.20 8.59 8.98 9.38	8.53 8.94 9.34 9.75	8.86 9.28 9.70 10.13	15.75 16.50 17.25 18.00
$\begin{array}{c} 1 \frac{9}{1 \cdot 5} \\ 1 \frac{5}{1 \cdot 5} \\ 1 \frac{1}{1 \cdot 1} \frac{1}{1 \cdot 5} \\ 1 \frac{3}{4} \end{array}$	7.81 8.13 8.44 8.75	8.20 8.53 8.86 9.19	8.59 8.94 9.28 9.63			9.77 10.16 10.55 10.94	10.16 10.56 10.97 11.38	10.55 10.97 11.39 11.81	18.75 19.50 20.25 21.00
$\begin{array}{c} 1\frac{1}{1}\frac{8}{60} \\ 1\frac{7}{2} \\ 1\frac{1}{1}\frac{5}{6} \\ 2 \end{array}$			10.31 10.66	10.78 11.14	11.25	11.33 11.72 12.11 12.50	11.78 12.19 12.59 13.00	12.23 12.66 13.08 13.50	21.75 22.50 23.25 24.00

Thickness in Inches.	7''	71/4	$7\frac{1}{2}^{\prime\prime}$	73//	8′′	81/1	81/1	83/11	12"
1 16 8 3 16 4	.438 .875 1.31 1.75	.453 .906 1.36 1.81	.469 .938 1.41 1.88	.484 .969 1.45 1.94	.500 1.00 1.50 2.00	.516 1.03 1.55 2.06	.531 1.06 1.59 2.13	.547 1.09 1.64 2.19	.750 1.50 2.25 3.00
5 13 8 7 16	2.19 2.63 3.06 3.50	2.27 2.72 3.17 3.63	2.34 2.81 3.28 3.75	2.42 2.91 3.39 3.88	2.50 3.00 3.50 4.00	2.58 3.09 3.61 4.13	2.66 3.19 3.72 4.25	2.73 3.28 3.83 4.38	3.75 4.50 5.25 6.00
9 16 5 8 11 16 3	3.94 4.38 4.81 5.25	4.08 4.53 4.98 5.44	4.22 4.69 5.16 5.63	4.36 4.84 5.33 5.81	4.50 5.00 5.50 6.00	4.64 5.16 5.67 6.19	4.78 5.31 5.84 6.38	4.92 5.47 6.02 6.56	6.75 7.50 8.25 9.00
$1 \frac{\frac{13}{166}}{\frac{7}{8}}$ $1 \frac{15}{16}$	5.69 6.13 6.56 7.00	5.89 6.34 6.80 7.25	6.09 6.56 7.03 7.50	6.30 6.78 7.27 7.75	6.50 7.00 7.50 8.00	6.70 7.22 7.73 8.25	6.91 7.44 7.97 8.50	7.11 7.66 8.20 8.75	9.75 10.50 11.25 12.00
$ \begin{array}{c} 1 \frac{1}{16} \\ 1 \frac{1}{8} \\ 1 \frac{3}{16} \\ 1 \frac{4}{4} \end{array} $	7.44 7.88 8.31 8.75	7.70 8.16 8.61 9.06	7.97 8.44 8.91 9.38	8.23 8.72 9.20 9.69	8.50 9.00 9.50 10.00	8.77 9.28 9.80 10.31	9.03 9.56 10.09 10.63	9.30 9.84 10.39 10.94	12.75 13.50 14.25 15.00
$\begin{array}{c} 1\frac{5}{16} \\ 1\frac{3}{8} \\ 1\frac{7}{16} \\ 1\frac{1}{2} \end{array}$	9.19 9.63 10.06 10.50	9.52 9.97 10.42 10.88	9.84 10.31 10.78 11.25	10.17 10.66 11.14 11.63	10.50 11.00 11.50 12.00	10.83 11.34 11.86 12.38	11.16 11.69 12.22 12.75	11.48 12.03 12.58 13.13	15.75 16.50 17.25 18.00
$\begin{array}{c} 1\frac{9}{16} \\ 1\frac{5}{8} \\ 1\frac{11}{16} \\ 1\frac{3}{4} \end{array}$	10.94 11.38 11.81 12.25	11.33 11.78 12.23 12.69	12.19 12.66	12.11 12.59 13.08 13.56	12.50 13.00 13.50 14.00	12.89 13.41 13.92 14.44	13.28 13.81 14.34 14.88	13.67 14.22 14.77 15.31	18.75 19.50 20.25 21.00
$\begin{array}{c} 1\frac{1}{1}\frac{3}{16} \\ 1\frac{7}{8} \\ 1\frac{1}{1}\frac{5}{6} \\ 2 \end{array}$	13.13 13.56	13.59 14.05	14.06 14.53	14.05 14.53 15.02 15.50	14.50 15.00 15.50 16.00	14.95 15.47 15.98 16.50	15.41 15.94 16.47 17.00	15.86 16.41 16.95 17.50	21.75 22.50 23.25 24.00

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Thickness in Inches.	9"	91111	91111	93//	10′′	101/1	101/2	103//	12"
$\begin{array}{c} \frac{1}{1_{6}} \\ \frac{1}{8} \\ \frac{3}{1_{6}} \\ \frac{1}{4} \end{array}$	.563 1.13 1.69 2.25	.578 1.16 1.73 2.31	.594 1.19 1.78 2.38	.609 1.22 1.83 2.44	.625 1.25 1.88 2.50	.641 1.28 1.92 2.56	.656 1.31 1.97 2.63	.672 1.34 2.02 2.69	.750 1.50 2.25 3.00
5 16 3 8 7 16 12	2.81 3.38 3.94 4.50	2.89 3.47 4.05 4.63	2.97 3.56 4.16 4.75	3.05 3.66 4.27 4.88	3.13 3.75 4.38 5.00	3.20 3.84 4.48 5.13	3.28 3.94 4.59 5.25	3.36 4.03 4.70 5.38	3.75 4.50 5.25 6.00
$\begin{array}{r} \frac{9}{16} \\ \frac{5}{8} \\ \frac{11}{16} \\ \frac{3}{4} \end{array}$	5.06 5.63 6.19 6.75	5.20 5.78 6.36 6.94	5.34 5.94 6.53 7.13	5.48 6.09 6.70 7.31	5.63 6.25 6.88 7.50	5.77 6.41 7.05 7.69	5.91 6.56 7.22 7.88	6.05 6.72 7.39 8.06	6.75 7.50 8.25 9.00
$\frac{\frac{1}{1}\frac{3}{6}}{\frac{7}{8}}$ $\frac{\frac{1}{1}\frac{5}{6}}{1}$	7.31 7.88 8.44 9.00	7.52 8.09 8.67 9.25	7.72 8.31 8.91 9.50	7.92 8.53 9.14 9.75	8.13 8.75 9.38 10.00	8.33 8.97 9.61 10.25	8.53 9.19 9.84 10.50	8.73 9.41 10.08 10.75	9.75 10.50 11.25 12.00
$ \begin{array}{c} 1\frac{1}{16} \\ 1\frac{1}{8} \\ 1\frac{3}{16} \\ 1\frac{1}{4} \end{array} $			11.28	10.36 10.97 11.58 12.19	10.63 11.25 11.88 12.50	10.89 11.53 12.17 12.81	11.16 11.81 12.47 13.13	11.42 12.09 12.77 13.44	12.75 13.50 14.25 15.00
$\begin{array}{c} 1\frac{5}{16} \\ 1\frac{3}{8} \\ 1\frac{7}{16} \\ 1\frac{1}{2} \end{array}$	11.81 12.38 12.94 13.50	12.72	13.06 13.66	12.80 13.41 14.02 14.63	13.13 13.75 14.38 15.00	13.45 14.09 14.73 15.38	13.78 14.44 15.09 15.75	14.11 14.78 15.45 16.13	15.75 16.50 17.25 18.00
$ \begin{array}{c} 1\frac{9}{16} \\ 1\frac{5}{8} \\ 1\frac{11}{16} \\ 1\frac{3}{4} \end{array} $	14.06 14.63 15.19 15.75	15.03	15.44 16.03	15.23 15.84 16.45 17.06	15.63 16.25 16.88 17.50	16.02 16.66 17.30 17.94	16.41 17.06 17.72 18.38	16.80 17.47 18.14 18.81	18.75 19.50 20.25 21.00
$\begin{array}{c} 1\frac{1}{3}\frac{3}{6} \\ 1\frac{7}{8} \\ 1\frac{1}{1}\frac{5}{6} \\ 2 \end{array}$	16.88	17.34 17.92	17.81 18.41		19.38	18.58 19.22 19.86 20.50	19.03 19.69 20.34 21.00	19.48 20.16 20.83 21.50	21.75 22.50 23.25 24.00

(CONCLUDED.)

Thickness in Inches.	11"	1114''	11½''	113//	12′′	12½″	12½''	12311	e areas of
1 16 1 8 3 16 14	.688 1.38 2.06 2.75	.703 1.41 2.11 2.81	.719 1.44 2.16 2.88	.734 1.47 2.20 2.94	.750 1.50 2.25 3.00	.766 1.53 2.30 3.06	.781 1.56 2.34 3.13	.797 1.59 2.39 3.19	The areas for 12" width are repeated on each page to facilitate making the additions necessary to obtain the areas of
5 16 38 87 16	3.44 4.13 4.81 5.50	3.52 4.22 4.92 5.63	3.59 4.31 5.03 5.75	3.67 4.41 5.14 5.88	3.75 4.50 5.25 6.00	3.83 4.59 5.36 6.13	3.91 4.69 5.47 6.25	3.98 4.78 5.58 6.38	ditions necess
$\frac{9}{16}$ $\frac{5}{5}$ $\frac{8}{116}$ $\frac{11}{16}$ $\frac{3}{4}$	6.19 6.88 7.56 8.25	6.33 7.03 7.73 8.44	6.47 7.19 7.91 8.63	6.61 7.34 8.08 8.81	6.75 7.50 8.25 9.00	6.89 7.66 8.42 9.19	7.03 7.81 8.59 9.38	7.17 7.97 8.77 9.56	making the ad
$1 \frac{\frac{13}{16}}{\frac{7}{8}}$ $1 \frac{15}{16}$	8.94 9.63 10.31 11.00	9.14 9.84 10.55 11.25	9.34 10.06 10.78 11.50	9.55 10.28 11.02 11.75	9.75 10.50 11.25 12.00	9.95 10.72 11.48 12.25	10.16 10.94 11.72 12.50	10.36 11.16 11.95 12.75	to facilitate
$ \begin{array}{c} 1\frac{1}{16} \\ 1\frac{1}{8} \\ 1\frac{3}{16} \\ 1\frac{1}{4} \end{array} $	11.69 12.38 13.06 13.75	11.95 12.66 13.36 14.06	12.22 12.94 13.66 14.38	12.48 13.22 13.95 14.69	12.75 13.50 14.25 15.00	13.02 13.78 14.55 15.31	13.28 14.06 14.84 15.63	13.55 14.34 15.14 15.94	on each page
$ \begin{array}{c} 1\frac{5}{16} \\ 1\frac{3}{8} \\ 1\frac{7}{16} \\ 1\frac{1}{2} \end{array} $	14.44 15.13 15.81 16.50	14.77 15.47 16.17 16.88	15.09 15.81 16.53 17.25	15.42 16.16 16.89 17.63	15.75 16.50 17.25 18.00	16.08 16.84 17.61 18.38	16.41 17.19 17.97 18.75	16.73 17.53 18.33 19.13	h are repeated
$1\frac{9}{16} \\ 1\frac{5}{8} \\ 1\frac{11}{16} \\ 1\frac{3}{4}$	17.19 17.88 18.56 19.25	17.58 18.28 18.98 19.69	17.97 18.69 19.41 20.13	18.36 19.09 19.83 20.56	18.75 19.50 20.25 21.00	19.14 19.91 20.67 21.44	19.53 20.31 21.09 21.88	19.92 20.72 21.52 22.31	s for 12" widtl
$1\frac{1}{16}$ $1\frac{7}{8}$ $1\frac{1}{16}$ 2	19.94 20.63 21.31 22.00	20.39 21.09 21.80 22.50	20.84 21.56 22.28 23.00	21.30 22.03 22.77 23.50	21.75 22.50 23.25 24.00	22.20 22.97 23.73 24.50	22.66 23.44 24.22 25.00	23.11 23.91 24.70 25.50	The area

### WEIGHTS OF FLAT ROLLED STRIPS, HOOP OR BAND STEEL.

#### PER LINEAL FOOT.

#### Thicknesses by Birmingham Wire Gauge.

One cubic foot of steel weighs 489.6 pounds. For widths from  $\frac{1}{4}$  inch to  $\frac{3}{4}$  inch and thicknesses from No. 19 to No. 11 B.W.G.

******	1 37 45	74 10	37 48	27 40	37 /5	37 44	37 40	1 37 40	1 37 44
Width in Inches.	No. 19. .042 In.	No. 18. .049 In.	No. 17. .058 In.	No. 16, .065 In.	No. 15. .072 In.	No. 14. .083 In.	No. 13. .095 In.	No. 12. .109 In.	No. 11. .120 In.
$\begin{array}{c} \frac{1}{4} \\ \frac{1}{6} \\ \frac{7}{6} \\ \frac{9}{3} \\ \frac{2}{2} \\ \frac{1}{6} \\ \frac{9}{4} \end{array}$	.036 .038 .040 .042	.042 .044 .047 .049	.049 .052 .055 .059	.055 .059 .062 .066	.061 .065 .069 .073	.071 .075 .079 .084	.081 .086 .091 .096	.093 .098 .104 .110	.102 .108 .115 .121
5 16 21 14 13 22 3 4	.045 .047 .049 .051	.052 .055 .057 .060	.062 .065 .068 .071	.069 .073 .076 .079	.077 .080 .084 .088	.088 .093 .097 .101	.101 .106 .111 .116	.116 .122 .127 .133	.128 .134 .140 .147
318 514 5121714 286 1195 216	.054 .056 .058 .060	.062 .065 .068 .070	.074 .077 .080 .083	.083 .086 .090 .093	.092 .096 .099 .103	.106 .110 .115 .119	.121 .126 .131 .136	.139 .145 .151 .156	.153 .159 .166 .172
7 169 294 182 183 14	.062 .065 .067 .069	.073 .075 .078 .081	.086 .089 .092 .096	.097 .100 .104 .107	.107 .111 .115 .119	.123 .128 .132 .137	.141 .146 .151 .156	.162 .168 .174 .180	.179 .185 .191 .198
12°33 4°7- 215 4	.071 .074 .076 .078	.083 .086 .089 .091	.099 .102 .105 .108	.111 .114 .117 .121	.122 .126 .130 .134	.141 .146 .150 .154	.162 .167 .172 .177	.185 .191 .197 .203	.204 .210 .217 .223
9 13744929 1894 1892 364	.080 .083 .085 .087	.094 .096 .099 .102	.111 .114 .117 .120	.124 .128 .131 .135	.138 .142 .145 .149	.159 .163 .168 .172	.182 .187 .192 .197	.208 .214 .220 .226	.230 .236 .242 .249
500 1 4 1 2 3 4 6 2 5 4 6	.089 .091 .094 .096	.104 .107 .109 .112	.123 .126 .129 .132	.138 .142 .145 .148	.153 .157 .161 .164	.176 .181 .185 .190	.202 .207 .212 .217	.232 .237 .243 .249	.255 .261 .268 .274
165438474 11462894694	.098 .100 .103 .105 .107	.115 .117 .120 .122 .125	.136 .139 .142 .145 .148	.152 .155 .159 .162 .166	.168 .172 .176 .180 .184	.194 .198 .203 .207 .212	.222 .227 .232 .237 .242	.255 .261 .266 .272 .278	.281 .287 .293 .300

One cubic foot of steel weighs 489.6 pounds.

For thicknesses from  $\frac{1}{16}$  inch to  $\frac{9}{16}$  inch and widths from  $\frac{1}{4}$  inch to  $\frac{3}{4}$  inch.

			16	1 10					4
Thickness in Inches.	1//	17// 64	9//	19// 64	5//	21// 64	11//	23// 64	3//
$ \begin{array}{c} 1 \\ 16 \\ 5 \\ 64 \\ 3 \\ 3 \\ 2 \\ 7 \\ 64 \end{array} $	.053 .066 .080 .093	.056 .071 .085 .099	.060 .075 .090 .105	.063 .079 .095 .110	.066 .083 .100 .116	.070 .087 .105 .122	.073 .091 .110 .128	.076 .095 .115 .134	.080 .100 .120 .139
$\begin{array}{c} \frac{1}{8} \\ 9 \\ 6 \\ 5 \\ \frac{3}{2} \\ \frac{1}{6} \\ \frac{1}{4} \end{array}$	.106 .120 .133 .146	.113 .127 .141 .155	.120 .134 .149 .164	.126 .142 .158 .173	.133 .149 .166 .183	.139 .157 .174 .192	.146 .164 .183 .201	.153 .172 .191 .210	.159 .179 .199 .219
$ \begin{array}{c} 3 \\ 1 \\ 3 \\ 6 \end{array} $ $ \begin{array}{c} 7 \\ 3 \\ 2 \\ 1 \\ 6 \end{array} $	.159 .173 .186 .199	.169 .183 .198 .212	.179 .194 .209 .224	.189 .205 .221 .237	.199 .216 .232 .249	.209 .227 .244 .261	.219 .237 .256 .274	.229 .248 .267 .286	.239 .259 .279 .299
$\begin{array}{c} \frac{1}{4} \\ \frac{1}{7} \\ \frac{7}{6} \\ \frac{9}{3} \\ \frac{1}{2} \\ \frac{1}{6} \\ 4 \end{array}$	.213 .226 .239 .252	.226 .240 .254 .268	.239 .254 .269 .284	.252 .268 .284 .300	.266 .282 .299 .315	.279 .296 .314 .331	.292 .310 .329 .347	.305 .325 .344 .363	.319 .339 .359 .379
5 6 141 261 132 4 123 4	.266 .279 .292 .305	.282 .296 .310 .325	.299 .314 .329 .344	.315 .331 .347 .363	.332 .349 .365 .382	.349 .366 .383 .401	.365 .383 .402 .420	.382 .401 .420 .439	.398 .418 .438 .458
3 8 5 43 247 4 2 61 3247 4	.319 .332 .345 .359	.339 .353 .367 .381	.359 .374 .388 .403	.379 .394 .410 .426	.398 .415 .432 .448	.418 .436 .453 .471	.438 .457 .475 .493	.458 .477 .496 .515	.478 .498 .518 .538
7 129 645 23 64 133 64	.372 .385 .398 .412	.395 .409 .423 .437	.418 .433 .448 .463	.442 .457 .473 .489	.465 .481 .498 .515	.488 .506 .523 .540	.511 .530 .548 .566	.535 .554 .573 .592	.558 .578 .598 .618
364725549 16	.425 .438 .452 .465 .478	.452 .466 .480 .494 .508	.478 .493 .508 .523 .538	.505 .520 .536 .552 .567	.564 .581	.558 .575 .593 .610 .628	.584 .603 .621 .639 .657	.611 .630 .649 .668	.638 .657 .677 .697 .717

Thickness in Inches.	25// 64	13//	27//	7/16	29// 64//	15// 32//	31// 64//	1//	12′′
$\begin{array}{c} \frac{1}{16} \\ \frac{5}{644} \\ \frac{3}{32} \\ \frac{7}{644} \end{array}$	.083 .104 .125 .145	.086 .108 .129 .151	.090 .112 .134 .157	.093 .116 .139 .163	.096 .120 .144 .169	.100 .125 .149 .174	.103 .129 .154 .180	.106 .133 .159 .186	2.53 3.19 3.83 4.46
\$\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	.166 .187 .208 .228	.173 .194 .216 .237	.179 .202 .224 .247	.186 .209 .232 .256	.193 .217 .241 .265	.199 .224 .249 .274	.206 .232 .257 .283	.212 .239 .266 .292	5.10 5.74 6.38 7.01
3 6 3 4 1 1 6 7 3 1 6 7 3 1 6 7	.249 .270 .291 .311	.259 .281 .302 .324	.269 .291 .314 .336	.279 .302 .325 .349	.289 .313 .337 .361	.299 .324 .349 .374	.309 .335 .360 .386	.319 .345 .372 .398	7.65 8.29 8.93 9.56
14 14 16 9 29 16	.332 .353 .374 .394	.345 .367 .388 .410	.359 .381 .403 .426	.372 .395 .418 .442	.385 .409 .433 .457	.398 .423 .448 .473	.412 .437 .463 .489	.425 .452 .478 .505	10.20 10.84 11.48 12.11
5 16 21 61 13 22 23 4	.415 .436 .457 .477	.432 .453 .475 .496	.448 .471 .493 .515	.465 .488 .511 .535	.481 .506 .530 .554	.498 .523 .548 .573	.515 .540 .566 .592	.531 .558 .584 .611	12.75 13.39 14.03 14.66
300 514362714 216 120216	.498 .519 .540 .560	.518 .540 .561 .583	.538 .560 .583 .605	.558 .581 .604 .628	.578 .602 .626 .650	.598 .623 .647 .672	.618 .643 .669 .695	.638 .664 .691 .717	15.30 15.94 16.58 17.21
7691452114	.581 .602 .623 .643	.604 .626 .647 .669	.628 .650 .672 .695	.651 .674 .697 .721	.674 .698 .722 .746	.697 .722 .747 .772	.721 .746 .772 .798	.744 .770 .797 .823	17.85 18.49 19.13 19.76
33472254 96153869 1	.664 .685 .706 .726 .747	.691 .712 .734 .755 .777	.717 .740 .762 .784 .807	.744 .767 .790 .813 .837	.770 .794 .818 .843 .867	.797 .822 .847 .872 .896	.823 .849 .875 .901 .926	.850 .877 .903 .930	20.40 21.04 21.68 22.31 22.95

								1	
Thickness in Inches.	33//	17//	351/ 64	9 17	37// 64	19//	39// 64	<u>5</u> //	12"
$\begin{array}{c} \frac{1}{16} \\ \frac{5}{64} \\ \frac{3}{32} \\ \frac{7}{64} \end{array}$	.110	.113	.116	.120	.123	.126	.129	.133	2.53
	.137	.141	.145	.149	.154	.158	.162	.166	3.19
	.164	.169	.174	.179	.184	.189	.194	.199	3.83
	.192	.198	.203	.209	.215	.221	.227	.232	4.46
$ \begin{array}{r}                                     $	.219	.226	.232	.239	.246	.252	.259	.266	5.10
	.247	.254	.261	.269	.276	.284	.291	.299	5.74
	.274	.282	.291	.299	.307	.315	.324	.332	6.38
	.301	.310	.320	.329	.338	.347	.356	.365	7.01
$\begin{array}{c} \frac{3}{16} \\ \frac{1}{6} \\ \frac{3}{6} \\ \frac{4}{4} \\ \\ \frac{1}{6} \\ \frac{1}{4} \end{array}$	.329	.339	.349	.359	.369	.379	.388	.398	7.65
	.356	.367	.378	.388	.399	.410	.421	.432	8.29
	.383	.395	.407	.418	.430	.442	.453	.465	8.93
	.411	.423	.436	.448	.461	.473	.486	.498	9.56
$\begin{array}{c} \frac{1}{4} \\ \frac{1}{6} \frac{7}{4} \\ \frac{9}{3} \frac{2}{2} \\ \frac{1}{6} \frac{9}{4} \end{array}$	.438	.452	.465	.478	.491	.505	.518	.531	10.20
	.466	.480	.494	.508	.522	.536	.550	.564	10.84
	.493	.508	.523	.538	.553	.568	.583	.598	11.48
	.520	.536	.552	.568	.584	.599	.615	.631	12.11
$\begin{array}{c} 5 \\ \hline 1 & 6 \\ \hline 2 & 1 \\ \hline 4 \\ \hline 1 \\ \hline 3 & 2 \\ \hline 2 & 3 \\ \hline 4 \\ \end{array}$	.548	.564	.581	.598	.614	.631	.647	.664	12.75
	.575	.593	.610	.628	.645	.662	.680	.697	13.39
	.603	.621	.639	.657	.676	.694	.712	.730	14.03
	.630	.649	.668	.687	.706	.725	.745	.764	14.66
385 254 327 4 327 4	.657 .685 .712 .740	.677 .706 .734 .762	.697 .726 .755 .784	.717 .747 .777 .807	.737 .768 .799 .829	.757 .789 .820 .852	.777 .809 .842 .874	.797 .830 .863 .896	15.30 15.94 16.58 17.21
7 129 645 1321 364	.767 .794 .822 .849	.790 .818 .847 .875	.813 .843 .872 .901	.837 .867 .896 .926	.860 .891 .921 .952	.883 .915 .946 .978	.906 .939 .971 1.00	.930 .963 .996 1.03	17.85 18.49 19.13 19.76
1 2 3644 1323 54 9 16	.877 .904 .931 .959 .986	.903 .931 .960 .988 1.02	.930 .959 .988 1.02 1.05	.956 .986 1.02 1.05 1.08	.983 1.01 1.04 1.07 1.11	1.01 1.04 1.07 1.10 1.14	1.04 1.07 1.10 1.13 1.17	1.06 1.10 1.13 1.16 1.20	20.40 21.04 21.68 22.31 22.95

Thickness in Inches.	41//64	$\frac{2}{3}\frac{1}{2}$	43// 64	11/1	<u>45</u> //64	23// 32//	47/1 64	3//	12"
$\begin{array}{c} \frac{1}{16} \\ \frac{5}{64} \\ \frac{3}{32} \\ \frac{7}{64} \end{array}$	.136	.139	.143	.146	.149	.153	.156	.159	2.53
	.170	.174	.178	.183	.187	.191	.195	.199	3.19
	.204	.209	.214	.219	.224	.229	.234	.239	3.83
	.238	.244	.250	.256	.261	.267	.273	.279	4.46
189	.272	.279	.286	.292	.299	.305	.312	.319	5.10
65	.306	.314	.321	.329	.336	.344	.351	.359	5.74
311	.340	.349	.357	.365	.374	.382	.390	.398	6.38
164	.374	.383	.393	.402	.411	.420	.429	.438	7.01
$\begin{array}{c} 3 \\ \overline{1} \\ \overline{6} \\ \overline{6} \\ \overline{4} \\ \overline{3} \\ \overline{6} \\ \overline{4} \\ \overline{3} \\ \overline{1} \\ \overline{6} \\ \overline{4} \\ \overline{6} \\ \overline{6} \\ \overline{4} \\ \overline{6} \\ \overline{6} \\ \overline{6} \\ \overline{4} \\ \overline{6} $	.408	.418	.428	.438	.448	.458	.468	.478	7.65
	.442	.453	.464	.475	.486	.496	.507	.518	8.29
	.476	.488	.500	.511	.523	.535	.546	.558	8.93
	.510	.523	.535	.548	.560	.573	.585	.598	9.56
$\begin{array}{c} \frac{1}{4} \\ \frac{1}{6} \\ \frac{7}{6} \\ \frac{9}{3} \\ \frac{1}{2} \\ \frac{1}{6} \\ \frac{9}{4} \end{array}$	.545	.558	.571	.584	.598	.611	.624	.638	10.20
	.578	.593	.607	.621	.635	.649	.663	.677	10.84
	.613	.628	.642	.657	.672	.687	.702	.717	11.48
	.647	.662	.678	.694	.710	.725	.741	.757	12.11
5 11261441 22613234	.681 .715 .749 .783	.697 .732 .767 .802	.714 .750 .785 .821	.730 .767 .804 .840	.747 .784 .822 .859	.764 .802 .840 .878	.780 .819 .858 .897	.797 .827 .877 .916	12.75 13.39 14.03 14.66
3]00 5]443]247-14	.817	.837	.857	.877	.896	.916	.936	.956	15.30
	.851	.872	.892	.913	.934	.955	.975	.996	15.94
	.885	.906	.928	.950	.971	.993	1.01	1.04	16.58
	.919	.941	.964	.986	1.01	1.03	1.05	1.08	17.21
7 169455214 2615214	1.02	.976 1.01 1.05 1.08	.999 1.04 1.07 1.11	1.02 1.06 1.10 1.13	1.05 1.08 1.12 1.16	1.07 1.11 1.15 1.18	1.09 1.13 1.17 1.21	1.12 1.16 1.20 1.24	17.85 18.49 19.13 19.76
1023/44/025/49/60	1.19	1.15 1.19 1.22	1.14 1.18 1.21 1.25 1.28	1.17 1.21 1.24 1.28 1.31	1.20 1.23 1.27 1.31 1.34	1.22 1.26 1.30 1.34 1.37	1.25 1.29 1.33 1.37 1.40	1.28 1.31 1.35 1.39 1.43	20.40 21.04 21.68 22.31 22.95

One cubic foot of steel weighs 489.6 pounds. For Thicknesses from  $\frac{3}{16}$  in. to 2 in. and Widths from 1 in. to  $12\frac{3}{4}$  in.

Thickness in Inches.	1''	11/1	1½''	13//	2"	21/1	21/1	2311	12''
$\frac{\frac{3}{16}}{\frac{1}{4}}$	.638 .850	.797 1.06	.957 1.28	1.11 1.49	1.28 1.70		1.59 2.12	1.75 2.34	7.65 10.20
5 16 38 7 16	1.06 1.28 1.49 1.70	1.33 1.59 1.86 2.12	1.59 1.92 2.23 2.55	1.86 2.23 2.60 2.98	2.55 2.98	2.39 2.87 3.35 3.83	2.65 3.19 3.72 4.25	2.92 3.51 4.09 4.67	12.75 15.30 17.85 20.40
9 15 8 11 3 4	1.92 2.12 2.34	2.39 2.65 2.92	2.87 3.19 3.51	3.35 3.72 4.09	3.83 4.25 4.67	4.30 4.78 5.26	4.78 5.31 5.84	5.26 5.84 6.43	22.95 25.50 28.05
	2.55	3.19	3.83	4.47	5.10	5.75	6.38	7.02	30.60
	2.76	3.45	4.14	4.84	5.53	6.21	6.90	7.60	33.15
$ \begin{array}{c} \frac{13}{16} \\ \frac{7}{8} \\ \frac{15}{16} \\ 1 \end{array} $	2.98	3.72	4.47	5.20	5.95	6.69	7.44	8.18	35.70
	3.19	3.99	4.78	5.58	6.38	7.18	7.97	8.77	38.25
	3.40	4.25	5.10	5.95	6.80	7.65	8.50	9.35	40.80
$\begin{array}{c} 1\frac{1}{16} \\ 1\frac{1}{8} \\ 1\frac{3}{16} \\ 1\frac{1}{4} \end{array}$	3.61	4.52	5.42	6.32	7.22	8.13	9.03	9.93	43.35
	3.83	4.78	5.74	6.70	7.65	8.61	9.57	10.52	45.90
	4.04	5.05	6.06	7.07	8.08	9.09	10.10	11.11	48.45
	4.25	5.31	6.38	7.44	8.50	9.57	10.63	11.69	51.00
$\begin{array}{c} 1\frac{5}{16} \\ 1\frac{3}{8} \\ 1\frac{7}{16} \\ 1\frac{1}{2} \end{array}$	4.46	5.58	6.69	7.81	8.93	10.04	11.16	12.27	53.55
	4.67	5.84	7.02	8.18	9.35	10.52	11.69	12.85	56.10
	4.89	6.11	7.34	8.56	9.78	11.00	12.22	13.44	58.65
	5.10	6.38	7.65	8.93	10.20	11.48	12.75	14.03	61.20
$ \begin{array}{c} 1\frac{9}{16} \\ 1\frac{5}{8} \\ 1\frac{1}{16} \\ 1\frac{3}{4} \end{array} $	5.32	6.64	7.97	9.30	10.63	11.95	13.28	14.61	63.75
	5.52	6.90	8.29	9.67	11.05	12.43	13.81	15.19	66.30
	5.74	7.17	8.61	10.04	11.47	12.91	14.34	15.78	68.85
	5.95	7.44	8.93	10.42	11.90	13.40	14.88	16.37	71.40
$egin{array}{cccccccccccccccccccccccccccccccccccc$	6.16	7.70	9.24	10.79	12.33	13.86	15.40	16.95	73.95
	6.38	7.97	9.57	11.15	12.75	14.34	15.94	17.53	76.50
	6.59	8.24	9.88	11.53	13.18	14.83	16.47	18.12	79.05
	6.80	8.50	10.20	11.90	13.60	15.30	17.00	18.70	81.60

Thickness in Inches.	3′′	31/1	31/1	33//	4"	41//	41/1	43//	12"
3 16 4	1.91 2.55	2.07 2.76		2.39 3.19	2.55 3.40	2.71 3.61	2.87 3.83	3.03 4.04	7.65 10.20
5 13 80 17 6 12	3.19 3.83 4.46 5.10	3.45 4.15 4.83 5.53			4.25 5.10 5.95 6.80	4.52 5.42 6.32 7.22	4.78 5.74 6.70 7.65	5.05 6.06 7.07 8.08	12.75 15.30 17.85 20.40
9 16 3 11 16 3 4	5.74 6.38 7.02 7.65	6.22 6.91 7.60 8.29	6.70 7.44 8.18 8.93	7.97 8.76	7.65 8.50 9.35 10.20	8.13 9.03 9.93 10.84	8.61 9.57 10.52 11.48	9.09 10.10 11.11 12.12	22.95 25.50 28.05 30.60
13/56 7/8 15/56 1	8.29 8.93 9.57 10.20		9.67 10.41 11.16 11.90	11.95	11.05 11.90 12.75 13.60	11.74 12.65 13.55 14.45	12.43 13.39 14.34 15.30	13.12 14.13 15.14 16.15	33.15 35.70 38.25 40.80
$ \begin{array}{c} 1\frac{1}{16} \\ 1\frac{8}{8} \\ 1\frac{3}{16} \\ 1\frac{1}{4} \end{array} $	10.84 11.48 12.12 12.75	11.74 12.43 13.12 13.81	13.39 14.13	14.34 15.14	14.45 15.30 16.15 17.00	15.35 16.26 17.16 18.06	16.26 17.22 18.17 19.13	17.16 18.17 19.18 20.19	43.35 45.90 48.45 51.00
1 \frac{5}{1 \frac{5}{1 \frac{5}{5}}} \\ 1 \frac{1}{1 \frac{5}{1 \frac{5}{5}}} \\ 1 \frac{1}{1 \frac{1}{2}} \\ 1 \frac{1}{2}		15.20 15.88		17.53 18.33	17.85 18.70 19.55 20.40	18.96 19.87 20.77 21.68	20.08 21.04 21.99 22.95	21.20 22.21 23.22 24.23	53.55 56.10 58.65 61.20
$ \begin{array}{c} 1 & \frac{9}{160} \\ 1 & \frac{5}{160} \\ 1 & \frac{1}{16} \\ 1 & \frac{3}{4} \end{array} $	16.58	17.27 17.96 18.65 19.34	19.34	20.72 21.51	21.25 22.10 22.95 23.80	22.58 23.48 24.38 25.29	23.91 24.87 25.82 26.78	25.24 26.25 27.26 28.27	63.75 66.30 68.85 71.40
1 1 2 5 6 1 1 1 2 2	19.13 19.77	20.03 20.72 21.41 22.10	22.31 23.06	23.91 24.70	24.65 25.50 26.35 27.20	26.19 27.10 28.00 28.90	27.73 28.69 29.64 30.60	29.27 30.28 31.29 32.30	73.95 76.50 79.05 81.60

Thickness in Inches.	5"	51/1	5½''	53"	6"	61//	6½"	63/1	12′′
$\frac{\frac{3}{16}}{\frac{1}{4}}$	3.19 4.25	3.35 4.46	3.51 4.67	3.67 4.89	3.83 5.10	3.99 5.31	4.14 5.53	4.30 5.74	7.65 10.20
5 13 8 7 6	5.31 6.38 7.44 8.50	5.58 6.69 7.81 8.93	5.84 7.02 8.18 9.35	6.11 7.34 8.56 9.77	6.38 7.65 8.93 10.20	6.64 7.97 9.29 10.63	6.90 8.29 9.67 11.05	7.17 8.61 10.04 11.48	12.75 15.30 17.85 20.40
9 1558 116 34	9.57 10.63 11.69 12.75	10.04 11.16 12.27 13.39	10.52 11.69 12.85 14.03	11.00 12.22 13.44 14.67	11.48 12.75 14.03 15.30	11.95 13.28 14.61 15.94	12.43 13.81 15.20 16.58	12.91 14.34 15.78 17.22	22.95 25.50 28.05 30.60
$\frac{\frac{1}{1}\frac{3}{6}}{\frac{7}{8}}$ $\frac{\frac{1}{1}\frac{5}{6}}{1}$	13.81 14.87 15.94 17.00	14.50 15.62 16.74 17.85	15.19 16.36 17.53 18.70	15.88 17.10 18.33 19.55	16.58 17.85 19.13 20.40	17.27 18.60 19.92 21.25	17.95 19.34 20.72 22.10	18.65 20.08 21.51 22.95	33.15 35.70 38.25 40.80
$ \begin{array}{c} 1\frac{1}{16} \\ 1\frac{1}{8} \\ 1\frac{3}{16} \\ 1\frac{1}{4} \end{array} $	18.06 19.13 20.19 21.25	18.96 20.08 21.20 22.32	19.87 21.04 22.21 23.38	20.77 21.99 23.22 24.44	21.68 22.95 24.23 25.50	23.91 25.23	23.48 24.87 26.24 27.62	24.39 25.82 27.25 28.69	43.35 45.90 48.45 51.00
$ \begin{array}{c} 1\frac{5}{16} \\ 1\frac{3}{8} \\ 1\frac{7}{16} \\ 1\frac{1}{2} \end{array} $	22.32 23.38 24.44 25.50	23.43 24.54 25.66 26.78	24.54 25.71 26.38 28.05	25.66 26.88 28.10 29.33	26.78 28.05 29.33 30.60	27.90 29.22 30.55 31.88	29.01 30.39 31.77 33.15	30.12 31.56 32.99 34.43	53.55 56.10 58.65 61.20
$\begin{array}{c} 1\frac{9}{16} \\ 1\frac{5}{8} \\ 1\frac{11}{6} \\ 1\frac{3}{4} \end{array}$	26.57 27.63 28.69 29.75	29.01 30.12	29.22 30.39 31.55 32.73	30.55 31.77 32.99 34.22	31.88 33.15 34.43 35.70	35.86	34.53 35.91 37.30 38.68	35.86 37.29 38.73 40.17	63.75 66.30 68.85 71.40
$egin{array}{c} 1 rac{1}{1} rac{3}{6} \ 1 rac{7}{8} \ 1 rac{1}{1} rac{5}{6} \ 2 \end{array}$	30.81 31.87 32.94 34.00	34.59	36.23	35.43 36.65 37.88 39.10	36.98 38.25 39.53 40.80		40.05 41.44 42.82 44.20	41.60 43.03 44.46 45.90	73.95 76.50 79.05 81.60

Thickness in Inches.	7"	71/1	71/1	73//	8"	81111	81/1	83//	12′′
$\frac{\frac{3}{16}}{\frac{1}{4}}$	4.46 5.95	4.62 6.16	4.78 6.36	4.94 6.58	5.10 6.80	5.26 7.01	5.42 7.22	5.58 7.43	7.65 10.20
5 13 8 7 1 1 2	7.44 8.93 10.41 11.90	7.70 9.25 10.78 12.32	7.97 9.57 11.16 12.75	8.23 9.88 11.53 13.18	8.50 10.20 11.90 13.60	8.76 10.52 12.27 14.03	9.03 10.84 12.64 14.44	9.29 11.16 13.02 14.87	12.75 15.30 17.85 20.40
$\begin{array}{c} \frac{9}{16} \\ 55 \\ 8 \\ 11 \\ 16 \\ 3 \\ 4 \end{array}$	13.39 14.87 16.36 17.85	13.86 15.40 16.94 18.49	14.34 15.94 17.53 19.13	14.82 16.47 18.12 19.77	15.30 17.00 18.70 20.40	15.78 17.53 19.28 21.04	16.26 18.06 19.86 21.68	16.74 18.59 20.45 22.32	22.95 25.50 28.05 30.60
$\begin{array}{c} \frac{1}{1}\frac{3}{6} \\ \frac{7}{8} \\ \frac{1}{1}\frac{5}{6} \end{array}$	19.34 20.83 22.32 23.80	20.03 21.57 23.11 24.65	20.72 22.32 23.91 25.50	21.41 23.05 24.70 26.35	22.10 23.80 25.50 27.20	22.79 24.55 26.30 28.05	23.48 25.30 27.10 28.90	24.17 26.04 27.89 29.75	33.15 35.70 38.25 40.80
$\begin{array}{c} 1\frac{1}{16} \\ 1\frac{1}{8} \\ 1\frac{3}{16} \\ 1\frac{1}{4} \end{array}$	25.29 26.78 28.26 29.75	26.19 27.73 29.27 30.81	27.10 28.68 30.28 31.88	28.00 29.64 31.29 32.94	28.90 30.60 32.30 34.00	29.80 31.56 33.31 35.06	30.70 32.52 34.32 36.12	31.61 33.47 35.33 37.20	43.35 45.90 48.45 51.00
$ \begin{array}{c} 1\frac{5}{16} \\ 1\frac{3}{8} \\ 1\frac{7}{16} \\ 1\frac{1}{2} \end{array} $	31.23 32.72 34.21 35.70	35.44	33.48 35.06 36.66 38.26	34.59 36.23 37.88 39.53	35.70 37.40 39.10 40.80	38.57 40.32	37.93 39.74 41.54 43.35	39.05 40.91 42.77 44.63	53.55 56.10 58.65 61.20
$1\frac{9}{16}$ $1\frac{5}{8}$ $1\frac{11}{6}$ $1\frac{3}{4}$	37.19 38.67 40.16 41.65	40.05 41.59	43.03	42.82	42.50 44.20 45.90 47.60	45.58 47.33	46.96 48.76	46.49 48.34 50.20 52.07	63.75 66.30 68.85 71.40
$\begin{array}{c} 1\frac{1}{1}\frac{3}{6} \\ 1\frac{7}{8} \\ 1\frac{15}{16} \\ 2 \end{array}$	43.14 44.63 46.12 47.60	46.22 47.76	47.82 49.41	49.40 51.05	49.30 51.00 52.70 54.40	52.60 54.35	54.20	53.92 55.79 57.64 59.50	73.95 76.50 79.05 81.60

Thickness in Inches.	9"	91111	91/1	93//	10"	101/1	101/1	103/1	12"
$\frac{\frac{3}{16}}{\frac{1}{4}}$	5.74	5.90	6.06	6.22	6.38	6.54	6.70	6.86	7.65
	7.65	7.86	8.08	8.29	8.50	8.71	8.92	9.14	10.20
5 13 3 7 16 12	9.56 11.48 13.40 15.30	9.83 11.80 13.76 15.73	10.10 12.12 14.14 16.16	10.36 12.44 14.51 16.58	10.62 12.75 14.88 17.00	10.89 13.07 15.25 17.42	11.16 13.39 15.62 17.85	11.42 13.71 15.99 18.28	12.75 15.30 17.85 20.40
$\frac{9}{156}$ $\frac{5}{8}$ $\frac{11}{16}$ $\frac{3}{4}$	17.22	17.69	18.18	18.65	19.14	19.61	20.08	20.56	22.95
	19.13	19.65	20.19	20.72	21.25	21.78	22.32	22.85	25.50
	21.04	21.62	22.21	22.79	23.38	23.96	24.54	25.13	28.05
	22.96	23.59	24.23	24.86	25.50	26.14	26.78	27.42	30.60
$\frac{\frac{1}{1}\frac{3}{6}}{\frac{7}{8}}$ $\frac{\frac{1}{5}}{1}\frac{5}{6}$	24.86	25.55	26.24	26.94	27.62	28.32	29.00	29.69	33.15
	26.78	27.52	28.26	29.01	29.75	30.50	31.24	31.98	35.70
	28.69	29.49	30.28	31.08	31.88	32.67	33.48	34.28	38.25
	30.60	31.45	32.30	33.15	34.00	34.85	35.70	36.55	40.80
$\begin{array}{c} 1\frac{1}{16} \\ 1\frac{1}{8} \\ 1\frac{3}{16} \\ 1\frac{1}{4} \end{array}$	32.52	33.41	34.32	35.22	36.12	37.03	37.92	38.83	43.35
	34.43	35.38	36.34	37.29	38.25	39.21	40.17	41.12	45.90
	36.34	37.35	38.36	39.37	40.38	41.39	42.40	43.40	48.45
	38.26	39.31	40.37	41.44	42.50	43.56	44.63	45.69	51.00
$\begin{array}{c} 1\frac{5}{16} \\ 1\frac{3}{8} \\ 1\frac{7}{16} \\ 1\frac{1}{2} \end{array}$	40.16	41.28	42.40	43.52	44.64	45.75	46.86	47.97	53.55
	42.08	43.25	44.41	45.58	46.75	47.92	49.08	50.25	56.10
	44.00	45.22	46.44	47.66	48.88	50.10	51.32	52.54	58.65
	45.90	47.18	48.45	49.73	51.00	52.28	53.55	54.83	61.20
$\begin{array}{c} 1\frac{9}{16} \\ 1\frac{5}{8} \\ 1\frac{11}{6} \\ 1\frac{3}{4} \end{array}$	47.82	49.14	50.48	51.80	53.14	54.46	55.78	57.11	63.75
	49.73	51.10	52.49	53.87	55.25	56.63	58.02	59.40	66.30
	51.64	53.07	54.51	55.94	57.38	58.81	60.24	61.68	68.85
	53.56	55.04	56.53	58.01	59.50	60.99	62.48	63.97	71.40
$\begin{array}{c} 1\frac{1}{1}\frac{3}{6} \\ 1\frac{7}{8} \\ 1\frac{1}{1}\frac{5}{6} \\ 2 \end{array}$	55.46	57.00	58.54	60.09	61.62	63.17	64.70	66.24	73.95
	57.38	58.97	60.56	62.16	63.75	65.35	66.94	68.53	76.50
	59.29	60.94	62.58	64.23	65.88	67.52	69.18	70.83	79.05
	61.20	62.90	64.60	66.30	68.00	69.70	71.40	73.10	81.60

(CONCLUDED.)

Thickness in Inches.	11′′	1114''	$11\frac{1}{2}''$	113//	12′′	$12rac{1}{4}^{\prime\prime}$	$12rac{1}{2}^{\prime\prime}$	1237	1
$\frac{\frac{3}{16}}{\frac{1}{4}}$	7.02 9.34	7.17 9.57	7.32 9.78	7.49 10.00	7.65 10.20	7.82 10.42	7.98 10.63	8.13 10.84	
$\begin{array}{r} \frac{5}{16} \\ \frac{3}{8} \\ \frac{7}{16} \\ \frac{1}{2} \end{array}$	11.68 14.03 16.36 18.70	11.95 14.35 16.74 19.13	12.22 14.68 17.12 19.55	12.49 14.99 17.49 19.97	12.75 15.30 17.85 20.40	13.01 15.62 18.23 20.82	13.28 15.94 18.60 21.25	13.55 16.26 18.97 21.67	1 10.0
$\frac{9}{16}$ $\frac{5}{8}$ $\frac{11}{16}$ $\frac{3}{4}$	21.02 23.38 25.70 28.05	21.51 23.91 26.30 28.68	22.00 24.44 26.88 29.33	22.48 24.97 27.47 29.97	22.95 25.50 28.05 30.60	23.43 26.03 28.64 31.25	23.90 26.56 29.22 31.88	24.39 27.09 29.80 32.52	1
$ \begin{array}{c} \frac{13}{16} \\ \frac{7}{8} \\ \frac{15}{16} \end{array} $	30.40 32.72 35.06 37.40	31.08 33.47 35.86 38.25	31.76 34.21 36.66 39.10	32.46 34.95 37.46 39.95	33.15 35.70 38.25 40.80	33.83 36.44 39.05 41.65	34.53 37.19 39.84 42.50	35.22 37.93 40.64 43.35	
$ \begin{array}{c} 1\frac{1}{16} \\ 1\frac{1}{8} \\ 1\frac{3}{16} \\ 1\frac{1}{4} \end{array} $	39.74 42.08 44.42 46.76	40.64 43.04 45.42 47.82	41.54 44.00 46.44 48.88	42.45 44.94 47.45 49.94	43.35 45.90 48.45 51.00	44.25 46.86 49.46 52.06	45.16 47.82 50.46 53.12	46.06 48.77 51.48 54.19	
$\begin{array}{c} 1\frac{5}{16} \\ 1\frac{3}{8} \\ 1\frac{7}{16} \\ 1\frac{1}{2} \end{array}$	49.08 51.42 53.76 56.10	50.20 52.59 54.99 57.37	51.32 53.76 56.21 58.65	52.44 54.93 57.43 59.93	53.55 56.10 58.65 61.20		55.78 58.44 61.10 63.75	56.90 59.60 62.32 65.03	
$\begin{array}{c} 1\frac{9}{16} \\ 1\frac{5}{8} \\ 1\frac{1}{16} \\ 1\frac{3}{4} \end{array}$	58.42 60.78 63.10 65.45	59.76 62.16 64.55 66.93	61.10 63.54 65.98 68.43	62.43 64.92 67.42 69.92	63.75 66.30 68.85 71.40	65.08 67.68 70.29 72.90	66.40 69.06 71.72 74.38	67.74 70.44 73.15 75.87	14. 6 101.
$ \begin{array}{c} 1\frac{13}{16} \\ 1\frac{7}{8} \\ 1\frac{15}{16} \\ 2 \end{array} $	67.80 70.12 72.46 74.80	74.11	70.86 73.31 75.76 78.20	74.90 77.41	73.95 76.50 79.05 81.60	75.48 78.09 80.70 83.30	82.34	78.57 81.28 83.99 86.70	The

The weights for 12" width are repeated on each page to facilitate making the additions necessary to obtain the weights of plates of any width greater than 12". Thus, to find the weight of  $1542'' \times 78''$ , add the weights to be found in the same line for  $342 \times 78$  and  $12 \times 78 = 10.41 + 35.70 = 46.11$  pounds. Weight of plate  $4' 642'' \times 68'' = 4 \times 25.50 + 13.81 = 115.81$  pounds.

For Diameters from  $\frac{1}{10}$  to 100, advancing by Tenths.

	Tot Diameters from 10 to 199, was already								
Diameter.	Area.	Circumferenco.	Diameter.	Area.	Circumference.				
0.0 .1 .2 .3 .4	.007854 .031416 .070686 .12566	.31416 .62832 .94248 1.2566	4.0 .1 .2 .3 .4	12.5664 13.2025 13.8544 14.5220 15.2053	12.5664 12.8805 13.1947 13.5088 13.8230				
.5 .6 .7 .8	.19635 .28274 .38485 .50266 .63617	1.5708 1.8850 2.1991 2.5133 2.8274	.5 .6 .7 .8	15.9043 16.6190 17.3494 18.0956 18.8574	14.1372 14.4513 14.7655 15.0796 15.3938				
1.0 .1 .2 .3 .4	.7854 .9503 1.1310 1.3273 1.5394	3.1416 3.4558 3.7699 4.0841 4.3982	5.0 .1 .2 .3 .4	19.6350 20.4282 21.2372 22.0618 22.9022	15.7080 16.0221 16.3363 16.6504 16.9646				
.5 .6 .7 .8	1.7671 2.0106 2.2698 2.5447 2.8353	4.7124 5.0265 5.3407 5.6549 5.9690	.5 .6 .7 .8	23.7583 24.6301 25.5176 26.4208 27.3397	17.2788 17.5929 17.9071 18.2212 18.5354				
2.0 .1 .2 .3 .4	3.1416 3.4636 3.8013 4.1548 4.5239	6.2832 6.5973 6.9115 7.2257 7.5398	6.0 .1 .2 .3 .4	28.2743 29.2247 30.1907 31.1725 32.1699	18.8496 19.1637 19.4779 19.7920 20.1062				
.5 .6 .7 .8	4.9087 5.3093 5.7256 6.1575 6.6052	7.8540 8.1681 8.4823 8.7965 9.1106	.5 .6 .7 .8	33.1831 34.2119 35.2565 36.3168 37.3928	20.4204 20.7345 21.0487 21.3628 21.6770				
3.0 .1 .2 .3 .4	7.0686 7.5477 8.0425 8.5530 9.0792	9.4248 9.7389 10.0531 10.3673 10.6814	7.0 .1 .2 .3 .4	38.4845 39.5919 40.7150 41.8539 43.0084	21.9911 22.3053 22.6195 22.9336 23.2478				
.5 .6 .7 .8	9.6211 10.1788 10.7521 11.3411 11.9459	10.9956 11.3097 11.6239 11.9381 12.2522	.5 .6 .7 .8	44.1786 45.3646 46.5663 47.7836 49.0167	23.5619 23.8761 24.1903 24.5044 24.8186				

Diameter.	Area.	Circumference.	Diameter.	Area.	Circumference.
8.0 .1 .2 .3	50.2655 51.5300 52.8102 54.1061 55.4177	25.1327 25.4469 25.7611 26.0752 26.3894	12.0 .1 .2 .3 .4	113.0973 114.9901 116.8987 118.8229 120.7628	37.6991 38.0133 38.3274 38.6416 38.9557
.5 .6 .7 .8	56.7450 58.0880 59.4468 60.8212 62.2114	26.7035 27.0177 27.3319 27.6460 27.9602	.5 .6 .7 .8	122.7185 124.6898 126.6769 128.6796 130.6981	39.2699 39.5841 39.8982 40.2124 40.5265
9.0 .1 .2 .3 .4	63.6173 65.0388 66.4761 67.9291 69.3978	28.2743 28.5885 28.9027 29.2168 29.5310	13.0 .1 .2 .3 .4	132.7323 134.7822 136.8478 138.9291 141.0261	40.8407 41.1549 41.4690 41.7832 42.0973
.5 .6 .7 .8	70.8822 72.3823 73.8981 75.4296 76.9769	29.8451 30.1593 30.4734 30.7876 31.1018	.5 .6 .7 .8	143.1388 145.2672 147.4114 149.5712 151.7468	42.4115 42.7257 43.0398 43.3540 43.6681
10.0 .1 .2 .3 .4	78.5398 80.1185 81.7128 83.3229 84.9487	31.4159 31.7301 32.0442 32.3584 32.6726	14.0 .1 .2 .3 .4	153.9380 156.1450 158.3677 160.6061 162.8602	43.9823 44.2965 44.6106 44.9248 45.2389
.5 .6 .7 .8	86.5901 88.2473 89.9202 91.6088 93.3132	32.9867 33.3009 33.6150 33.9292 34.2434	.5 .6 .7 .8	165.1300 167.4155 169.7167 172.0336 174.3662	45.5531 45.8673 46.1814 46.4956 46.8097
11.0 .1 .2 .3 .4	95.0332 96.7689 98.5203 100.2875 102.0703	34.5575 34.8717 35.1858 35.5000 35.8142	15.0 .1 .2 .3 .4	176.7146 179.0786 181.4584 183.8539 186.2650	47.1239 47.4380 47.7522 48.0664 48.3805
.5 .6 .7 .8	103.8689 105.6832 107.5132 109.3588 111.2202	36.1283 36.4425 36.7566 37.0708 37.3850	.5 .6 .7 .8	188.6919 191.1345 193.5928 196.0668 198.5565	48.6947 49.0088 49.3230 49.6372 49.9513

Diameter.	Area.	Circumference.	Diameter.	Area.	Circumference.
16.0 .1 .2 .3 .4	201.0619 203.5831 206.1199 208.6724 211.2407	50.2655 50.5796 50.8938 51.2080 51.5221	20.0 .1 .2 .3 .4	314.1593 317.3087 320.4739 323.6547 326.8513	62.8319 63.1460 63.4602 63.7743 64.0885
.5 .6 .7 .8	213.8246 216.4243 219.0397 221.6708 224.3176	51.8363 52.1504 52.4646 52.7788 53.0929	.5 .6 .7 .8	330.0636 333.2916 336.5353 339.7947 343.0698	64.4026 64.7168 65.0310 65.3451 65.6593
17.0 .1 .2 .3 .4	226.9801 229.6583 232.3522 235.0618 237.7871	53.4071 53.7212 54.0354 54.3496 54.6637	21.0 .1 .2 .3 .4	346.3606 349.6671 352.9894 356.3273 359.6809	65.9734 66.2876 66.6018 66.9159 67.2301
.5 .6 .7 .8	240.5282 243.2849 246.0574 248.8456 251.6494	54.9779 55.2920 55.6062 55.9203 56.2345	.5 .6 .7 .8	363.0503 366.4354 369.8361 373.2526 376.6848	67.5442 67.8584 68.1726 68.4867 68.8009
18.0 .1 .2 .3 .4	254.4690 257.3043 260.1553 263.0220 265.9044	56.5486 56.8628 57.1770 57.4911 57.8053	22.0 .1 .2 .3 .4	380.1327 383.5963 387.0756 390.5707 394.0814	69.1150 69.4292 69.7434 70.0575 70.3717
.5 .6 .7 .8	268.8025 271.7164 274.6459 277.5911 280.5521	58.1195 58.4336 58.7478 59.0619 59.3761	.5 .6 .7 .8 .9	397.6078 401.1500 404.7078 408.2814 411.8707	70.6858 71.0000 71.3142 71.6283 71.9425
19.0 .1 .2 .3 .4	283.5287 286.5211 289.5292 292.5530 295.5925	59.6903 60.0044 60.3186 60.6327 60.9469	23.0 .1 .2 .3 .4	415.4756 419.0963 422.7327 426.3848 430.0526	72.2566 72.5708 72.8849 73.1991 73.5133
.5 .6 .7 .8	298.6477 301.7186 304.8052 307.9075 311.0255	61.2611 61.5752 61.8894 62.2035 62.5177	.5 .6 .7 .8	433.7361 437.4354 441.1503 444.8809 448.6273	73.8274 74.1416 74.4557 74.7699 75.0841

Diameter.	Area.	Circumference.	Diameter.	Area.	Circumference.
24.0 .1 .2 .3 .4	452.3893 456.1671 459.9606 463.7698 467.5947	75.3982 75.7124 76.0265 76.3407 76.6549	28.0 .1 .2 .3 .4	615.7522 620.1582 624.5800 629.0175 633.4707	87.9646 88.2788 88.5929 88.9071 89.2212
.5 .6 .7 .8	471.4352 475.2916 479.1636 483.0513 486.9547	76.9690 77.2832 77.5973 77.9115 78.2257	.5 .6 .7 .8	637.9397 642.4243 646.9246 651.4407 655.9724	89,5354 89,8495 90,1637 90,4779 90,7920
25.0 .1 .2 .3 .4	490.8739 494.8087 498.7592 502.7255 506.7075	78.5398 78.8540 79.1681 79.4823 79.7965	29.0 .1 .2 .3	660.5199 665.0830 669.6619 674.2565 678.8668	91.1062 91.4203 91.7345 92.0487 92.3628
.5 .6 .7 .8	510.7052 514.7185 518.7476 522.7924 526.8529	80.1106 80.4248 80.7389 81.0531 81.3672	.5 .6 .7 .8	683.4928 688.1345 692.7919 697.4650 702.1538	92.6770 92.9911 93.3053 93.6195 93.9336
26.0 .1 .2 .3 .4	530.9292 535.0211 539.1287 543.2521 547.3911	81.6814 81.9956 82.3097 82.6239 82.9380	30.0 .1 .2 .3 .4	706.8583 711.5786 716.3145 721.0662 725.8336	94.2478 94.5619 94.8761 95.1903 95.5044
.5 .6 .7 .8	551.5459 555.7163 559.9025 564.1044 568.3220	83.2522 83.5664 83.8805 84.1947 84.5088	.5 .6 .7 .8	730.6167 735.4154 740.2299 745.0601 749.9060	95.8186 96.1327 96.4469 96.7611 97.0752
27.0 .1 .2 .3 .4	572.5553 576.8043 581.0690 585.3494 589.6455	84.8230 85.1372 85.4513 85.7655 86.0796	31.0 .1 .2 .3 .4	754.7676 759.6450 764.5380 769.4467 774.3712	97.3894 97.7035 98.0177 98.3319 98.6460
.5 .6 .7 .8	593.9574 598.2849 602.6282 606.9871 611.3618	86.3938 86.7080 87.0221 87.3363 87.6504	.5 .6 .7 .8	779.3113 784.2672 789.2388 794.2260 799.2290	98.9602 99.2743 99.5885 99.9026 100.2168

Diameter.	Area.	Circumference.	Diameter.	Area.	Circumference.
32.0 .1 .2 .3 .4	804.2477 809.2821 814.3322 819.3980 824.4796	100.5310 100.8451 101.1593 101.4734 101.7876	36.0 .1 .2 .3 .4	1017.8760 1023.5387 1029.2172 1034.9113 1040.6212	113.0973 113.4115 113.7257 114.0398 114.3540
.5 .6 .7 .8	829.5768 834.6898 839.8185 844.9628 850.1229	102.1018 102.4159 102.7301 103.0442 103.3584	.5 .6 .7 .8	1046.3467 1052.0880 1057.8449 1063.6176 1069.4060	114.6681 114.9823 115.2965 115.6106 115.9248
33.0 .1 .2 .3 .4	855.2986 860.4902 865.6973 870.9202 876.1588	103.6726 103.9867 104.3009 104.6150 104.9292	37.0 .1 .2 .3 .4	1075.2101 1081.0299 1086.8654 1092.7166 1098.5835	116.2389 116.5531 116.8672 117.1814 117.4956
.5 .6 .7 .8	881.4131 886.6831 891.9688 897.2703 902.5874	105.2434 105.5575 105.8717 106.1858 106.5000	.5 .6 .7 .8	1104.4662 1110.3645 1116.2786 1122.2083 1128.1538	117.8097 118.1239 118.4380 118.7522 119.0664
34.0 .1 .2 .3 .4	907.9203 913.2688 918.6331 924.0131 929.4088	106.8142 107.1283 107.4425 107.7566 108.0708	38.0 .1 .2 .3 .4	1134.1149 1140.0918 1146.0844 1152.0927 1158.1167	119.3805 119.6947 120.0088 120.3230 120.6372
.5 .6 .7 .8 .9	934.8202 940.2473 945.6901 951.1486 956.6228	108.3849 108.6991 109.0133 109.3274 109.6416	.5 .6 .7 .8	1164.1564 1170.2118 1176.2830 1182.3698 1188.4724	120.9513 121.2655 121.5796 121.8938 122.2080
35.0 .1 .2 .3 .4	962.1128 967.6184 973.1397 978.6768 984.2296	109.9557 110.2699 110.5841 110.8982 111.2124	39.0 .1 .2 .3 .4	1194.5906 1200.7246 1206.8742 1213.0396 1219.2207	122.5221 122.8363 123.1504 123.4646 123.7788
.5 .6 .7 .8	989.7980 995.3822 1000.9821 1006.5977 1012.2290	111.5265 111.8407 112.1549 112.4690 112.7832	.5 .6 .7 .8	1225.4175 1231.6300 1237.8582 1244.1021 1250.3617	124.0929 124.4071 124.7212 125.0354 125.3495

Diameter.	Area.	Circumference.	Diameter.	Area.	Circumference.
40.0 .1 .2 .3 .4	1256.6371 1262.9281 1269.2348 1275.5573 1281.8955	125.6637 125.9779 126.2920 126.6062 126.9203	44.0 .1 .2 .3 .4	1520.5308 1527.4502 1534.3853 1541.3360 1548.3025	138.2301 138.5442 138.8584 139.1726 139.4867
.5 .6 .7 .8	1288.2493 1294.6189 1301.0042 1307.4052 1313.8219	127.2345 127.5487 127.8628 128.1770 128.4911	.5 .6 .7 .8	1555.2847 1562.2826 1569.2962 1576.3255 1583.3706	139.8009 140.1153 140.4292 140.7434 141.0575
41.0 .1 .2 .3 .4	1320.2543 1326.7024 1333.1663 1339.6458 1346.1410	128.8053 129.1195 129.4336 129.7478 130.0619	45.0 .1 .2 .3 .4	1590.4313 1597.5077 1604.5999 1611.7077 1618.8313	141.3717 141.6858 142.0000 142.3142 142.6283
.5 .6 .7 .8	1352.6520 1359.1786 1365.7210 1372.2791 1378.8529	130.3761 130.6903 131.0044 131.3186 131.6327	.5 .6 .7 .8	1625.9705 1633.1255 1640.2962 1647.4826 1654.6847	142.9425 143.2566 143.5708 143.8849 144.1991
42.0 .1 .2 .3 .4	1385.4424 1392.0476 1398.6685 1405.3051 1411.9574	131.9469 132.2611 132.5752 132.8894 133.2035	46.0 .1 .2 .3 .4	1661.9025 1669.1360 1676.3853 1683.6502 1690.9308	144.5133 144.8274 145.1416 145.4557 145.7699
.5 .6 .7 .8	1418.6254 1425.3092 1432.0086 1438.7238 1445.4546	133.5177 133.8318 134.1460 134.4602 134.7743	.5 .6 .7 .8	1698.2272 1705.5392 1712.8670 1720.2105 1727.5697	146.0841 146.3982 146.7124 147.0265 147.3407
43.0 .1 .2 .3 .4	1452.2012 1458.9635 1465.7415 1472.5352 1479.3446	135.0885 135.4026 135.7168 136.0310 136.3451	47.0 .1 .2 .3 .4	1734.9445 1742.3351 1749.7414 1757.1635 1764.6012	147.6550 147.9690 148.2832 148.5973 148.9115
.5 .6 .7 .8	1486.1697 1493.0105 1499.8670 1506.7393 1513.6272	136.6593 136.9734 137.2876 137.6018 137.9159	.5 .6 .7 .8	1772.0546 1779.5237 1787.0086 1794.5091 1802.0254	149.2257 149.5398 149.8540 150.1681 150.4823

Diameter.	Area.	Circumference.	Diameter.	Area.	Circumference.
48.0 .1 .2 .3 .4	1809.5574 1817.1050 1824.6684 1832.2475 1839.8423	150.7964 151.1106 151.4248 151.7389 152.0531	52.0 .1 .2 .3 .4	2123.7166 2131.8926 2140.0843 2148.2917 2156.5149	163.3628 163.6770 163.9911 164.3053 164.6195
.5 .6 .7 .8	1847.4528 1855.0790 1862.7210 1870.3786 1878.0519	152.3672 152.6814 152.9956 153.3097 153.6239	.5 .6 .7 .8	2164.7537 2173.0082 2181.2785 2189.5644 2197.8661	164.9336 165.2479 165.5619 165.8761 166.1903
49.0 .1 .2 .3 .4	1885.7409 1893.4457 1901.1662 1908.9024 1916.6543	153.9380 154.2522 154.5664 154.8805 155.1947	53.0 .1 .2 .3 .4	2206.1834 2214.5165 2222.8653 2231.2298 2239.6100	166.5044 166.8186 167.1327 167.4469 167.7610
.5 .6 .7 .8	1924.4218 1932.2051 1940.0042 1947.8189 1955.6493	155.5088 155.8230 156.1372 156.4513 156.7655	.5 .6 .7 .8	2248.0059 2256.4175 2264.8448 2273.2879 2281.7466	168.0752 168.3894 168.7035 169.0177 169.3318
50.0 .1 .2 .3 .4	1963.4954 1971.3572 1979.2348 1987.1280 1995.0370	157.0796 157.3938 157.7080 158.0221 158.3363	54.0 .1 .2 .3 .4	2290.2210 2298.7112 2307.2171 2315.7386 2324.2759	169.6460 169.9602 170.2743 170.5885 170.9026
.5 .6 .7 .8	2002.9617 2010.9020 2018.8581 2026.8299 2034.8174	158.6504 158.9646 159.2787 159.5929 159.9071	.5 .6 .7 .8	2332.8289 2341.3976 2349.9820 2358.5821 2367.1979	171.2168 171.5310 171.8451 172.1593 172.4735
51.0 .1 .2 .3 .4	2042.8206 2050.8395 2058.8742 2066.9245 2074.9905	160.2212 160.5354 160.8495 161.1637 161.4779	55.0 .1 .2 .3 .4	2375.8294 2384.4767 2393.1396 2401.8183 2410.5126	172.7876 173.1017 173.4159 173.7301 174.0442
.5 .6 .7 .8	2083.0723 2091.1697 2099.2829 2107.4118 2115.5563	161.7920 162.1062 162.4203 162.7345 163.0487	.5 .6 .7 .8	2419.2227 2427.9485 2436.6899 2445.4471 2454.2200	174.3584 174.6726 174.9867 175.3009 175.6150

Diameter,	Area.	Circumference.	Diameter.	Area.	Circumference.
56.0 .1 .2 .3 .4	2463.0086 2471.8130 2480.6330 2489.4687 2498.3201	175.9292 176.2433 176.5575 176.8717 177.1858	60.0 .1 .2 .3 .4	2827.4334 2836.8660 2846.3144 2855.7784 2865.2582	188.4956 188.8097 189.1239 189.4380 189.7522
.5 .6 .7 .8	2507.1873 2516.0701 2524.9687 2533.8830 2542.8129	177.5000 177.8141 178.1283 178.4425 178.7566	.5 .6 .7 .8	2874.7536 2884.2648 2893.7917 2903.3343 2912.8926	190.0664 190.3805 190.6947 191.0088 191.3230
57.0 .1 .2 .3	2551.7586 2560.7200 2569.6971 2578.6899 2587.6985	179,0708 179,3849 179,6991 180,0133 180,3274	61.0 .1 .2 .3 .4	2922.4666 2932.0563 2941.6617 2951.2828 2960.9197	191.6372 191.9513 192.2655 192.5796 192.8938
.5 .6 .7 .8 .9	2596.7227 2605.7626 2614.8183 2623.8896 2632.9767	180.6416 180.9557 181.2699 181.5841 181.8982	.5 .6 .7 .8	2970.5722 2980.2405 2989.9244 2999.6241 3009.3395	193.2079 193.5221 193.8363 194.1504 194.4646
58.0 .1 .2 .3 .4	2642.0794 2651.1979 2660.3321 2669.4820 2678.6476	182.2124 182.5265 182.8407 183.1549 183.4690	62.0 .1 .2 .3 .4	3019.0705 3028.8173 3038.5798 3048.3580 3058.1520	194.7787 195.0929 195.4071 195.7212 196.0354
.5 .6 .7 .8	2687.8289 2697.0259 2706.2386 2715.4670 2724.7112	183,7832 184,0973 184,4115 184,7256 185,0398	.5 .6 .7 .8	3067.9616 3077.7869 3087.6279 3097.4847 3107.3571	196.3495 196.6637 196.9779 197.2920 197.6062
59.0 .1 .2 .3	2733.9710 2743.2466 2752.5378 2761.8448 2771.1675	185.3540 185.6681 185.9823 186.2964 186.6106	63.0 .1 .2 .3 .4	3117.2453 3127.1492 3137.0688 3147.0040 3156.9550	197.9203 198.2345 198.5487 198.8628 199.1770
.5 .6 .7 .8	2780.5058 2789.8599 2799.2297 2808.6152 2818.0165	186.9248 187.2389 187.5531 187.8672 188.1814	.5 .6 .7 .8	3166.9217 3176.9043 3186.9023 3196.9161 3206.9456	199.4911 199.8053 200.1195 200.4336 200.7478

Diameter.	Area.	Circumference.	Diameter.	Area.	Circumference.
64.0 .1 .2 .3	3216.9909 3227.0518 3237.1285 3247.2222 3257.3289	201.0620 201.3761 201.6902 202.0044 202.3186	68.0 .1 .2 .3 .4	3631.6811 3642.3704 3653.0754 3663.7960 3674.5324	213.6283 213.9425 214.2566 214.5708 214.8849
.5 .6 .7 .8 .9	3267.4527 3277.5922 3287.7474 3297.9183 3308.1049	202.6327 202.9469 203.2610 203.5752 203.8894	.5 .6 .7 .8	3685,2845 3696,0523 3706,8359 3717,6351 3728,4500	215.1991 215.5133 215.8274 216.1416 216.4556
65.0 .1 .2 .3 .4	3318.3072 3328.5253 3338.7590 3349.0085 3359.2736	204.2035 204.5176 204.8318 205.1460 205.4602	69.0 .1 .2 .3 .4	3739.2807 3750.1270 3760.9891 3771.8668 3782.7603	216.7699 217.0841 217.3982 217.7124 218.0265
.5 .6 .7 .8	3369.5545 3379.8510 3390.1633 3400.4913 3410.8350	205.7743 206.0885 206.4026 206.7168 207.0310	.5 .6 .7 .8	3793.6695 3804.5944 3815.5350 3826.4913 3837.4633	218.3407 218.6548 218.9690 219.2832 219.5973
66.0 .1 .2 .3 .4	3421.1944 3431.5695 3441.9603 3452.3669 3462.7891	207.3451 207.6593 207.9734 208.2876 208.6017	70.0 .1 .2 .3 .4	3848.4510 3859.4544 3870.4736 3881.5084 3892.5590	219.9115 220.2256 220.5398 220.8540 221.1681
.5 .6 .7 .8	3473.2270 3483.6807 3494.1500 3504.6351 3515.1359	208.9159 209.2301 209.5442 209.8584 210.1725	.5 .6 .7 .8 .9	3903.6252 3914.7072 3925.8049 3936.9182 3948.0473	221.4823 221.7964 222.1106 222.4248 222.7389
67.0 .1 .2 .3 .4	3525.6524 3536.1845 3546.7324 3557.2960 3567.8754	210.4867 210.8009 211.1150 211.4292 211.7433	71.0 .1 .2 .3 .4	3959.1921 3970.3526 3981.5289 3992.7208 4003.9284	223.0531 223.3672 223.6814 223.9956 224.3097
.5 .6 .7 .8	3578.4704 3589.0811 3599.7075 3610.3497 3621.0075	212.0575 212.3717 212.6858 213.0000 213.3141	.5 .6 .7 .8	4015.1518 4026.3908 4037.6456 4048.9160 4060.2022	224.6239 224.9380 225.2522 225.5664 225.8805

Diameter.	Area.	Circumference.	Diameter.	Area.	Circumference.
72.0 .1 .2 .3 .4	4071.5041 4082.8217 4094.1550 4105.5040 4116.8687	226.1947 226.5088 226.8230 227.1371 227.4513	76.0 .1 .2 .3 .4	4536.4598 4548.4057 4560.3673 4572.3446 4584.3377	238.7610 239.0752 239.3894 239.7035 240.0177
.5 .6 .7 .8	4128.2491 4139.6452 4151.0571 4162.4846 4173.9279	227.7655 228.0796 228.3938 228.7079 229.0221	.5 .6 .7 .8	4596.3464 4608.3708 4620.4110 4632.4669 4644.5384	240.3318 240.6460 240.9602 241.2743 241.5885
73.0 .1 .2 .3 .4	4185.3868 4196.8615 4208.3519 4219.8579 4231.3797	229.3363 229.6504 229.9646 230.2787 230.5929	77.0 .1 .2 .3 .4	4656.6257 4668.7287 4680.8474 4692.9818 4705.1319	241.9026 242.2168 242.5310 242.8451 243.1592
.5 .6 .7 .8	4242.9172 4254.4704 4266.0394 4277.6240 4289.2243	230.9071 231.2212 231.5354 231.8495 232.1637	.5 .6 .7 .8	4717.2977 4729.4792 4741.6765 4753.8894 4766.1181	243.4734 243.7876 244.1017 244.4159 244.7301
74.0 .1 .2 .3 .4	4300.8403 4312.4721 4324.1195 4335.7827 4347.4616	232.4779 232.7920 233.1062 233.4203 233.7345	78.0 .1 .2 .3 .4	4778.3624 4790.6225 4802.8983 4815.1897 4827.4969	245.0442 245.3584 245.6725 245.9867 246.3009
.5 .6 .7 .8	4359,1562 4370,8664 4382,5924 4394,3341 4406,0916	234.0487 234.3628 234.6770 234.9911 235.3053	.5 .6 .7 .8	4839.8198 4852.1584 4864.5128 4876.8828 4889.2685	246.6150 246.9292 247.2433 247.5575 247.8717
75.0 .1 .2 .3 .4	4417.8647 4429.6535 4441.4580 4453.2783 4465.1142	235.6194 235.9336 236.2478 236.5619 236.8761	79.0 .1 .2 .3 .4	4901.6699 4914.0871 4926.5199 4938.9685 4951.4328	248.1858 248.5000 248.8141 249.1283 249.4425
.5 .6 .7 .8	4476.9659 4488.8332 4500.7163 4512.6151 4524.5296	237.1902 237.5044 237.8186 238.1327 238.4469	.5 .6 .7 .8	4963.9127 4976.4084 4988.9198 5001.4469 5013.9897	249.7566 250.0708 250.3850 250.6991 251.0133

Diameter.	Area.	Circumference.	Diameter.	Area.	Circumference.
80.0 .1 .2 .3 .4	5026.5482 5039.1225 5051.7124 5064.3180 5076.9394	251.3274 251.6416 251.9557 252.2699 252.5840	84.0 .1 .2 .3 .4	5541.7694 5554.9720 5568.1902 5581.4242 5594.6739	263.8938 264.2079 264.5221 264.8363 265.1514
.5 .6 .7 .8	5089.5764 5102.2292 5114.8977 5127.5819 5140.2818	252.8982 253.2124 253.5265 253.8407 254.1548	.5 .6 .7 .8	5607.9392 5621.2203 5634.5171 5647.8296 5661.1578	265.4646 265.7787 266.0929 266.4071 266.7212
81.0 .1 .2 .3 .4	5152.9973 5165.7287 5178.4757 5191.2384 5204.0168	254.4690 254.7832 255.0973 255.4115 255.7256	85.0 .1 .2 .3 .4	5674.5017 5687.8614 5701.2367 5714.6277 5728.0345	267.0354 267.3495 267.6637 267.9779 268.2920
.5 .6 .7 .8	5216.8110 5229.6208 5242.4463 5255.2876 5268.1446	256.0398 256.3540 256.6681 256.9823 257.2966	.5 .6 .7 .8	5741.4569 5754.8951 5768.3490 5781.8185 5795.3038	268.6062 268.9203 269.2345 269.5486 269.8628
82.0 .1 .2 .3 .4	5281.0173 5293.9056 5306.8097 5319.7295 5332.6650	257.6106 257.9247 258.2389 258.5531 258.8672	86.0 .1 .2 .3	5808.8048 5822.3215 5835.8539 5849.4020 5862.9659	270.1770 270.4911 270.8053 271.1194 271.4336
.5 .6 .7 .8	5345.6162 5358.5832 5371.5658 5384.5641 5397.5782	259.1814 259.4956 259.8097 260.1239 260.4380	.5 .6 .7 .8	5876.5454 5890.1407 5903.7516 5917.3783 5931.0206	271.7478 272.0619 272.3761 272.6902 273.0044
83.0 .1 .2 .3 .4	5410.6079 5423.6534 5436.7146 5449.7915 5462.8840	260.7522 261.0663 261.3805 261.6947 262.0088	87.0 .1 .2 .3 .4	5944.6787 5958.3525 5972.0420 5985.7472 5999.4681	273.3186 273.6327 273.9469 274.2610 274.5752
.5 .6 .7 .8	5475.9923 5489.1163 5502.2561 5515.4115 5528.5826	262.3230 262.6371 262.9513 263.2655 263.5796	.5 .6 .7 .8	6013.2047 6026.9570 6040.7250 6054.5088 6068.3082	274.8894 275.2035 275.5177 275.8318 276.1460

Diameter.	Area.	Circumference.	Diameter.	Area.	Circumference.
88.0 .1 .2 .3 .4	6082.1234 6095.9542 6109.8008 6123.6631 6137.5411	276.4602 276.7743 277.0885 277.4026 277.7168	92.0 .1 .2 .3 .4	6647.6101 6662.0692 6676.5441 6691.0347 6705.5410	289.0265 289.3407 289.6548 289.9690 290.2832
.5 .6 .7 .8	6151.4348 6165.3442 6179.2693 6193.2101 6207.1666	278.0309 278.3451 278.6593 278.9740 279.2876	.5 .6 .7 .8	6720.0630 6734.6008 6749.1542 6763.7233 6778.3082	290.5973 290.9115 291.2256 291.5398 291.8540
89.0 .1 .2 .3 .4	6221.1389 6235.1268 6249.1304 6263.1498 6277.1849	279.6017 279.9159 280.2301 280.5442 280.8584	93.0 .1 .2 .3 .4	6792.9087 6807.5250 6822.1569 6836.8046 6851.4680	292.1681 292.4823 292.7964 293.1106 293.4248
.5 .6 .7 .8	6291.2356 6305.3021 6319.3843 6333.4822 6347.5958	281.1725 281.4867 281.8009 282.1150 282.4292	.5 .6 .7 .8	6866.1471 6880.8419 6895.5524 6910.2786 6925.0205	293.7389 294.0531 294.3672 294.6814 294.9956
90.0 .1 .2 .3 .4	6361.7251 6375.8701 6390.0309 6404.2073 6418.3995	282.7433 283.0575 283.3717 283.6858 284.0000	94.0 .1 .2 .3 .4	6939.7782 6954.5515 6969.3106 6984.1453 6998.9658	295.3097 295.6239 295.9380 296.2522 296.5663
.5 .6 .7 .8	6432.6073 6446.8309 6461.0701 6475.3251 6489.5958	284.3141 284.6283 284.9425 285.2566 285.5708	.5 .6 .7 .8	7013.8019 7028.6538 7043.5214 7058.4047 7073.3033	296.8805 297.1947 297.5088 297.8230 298.1371
91.0 .1 .2 .3 .4	6503.8822 6518.1843 6532.5021 6546.8356 6561.1848	285.8849 286.1991 286.5133 286.8274 287.1416	95.0 .1 .2 .3 .4	7088.2184 7103.1488 7118.1950 7133.0568 7148.0343	298.4513 298.7655 299.0796 299.3938 299.7079
.5 .6 .7 .8	6575.5498 6589.9304 6604.3268 6618.7388 6633.1666	287.4557 287.7699 288.0840 288.3982 288.7124	.5 .6 .7 .8	7163.0276 7178.0366 7193.0612 7208.1016 7223.1577	300.0221 300.3363 300.6504 300.9646 301.2787

(CONCLUDED.)

Diameter.	Area.	Circumference.	Diameter.	Area.	Circumference.
96.0 .1 .2 .3 .4	7238.2295 7253.3170 7268.4202 7283.5391 7298.6737	301.5929 301.9071 302.2212 302.5354 302.8405	98.0 .1 .2 .3 .4	7542.9640 7558.3656 7573.7830 7589.2161 7604.6648	307.8761 308.1902 308.5044 308.8186 309.1327
.5 .6 .7 .8	7313.8240 7328.9901 7344.1718 7359.3693 7374.5824	303.1637 303.4779 303.7920 304.1062 304.4203	.5 .6 .7 .8	7620.1293 7635.6095 7651.1054 7666.6170 7682.1444	309.4469 309.7610 310.0752 310.3894 310.7035
97.0 .1 .2 .3 .4	7389.8113 7405.0559 7420.3162 7435.5922 7450.8839	304.7345 305.0486 305.3628 305.6770 305.9911	99.0 .1 .2 .3 .4	7697.6893 7713.2461 7728.8206 7744.4107 7760.0166	311.0177 311.3318 311.6460 311.9602 312.2743
.5 .6 .7 .8	7466.1913 7481.5144 7496.8532 7512.2078 7527.5780	306.3053 306.6194 306.9336 307.2478 307.5619	.5 .6 .7 .8	7775.6382 7791.2754 7806.9284 7822.5971 7838.2815	312.5885 312.9026 313.2168 313.5309 313.8451
			100.0	7853.9816	314.1593

To find from the table areas or circumferences for larger diameters than those given.

#### CASE I.

For diameters greater than 100 and less than 1001:

Take from the table the area or circumference for a circle the diameter of which is one-tenth of the given diameter.

To obtain the required area or circumference, multiply the area so found by 100 and the circumference so found by 10.

For Example.—What is the area and circumference corresponding to a diameter

of 459?
From the tables the area and circumference for diameter 45.9 are 1654.6847 and 144.1991. Therefore 165 468.47 and 1441.991 are the area and circumference required.

#### CASE II.

For diameters greater than 1000:

Divide the given diameter by any convenient factor which will give as a quotient a diameter found in the table, and take from the table the area or circumference for this diameter.

To obtain the required area or circumference multiply the area so found by the

square of the factor and the circumference so found by the factor.

For Example.—What is the area and circumference corresponding to a diameter of 1983?

 $1983 \div 3 = 661$ . From the tables and Case I the area and circumference for diameter 661 are 343156.95 and 2076.593. Therefore  $343156.95 \times 9 = 3088412.55 =$  area required, and  $20765.93 \times 3 = 6229.779 =$  circumference required.

### LOGARITHMS OF NUMBERS, FROM 0 TO 1000.

-			63			I _	-			
No.	0	1	2	3	4	5	6	7	8	9
0	0	00000	30103	47712	60206	69897	77815	84510	90309	95424
10	00000	00432	00860	01283	01703	02118	02530	02938	03342	03742
11	04139	04532	04921	05307	05690	06069	06445	06818	07188	07554
12	07918	08278	08636	08990	09342	09691	10037	10380	10721	11059
13	11394	11727	12057	12385	12710	13033	13353	13672	13987	14301
14	14613	14921	15228	15533	15836	16136	16435	16731	17026	17318
15	17609	17897	18184	18469	18752	19033	19312	19590	19865	20139
16	20412	20682	20951	21218	21484	21748	22010	22271	22530	22788
17	23045	23299	23552	23804	24054	24303	24551	24797	25042	25285
18	25527	25767	26007	26245	26481	26717	26951	27184	27415	27646
19	27875	28103	28330	28555	28780	29003	29225	29446	29666	29885
20	30103	30319	30535	30749	30963	31175	31386	31597	31806	32014
21	32222	32428	32633	32838	33041	33243	33445	33646	33845	34044
22	34242	34439	34635	34830	35024	35218	35410	35602	35793	35983
23	36173	36361	36548	36735	36921	37106	37291	37474	37657	37839
24	38021	38201	38381	38560	38739	38916	39093	39269	39445	39619
25	39794	39967	40140	40312	40483	40654	40824	40993	41162	41330
26	41497	41664	41830	41995	42160	42324	42488	42651	42813	42975
27	43136	43296	43456	43616	43775	43933	44090	44248	44404	44560
28	44716	44870	45024	45178	45331	45484	45636	45788	45939	46089
29	46240	46389	46538	46686	46834	46982	47129	47275	47421	47567
30	47712	47856	48000	48144	48287	48430	48572	48713	48855	48995
31	49136	492 <b>7</b> 6	49415	49554	49693	49831	49968	50105	50242	50379
32	50515	50650	50785	50920	51054	51188	51321	51454	51587	51719
33	51851	51982	52113	52244	52374	52504	52633	52763	52891	53020
34	53148	532 <b>7</b> 5	53402	53529	53655	53.81	53907	54033	54157	54282
35	54407	54530	54654	54777	54900	55022	55145	55266	55388	55509
36	55630	55750	55870	55990	56110	56229	56348	56466	56584	56702
37	56820	56937	57054	57170	57287	57403	57518	57634	57749	57863
38	57978	58092	58206	58319	58433	58546	58658	58771	58883	58995
39	59106	59217	59328	59439	59549	59659	59769	59879	59988	60097
40	60206	60314	60422	60530	60638	60745	60852	60959	61066	61172
41	61278	61384	61489	61595	61700	61804	61909	62013	62118	62221
42	62325	62428	62531	62634	62736	62838	62941	63042	63144	63245
43	63347	63447	63548	63648	63749	63848	63948	64048	64147	64246
44	64345	64443	64542	64640	64738	64836	64933	65030	65127	65224
45	65321	65417	65513	65609	65705	65801	65896	65991	66086	66181
46	66276	66370	66464	66558	66651	66745	66838	66931	67024	67117
47	67210	67302	67394	67486	67577	67669	67760	67851	67942	68033
48	68124	68214	68304	68394	68484	68574	68663	68752	68842	68980
49	69020	69108	69196	6\$284	69372	69460	69548	69635	69722	69810
50	69897	69983	70070	70156	70243	70329	70415	70500	70586	70671
51	70757	70842	70927	71011	71096	71180	71265	71349	71433	71516
52	71600	71683	71767	71850	71933	72015	72098	72181	72263	72345
53	72428	72509	72591	72672	72754	72835	72916	72997	73078	73158
54	73239	73319	73399	73480	73559	73639	73719	73798	73878	73957

### LOGARITHMS OF NUMBERS, FROM 0 TO 1000.

(Continued.)

		ı	1	1	1		i	1		
No.	0	1	2	3	4	5	6	7	8	9
55	74036	74115	74193	74272	74351	74429	74507	74585	74663	74741
56	74818	74896	74973	75050	75127	75204	75281	75358	75434	75511
57	75587	75663	75739	75815	75891	75966	76042	76117	76192	76267
58	76342	76417	76492	76566	76641	76715	76789	76863	76937	77011
59	77085	77158	77232	77305	77378	77451	77524	77597	77670	77742
60	77815	77887	77959	78031	78103	78175	78247	78318	78390	78461
61	78533	78604	78675	78746	78816	78887	78958	79028	79098	79169
62	79239	79309	79379	79448	79518	79588	79657	79726	79796	79865
63	79934	80002	80071	80140	80208	80277	80345	80413	80482	80550
64	80618	80685	80753	80821	80888	80956	81023	81090	81157	81224
65	81291	81358	81424	81491	81557	81624	81690	81756	81822	81888
66	81954	82020	82085	82151	82216	82282	82347	82412	82477	82542
67	82607	82672	82736	82801	82866	82930	82994	83058	83123	83187
68	83250	83314	83378	83442	83505	83569	83632	83695	83758	83821
69	83884	83947	84010	84073	84136	84198	84260	84323	84385	84447
70	84509	84571	84633	84695	84757	84818	84880	84941	85003	85064
71	85125	85187	85248	85309	85369	85430	85491	85551	85612	85672
72	85733	85793	85853	85913	85973	86033	86093	86153	86213	86272
73	86332	86391	86451	86510	86569	86628	86687	86746	86805	86864
74	86923	86981	87040	87098	87157	87215	87273	87332	87390	87448
75	87506	87564	87621	87679	87737	87794	87852	87909	87966	88024
76	88081	88138	88195	88252	88309	88366	88422	88479	88536	88592
77	88649	88705	88761	88818	88874	88930	88986	89042	89098	89153
78	89209	89265	89320	89376	89431	89487	89542	89597	89652	89707
79	89762	89817	89872	89927	89982	90036	90091	90145	90200	90254
80	90309	90363	90417	90471	90525	90579	90633	90687	90741	90794
81	90848	90902	90955	91009	91062	91115	91169	91222	91275	91328
82	91381	91434	91487	91540	91592	91645	91698	91750	91803	91855
83	91907	91960	92012	92064	92116	92168	92220	92272	92324	92376
84	92427	92479	92531	92582	92634	92685	92737	92788	92839	92890
85	92941	92993	93044	93095	93146	93196	93247	93298	93348	93399
86	93449	93500	93550	93601	93651	93701	93751	93802	93852	93902
87	93951	94001	94051	94101	94151	94200	94250	94300	94349	91398
88	94448	94497	94546	94596	94645	94694	94743	94792	94841	94890
89	94939	94957	95036	95085	95133	95182	95230	95279	95327	95376
90	95424	95472	95520	95568	95616	95664	95712	95760	95808	95856
91	95904	95951	95999	96047	96094	96142	96189	96236	96284	96331
92	96378	96426	96473	96520	96567	96614	96661	96708	96754	96801
93	96848	96895	96941	96988	97034	97081	97127	97174	97220	97266
94	97312	97359	97405	97451	97497	97543	97589	97635	97680	97726
95	97772	97818	97863	97909	97954	98000	98045	98091	98136	98181
96	98227	98272	98317	98362	98407	98452	98497	98542	98587	98632
97	98677	98721	98766	98811	98855	98900	98945	98989	99033	99078
98	99122	99166	99211	99255	99299	99343	99387	99431	99475	99519
99	99563	99607	99651	99694	99738	99782	99825	99869	99913	99956

0	,	Sine.	Cosecant.	Tangent.	Cotangent.	Secant.	Cosine.	1	0
0	0 10 20 30 40 50	.000000 .002909 .005818 .008727 .011635 .014544	Infinite. 343.77516 171.88831 114.59301 85.945609 68.757360	.000000 .002909 .005818 .008727 .011636 .014545	Infinite. 343.77371 171.88540 114.58865 85.939791 68.750087	1.00000 1.00000 1.00002 1.00004 1.00007 1.00011	1.000000 .999996 .999983 .999962 .999932 .999894	0 50 40 30 20 10	90
1	0 10 20 30 40 50	.017452 .020361 .023269 .026177 .029085 .031992	57.298688 49.114062 42.975713 38.201550 34.382316 31.257577	.017455 .020365 .023275 .026186 .029097 .032009	57.289962 49.103881 42.964077 38.188459 34.367771 31.241577	1.00015 1.00021 1.00027 1.00034 1.00042 1.00051	.999848 .999793 .999729 .999657 .999577 .999488	0 50 40 30 20 10	89
2	0 10 20 30 40 50	.034899 .037806 .040713 .043619 .046525 .049431	28.653708 26.450510 24.562123 22.925586 21.493676 20.230284	.034921 .037834 .040747 .043661 .046576 .049491	28.636253 26.431600 24.541758 22.903766 21.470401 20.205553	1.00061 1.00072 1.00083 1.00095 1.00108 1.00122	.999391 .999285 .999171 .999048 .998917 .998778	0 50 40 30 20 10	88
3	0 10 20 30 40 50	.052336 .055241 .058145 .061049 .063952 .066854	19.107323 18.102619 17.198434 16.380408 15.636793 14.957882	.052408 .055325 .058243 .061163 .064083 .067004	19.081137 18.074977 17.169337 16.349855 15.604784 14.924417	1,00137 1,00153 1,00169 1,00187 1,00205 1,00224	.998630 .998473 .998308 .998135 .997357 .997763	0 50 40 30 20 10	87
4	0 10 20 30 40 50	.069756 .072658 .075559 .078459 .081359 .084258	14 335587 13.763115 13.234717 12.745495 12.291252 11.868370	.069927 .072851 .075776 .078702 .081629 .084558	14.3 0666 13.726738 13.196888 12.706205 12.250505 11.826167	1.00244 1.00265 1.00287 1.00309 1.00333 1.00357	.997564 .997357 .997141 .996917 .996685 .996444	0 50 40 30 20 10	86
5	0 10 20 30 40 50	.087156 .090053 .092950 .095846 .098741 .101635	11.473713 11.104549 10.758488 10.433431 10.127522 9.8391227	.087489 .090421 .093354 .096289 .099226 .102164	11.430052 11.059431 10.711913 10.385397 10.078031 9.7881732	1.00382 1.00408 1.00435 1.00463 1.00491 1.00521	.996195 .995937 .995671 .995396 .995113 .994822	0 50 40 30 20 10	85
6	0 10 20	.104528 .107421 .110313	9.5667722 9.3091699 9.0651512	.105104 .108046 .110990	9.5143645 9 2553035 9.0098261	1.00551 1.00582 1.00614	.994522 .994214 .993897	0 50 40	84 83
0	,	Cosine.	Secant.	Cotangent.	Tangent.	Cosecant.	Sine.	,	0

For functions from 83°-40′ to 90° read from bottom of table upward.

					1				
С	,	Sine.	Cosecant.	Tangent.	Cotangent.	Secant.	Cosine.	,	0
6	30 40 50	.113203 .116093 .118982	8.8336715 8.6137901 8.4045586	.113936 .116883 .119833	8.7768874 8.5555468 8.3449558	1.00647 1.00681 1.00715	.993572 .993238 .992896	30 20 10	
7	0 10 20 30 40 50	.121869 .124756 .127642 .130526 .133410 .136292	8.2055090 8.0156450 7.8344335 7.6612976 7.4957100 7.3371909	.122785 .125738 .128694 .131653 .134613 .137576	8.1443464 7.9530224 7.7703506 7.5957541 7.4287064 7.2687255	1.00751 1.00787 1.00825 1.00863 1.00902 1.00942	.992546 .992187 .991820 .991445 .991061 .990669	0 50 40 30 20 10	83
8	0 10 20 30 40 50	.139173 .142053 .144932 .147809 .150686 .153561	7.1852965 7.0396220 6.8997942 6.7654691 6.6363293 6.5120812	.140541 .143508 .146478 .149451 .152426 .155404	7.1153697 6.9682335 6.8269437 6.6911562 6.5605538 6.4348428	1.00983 1.01024 1.01067 1.01111 1.01155 1.01200	.990268 .989859 .989442 .989016 .988582 .988139	0 50 40 30 20 10	82
9	0 10 20 30 40 50	.156434 .159307 .162178 .165048 .167916 .170783	6.3924532 6.2771933 6.1660674 6.0588980 5.9553625 5.8553921	.158384 .161368 .164354 .167343 .170334 .173329	6.3137515 6.1970279 6.0844381 5.9757644 5.8708042 5.7693688	1.01247 1.01294 1.01342 1.01391 1.01440 1.01491	.987688 .987229 .986762 .986286 .985801 .985309	0 50 40 30 20 10	81
10	0 10 20 30 40 50	.173648 .176512 .179375 .182236 .185095 .187953	5.7587705 5.6653331 5.5749258 5.4874043 5.4026333 5.3204860	.176327 .179328 .182332 .185339 .188359 .191363	5.6712818 5.5763786 5.4845052 5.3955172 5.3092793 5.2256647	1.01543 1.01595 1.01649 1.01703 1.01758 1.01815	.984808 .984298 .983781 .983255 .982721 .982178	0 50 40 30 20 10	80
11	0 10 20 30 40 50	.190809 .193664 .196517 .199368 .202218 .205065	5.2408431 5.1635924 5.0886284 5.0158317 4.9451687 4.8764907	.194380 .197401 .200425 .203452 .206483 .209518	5.1445540 5.0658352 4.9894027 4.9151570 4.8430045 4.7728568	1.01872 1.01930 1.01989 1.02049 1.02110 1.02171	.981627 .981068 .980500 .979925 .979341 .978748	0 50 40 30 20 10	79
12	0 10 20 30 40 50	.207912 .210756 .213599 .216440 .219279 .222116	4.8097343 4.7448206 4.6816748 4.6202263 4.5604080 4.5021565	.212557 .215599 .218645 .221695 .224748 .227806	4.7046301 4.6382457 4.5736287 4.5107085 4.4494181 4.3896940	1.02234 1.02298 1.02362 1.02428 1.02494 1.02562	.978148 .977539 .976921 .976296 .975662 .975020	0 50 40 30 20 10	78
0	,	Cosine.	Secant.	Cotangent.	Tangent.	Cosecant.	Sine.	,	0

For functions from 77°-10' to 83°-30' read from bottom of table upward.

					Ī			1	
0	'	Sine.	Cosecant.	Tangent.	Cotangent.	Secant.	Cosine.	'	0
13	0 10 20 30 40 50	.224951 .227784 .230616 .233445 .236273 .239098	4.4454115 4.3901158 4.3362150 4.2836576 4.2323943 4.1823785	.230868 .233934 .237004 .240079 .243158 .246241	4.3314759 4.2747066 4.2193318 4.1652998 4.1125614 4.0610700	1.02630 1.02700 1.02770 1.02842 1.02914 1.02987	.974370 .973712 .973045 .972370 .971687 .970995	0 50 40 30 20 10	77
14	0 10 20 30 40 50	.241922 .244743 .247563 .250380 .253195 .256008	4.1335655 4.0859130 4.0393804 3.9939292 3.9495224 3.9061250	.249328 .252420 .255517 .258618 .261723 .264834	4.0107809 3.9616518 3.9136420 3.8667131 3.8208281 3.7759519	1.03061 1.03137 1.03213 1.03290 1.03363 1.03447	.970296 .969588 .968872 .968148 .967415 .966675	0 50 40 30 20 10	76
15	0 10 20 30 40 50	.258819 .261628 .264434 .267238 .270040 .272840	3.8637033 3.8222251 3.7816596 3.7419775 3.7031506 3.6651518	.267949 .271069 .274195 .277325 .280460 .283600	3.7320508 3.6890927 3.6470467 3.6058835 3.5655749 3.5260938	1.03528 1.03609 1.03691 1.03774 1.03858 1.03944	.965926 .965169 .964404 .963630 .962849 .962059	0 50 40 30 20 10	75
16	0 10 20 30 40 50	.275637 .278432 .281225 .284015 .286803 .289589	3.6279553 3.5915363 3.5558710 3.5209365 3.4867110 3.4531735	.286745 .289896 .293052 .296214 .299380 .302553	3.4874144 3.4495120 3.4123626 3.3759434 3.3402326 3.3052091	1.04030 1.04117 1.04206 1.04295 1.04385 1.04477	.961262 .960456 .959642 .958820 .957990 .957151	0 50 40 30 20 10	74
17	0 10 20 30 40 50	.292372 .295152 .297930 .300706 .303479 .306249	3.4203036 3.3880820 3.3564900 3.3255095 3.2951234 3.2653149	.305731 .308914 .312104 .315299 .318500 .321707	3.2708526 3.2371438 3.2040638 3.1715948 3.1397194 3.1084210	1.04569 1.04663 1.04757 1.04853 1.04950 1.05047	.956305 .955450 .954588 .953717 .952838 .951951	0 50 40 30 20 10	73
18	0 10 20 30 40 50	.309017 .311782 .314545 .317305 .320062 .322816	3.2360680 3.2073673 3.1791978 3.1515453 3.1243959 3.0977363	.324920 .328139 .331364 .334595 .337833 .341077	3.0776835 3.0474915 3.0178301 2.9886850 2.9600422 2.9318885	1.05146 1.05246 1.05347 1.05449 1.05552 1.05657	.951057 .950154 .949243 .948324 .947397 .946462	0 50 40 30 20 10	72
19	0 10 20	.325568 .328317 .331063	3.0715535 3.0458352 3.0205693	.344328 .347585 .350848	2.9042109 2.8769970 2.8502349	1.05762 1.05869 1.05976	.945519 .944568 .943609	0 50 40	71
0	,	Cosine.	Secant.	Cotangent.	Tangent.	Cosecant.	Sine.	'	0

For functions from 70°-40′ to 77°-0′ read from bottom of table upward.

0	,	Sine.	Cosecant.	Tangent.	Cotangent.	Secant.	Cosine.	,	ō
19	30 40 50	.333807 .336547 .339285	2.9957443 2.9713490 2.9473724	.354119 .357396 .360680	2.8239129 2.7980198 2.7725448	1.06085 1.06195 1.06306	.942641 .941666 .940684	30 20 10	
20	0 10 20 30 40 50	.342020 .344752 .347481 .350207 .352931 .355651	2.9238044 2.9006346 2.8778532 2.8554510 2.8334185 2.8117471	.363970 .367268 .370573 .373885 .377204 .380530	2.7474774 2.7228076 2.6985254 2.6746215 2.6510867 2.6279121	1.06418 1.06531 1.06645 1.06761 1.06878 1.06995	.939693 .938694 .937687 .936672 .935650 .934619	0 50 40 30 20 10	70
21	0 10 20 30 40 50	.358368 .361082 .363793 .366501 .369206 .371908	2.7904281 2.7694532 2.7488144 2.7285038 2.7085139 2.6888374	.383864 .387205 .390554 .393911 .397275 .400647	2.6050891 2.5826094 2.5604649 2.5386479 2.5171507 2.4959661	1.07115 1.07235 1.07356 1.07479 1.07602 1.07727	.933580 .932534 .931480 .930418 .929348 .928270	0 50 40 30 20 10	69
22	0 10 20 30 40 50	.374607 .377302 .379994 .382683 .385369 .388052	2.6694672 2.6503962 2.6316180 2.6131259 2.5949137 2.5769753	.404026 .407414 .410810 .414214 .417626 .421046	2.4750869 2.4545061 2.4342172 2.4142136 2.3944889 2.3750372	1.07853 1.07981 1.08109 1.08239 1.08370 1.08503	.927184 .926090 .924989 .923880 .922762 .921638	0 50 40 30 20 10	68
23	0 10 20 30 40 50	.390731 .393407 .396080 .398749 .401415 .404078	2.5593047 2.5418961 2.5247440 2.5078428 2.4911874 2.4747726	.424475 .427912 .431358 .434812 .438276 .441748	2.3558524 2.3369287 2.3182606 2.2998425 2.2816693 2.2637357	1.08636 1.08771 1.08907 1.09044 1.09183 1.09323	.920505 .919364 .918216 .917060 .915896 .914725	0 50 40 30 20 10	67
24	0 10 20 30 40 50	.406737 .409392 .412045 .414693 .417338 .419980	2.4585933 2.4426448 2.4269222 2.4114210 2.3961367 2.3810650	.445229 .448719 .452218 .455726 .459244 .462771	2.2460368 2.2285676 2.2113234 2.1942997 2.1774920 2.1608958	1.09464 1.09606 1.09750 1.09895 1.10041 1.10189	.913545 .912358 .911164 .909961 .908751	0 50 40 30 20 10	66
25	0 10 20 30 40 50	.422618 .425253 .427884 .430511 .433135 .435755	2.3662016 2.3515424 2.3370833 2.3228205 2.3087501 2.2948685	.466308 .469854 .473410 .476976 .480551 .484137	2.1445069 2.1283213 2.1123348 2.0965436 2.0809438 2.0655318	1.10338 1.10488 1.10640 1.10793 1.10947 1.11103	.906308 .905075 .903834 .902585 .901329 .900065	0 50 40 30 20 10	65 64
0	,	Cosine.	Secant.	Cotangent.	Tangent.	Cosecant.	Sine.		0

For functions from 64°-10′ to 70°-30′ read from bottom of table upward.

			1		1	1		1	
0	,	Sine.	Cosecant.	Tangent.	Cotangent.	Secant.	Cosine.	,	0
26	0 10 20 30 40 50	.438371 .440984 .443593 .446198 .448799 .451397	2.2811720 2.2676571 2.2543204 2.2411585 2.2281681 2.2153460	.487733 .491339 .494955 .498582 .502219 .505867	2.0503038 2.0352565 2.0203862 2.0056897 1.9911637 1.9768050	1.11260 1.11419 1.11579 1.11740 1.11903 1.12067	.898794 .897515 .896229 .894934 .893633 .892323	0 50 40 30 20 10	64
27	0 10 20 30 40 50	.453990 .456580 .459166 .461749 .464327 .466901	2.2026893 2.1901947 2.1778595 2.1656806 2.1536553 2.1417808	.509525 .513195 .516876 .520567 .524270 .527984	1.9626105 1.9485772 1.9347020 1.9209821 1.9074147 1.8939971	1.12233 1.12400 1.12568 1.12738 1.12910 1.13083	.891007 .889682 .888350 .887011 .885664 .884309	0 50 40 30 20 10	63
28	* 0 10 20 30 40 50	.469472 .472038 .474600 .477159 .479713 .482263	2.1300545 2.1184737 2.1070359 2.0957385 2.0845792 2.0735556	.531709 .535547 .539195 .542956 .546728 .550515	1.8807265 1.8676003 1.8546159 1.8417409 1.8290628 1.8164892	1.13257 1.13433 1.13610 1.13789 1.13970 1.14152	.882948 .881578 .880201 .878817 .877425 .876026	0 50 40 30 20 10	62
29	0 10 20 30 40 50	.484810 .487352 .489890 .492424 .494953 .497479	2.0626653 2.0519061 2.0412757 2.0307720 2.0203929 2.0101362	.554309 .558118 .561939 .565773 .569619 .573478	1.8040478 1.7917362 1.7795524 1.7674940 1.7555590 1.7437453	1.14335 1.14521 1.14707 1.14896 1.15085 1.15277	.874620 .873206 .871784 .870356 .868920 .867476	0 50 40 30 20 10	61
30	0 10 20 30 40 50	.500000 .502517 .505030 .507538 .510043 .512543	2.0000000 1.9899822 1.9800810 1.9702944 1.9606206 1.9510577	.577350 .581235 .585134 .589045 .592970 .596908	1.7320508 1.7204736 1.7090116 1.6976631 1.6864261 1.6752988	1.15470 1.15665 1.15861 1.16059 1.16259 1.16460	.866025 .864567 .863102 .861629 .860149 .858662	0 50 40 30 20 10	60
31	0 10 20 30 40 50	.515038 .517529 .520016 .522499 .524977 .527450	1.9416040 1.9322578 1.9230173 1.9138809 1.9048469 1.8959138	.600861 .604827 .608807 .612801 .616809 .620832	1.6642795 1.6533663 1.6425576 1.6318517 1.6212469 1.6107417	1.16663 1.16868 1.17075 1.17283 1.17493 1.17704	.857167 .855665 .854156 .852640 .851117 .849586	0 50 40 30 20 10	59
32	0 10 20	.529919 .532384 .534844	1.8870799 1.8783438 1.8697040	.624869 .628921 .632988	1.6003345 1.5900238 1.5798079	1.17918 1.18133 1.18350	.848048 .846503 .844951	0 50 40	58 57
0	,	Cosine.	Secant.	Cotangent.	Tangent.	Cosecant.	Sine.	,	0

For functions from 57°-40' to 64°-0' read from bottom of table upward.

0	,	Sine.	Cosecant.	Tangent.	Cotangent.	Secant.	Cosine.	,	0
32	30 40 50	.537300 .539751 .542197	1.8611590 1.8527073 1.8443476	.637079 .641167 .645280	1.5696856 1.5596552 1.5497155	1.18569 1.18790 1.19012	.843391 .841825 .840251	30 20 10	
33	0 10 20 30 40 50	.544639 .547076 .549509 .551937 .554360 .556779	1.8360785 1.8278985 1.8198065 1.8118010 1.8038809 1.7960449	.649408 .653531 .657710 .661886 .666077 .670285	1.5398650 1.5301025 1.5204261 1.5108352 1.5013282 1.4919039	1.19236 1.19463 1.19691 1.19920 1.20152 1.20386	.838671 .837083 .835488 .833886 .832277 .830661	0 50 40 30 20 10	57
34	0 10 20 30 40 50	.559193 .561602 .564007 .566406 .568801 .571191	1.7882916 1.7806201 1.7730290 1.7655173 1.7580837 1.7507273	.674509 .678749 .683007 .687281 .691573 .695881	1.4825610 1.4732983 1.4641147 1.4550090 1.4459801 1.4370268	1.20622 1.20859 1.21099 1.21341 1.21584 1.21830	.829038 .827407 .825770 .824126 .822475 .820817	0 50 40 30 20 10	56
35	10 20 30 40 50	.573576 .575957 .578332 .580703 .583069 .585429	1.7434468 1.7362413 1.7291096 1.7220508 1.7150639 1.7081478	.700208 .704552 .708913 .713293 .717691 .722108	1.4281480 1.4193427 1.4106098 1.4019483 1.3933571 1.3848355	1.22077 1.22327 1.22579 1.22833 1.23089 1.23347	.819152 .817480 .815801 .814116 .812423 .810723	0 50 40 30 20 10	55
36	0 10 20 30 40 50	.587785 .590136 .592482 .594823 .597159 .599489	1.7013016 1.6945244 1.6878151 1.6811730 1.6745970 1.6680864	.726543 .730996 .735469 .739961 .744472 .749003	1.3763810 1.3679959 1.3596764 1.3514224 1.3432331 1.3351075	1.23607 1.23869 1.24134 1.24400 1.24669 1.24940	.809017 .807304 .805584 .803857 .802123 .800383	0 50 40 30 20 10	54
37	0 10 20 30 40 50	.601815 .604136 .606451 .608761 .611067 .613367	1.6616401 1.6552575 1.6489376 1.6426796 1.6364828 1.6303462	.753554 .758125 .762716 .767627 .771959 .776612	1.3270448 1.3190441 1.3111046 1.3032254 1.2954057 1.2876447	1.25214 1.25489 1.25767 1.26047 1.26330 1.26615	.798636 .796882 .795121 .793353 .791579 .789798	0 50 40 30 20 10	53
38	0 10 20 30 40 50	.615661 .617951 .620235 .622515 .624789 .627057	1.6242692 1.6182510 1.6122908 1.6063879 1.6005416 1.5947511	.781286 .785981 .790698 .795436 .800196 .804080	1.2799416 1.2722957 1.2647062 1.2571723 1.2496933 1.2422685	1.26902 1.27191 1.27483 1.27778 1.28075 1.28374	.788011 .786217 .784416 .782608 .780794 .778973	0 50 40 30 20 10	52 51
o	,	Cosine.	Secant.	Cotangent.	Tangent.	Cosecant.	Sine.	,	0

For functions from 51°-10′ to 57°-30′ read from bottom of table upward.

-			1		1	1	1	1	1
0	,	Sine.	Cosecant.	Tangent.	Cotangent.	Secant.	Cosine.	,	0
39	0 10 20 30 40 50	.629320 .631578 .633831 .636078 .638320 .640557	1.5890157 1.5833318 1.5777077 1.5721337 1.5666121 1.5611424	.809784 .814612 .819463 .824336 .829234 .834155	1.2348972 1.2275786 1.2203121 1.2130970 1.2059327 1.1988184	1.28676 1.28980 1.29287 1.29597 1.29909 1.30223	.777146 .775312 .773472 .771625 .769771 .767911	0 50 40 30 20 10	51
40	0 10 20 30 40 50	.642788 .645013 .647233 .649448 .651657 .653861	1.5557238 1.5503558 1.5450378 1.5397690 1.5345491 1.5293773	.839100 .844069 .849062 .854081 .859124 .864193	1.1917536 1.1847376 1.1777698 1.1708496 1.1639763 1.1571495	1.30541 1.30861 1.31183 1.31509 1.31837 1.32168	.766044 .764171 .762292 .760406 .758514 .756615	0 50 40 30 20 10	50
41	0 10 20 30 40 50	.656059 .658252 .660439 .662620 .664796 .666966	1.5242531 1.5191759 1.5141452 1.5091605 1.5042211 1.4993267	.869287 .874407 .879553 .884725 .889924 .895151	1.1503684 1.1436326 1.1369414 1.1302944 1.1236909 1.1171305	1.32501 1.32838 1.33177 1.33519 1.33864 1.34212	.754710 .752798 .750880 .748956 .747025 .745088	0 50 40 30 20 10	49
42	0 10 20 30 40 50	.669131 .671289 .673443 .675590 .677732 .679868	1.4944765 1.4896703 1.4849073 1.4801872 1.4755095 1.4708736	.900404 .905685 .910994 .916331 .921697 .927091	1.1106125 1.1041365 1.0977020 1.0913085 1.0849554 1.0786423	1.34563 1.34917 1.35274 1.35634 1.35997 1.36363	.743145 .741195 .739239 .737277 .735309 .733335	0 50 40 30 20 10	48
43	0 10 20 30 40 50	.681998 .684123 .686242 .688355 .690462 .692563	1.4662792 1.4617257 1.4572127 1.4527397 1.4483063 1.4439120	.932515 .937968 .943451 .948965 .954508 .960083	1.0723687 1.0661341 1.0599381 1.0537801 1.0476598 1.0415767	1.36733 1.37105 1.37481 1.37860 1.38242 1.38628	.731354 .729367 .727374 .725374 .723369 .721357	0 50 40 30 20 10	47
44	0 10 20 30 40 50	.694658 .696748 .698832 .700909 .702981 .705047	1.4395565 1.4352393 1.4309602 1.4267182 1.4225134 1.4183454	.965689 .971326 .976996 .982697 .988432 .994199	1.0355303 1.0295203 1.0235461 1.0176074 1.0117088 1.0058348	1.39016 1.39409 1.39804 1.40203 1.40606 1.41012	.719340 .717316 .715286 .713251 .711209 .709161	0 50 40 30 20 10	46
45	0	.707107	1.4142136	1.000000	1.00000000	1.41421	.707107	0	45
0	,	Cosine.	Secant.	Cotangent.	Tangent.	Cosecant.	Sine.	,	0

For functions from 45°-0' to 51°-0' read from bottom of table upward.

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.			
1	1	1	1.0000000	1.0000000	1.000000000			
2	4	8	1.4142136	1.2599210	.500000000			
3		27	1.7320508	1.4422496	.333333333			
4		64	2.0000000	1.5874011	.250000000			
5	25	125	2.2360680	1.7099759	.200000000			
7	36 49	216 343	2.4494897	1.8171206 $1.9129312$	.166666667 .142857143			
8		512	2.6457513 $2.8284271$	2.0000000	.125000000			
9		729	3.0000000	2.0800837	.111111111			
10		1000	3.1622777	2.1544347	.100000000			
11	121	1331	3.3166248	2.2239801	.090909091			
12		1728	3.4641016	2.2894286	.083333333			
13	169	2197	3.6055513	2.3513347	.076923077			
14	196	2744	3.7416574	2.4101422	.071428571			
15	225	3375	3.8729833	2.4662121	.066666667			
16		4096	4.0000000	2.5198421	.062500000			
17	289	4913	4.1231056	2.5712816	.058823529			
18 19	324 361	5832 6859	4.2426407 4.3588989	2.6207414 $2.6684016$	.05555556 .052631579			
	1	1						
20 21	400 441	8000 9261	4.4721360 $4.5825757$	2.7144177 $2.7589243$	.050000000 $.047619048$			
$\frac{21}{22}$	484	10648	4.6904158	2.8020393	.045454545			
23	529	12167	4.7958315	2.8138670	.043478261			
24	576	13824	4.8989795	2.8844991	.041666667			
25	625	15625	5.0000000	2.9240177	.040000000			
26	676	17576	5.0990195	2.9624960	.038461538			
27	729	19683	5.1961524	3.0000000	.037037037			
28	784	21952	5.2915026	3.0365889	.035714286			
29		24389	5.3851648	3.0723168	.034482759			
30		27000	5.4772256	3.1072325	.033333333			
31	961	29791	5.5677644	3.1413806	.032258065			
32 33		32768 35937	5.6568542 5.7445626	3.1748021 3.2075313	.031250000 .030303030			
34		39304	5.8309519	3.2396118	.029411765			
35	1225	42875	5.9160798	3.2710663	.028571429			
36		46656	6.0000000	3.3019272	.02777778			
37	1369	50653	6.0827625	3.3322218	.027027027			
38		54872	6.1644140	3.3619754	.026315789			
39	1521	59319	6.2449980	3.3912114	.025641026			
40		64000	6.3245553	3.4199519	.025090000			
41		68921	6.4031242	3.4482172	.024390244			
42		74088	6.4807407	3.4760266	.023809524			
43 44		79507 85184	6.5574385 6.6332496	3.5033981 3.5303483	023255814 022727273			
44		91125	6.7082039	3.5568933	.02222222			
46		97336	6.7823300	3.5830479	.021739130			
47	2209	103823	6.8556546	3.6088261	.021276600			
48	2304	110592	6.9282032	3.6342411	.020833333			
49	2401	117649	7.0000000	3.6593057	.020408163			
50		125000	7.0710678	3.6840314	.020000000			
51		132651	7 1414284	3.7084298	.019607843			
52		140608	7.2111026	3.7325111	.019230769			
58		148877	7.2801099 7.3484692	3.7562858	.018867925			
54 55		157464 166375	7.3484692 7.4161985	3.7797631 $3.8029525$	.018518519			
56 56		175616	7.4833148	3.8258624	.018181818			
57		185193	7.5498344	3.8485011	.017543860			
58		195112	7.6157731	3.8708766	.017241379			
59		205379	7.6811457	3.8929965	.016949153			

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
60	3600	216000	7.7459667	3.9148676	.016666667
61	3721	226981	7.8102497	3.9364972	.016393443
62	3844	238328	7.8740079	3.9578915	.016129032
63	3969	250047	7.9372539	3.9790571	.015873016
64	4096	262144	8.0000000	4.0000000	.015625000
65	4225	274625	8.0622577	4.0207256	.015384615
66	4356	287496	8.1240384	4.0412401	.015151515
67	4489	300763	8.1853528	4.0615480	.014925373
68	4624	314432	8.2462113	4.0816551	.014705882
69	4761	328509	8.3066239	4.1015661	.014492754
1					
70	4900	343000	8.3666003	4.1212853	.014285714
71	5041	357911	8.4261498	4.1408178	.014084507
72	5184	373248	8.4852814	4.1601676	.013888889
73	5329	389017	8.5440037	4.1793390	.013698630
74	5476	405224	8.6023253	4.1983364	.013513514
75	5625	421875	8.6602540	4.2171633	.013333333
76	5776	438976	8.7177979	4.2358236	.013157895
77	5929	456533	8.7749644	4.2543210	.012987013
78	6084	474552	8.8317609	4.2726586	.012820513
79	6241	493039	8.8881944	4.2908404	.012658228
80		512000	8.9442719	4.3088695	.012500000
	6400				
81	6561	531441	9.0000000	4.3267487	.012345679
82	6724	551368	9.0553851	4.3444815	.012195122
83	6889	571787	9.1104336	4.3620707	.012048193
84	7056	592704	9.1651514	4.3795191	.011904762
85	7225	614125	9.2195445	4.3968296	.011764706
86	7396	636056	9.2736185	4.4140049	.011627907
87	7569	658503	9.3273791	4.4310476	.011494253
88	7744	681472	9.3808315	4.4479602	.011363636
89	7921	704969	9.4339811	4.4647451	.011235955
90	8100	729000	9.4868330	4.4814047	.011111111
91	8281	753571	9.5393920	4.4979414	.010989011
92	8464	778688	9.5916630	4.5143574	.010869565
93	8649	804357	9.6436508	4.5306549	.010752688
94	8836	830584	9.6953597	4.5468359	.010638298
95	9025	857375	9.7467943	4.5629026	.010526316
96	9216	884736	9.7979590	4.5788570	.010416667
97	9409	912673	9.8488578	4.5947009	.010309278
98		941192	9.8994949	4.6104363	.010309278
99	9604	970299	9.9498744	4.6260650	.01010101010
	9801				
100	10000	1000000	10.0000000	4.6415888	.010000000
101	10201	1030301	10.0498756	4.6570095	.009900990
102	10404	1061208	10.0995049	4.6723287	.009803922
103	10609	1092727	10.1488916	4.6875482	.009708738
104	10816	1124864	10.1980390	4.7026694	.009615385
105	11025	1157625	10.2469508	4.7176940	.009523810
106	11236	1191016	10.2956301	4.7326235	.009433962
107	11449	1225043	10.3440804	4.7474594	.009345794
108	11664	1259712	10.3923048	4.7622032	.009259259
109	11881	1295029	10.4403065	4.7768562	.009174312
110	12100	1331000	10.4880885	4.7914199	.009090909
111	12321	1367631	10.5356538	4.8058955	.009009009
112	12544	1404928	10.5830052	4.8202845	.008928571
113	12769	1442897	10.6301458	4.8345881	.008849558
114					.008771930
	12996	1481544	10.6770783	4.8488076	.008695652
115	13225	1520875	10.7238053	4.8629442	
116	13456	1560896	10.7703296	4.8769990	.008620690
117	13689	1601613	10.8166538	4.8909732	.008547009
118	13924	1643032	10.8627805	4.9048681	.008474576
119	14161	1685159	10.9087121	4.9186847	.008403361

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.							
120	14400	1728000	10.9544512	4.9324242	.008333333							
121	14641	1771561	11.0000000	4.9460874	.008264463							
122	14884	1815848	11.0453610	4.9596757	.008196721							
123	15129	1860867	11.0905365	4.9731898	.008130081							
124	15376	1906624	11.1355287	4.9866310	.008064516							
125 126	15625 15876	1953125 2000376	11.1803399 11.2249722	5.0000000 5.0132979	.008000000							
127	16129	2048383	11.2694277	5.0265257	.007936508							
128	16384	2097152	11.3137085	5.0396842	.007812500							
129	16641	2146689	11.3578167	5.0527743	.007751938							
130	16900	2197000	11.4017543	5.0657970	.007692308							
131	17161	2248091	11.4455231	5.0787531	.007633588							
132	17424	2299968	11.4891253	5.0916434	.007575758							
133	17689	2352637	11.5325626	5.1044687	.007518797							
134	17956	2406104	11.5758369	5.1172299	.007462687							
135	18225	2460375	11.6189500	5.1299278	.007407407							
136 137	18496 18769	$\begin{array}{c} 2515456 \\ 2571353 \end{array}$	11.6619038 11.7046999	5.1425632	.007352941							
138	19044	2628072	11.7473401	5.1551367 5.1676493	.007299270 .00724637 <b>7</b>							
139	19321	2685619	11.7898261	5.1801015	.007194245							
140	19600	2744000	11.8321596	5.1924941	.007142857							
141	19881	2803221	11.8743421	5.2048279	.007092199							
142	20164	2863288	11.9163753	5.2171034	.007042254							
143	20449	2924207	11.9582607	5.2293215	.006993007							
144	20736	2985984	12.0000000	5.2414828	.006944444							
145	21025	3048625	12.0415946	5.2535879	.006896552							
146	21316	3112136	12.0830460	5.2656374	.006849315							
147 148	21609 21904	$3176523 \\ 3241792$	$\begin{array}{c} 12.1243557 \\ 12.1655251 \end{array}$	5.2776321 5.2895725	.006802721 .006756757							
149	22201	3307949	12.2065556	5.3014592	.006711409							
150	22500	3375000	12.2474487	5.3132928	.006666667							
151	22801	3442951	12.2882057	5.3250740	.006622517							
152	23104	3511808	12.3288280	5.3368033	.006578947							
153	23409	3581577	12.3693169	5.3484812	.006535948							
154	23716	3652264	12.4096736	5.3601084	.006493506							
155	24025	3723875	12.4498996	5.3716854	.006451613							
156	24336	3796416	12.4899960	5.3832126	.006410256							
157 158	24649 24964	$\frac{3869893}{3944312}$	$\begin{array}{c} 12.5299641 \\ 12.5698051 \end{array}$	5.3946907 5.4061202	.006369427 .006329114							
159	25281	4019679	12.6095202	5.4175015	.006289308							
160	25600	4096000	12.6491106	5.4288352	.006250000							
161	25921	4173281	12.6885775	5.4401218	.006211180							
162	26244	4251528	12.7279221	5.4513618	.006172840							
163	26569	4330747	12.7671453	5.4625556	.006134969							
164	26896	4410944	12.8062485	5.4737037	.006097561							
165	27225	4492125	12.8452326	5.4848066	.006060606							
166 167	$27556 \ 27889$	$4574296 \\ 4657463$	$12.8840987 \\ 12.9228480$	5.4958647 5.5068784	.006024096 .005988024							
168	28224	4741632	12.9614814	5.5178484	.005952381							
169	28561	4826809	13.0000000	5.5287748	.005917160							
170	28900	4913000	13.0384048	5.5396583	.005882353							
171	29241	5000211	13.0766968	5.5504991	.005847953							
172	29584	5088448	13.1148770	5.5612978	.005813953							
173	29929	5177717	13.1529464	5.5720546	.005780347							
174	30276	5268024	13.1909060	5.5827702	.005747126							
175	30625	5359375	13.2287566	5.5934447	.005714286							
176 177	30976 31329	5451776 5545233	13.2664992 13.3041347	5.6040787 5.6146724	.005681818 .005649718							
178	31684	5639752	13,3416641	5.6252263	.005617978							
179	32041	5735339	13.3790882	5.6357408	.005586592							
		0.30090										

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No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
180	32400	5832000	13.4164079	5.6462162	.00555556
181	32761	5929741	13.4536240	5.6566528	.005524862
182	33124	6028568	13.4907376	5.6670511	.005494505
183	33489	6128487	13.5277493	5.6774114	.005464481
184	33856	6229504	13.5646600	5.6877340	.005434783
185	34225	6331625	13.6014705	5.6980192	.005405405
186	34596	6434856	13.6381817	5.7082675	.005376344
187	34969	6539203	13.6747943	5.7184791	.005347594
188	35344	6644672	13.7113092	5.7286543	.005319149
189	35721	6751269	13.7477271	5.7387936	.005291005
190	36100	6859000	13,7840488	5.7488971	.005263158
191	36481	6967871	13.8202750	5.7589652	.005235602
192	36864	7077888	13.8564065	5.7689982	.005208333
193	37249	7189057	13.8924440	5.7789966	.005181347
194	37636	7301384	13.9283883	5.7889604	.005154639
195	38025	7414875	13.9642400	5.7988900	.005128205
196	38416	7529536	14.0000000	5.8087857	.005102041
197	38809	7645373	14.0356688	5.8186479	.005076142
198	39204	7762392	14.0712473	5.8284767	.005050505
199	39601	7880599	14.1067369	5.8382725	.005025126
200	40000	8000000	14.1421356	5.8480355	.005000000
201	40401	8120601	14.1774469	5.8577660	.004975124
202	40804	8242408	14.2126704	5.8674643	.004950495
203	41209	8365427	14.2478068	5.8771307	.004926108
204	41616	8489664	14.2828569	5.8867653	.004901961
205	42025	8615125	14.3178211	5.8963685	.004878049
206	42436	8741816	14.3527001	5.9059406	.004854369
207	42849	8869743	14.3874946	5.9154817	.004830918
208	43264	8998912	14.4222051	5.9249921	.004807692
209	43681	9129329	14.4568323	5.9344721	.004784689
210	44100	9261000	14.4913767	5.9439220	.004761905
211	44521	9393931	14.5258390	5.9533418	.004739336
212	41914	9528128	14.5602198	5.9627320	.004716981
213	45369	9663597	14.5945195	5.9720926	.004694836
214	45796	9800344	14.6287388	5.9814240	.004672897
215	46225	9938375	14.6628783	5.9907264	.004651163
216	46656	10077696	14.6969385	6.0000000	.004629630
217	47089	10218313	14.7309199	6.0092450	.004608295
218	47524	10360232	14.7648231	6.0184617	.004587156
219	47961	10503459	14.7986486	6.0276502	.004566210
220	48400	10648000	14.8323970	6.0368107	.004545455
221	48841	10793861	14.8660687	6.0459435	.004524887
222	49284	10941048	14.8996644	6.0550489	.004504505
223	49729	11089567	14.9331845	6.0641270	.004484305
224	50176 50625	11239424	14.9666295 15.0000000	6.0731779	.004464286
225 226	51076	11390625 11543176	15.0332964	6.0822020 6.0911994	.004444444
226	51529	11697083	15.0665192	6.1001702	.004424779
227	51984	11852352	15.0996689	6.1001702	.004405286
229	52441	12008989	15.1327460	6.1180332	.004366812
230 231	52900 \$3361	12167000 12326391	15.1657509 15.1986842	6.1269257	.004347826
231	53824	12320391	15.1980842	6.1357924 $6.1446337$	.004329004 .004310345
233	54289	12649337	15.2643375	6.1534495	.004291845
234	54756	12812904	15.2970585	6.1622401	.004273504
235	55225	12977875	15.3297097	6.1710058	.004255319
236	55696	13144256	15.3622915	6.1797466	.004237288
237	56169	13312053	15.3948043	6.1884628	.004219409
238	56644	13481272	15.4272486	6.1971544	.004201681
- 239	57121	13651919	15.4596248	6.2058218	.004184100

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No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
240	57600	13824000	15.4919334	6.2144650	.004166667
241	58081	13997521	15.5241747	6.2230843	.004149378
242	58564	14172488	15.5563492	6.2316797	.004132231
243	59049	14348907	15.5884573	6.2402515	.004115226
244					
	59536	14526784	15.6204994	6.2487998	.004098361
245	60025	14706125	15.6524758	6.2573248	.004081633
246	60516	14886936	15.6843871	6.2658266	.004065041
247	61009	15069223	15.7162336	6.2743054	.004048583
248	61504	15252992	15.7480157	6.2827613	.004032258
249	62001	15438249	15.7797338	6.2911946	.004016064
250	62500	15625000	15.8113883	6.2996053	.004000000
$\begin{array}{c} 250 \\ 251 \end{array}$					
	63001	15813251	15.8429795	6.3079935	.003984064
252	63504	16/03008	15.8745079	6.3163596	.003968254
253	64009	16194277	15.9059737	6.3247035	.003952569
254	64516	16387064	15.9373775	6.3330256	.003937008
255	65025	16581375	15.9687194	6.3413257	.003921569
256	65536	16777216	16.0000000	6.3496042	.003906250
257	66049	16974593	16.0312195	6.3578611	.003891051
258	66564	17173512	16.0623784	6.3660968	.003875969
259	67081	17373979	16.0934769	6.3743111	.003861004
260	67600	17576000	16.1245155	6.3825043	.003846154
261	68121	17779581	16.1554944	6.3906765	.003831418
262	68644	17984728	16.1864141	6.3988279	.003816794
263	69169	18191447	16.2172747	6.4069585	.003802281
264	69696	18399744	16.2480768	6.4150687	.003787879
265	70225	18609625	16.2788206	6.4231583	.003773585
266	70756	18821096	16.3095064	6.4312276	.003759398
267	71289	19034163	16.3401346	6.4392767	.003745318
268	71824	19248832	16.3707055	6.4473057	.003731343
269	72361	19465109	16.4012195	6.4553148	.003717472
270	72900	19683000	16.4316767	6.4633041	.003703704
271	73441	19902511	16.4620776	6.4712736	.003690037
272	73984	20123648	16.4924225	6.4792236	.003676471
273	74529	20346417	16.5227116	6.4871541	.003663004
274	75076	20570824	16.5529454	6.4950653	.003649635
275	75625	20796875	16.5831240	6.5029572	.003636364
$\overline{276}$	76176	21024576	16.6132477	6.5108300	.003623188
277	76729	21253933	16.6433170	6.5186839	.003610108
278	77284	21484952	16.6733320	6.5265189	.003597122
279	77841			6.5343351	.003584229
		21717639	16.7032931		
280	78400	21952000	16.7332005	6.5421326	.003571429
281	78961	22188041	16.7630546	6.5499116	.003558719
282	79524	22425768	16.7928556	6.5576722	.003546099
283	80089	22665187	16.8226038	6.5654144	.003533569
284	80656	22906304	16.8522995	6.5731385	.003521127
285	81225	23149125	16.8819430	6.5808443	.003508772
286	81796	23393656	16.9115345	6.5885323	.003496503
287	82369	23639903	16.9410743	6.5962023	.003484321
288	82944			6.6038545	.003472222
289	83521	23887872	16.9705627		.003460208
		24137569	17.0000000	6.6114890	
290	84100	24389000	17.0293864	6.6191060	.003448276
291	84681	24642171	17.0587221	6.6267054	.003436426
292	85264	24897088	17.0880075	6.6342874	.003424658
293	85849	25153757	17.1172428	6.6418522	.003412969
294	86436	25412184	17.1464282	6.6493998	.003401361
295	87025	25672375	17.1755640	6.6569302	.003389831
296	87616	25934336	17.2046505	6.6644437	.003378378
297	88209	26198073	17.2336879	6.6719403	.003367003
298	88804	26463592	17.2626765	6.6794200	.003355705
299	89401			6.6868831	.003344482
299	03401	26730899	17.2916165	0.0000001	.000011104

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
300	90000	27000000	17.3205081	6.6943295	.003333333
301	90601	27270901	17.3493516	6.7017593	.003322259
302	91204	27543608	17.3781472	6.7091729	.003311258
303	91809	27818127	17.4068952	6.7165700	.003300330
304	92416	28094464	17.4355958	6.7239508	.003289474
305	93025	28372625	17.4642492	6.7313155	.003278689
306	93636	28652616	17.4928557	6.7386641	.003267974
307	94249	28934443	17.5214155	6.7459967	.003257329
308	94864	29218112	17.5499288	6.7533134	.003246753
309	95481	29503629	17.5783958	6.7606143	.003236246
310	96100	29791000	17.6068169	6.7678995	.003225806
311	96721	30080231	17.6351921	6.7751690	.003215434
312	97344	30371328	17.6635217	6.7824229	.003205128
313	97969	30664297	17.6918060	6.7896613	.003194888
314	98596	30959144	17.7200451	6.7968844	.003184713
315	99225	31255875	17.7482393	6.8040921	.003174603
316	99856	31554496	17.7763888	6.8112847	.003164557
317	100489	31855013	17.8044938	6.8184620	.003154574
318	101124	32157432	17.8325545	6.8256242	.003144654
319	101761	32461759	17.8605711	6.8327714	.003134796
320	102400	32768000	17.8885438	6.8399037	.003125000
321	103041	33076161	17.9164729	6.8470213	.003115265
322	103684	33386248	17.9443584	6.8541240	.003105590
323	104329	33698267	17.9722008	6.8612120	.003095975
324	104976	34012224	18.0000000	6.8682855	.003086420
325	105625	34328125	18.0277564	6.8753443	.003076923
326	106276	34645976	18.0554701	6.8823888	.003067485
327	106929	34965783	18.0831413	6.8894188	.003058104
328	107584	35287552	18.1107703	6.8964345	.003048780
329	108241	35611289	18.1383571	6.9034359	.003039514
330	108900	35937000	18.1659021	6.9104232	.003030303
331	109561	36264691	18.1934054	6.9173964	.003021148
332	110224	36594368	18.2208672	6.9243556	.003012048
333	110889	36926037	18.2482876	6.9313008	.003003003
334	111556	37259704	18.2756669	6.9382321	.002994012
335	112225 112896	37595875	18.3030052 18.3303028	6.9451496	.002985075
336 337	113569	3793305 <b>6</b> 38272753	18.3575598	6.9520533 6.9589434	002976190 002967359
338	114244	38614472	18.3847763	6.9658198	.002958580
339	114921	38958219	18.4119526	6.9726826	.002949853
340	115600	39304000	18.4390889	6.9795321	.002941176
341	116281	39651821 40001688	18.4661853 18.4932420	6.9863681 6.9931906	.002932551 .002923977
342 343	116964 117649	40353607	18.5202592	7.0000000	.002925977
344	118336	40707584	18 5472370	7.0067962	.002915452
345	119025	41063625	18.5741756	7.0135791	.002898551
346	119716	41421736	18.6010752	7.0203490	.002890173
347	120409	41781923	18.6279360	7.0271058	.002881844
348	121104	42144192	18.6547581	7.0338497	.002873563
349	121801	42508549	18.6815417	7.0405806	.002865330
350	122500	42875000	18,7082869	7.0472987	.002857143
351	123201	43243551	18.7349940	7.0540041	.002849003
352	123904	43614208	18.7616630	7.0606967	.002840909
353	124609	43986977	18.7882942	7.0673767	.002832861
354	125316	44361864	18.8148877	7.0740440	.002824859
355	126025	44738875	18.8414437	7.0806988	.002816901
356	126736	45118016	18.8679623	7.0873411	.002808989
357	127449	45499293	18.8944436	7.0939709	.002801120
358	128164	45882712	18.92 8879	7.1005885	.002793296
359	128881	46268279	18.9472953	7.1071937	.002785515

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No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
360	129600	46656000	18.9736660	7.1137866	.002777778
361	130321	47045881	19.0000000	7.1203674	.002770083
362	131044	47437928	19.0262976	7.1269360	.002762431
363	131769	47832147	19.0525589	7.1334925	.002754821
364	132496	48228544	19.0787840	7.1400370	.002747253
365	133225	48627125	19.1049732	7.1465695	.002739726
366	133956	49027896	19.1311265	7.1530901	.002732240
367	134689	49430863	19.1572441	7.1595988	.002724796
368	135424	49836032	19.1833261	7.1660957	.002717391
369	136161	50243409	19.2093727	7.1725809	.002710027
370	136900	50653000	19.2353841	7.1790544	.002702703
371	137641	51064811	19.2613603	7.1855162	.002695418
372	138384	51478848	19.2873015	7.1919663	.002688172
373	139129	51895117	19.3132079	7.1984050	.002680965
374	139876	52313624	19.3390796	7.2048322	.002673797
375	140625	52734375	19.3649167	7.2112479	.002666667
376	141376	53157376	19.3907194	7.2176522	.002659574
377	142129	53582633	19.4164878	7.2240450	.002652520
378	142884	54010152	19.4422221	7.2304268	.002645503
379	143641	54439939	19.4679223	7.2367972	.002638522
380	144400	5487200 <b>0</b>	19.4935887	7.2431565	.002631579
381	145161	55306341	19.5192213	7.2495045	.002624672
382	145924	55742968	19.5448203	7.2558415	.002617801
383	146689	56181887	19.5703858	7.2621675	.002610966
384	147456	56623104	19.5959179	7.2684824	.002604167
385	148225	57066625	19.6214169	7.2747864	.002597403
386	148996 149769	57512456 57960603	19.6468827	$7.2810794 \\ 7.2873617$	.002590674 $.002583979$
387 388	150544	58411072	$\begin{array}{c} 19.6723156 \\ 19.6977156 \end{array}$	7.2936330	.002577320
389	151321	58863869	19.7230829	7.2998936	.002570694
1					
390	152100	59319000	19.7484177	7.3061436	.002564103
391	152881 153664	59776471 60236288	$19.7737199 \\ 19.7989899$	7.3123828	.002557545 $.002551020$
392 393	154449	60698457	19.8242276	7.3186114 $7.3248295$	.002531020
394	155236	61162984	19.8494332	7.3310369	.002538071
395	156025	61629875	19.8746069	7.3372339	.002531646
396	156816	62099136	19.8997487	7.3434205	.002525253
397	157609	62570773	19.9248588	7.3495966	.002518892
398	158404	63044792	19.9499373	7.3557624	.002512563
399	159201	63521199	19.9749844	7.3619178	.002506266
400	160000	64000000	20.0000000	7.3680630	.002500000
401	160801	64481201	20.0249844	7.3741979	.002493766
402	161604	64964808	20.0499377	7.3803227	.002487562
403	162409	65450827	20.0748599	7.3864373	.002481390
404	163216	65939264	20.0997512	7.3925418	.002475248
405	164025	66430125	20.1246118	7.3986363	.002469136
406	164836	66923416	20.1494417	7.4047206	.002463054
407	165649	67419143	20.1742410	7.4107950	.002457002
408	166464	67917312	20.1990099	7.4168595 $7.4229142$	.002450980
409	167281	68417929	20.2237484		.002444988
410	168100	68921000	20.2484567	7.4289589	.002439024
411	168921	69426531	20.2731349	7.4349938	.002433090
412	169744	69934528	20.2977831	7.4410189	.002427184
413	170569	70444997	20.3224014	7.4470342	.002421308 .002415459
414 415	$\begin{array}{c} 171396 \\ 172225 \end{array}$	70957944	20.3469899	7.4530399 7.4590359	.002415459
416	173056	71473375 71991296	20.3715488 20.3960781	7.4650223	.002403059
417	173889	71991296 72511713	20.4205779	7.4709991	.002398082
418	174724	73034632	20.4450483	7.4769664	.002392344
419	175561	73560059	20.4694895	7.4829242	.002332544
110	110001	10000000	20.3003000	1.1020212	.00200000

No.   Squares   Cubes   Square Roots   Cube Roots   Reciprocals		1	1	1	1	
421 177241 74618461 20.5182845 7.4918113 .0022375297 422 178084 75151448 20.5126386 7.5007406 .002369698 423 178929 75688067 20.5669638 7.5066607 .002364066 424 179776 76225024 20.5012608 7.51025715 .002258419 425 180625 76765625 20.6155281 7.5184730 .002254941 426 181476 77808776 20.6397674 7.5243652 .002347418 427 182529 77854483 20.6639783 7.5184730 .002352941 428 183184 78402752 20.6831609 7.5361221 .002336449 429 184041 78953589 20.7123152 7.5419867 .002331094 429 184041 78953589 20.7123152 7.5419867 .002331094 430 184900 79507000 20.7364414 7.5478423 .002345921 431 185761 80062991 20.7605395 7.55638588 .002290184 432 186624 80621568 20.7846097 7.55638588 .002290184 433 187489 8118273 20.8066520 7.55638588 .002290184 434 188356 81746504 20.8326667 7.5711743 .002304409 435 189225 82312875 20.856636 7.5769849 .002238831 436 19006 82881856 20.8806130 7.5687869 .002298851 437 190069 82881856 20.8806130 7.5687869 .002298851 438 191844 84027672 20.9284495 7.5943633 .002288383 438 191844 84027672 20.9284495 7.5043633 .002288383 440 193600 85184000 20.9761770 7.659369 .002298851 441 194481 88766121 21.0000000 7.6116626 .002267574 442 195364 8836888 21.0237660 7.617416 .0022672727 441 194481 88766121 21.0000000 7.6116626 .002267574 444 197136 8752884 21.0719075 7.628887 .002237586 445 198025 88121125 21.0950231 7.6340043 .002227794 446 19800 8814623 21.1423745 7.6340637 .002227794 447 19809 8814623 21.1423745 7.6340647 .002227194 448 200704 89915892 21.1660105 7.6517247 .002237136 448 200704 89915892 21.1660105 7.6517247 .002237136 449 201601 9518849 21.9286706 7.6687665 .002217295 446 20304 92345408 21.242353 7.7138448 .002172984 450 202500 91125000 21.2132034 7.6680043 .002227294 461 219501 6000000 7.6116626 .002267574 462 204304 92345408 21.267906 7.6516246 .00221898 463 200764 89915892 21.660005 7.658793 .0022237506 466 217160 19763850 21.1423745 7.768903 .0022237506 467 208849 94584939 21.267606 7.658793 .002237506 468 21960 19786670 21.2660077 7.788903 .002236760 470 220000 108803000 21.679484 7.7748901 .0021	No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
421 177241 74618461 20.5182845 7.4918113 .0022375297 422 178084 75151448 20.5126386 7.5007406 .002369698 423 178929 75688067 20.5669638 7.5066607 .002364066 424 179776 76225024 20.5012608 7.51025715 .002258419 425 180625 76765625 20.6155281 7.5184730 .002254941 426 181476 77808776 20.6397674 7.5243652 .002347418 427 182529 77854483 20.6639783 7.5184730 .002352941 428 183184 78402752 20.6831609 7.5361221 .002336449 429 184041 78953589 20.7123152 7.5419867 .002331094 429 184041 78953589 20.7123152 7.5419867 .002331094 430 184900 79507000 20.7364414 7.5478423 .002345921 431 185761 80062991 20.7605395 7.55638588 .002290184 432 186624 80621568 20.7846097 7.55638588 .002290184 433 187489 8118273 20.8066520 7.55638588 .002290184 434 188356 81746504 20.8326667 7.5711743 .002304409 435 189225 82312875 20.856636 7.5769849 .002238831 436 19006 82881856 20.8806130 7.5687869 .002298851 437 190069 82881856 20.8806130 7.5687869 .002298851 438 191844 84027672 20.9284495 7.5943633 .002288383 438 191844 84027672 20.9284495 7.5043633 .002288383 440 193600 85184000 20.9761770 7.659369 .002298851 441 194481 88766121 21.0000000 7.6116626 .002267574 442 195364 8836888 21.0237660 7.617416 .0022672727 441 194481 88766121 21.0000000 7.6116626 .002267574 444 197136 8752884 21.0719075 7.628887 .002237586 445 198025 88121125 21.0950231 7.6340043 .002227794 446 19800 8814623 21.1423745 7.6340637 .002227794 447 19809 8814623 21.1423745 7.6340647 .002227194 448 200704 89915892 21.1660105 7.6517247 .002237136 448 200704 89915892 21.1660105 7.6517247 .002237136 449 201601 9518849 21.9286706 7.6687665 .002217295 446 20304 92345408 21.242353 7.7138448 .002172984 450 202500 91125000 21.2132034 7.6680043 .002227294 461 219501 6000000 7.6116626 .002267574 462 204304 92345408 21.267906 7.6516246 .00221898 463 200764 89915892 21.660005 7.658793 .0022237506 466 217160 19763850 21.1423745 7.768903 .0022237506 467 208849 94584939 21.267606 7.658793 .002237506 468 21960 19786670 21.2660077 7.788903 .002236760 470 220000 108803000 21.679484 7.7748901 .0021	490	176400	74088000	20 4939015	7 4888794	000380050
422         178084         75151448         20.5426886         7.5007406         .00236968           424         179776         76225024         20.5912603         7.516515         .002358491           425         180625         76765625         20.6165281         7.5125715         .002358491           426         181476         77808776         20.6397674         7.5184730         .00235491           428         183184         78402752         20.6881609         7.5362482         .002347418           429         184041         7890388         20.6712312         7.5418967         .002331024           430         184900         79507000         20.7864414         7.5478623         .002331084           431         185761         80062991         20.7605395         7.5536888         .002331085           433         187489         8182737         20.8086520         7.563548         .002309469           434         188356         81746504         20.826667         7.563548         .00239469           435         189225         28312875         20.856639         7.5676849         .00229851           436         190096         828453458         20.9044550         7.588573         .0022						
428						
424         179776         76225024         20.5912603         7.5125715         .002252941           426         181476         77808776         20.6397674         7.524852         .002347418           427         182329         77854483         20.6839783         7.5302482         .002341920           428         183184         78402752         20.6881009         7.5361221         .002336449           429         184041         7895389         20.7123152         7.5419867         .002233102           430         184900         79507000         20.7364414         7.5478423         .002235581           431         185761         80662991         20.760595         7.5565688         .002320186           432         185624         80621568         20.7846997         7.563588         .00230486           433         1857489         81182737         20.856636         7.5711743         .002290449           435         189225         82312575         20.856636         7.5711743         .0022904469           436         19096         83453453         20.9045450         7.589593         .002288833           437         190869         83453453         20.904546         7.5768595         .0						
425         180625         76765625         20.6135281         7.5184780         .002352941           427         182329         77854483         20.6639783         7.5302482         .002347418           428         183184         78402752         20.6881609         7.5361221         .002334492           429         184041         78953589         20.7123152         7.5419867         .002334029           430         184900         79507000         20.7364414         7.547423         .00233581           431         185761         8062991         20.7605395         7.559888         .002390188           432         186624         80621568         20.7846997         7.559368         .00230489           433         187489         81182737         20.8086520         7.565348         .00230449           435         189225         82312875         20.8566386         7.5768849         .002298578           437         190969         82881856         20.8806130         7.585788         .002298578           437         190969         83458458         20.9045450         7.5855898         .00228851           438         191844         80276772         20.952368         7.6001385         .0022	423	178929	75686967	20.5669638	7.5066607	.002364066
425	424	179776	76225024	20.5912603	7.5125715	.002358491
426         181476         77808776         20.6397674         7.5243652         .002347418           427         182329         77854483         20.6689783         7.5302482         .002336449           429         181041         78953589         20.7123152         7.5419867         .002336449           430         184900         79507000         20.786414         7.5478423         .002320186           432         186624         80621568         20.784414         7.5478423         .002320186           433         187489         81182737         20.808650         7.5595288         .002314815           434         188356         81746634         20.8326667         7.551343         .002390469           435         189225         82812875         20.8566366         7.571743         .002298578           436         190096         82881856         20.8866130         7.5827865         .002299578           437         19069         83453453         20.9045450         7.584560         .002299578           439         192721         84604519         20.9523268         7.601385         .002277794           440         193600         85184000         20.9761770         7.6059049         .0	425		76765625	20.6155281		009359941
427         183294         77854483         20,6639783         7,53612482         0.00241920           429         184041         78953589         20,7123152         7,5419867         0.02331002           430         184900         79507000         20,7364414         7,6478423         0.02325581           431         185761         80662991         20,7605395         7,5595268         0.02329186           432         186624         80621568         20,7846997         7,5595268         0.02341815           433         187489         81182737         20,8086520         7,55759849         0.0229851           434         188356         81746504         20,8326667         7,5711743         0.0229851           435         189225         82312875         20,856636         7,5768449         0.02298578           437         190969         8345453         20,9945450         7,5857863         0.0228836           438         191844         8027672         20,9523268         7,605394         0.002288105           440         193600         85184000         20,952308         7,6053949         0.0227727           441         194481         85766121         21,000000         7,6116626         0						000002041
428         183184         78402752         20.6881609         7.5361221         .002236049           429         184041         78953589         20.7123152         7.5419867         .002331002           430         184900         79507000         20.7605395         7.5536888         .002325581           431         185761         80062991         20.7605395         7.5536888         .002320186           432         186624         8061568         20.784697         7.5595268         .002314815           433         187489         81182737         20.8086520         7.5653548         .002309469           434         188356         81746504         20.8326667         7.5711743         .002298578           435         189225         82312875         20.8506386         7.5769849         .002298578           437         190969         83453453         20.914196         7.5943633         .002288105           439         191844         8027672         20.9244195         7.5943633         .002288105           439         192721         84604519         20.9523268         7.6016385         .002277794           440         193600         85184000         20.9761770         7.6059049 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td></t<>						
429         184041         78953589         20.7123152         7.5419867         .002331062           430         184900         79507000         20.7364414         7.5478423         .002320186           431         185761         80062991         20.7605395         7.5595268         .00231081           432         186624         80621668         20.7846097         7.5595268         .002309469           433         187489         81182737         20.8066520         7.5595268         .002309469           434         188356         81746504         20.8326667         7.5769849         .002309469           436         190066         82881856         20.8066320         7.5827665         .002298578           437         190969         83453453         20.9045450         7.588793         .002288106           439         192721         84604519         20.9523268         7.6013863         .002272727           441         19481         85766121         21.0000000         7.6116626         .0022772727           442         19364         8635088         21.0237960         7.611416         .002257386           443         196249         86938307         21.0475652         7.6231519 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td></td<>						
430         184900         79507000         20.7364414         7.5478423         .002325581           431         185761         80062991         20.7605395         7.553688         .002301841           432         186624         80621568         20.7846997         7.5596268         .002301841           433         187489         81182737         20.8086520         7.5653548         .0023094147           435         189225         82312875         20.856636         7.5769849         .0023094147           436         190069         82881856         20.8806130         7.5827865         .002298851           437         190969         83453453         20.9045450         7.588793         .00228830           438         191844         84027672         20.9523268         7.601385         .002287904           440         133600         85184000         20.9761770         7.6059049         .002277904           441         194361         85638887         21.037960         7.6174116         .002267443           442         195364         86350887         21.0475652         7.6231519         .002257794           444         197136         8752884         21.0713075         7.634607						.002336449
430         184900         79507000         20.7864414         7.5478428         .002325581           431         185761         80062991         20.7665395         7.5598268         .00231815           432         186624         80621568         20.7846997         7.5595268         .002301815           433         187489         81182737         20.8086520         7.56753548         .002304147           435         189225         82312875         20.856636         7.5769849         .002304147           436         19006         82881856         20.8806139         7.585798         .002298851           437         190969         84453453         20.9045450         7.5885793         .00228830           438         191844         84027672         20.9523268         7.601385         .002287794           440         193600         85184000         20.9761770         7.6059049         .002277794           441         19461         85766121         21.000000         7.6116626         .002267574           442         195364         86350887         21.0475652         7.6231519         .002257794           444         197136         8752884         21.0713075         7.6231519         .0	429	184041	78953589	20.7123152	7.5419867	.002331002
185761	490	104000	70507000	90 7964414	7 5470400	000005504
432         186624         80621568         20.7846097         7.5595268         .002309469           433         187489         81182737         20.8086520         7.5653548         .002309469           434         188356         81746504         20.8326667         7.5751743         .0023094147           435         189225         82312875         20.856638         7.5769849         .002298578           436         190096         82881856         20.8806130         7.5877865         .002298578           437         190969         83453453         20.904445         7.5885793         .002288380           438         192721         84604519         20.9284495         7.594363         .002287904           440         193600         85184000         20.9761770         7.6059049         .00227794           441         19481         85766121         21.000000         7.6116626         .002267574           442         195364         86359887         21.0237960         7.6174116         .0022672443           443         196249         86983807         21.0475652         7.6316067         .0022525252           445         198016         88716536         21.1187121         7.6403213         <						
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434 188356 81746504 20.8326667 7.5711743 .002204147 435 189225 82312875 20.8566536 7.5769849 .002298851 436 190096 82881856 20.8806130 7.5827865 .002293578 437 190969 83453453 20.9046450 7.5885793 .0022283105 438 191844 84027672 20.9284495 7.5943633 .0022283300 439 192721 84604519 20.9523268 7.6001385 .0022277904 440 193600 85184000 20.9761770 7.6059049 .002277277 441 194481 85766121 21.0000000 7.6116626 .002267574 442 195364 86350888 21.0237960 7.6174116 .002262443 443 196249 8693807 21.0475652 7.6231519 .002257356 444 197136 87528384 21.0713075 7.6288837 .002257252 445 198025 88121125 21.0950231 7.6346067 .002247191 446 198916 88716536 21.1187121 7.6403213 .002232136 447 199809 89314623 21.1463745 7.6460272 .002237136 448 200704 89915392 21.1660105 7.6517247 .002232143 449 201601 90518849 21.1886201 7.6574138 .002227171 450 202500 91125000 21.2132034 7.6687665 .002227171 451 203401 91733851 21.2367606 7.6687665 .002227179 454 204104 92345408 21.2602916 7.6674639 .002227229 455 204304 92345408 21.2602916 7.6687665 .0022217295 456 207025 94196375 21.3837629 7.6913717 .002197802 457 208849 9544393 21.3775583 7.7026246 .0022188184 459 210661 99576664 21.3072758 7.6857328 .002207566 456 207936 9418816 21.3574583 7.7026246 .002183849 458 209764 96071912 21.409346 7.7082388 .002183846 459 210681 96702579 21.2836857 7.6913717 .002197802 460 211600 97336000 21.4476106 7.7184426 .002183184 460 211600 97336000 21.4476106 7.7184426 .002183184 460 211600 97336000 21.4476106 7.7184426 .002183184 463 214369 99952847 21.5174348 7.7361877 .002197802 466 213444 9611128 21.409346 7.7082388 .002183646 467 218989 10487563 21.5664078 7.7689620 .002169507 468 21961 103161709 21.6564078 7.7689620 .002169507 469 21961 103161709 21.6564078 7.7689620 .002169507 470 220900 10382300 21.6794834 7.7808944 .002118644 472 222784 105154048 21.7255610 7.789460 .002132196 470 220900 10382300 21.6794834 7.7808940 .002123142 472 222784 105154048 21.7255610 7.7859928 .002109705 476 226576 107850176 21.8174242 7.8079254 .002109705 477 220900 103823			80621568			.002314815
434 188356 81746504 20.8326667 7.5711743 .002204147 435 189225 82312875 20.8566536 7.5769849 .002298851 436 190096 82881856 20.8806130 7.5827865 .002293578 437 190969 83453453 20.9045450 7.5885793 .002228330 438 191844 84027672 20.9284195 7.5943633 .002288310 439 192721 84604519 20.9523268 7.6001385 .002227904 440 193600 85184000 20.9761770 7.6059049 .00227727 441 194481 85766121 21.0000000 7.6116626 .002267574 442 195364 86350888 21.0237960 7.6174116 .002262443 443 196249 8693807 21.0475652 7.6231519 .002257386 444 197136 87528384 21.0713075 7.6288837 .002257262 445 198025 88121125 21.0950231 7.6346067 .002247191 446 198916 88716536 21.1187121 7.6403213 .002232136 447 199809 89314623 21.1460165 7.6517247 .002237186 448 200704 89915392 21.1660105 7.6517247 .002237136 449 201601 99518849 21.1886201 7.6574138 .002227171 450 202500 91125000 21.2132034 7.6630943 .002222712 451 203401 91733851 21.2367606 7.6687665 .002217295 454 206116 93576664 21.3072758 7.6857328 .0022075064 455 201304 92345408 21.2602916 7.6744303 .002212289 456 207025 94196375 21.3807290 7.6913717 .002197802 457 208849 95443993 21.3775583 7.7026246 .002217395 456 207025 94196375 21.3307290 7.6913717 .002197802 457 208849 95443993 21.3775583 7.7026246 .0022188184 460 211600 97336000 21.4476106 7.7194426 .002188184 458 209764 96071912 21.4009346 7.7082388 .002183406 457 208849 95443993 21.3775583 7.7026246 .002188184 468 209764 96071912 21.4009346 7.7082388 .002187804 469 211460 97336000 21.4476106 7.7194426 .002187802 460 211600 97336000 21.4476106 7.7194426 .002188184 468 21961 103161709 21.6564078 7.7684080 .002178092 467 208900 10382300 21.6794834 7.7864904 .002123142 472 222744 102503232 21.6564078 7.7684620 .002183193 468 21964 103161709 21.6564078 7.7684080 .002118293 474 222676 106496424 21.7715411 7.7999745 .002119705 475 226565 1071875 21.7914947 7.802454 .00210840 477 220900 10382300 21.6794834 7.7804904 .002123142 478 222784 109150333 21.8406329 7.78133892 .002109606 477 220900 10382300 21.6794834 7.7804904 .002123142 478 226576 107850	433	187489	81182737	20.8086520	7.5653548	.002309469
189225	434	188356		20.8326667	7.5711743	
436         190969         8281856         20.8806130         7.5827865         .002288303           437         190969         83453453         20.9045450         7.5885793         .002288303           438         191844         84027672         20.9284495         7.5943633         .002283303           439         192721         84604519         20.9561770         7.601385         .002277794           440         193600         85184000         20.9761770         7.6059049         .002277274           441         19481         85766121         21.000000         7.6116626         .002267574           442         195364         86350888         21.0237960         7.6174116         .00226443           443         196249         8698307         21.0475652         7.6231519         .002257386           444         197136         87528384         21.0713075         7.6288837         .002257386           445         198091         8811623         21.1423745         7.6403213         .0022247191           446         198916         88716586         21.1187121         7.6403213         .0022273736           448         200704         89915392         21.166105         7.6517247						
437         19069         83453453         20.9045450         7.5885793         .002288320           438         191844         84027672         20.9284495         7.5943633         .002283105           439         192721         84604519         20.9523268         7.6001385         .002277904           440         193600         85184000         20.9761770         7.6059049         .002277727           441         19481         85766121         21.000000         7.6116626         .002227774           442         195364         8635888         21.0237960         7.6174116         .002262443           443         196249         86938307         21.0476652         7.6231519         .002257386           444         197136         8752834         21.0193075         7.628837         .002257384           445         19805         88121125         21.0950231         7.6346067         .002247191           446         198916         88716536         21.1187121         7.6408213         .002224135           447         199809         89314623         21.1876201         7.6574138         .002227136           448         200704         89915392         21.1660105         7.6574138         .						
438         191844         84027672         20.9284195         7.5043638         .002283105           439         192721         84604519         20.9523268         7.6001385         .002277904           440         193600         85184000         20.9761770         7.6059049         .00227727           441         194481         85766121         21.000000         7.6116626         .002267574           442         195364         86350888         21.0237960         7.6174116         .00226743           443         196249         86938307         21.0476652         7.6231519         .002257366           444         197136         87528384         21.0718075         7.6386067         .002237366           445         198016         88716536         21.1187121         7.6406072         .002237136           447         199809         89314623         21.1187121         7.6406072         .002237136           448         200704         89915392         21.1660105         7.6517247         .002237136           449         201601         9015849         21.1896201         7.6574138         .0022277171           450         202500         91125000         21.2132034         7.663043 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td></t<>						
439         192721         84604519         20.9523268         7.600385         .002277904           440         193600         85184000         20.9761770         7.6059049         .0022772727           441         194481         85766121         21.0000000         7.6116626         .002267574           442         195364         86350888         21.0237960         7.6174116         .002267348           443         196249         86938307         21.047652         7.6231519         .002257386           444         197136         87528384         21.01718075         7.6231519         .0022525252           445         198025         88121125         21.0950231         7.6346067         .002247191           446         198916         88716586         21.1187121         7.6406072         .002237136           447         199809         89314623         21.11896201         7.6571438         .002227171           448         200704         89915392         21.1896201         7.6574438         .0022227171           450         202500         91125000         21.2132034         7.6630943         .002227222           451         203401         91733851         21.2367606         7.6744303						
439         192721         84604519         20.9523268         7.600385         .002277904           440         193600         85184000         20.9761770         7.6059049         .0022772727           441         194481         85766121         21.0000000         7.6116626         .002267574           442         195364         86350888         21.0237960         7.6174116         .002267348           443         196249         86938307         21.047652         7.6231519         .002257386           444         197136         87528384         21.01718075         7.6231519         .0022525252           445         198025         88121125         21.0950231         7.6346067         .002247191           446         198916         88716586         21.1187121         7.6406072         .002237136           447         199809         89314623         21.11896201         7.6571438         .002227171           448         200704         89915392         21.1896201         7.6574438         .0022227171           450         202500         91125000         21.2132034         7.6630943         .002227222           451         203401         91733851         21.2367606         7.6744303	438	191844	84027672	20.9284495	7.5943633	.002283105
440         193600         85184000         20.9761770         7.6059049         .002272727           441         194481         85766121         21.0000000         7.6116626         .002262443           442         195364         86350888         21.0237960         7.6174116         .002262443           443         196249         86938307         21.0475652         7.6231519         .002257836           444         197136         87528384         21.0713075         7.6288887         .0022525252           445         198025         88121125         21.0950231         7.6346067         .002247191           446         198916         88716536         21.1187121         7.6403213         .002247191           447         199809         89314623         21.1423745         7.640222         .002237136           448         200704         89915392         21.1660105         7.6574138         .002227171           450         202500         91125000         21.2132034         7.663043         .002227264           451         203401         91738551         21.2367606         7.6744303         .0022217295           452         204304         92345408         21.2602916         7.6744303	439	192721	84604519	20.9523268	7.6001385	.002277904
441         194481         85766121         21.0000000         7.6116626         .002267574           442         195364         86350888         21.0237960         7.6174116         .002262443           443         196249         86938307         21.0475652         7.6281519         .002257386           444         197136         87528384         21.0713075         7.6288837         .002257352           445         198016         88121125         21.0950231         7.6346067         .002247152           446         198916         88716536         21.1187121         7.6403213         .002242152           447         199809         89314623         21.1426745         7.6460272         .002237136           448         200704         89915392         21.1866105         7.657438         .002227714           450         202500         91125000         21.2132034         7.6630943         .002227222           451         203401         91733851         21.2367606         7.6687665         .002217295           452         204304         92345408         21.2602916         7.6744303         .002227506           453         205209         92556677         21.2837967         7.6806857	1					
442         195364         86350888         21.0237960         7.6174116         .002262443           443         196249         86938307         21.0475652         7.6231519         .002252252           444         197136         87528384         21.0713075         7.628887         .002252252           445         198916         88716536         21.1187121         7.6346067         .002242152           447         199809         89314623         21.1423745         7.6460272         .002237136           448         200704         89915392         21.1660105         7.6574138         .002227171           450         202500         91125000         21.2132034         7.6630943         .002227171           451         203401         91733851         21.2367606         7.6687665         .002217295           453         205209         92959677         21.2837967         7.6806837         .002207506           454         206116         93576664         21.3072758         7.6857328         .0022207506           455         207025         94196375         21.3307290         7.6913717         .002197802           456         207936         94818816         21.3571583         7.7026246						
443         196249         86938307         21.0475652         7.6231519         .002257386           444         197136         87528384         21.0713075         7.6288837         .002252252           445         198025         88121125         21.0950231         7.6288837         .002247191           446         198916         88716536         21.1187121         7.6403213         .002247191           448         200704         89315392         21.1660105         7.6517247         .002237136           448         200704         89915392         21.1660105         7.6574138         .002227171           450         202500         91125000         21.2132034         7.6630943         .002227295           451         203401         91733851         21.2367606         7.6687665         .002217295           452         204304         92345408         21.2602916         7.6744303         .002217295           453         205209         92959677         21.2837967         7.6806857         .002207506           454         206116         93576664         21.3072758         7.6857328         .002220543           455         207025         94196375         21.30729         7.691717         <						
443         196249         86938307         21.0475652         7.6231519         .0022572836           444         197136         87528384         21.0713075         7.6288837         .002252252           445         198025         88121125         21.0950231         7.6346067         .002247191           446         199809         89314623         21.1187121         7.6403213         .002242152           448         200704         89915392         21.1660105         7.6517247         .002237136           448         200704         89915849         21.1896201         7.6574138         .002227171           450         202500         91125000         21.2132034         7.6630943         .002227295           451         203401         91733851         21.2367606         7.6687655         .002217295           452         204304         92345408         21.2609916         7.6744303         .002217295           453         205209         9295677         21.2837967         7.6806857         .002207506           454         206116         93576664         21.3072758         7.6857328         .0022292643           455         207025         94196375         21.307290         7.913717	442	195364	86350888	21.0237960	7.6174116	.002262443
444         197136         87528384         21.0713075         7.6288837         .002252252           445         198016         88716536         21.1187121         7.6346067         .002247191           447         199809         89314623         21.1423745         7.6460272         .002237136           448         200704         89915392         21.1660105         7.6574138         .002227171           450         202500         91125000         21.2132034         7.6680943         .002227171           450         202500         91125000         21.2367606         7.6687665         .002217295           451         203401         91733851         21.2367606         7.6687665         .002217295           452         204304         92345408         21.2602916         7.6744303         .002212389           453         205209         92959677         21.2837967         7.6806857         .002207506           454         206116         93576664         21.3072758         7.6857328         .002207506           455         207936         94818816         21.3541565         7.6970023         .002192982           457         208849         95443993         21.3775583         7.7097024	443	196249	86938307	21.0475652		.002257336
445         198025         88121125         21.0950231         7.6346067         .002247191           446         198916         88716536         21.1187121         7.6403213         .002247152           447         199809         89314623         21.1423745         7.6408213         .002237136           448         200704         89915392         21.1660105         7.6517247         .002232143           449         201601         90518849         21.1896201         7.6574138         .0022272171           450         202500         91125000         21.2132034         7.6630943         .002222222           451         203401         91733851         21.2367606         7.6687665         .002217295           452         204304         92345408         21.2602916         7.6744303         .002212389           453         205209         92959677         21.2837967         7.6806857         .002207506           454         206116         93576664         21.3072758         7.6806857         .002202643           457         208849         95443993         21.3541565         7.6970023         .00218982           457         208849         964499671912         21.4009346         7.7082388				21.0713075		002252252
446         198916         88716536         21.1187121         7.6403213         .002242152           447         199809         89314623         21.1423745         7.6460272         .002237136           448         200704         89915592         21.1660105         7.6574138         .002227171           450         202500         91125000         21.2132034         7.6630943         .002222222           451         203401         91733851         21.2367606         7.6687665         .002217295           452         204304         92345408         21.2602916         7.6744303         .002212389           453         205209         92959677         21.2837967         7.6806857         .002207506           454         206116         93576664         21.3072758         7.691717         .002197802           456         207936         94196375         21.3307290         7.6913717         .002197802           457         208849         95443993         21.3775583         7.7026246         .002188184           458         209764         96071912         21.4009346         7.7026246         .002188184           459         210681         96702579         21.4242853         7.7138448						002202202
447         199809         89314623         21.1423745         7.6460272         .002237136           448         200704         89915392         21.1660105         7.6517247         .002232143           449         201601         90518849         21.1896201         7.6574138         .002227171           450         202500         91125000         21.2132034         7.6687665         .002217295           451         203401         91733851         21.2367606         7.6687665         .002217295           452         204304         92345408         21.2602916         7.6744303         .002212389           453         205209         92959677         21.2837967         7.6806857         .002207506           454         206116         93576664         21.3072758         7.680857         .002207506           455         207025         94196375         21.3307290         7.6913717         .002197802           457         208849         95443933         21.3775583         7.702246         .00218812           458         209764         96071912         21.4009346         7.7082388         .002183146           459         216681         96702579         21.4242853         7.7138448         <				01 1107101		
448         200704         89915392         21.1660105         7.6517247         .002232143           449         201601         90518849         21.1896201         7.6574138         .002227171           450         202500         91125000         21.2132034         7.6630943         .00222222           451         203401         91733851         21.2367606         7.6687665         .002217295           452         204304         92345408         21.2602916         7.6744303         .002217295           453         205209         92959677         21.2837967         7.6806857         .002207506           454         206116         93576664         21.3072758         7.6857328         .002207506           455         207025         94196375         21.3307290         7.6913717         .002197802           456         207936         94818816         21.3541565         7.6970023         .002192982           457         208849         95443993         21.3775583         7.7026246         .002188184           458         209764         96071912         21.4009346         7.7082388         .002183494           459         210681         96702579         21.4242853         7.7138448						
449         201601         90518849         21.1896201         7.6574138         .002227171           450         202500         91125000         21.2132034         7.6630943         .002222222           451         204301         91733851         21.2367606         7.6687665         .002217295           452         204304         92345408         21.2602916         7.6744303         .002212389           453         205209         92959677         21.2837967         7.6806857         .002207506           454         206116         93576664         21.3072758         7.6857328         .002202643           455         207025         94196375         21.3307290         7.6913717         .002197802           456         207936         94818816         21.3541565         7.6970023         .00219982           457         208849         95443993         21.3775583         7.7026246         .002188184           458         209764         96071912         21.4009346         7.7082388         .002188184           459         210681         96702579         21.4242853         7.7138448         .002178649           460         211600         97336000         21.4476106         7.7250325						
450         202500         91125000         21.2132034         7.6630943         .002222222           451         203401         91733851         21.2367606         7.6687665         .002217295           452         204304         92345408         21.2602916         7.6744303         .002212389           453         205209         92959677         21.2837967         7.6806857         .002207506           454         206116         93576664         21.3072758         7.6857328         .002202643           455         207025         94196375         21.3807290         7.6913717         .002197802           456         207936         94818816         21.3541565         7.6970023         .002197802           457         208849         95443993         21.3775583         7.7026246         .002188184           458         209764         96071912         21.4009346         7.7082388         .002188184           459         210681         96702579         21.4242853         7.7138448         .002178649           460         211600         97336000         21.4476106         7.7194426         .002189197           461         212521         97972181         21.4709106         7.7250325	448	200704	89915392	21.1660105	7.6517247	.002232143
450         202500         91125000         21.2132034         7.6630943         .002222222           451         203401         91733851         21.2367606         7.6687665         .002217295           452         204304         92345408         21.2602916         7.6744303         .002212389           453         205209         92959677         21.2837967         7.6806857         .002207506           454         206116         93576664         21.3072758         7.6837328         .002202643           455         207025         94196375         21.3307290         7.6913717         .002197802           456         207936         94818816         21.3541565         7.6970023         .002198982           457         208849         95443993         21.3775583         7.7026246         .002188184           458         209764         96071912         21.4009346         7.7082388         .002188184           459         210681         96702579         21.4242853         7.7138448         .002178649           460         211600         97336000         21.4476106         7.7194426         .00213919           461         212521         97972181         21.4709106         7.7250325	449	201601	90518849	21.1896201	7.6574138	.002227171
451         203401         91733851         21.2367606         7.6687665         .002217295           452         204304         92345408         21.2602916         7.6744303         .002217389           453         205209         92959677         21.2837967         7.6806857         .002207506           454         206116         93576664         21.3072758         7.6857328         .002202643           455         207025         94196375         21.3807290         7.6913717         .002197802           456         207936         94818816         21.3541565         7.6970023         .002192982           457         208849         95443993         21.3775583         7.7026246         .002188184           458         209764         96071912         21.409346         7.7082388         .002188106           459         210681         96702579         21.4242853         7.7138448         .002178649           460         211600         97336000         21.4476106         7.7194426         .002178913           461         212521         97972181         21.4709106         7.7250325         .002169197           462         213444         98611128         21.4941853         7.7361877				01 0190094		
452         204304         92345408         21.2602916         7.6744303         .002212389           453         205209         92959677         21.2837967         7.6806857         .002207506           454         206116         93576664         21.3072758         7.6857328         .002202643           455         207025         94196375         21.3307290         7.6913717         .002197802           456         207936         94818816         21.3541565         7.6970023         .002192982           457         208849         95443993         21.3775583         7.7026246         .002188184           458         209764         96071912         21.4009346         7.7082388         .002183406           459         210681         96702579         21.4242853         7.7138448         .002178649           460         211600         97336000         21.4476106         7.7194426         .002173913           461         212521         97972181         21.4709106         7.7250325         .002169197           462         213444         98611128         21.4941853         7.736147         .002159582           463         214369         99252847         21.5174348         7.7861877						
453         205209         92959677         21.2837967         7.6806857         .002207506           454         206116         93576664         21.3072758         7.6857328         .002202643           455         207025         94196375         21.3307290         7.6913717         .002197802           456         207936         94818816         21.3541565         7.6970023         .002192982           457         208849         95443993         21.3775583         7.7082388         .002188184           458         209764         96071912         21.4009346         7.7082388         .002188184           459         210681         96702579         21.4242853         7.7138448         .002178649           460         211600         97336000         21.4476106         7.7194426         .002173913           461         212521         97972181         21.4709106         7.7250325         .002169197           462         213444         98611128         21.4941853         7.7306141         .002164502           463         214369         99252847         21.5174348         7.7361877         .002159827           464         215296         9987344         21.5406592         7.7417532						
454         206116         93576664         21,3072758         7,6857328         .002202643           455         207025         94196375         21,3307290         7,6913717         .002197802           456         207936         94818816         21,3541565         7,6970023         .002192982           457         208849         95443993         21,3775583         7,7026246         .002188184           458         209764         96071912         21,4009346         7,7082388         .002188184           459         210681         96702579         21,4242853         7,7138448         .002178649           460         211600         97336000         21,4476106         7,7194426         .002173913           461         212521         97972181         21,4799106         7,7250325         .002169197           462         213444         98611128         21,4941853         7,736141         .002164502           463         214369         99252847         21,5174348         7,7361877         .002159827           464         215296         99897344         21,5406592         7,7417532         .002150588           466         216225         100544625         21,5638587         7,7634023	452	204304	92345408	21.2602916	7.6744303	.002212389
454         206116         93576664         21,3072758         7,6857328         .002202643           455         207025         94196375         21,3307290         7,6913717         .002197802           456         207936         94818816         21,3541565         7,6970023         .002192982           457         208849         95443993         21,3775583         7,7026246         .002188184           458         209764         96071912         21,4009346         7,7082388         .002188184           459         210681         96702579         21,4242853         7,7138448         .002178649           460         211600         97336000         21,4476106         7,7194426         .002173913           461         212521         97972181         21,4799106         7,7250325         .002169197           462         213444         98611128         21,4941853         7,736141         .002164502           463         214369         99252847         21,5174348         7,7361877         .002159827           464         215296         99897344         21,5406592         7,7417532         .002150588           466         216225         100544625         21,5638587         7,7634023	453	205209	92959677	21.2837967	7.6806857	.002207506
455         207025         94196375         21.3307290         7.6913717         .002197802           456         207936         94818816         21.3541565         7.6970023         .002192982           457         208849         95443993         21.3775583         7.7026246         .002188184           458         209764         96071912         21.4009346         7.7082388         .002183406           459         210681         96702579         21.4242853         7.7138448         .002178649           460         211600         97336000         21.4476106         7.7194426         .002173913           461         212521         97972181         21.4709106         7.7250325         .002169197           462         213444         98611128         21.4941853         7.7361877         .002159827           463         214369         99252847         21.5174348         7.7361877         .002159827           464         215296         99897344         21.5406592         7.7417532         .002155172           465         216225         100544625         21.5638587         7.7473109         .002155038           466         217156         101194696         21.5870331         7.7528666	454	206116	93576664	21.3072758	7.6857328	.002202643
456         207936         94818816         21.3541565         7.6970023         .002192982           457         208849         95443993         21.3775583         7.7026246         .002188184           458         209764         96071912         21.4009346         7.7082388         .002183406           459         210681         96702579         21.4242853         7.7138448         .002178649           460         211600         97336000         21.4476106         7.7194426         .002173913           461         212521         97972181         21.4709106         7.7250325         .002169197           462         213444         98611128         21.4941853         7.7306141         .002164502           463         214869         99252847         21.5174348         7.7361877         .002159827           464         215296         98897344         21.5106592         7.7417532         .002159827           465         216225         100544625         21.5638587         7.7473109         .002150588           466         217156         101194696         21.5870331         7.7584023         .002145923           468         219024         102503232         21.6333077         7.7639361						
457         208849         95443993         21.3775583         7.7026246         .002188184           458         209764         96071912         21.4009346         7.7082388         .002183406           459         210681         96702579         21.4242853         7.7138448         .002178649           460         211600         97336000         21.4476106         7.7194426         .002173913           461         212521         97972181         21.4709106         7.7250325         .002169197           462         213444         98611128         21.4941853         7.7306141         .002164502           463         214369         99252847         21.5174348         7.7361877         .002159827           464         215296         99897344         21.5406592         7.7417532         .002150783           465         216225         100544625         21.5638587         7.7473109         .002150538           466         217156         101194696         21.5870331         7.7528606         .002145923           468         219024         102503232         21.633077         7.7639361         .002136752           469         219961         103161709         21.6564078         7.7694620						
458         209764         96071912         21.4009346         7.7082388         .002183406           459         210681         96702579         21.4242853         7.7138448         .002178649           460         211600         97336000         21.4476106         7.7194426         .002173913           461         212521         97972181         21.4709106         7.7250325         .002169197           462         213444         98611128         21.4941853         7.7306141         .002164502           463         214369         99252847         21.5174348         7.7361877         .002159827           464         215296         99897344         21.5406592         7.7417532         .002150583           465         216225         100544625         21.5638587         7.7473109         .002150588           466         217156         101194696         21.5870331         7.7528606         .002145923           467         218089         101847563         21.6101828         7.7584023         .002141328           469         219024         102503232         21.6333077         7.7639361         .002136752           469         219961         103161709         21.6564078         7.7694620						
459         210681         96702579         21.4242853         7.7138448         .002178649           460         211600         97336000         21.4476106         7.7194426         .002173913           461         212521         97972181         21.4709106         7.7250325         .002169197           462         213444         98611128         21.4941853         7.73061817         .002164502           463         214369         99252847         21.5174348         7.7361877         .002159827           464         215296         99897344         21.5406592         7.7417532         .002155172           465         216225         100544625         21.5638587         7.7473109         .002155058           466         217156         101194696         21.5870331         7.7528606         .002145923           467         218089         101847563         21.6101828         7.7584023         .0021445923           468         219024         102503232         21.6333077         7.7639361         .002136752           469         219961         103161709         21.6564078         7.7749801         .002127660           471         221841         104487111         21.7025344         7.7859928 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>						
$\begin{array}{cccccccccccccccccccccccccccccccccccc$						
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	459	210681	96702579	21.4242853	7.7138448	.002178649
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	460	211600	97336000	21.4476106	7 7194496	002173013
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	464	215296	99897344		7.7417532	.002155172
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			100544625	21.5638587	7.7473109	.002150538
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						
$\begin{array}{cccccccccccccccccccccccccccccccccccc$						
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	469	219961	103161709		7.7094620	.002132196
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	470	220900	103823000	21.6794834	7,7749801	.002127660
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$						
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$					7.7009920	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$						
476         226576         107850176         21.8174242         7.8079254         .002100840           477         227529         108531333         21.8403297         7.8133892         .002096436           478         228484         109215352         21.8632111         7.8188456         .002092050	474					
476         226576         107850176         21.8174242         7.8079254         .002100840           477         227529         108531333         21.8403297         7.8133892         .002096436           478         228484         109215352         21.8632111         7.8188456         .002092050	475	225625	107171875	21.7944947	7.8024538	.002105263
477         227529         108531333         21.8403297         7.8133892         .002096436           478         228484         109215352         21.8632111         7.8188456         .002092050				21.8174242	7.8079254	.002100840
478 228484 109215352 21.8632111 7.8188456 .002092050						
475 ( 22941 ( 109902259 ( 21.8800080 ( 7.8242942 ) .002087083	470					
	479	223111	109902259	21.0000000 1	1.0242542 1	1002037033

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
480	230400	110592000	21.9089023	7.8297353	.002083333
481	231361	111284641	21.9317122	7.8351688	.002079002
482	232324	111980168	21.9544984	7.8405949	.002074689
483	233289	112678587	21.9772610	7.8460134	.002070393
484	234256	113379904	22.0000000	7.8514244	.002066116
485	235225	114084125	22.0227155	7.8568281	.002061856
486	236196	114791256	22.0454077	7.8622242	.002057613
487	237169	115501303	22.0680765	7.8676130	.002053388
488	238144	116214272	22.0907220	7.8729944	.002049180
489	239121	116930169	22.1133444	7.8783684	.002044990
490	240100	117649000	22.1359436	7.8837352	.002040816
491	241081	118370771	22.1585198	7.8890946	.002036660
492	242064	119095488	22.1810730	7.8944468	.002032520
493	243049	119823157	22.2036033	7.8997917	.002028398
494	244036	120553784	22.2261108	7.9051294	.002024291
495	245025	121287375	22.2485955	7.9104599	.002020202
496	246016	122023936	22.2710575	7.9157832	.002016129
497	247009	122763473	22.2934968	7.9210994	.002012072
498	248004	123505992	22.3159136	7.9264085	.002008032
499	249001	124251499	22.3383079	7.9317104	.002004008
500	250000	125000000	22.3606798	7.9370053	.002000000
501	251001	125751501	22.3830293	7.9422931	.001996008
502	252004	126506008	22.4053565	7.9475739	.001992032
503	253009	127263527	22.4276615	7.9528477	.001988072
504	254016	128024064	22.4499443	7.9581144	.001984127
505	255025	128787625	22.4722051	7.9633743	.001980198
506	256036	129554216	22.4944438	7.9686271	.001976285
507	257049	130323843	22.5166605	7.9738731	.001972387
508	258064	131096512	22.5388553	7.9791122	.001968504
509	259081	131872229	22.5610283	7.9843444	.001964637
510	260100	132651000	22.5831796	7.9895697	.001960784
511	261121	133432831	22.6053091	7.9947883	.001956947
512	262144	134217728	22.6274170	8.000000 <b>0</b>	.001953125
513	263169	135005697	22.6495033	8.0052049	.001949318
514	264196	135796744	22.6715681	8.0104032	.001945525
515	265225	136590875	22.6936114	8.0155946	.001941748
516	266256	137388096	22.7156334	8.0207794	.001937984
517	267289	138188413	22.7376340	8.0259574	.001934236
518	268324	138991832	22.7596134	8.0311287	.001930502
519	269361	139798359	22.7815715	8.0362935	.001926782
		140608000	22.8035085		
520	270400		22.8254244	8.0414515	.001923077
521	271441	141420761 142236648	22.8473193	8.0466030 8.0517479	.001919386
522	$\begin{array}{c} 272484 \\ 273529 \end{array}$		22.8691933	8.0568862	.001915709
523	274576	143055667 143877824	22.8910463	8.0620180	.001912046
524		144703125	22.9128785	8.0671432	
525 526	275625 276676	145531576	22.9346899	8.0722620	.001904762
520 527	277729	146363183	22.9564806	8.0773743	.001897533
	278784	147197952	22.9782506	8.0824800	.001893939
528 529	279841	148035889	23.0000000	8.0875794	.001890359
530	280900	148877000	23.0217289	8.0926723	.001886792
531	281961	149721291	23.0434372	8.0977589	.001883239
532	283024	150568768	23.0651252	8.1028390	.001879699
533	284089	151419437	23.0867928	8.1079128	.001876173
534	285156	152273304	23.1084400	8.1129803	.001872659
535	286225	153130375	23.1300670	8.1180414	.001869159
536	287296	153990656	23.1516738	8.1230962	.001865672
537	288369	154854153	23.1732605	8.1281447	.001862197
538	289444	155720872	23.1948270	8.1331870	.001858736
539	290521	156590819	23.2163735	8.1382230	.001855288

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.			
540	291600	157464000	23.2379001	8.1432529	.001851852			
541	292681	158340421	23.2594067	8.1482765	.001848429			
542	293764	159220088	23.2808935	8.1532939	.001845018			
543	294849	160103007	23.3023604	8.1583051	.001841621			
544	295936	160989184	23.3238076	8.1633102	.001838235			
545	297025	161878625	23.3452351	8.1683092	.001834862			
546	298116	162771336	23.3666429	8.1733020	.001831502			
547	299209	163667323	23.3880311	8.1782888	.001828154			
548	300304	164566592	23.4093998	8.1832695	.001824818			
549	301401	165469149	23.4307490	8.1882441	.001821494			
- 1								
550	302500	166375000	23.4520788	8.1932127	.001818182			
551	303601	167284151	23.4733892	8.1981753	.001814882			
552	304704	168196608	23.4946802	8.2031319	.001811594			
553	305809	169112377	23.5159520	8.2080825	.001808318			
554	306916	170031464	23.5372046	8.2130271	.001805054			
555	308025	170953875	23.5584380	8.2179657	.001801802			
556	309136	171879616	23.5796522	8.2228985	.001798561			
557	310249	172808693	23.6008474	8.2278254	.001795332			
558	311364	173741112	23.6220236	8.2327463	.001792115			
559	312481	1.74676879	23.6431808	8.2376614	.001788909			
560	313600	175616000	23.6643191	8.2425706	.001785714			
561	314721	176558481	23.6854386	8.2474740	.001782531			
562	315844	177504328	23,7065392	8.2523715	.001779359			
563	316969	178453547	23.7276210	8.2572633	.001776199			
564	318096	179406144	23.7486842	8.2621492	.001773050			
565	319225	180362125	23.7697286	8.2670294	.001769912			
566	320356	181321496	23.7907545	8.2719039	.001766784			
567	321489	182284263	23.8117618	8.2767726	.001763668			
568	322624	183250432	23.8327506	8.2816355	.001760563			
569	323761	184220009	23.8537209	8.2864928	.001757469			
	324900	185193000	23.8746728	8.2913444	.001754386			
570			23.8956063	8.2961903				
571	326041	186169411	23.9165215	8.3010304	.001751313			
572	327184 328329	187149248 188132517	23.9374184	8.3058651	.001745201			
573			23.9582971					
574	329476	189119224 190109375	23.9791576	8.3106941 8.3155175	.001742160			
575	330625	191102976	24.0000000	8.3203353	.001736111			
576	331776	192100033	24.0208243	8.3251475	.001733102			
577	332929	193100552	24.0206245	8.3299542	.001730104			
578	334084	194104539	24.0410300	8.3347553	.001730104			
579	335241			1				
580	336400	195112000	24.0831891	8.3395509	.001724138			
581	337561	196122941	24.1039416	8.3443410	.001721170			
582	338724	197137368	24.1246762	8.3491256	.001718213			
583	339889	198155287	24.1453929	8.3539047	.001715266			
584	341056	199176704	24.1660919	8.3586784	.001712329			
585	342225	200201625	24.1867732	8.3634466	.001709402			
586	343396	201230056	24.2074369	8.3682095	.001706485			
587	344569	202262003	24.2280829	8.3729668	.001703578			
588	345744	203297472	24.2487113	8.3777188	.001700680			
589	346921	204336469	24.2693222	8.3824653	.001697793			
590	348100	205379000	24.2899156	8.3872065	.001694915			
591	349281	206425071	24.3104916	8.3919423	.001692047			
592	350464	207474688	24.3310501	8.3966729	.001689189			
593	351649	208527857	24.3515913	8.4013981	.001686341			
594	352836	209584584	24.3721152	8.4061180	.001683502			
595	354025	210644875	24.3926218	8.4108326	.001680672			
596	355216	211708736	24.4131112	8.4155419	.001677852			
597	356409	212776173	24.4335834	8.4202460	.001675042			
598	357604	213847192	24.4540385	8.4249448	.001672241			
599	358801	214921799	24.4744765	8.4296383	.001669449			

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
600	360000	216000000	24.4948974	8.4343267	.001666667
601					
	361201	217081801	24.5153013	8.4390098	.001663894
602	362404	218167208	24.5356883	8.4436877	.001661130
603	363609	219256227	24.5560583	8.4483605	.001658375
604	364816	220348864	24.5764115	8.4530281	.001655629
605	366025	221445125	24.5967478	8.4576906	.001652893
606	367236	222545016	24.6170673	8.4623479	.001650165
607	368449	223648543	24.6373700	8.4670001	.001647446
608	369664	224755712	24.6576560	8.4716471	.001644737
609	370881	225866529	24.6779254	8.4762892	.001642036
610	372100	226981000	24.6981781	8.4809261	.001639344
611	373321	228099131	24.7184142	8.4855579	.001636661
612	374544	229220928	24.7386338	8.4901848	.001633987
613	375769	230346397	24.7588368	8.4948065	.001631321
614	376996	231475544	24.7790234	8.4994233	.001628664
615	378225	232608375	24.7991935	8.5040350	.001626016
616	379456	233744896	24.8193473	8.5086417	.001623377
617	380689	234885113	24.8394847	8.5132435	.001620746
618	381924	236029032	24.8596058	8.5178403	.001618123
619	383161	237176659	24.8797106	8.5224321	.001615509
620	384400	238328000	24.8997992	8.5270189	.001612903
621	385641	239483061	24.9198716	8.5316009	.001610306
622	386884	240641848	24.9399278	8.5361780	.001607717
623	388129	241804367	24.9599679	8.5407501	.001605136
624	389376	242970624	24.9799920	8.5453173	.001602564
625					
	390625	244140625	25.0000000	8.5498797	.001600000
626	391876	245314376	25.0199920	8.5544372	.001597444
627	393129	246491883	25.0399681	8.5589899	.001594896
628	394384	247673152	25.0599282	8.5635377	.001592357
629	395641	248858189	25.0798724	8.5680807	.001589825
630	396900	250047000	25.0998008	8.5726189	.001587302
631	398161	251239591	25.1197134	8.5771523	.001584786
632	399424	252435968	25.1396102	8.5816809	.001582278
633	400689		25.1590102 25.159 <b>4</b> 913		
604		253636137		8.5862047	.001579779
634	401956	254840104	25.1793566	8.5907238	.001577287
635	403225	256047875	25.1992063	8.5952380	.001574803
636	404496	257259456	25.2190404	8.5997476	.001572327
637	405769	258474853	25.2388589	8.6042525	.001569859
638	407044	259694072	25.2586619	8.6087526	.001567398
639	408321	260917119	25.2784493	8.6132480	.001564945
640	409600	262144000	25.2982213	8.6177388	.001562500
641	410881	263374721	25.3179778	8.6222248	.001560062
642	412164	264609288	25.3377189	8.6267063	.001557632
643	413449		25.3574447	8.6311830	.001557052
644		265847707			
	414736	267089984	25.3771551	8.6356551	.001552795
645	416025	268336125	25.3968502	8.6401226	.001550388
646	417316	269586136	25.4165301	8.6445855	.001547988
647	418609	270840023	25.4361947	8.6490437	.001545595
648	419904	272097792	25.4558441	8.6534974	.001543210
649	421201	273359449	25.4754784	8.6579465	.001540832
650	422500	274625000	25.4950976	8.6623911	.001538462
651	423801	275894451	25.5147016	8.6668310	.001536402
652	425104	277167808	25.5342907	8.6712665	.001533742
653	426409				
		278445077	25.5538647	8.6756974	.001531394
654	427716	279726264	25.5734237	8.6801237	.001529052
655	429025	281011375	25.5929678	8.6845456	.001526718
656	430336	282300416	25.6124969	8.6889630	.001524390
657	431649	283593393	25.6320112	8.6933759	.001522070
658	432964	284890312	25.6515107	8.6977843	.001519757
659	434281	286191179	25.6709953	8.7021882	.001517451

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
660	435600	287496000	25.6904652	8.7065877	.001515152
661	436921	288804781	25.7099203	8.7109827	.001512859
662	438244	290117528	25.7293607	8.7153734	.001510574
663	439569	291434247	25.7487864	8.7197596	.001508296
664	440896	292754944	25.7681975	8.7241414	.001506024
665	442225	294079625	25.7875939	8.7285187	.001503759
666	443556	295408296	25.8069758	8.7328918	.001501502
667	444889	296740963	25.8263431	8.7372604	.001499250
668	446224	298077632	25.8456960	8.7416246	.001497006
669	447561	299418309	25.8650343	8.7459846	.001494768
670	448900	300763000	25.8843582	8.7503401	.001492537
671	450241	302111711	25.9036677	8.7546913	.001490313
672	451584	303464448	25.9229628	8.7590383	.001488095
673	452929	304821217	25.9422435	8.7633809	.001485884
674	454276	306182024	25.9615100	8.7677192	.001483680
675	455625	307546875	25.9807621	8.7720532	.001481481
676	456976	308915776	26.0000000	8.7763830	.001479290
677	458329	310288733	26.0192237	8.7807084	.001477105
678	459684	311665752	26.0384331	8.7850296	.001474926
679	461041	313046839	26.0576284	8.7893466	.001472754
680	462400	314432000	26.0768096	8.7936593	.001470588
681	463761	315821241	26.0959767	8.7979679	.001468429
682	465124	317214568	26.1151297	8.8022721	.001466276
683	466489	318611987	26.1342687	8.8065722	.001464129
684	467856	320013504	26.1533937	8.8108681	.001461988
685	469225	321419125	26.1725047	8.8151598	.001459854
686	470596	322828856	26.1916017	8.8194474	.001457726
687 688	471969 473344	324242703 325660672	26.2106848 26.2297541	8.8237307 8.8280099	.001455604 .001453488
689	474721	327082769	26.2488095	8.8322850	.001451379
690	1	328509000	26.2678511	8.8365559	.001401373
691	476100 477481	329939371	26.2868789	8.8408227	.001447178
692	478864	331373888	26.3058929	8.8450854	.001445087
693	480249	332812557	26.3248932	8.8493440	.001443001
694	481636	334255384	26.3438797	8.8535985	.001440922
695	483025	335702375	26.3628527	8.8578489	.001438849
696	484416	337153536	26.3818119	8.8620952	.001436782
697	485809	338608873	26.4007576	8.8663375	.001434720
698	487204	340068392	26.4196896	8.8705757	.001432665
699	488601	341532099	26.4386081	8.8748099	.001430615
700	490000	343000000	26.4575131	8.8790400	.001428571
701	491401	344472101	26.4764046	8.8832661	.001426534
702	492804	345948408	26.4952826	8.8874882	.001424501
703	494209	347428927	26.5141472	8.8917063	.001422475
704	495616	348913664	26.5329983	8.8959204	.001420455
705	497025	350402625	26.5518361	8.9001304	.001418440
706	498436	351895816	26.5706605	8.9043366	.001416431
707	499849	353393243	26.5894716	8.9085387	.001414427
708 709	501264 502681	354894912 356400829	26.6082694 26.6270539	8.9127369 8.9169311	.001412429
		1			
710 711	504100	357911000	26.6458252	8.9211214	.001408451
711	505521 506944	359425431 360944128	26.6645833	8.9253078 8.9294902	.001406470 .001404494
712	508369	362467097	26.6833281 26.7020598	8.9336687	.001404494
714	509796	363994344	26.7207784	8.9378433	.001400560
715	511225	365525875	26.7394839	8.9420140	.001398601
716	512656	367061696	26.7581763	8.9461809	.001396648
717	514089	368601813	26.7768557	8.9503438	.001394700
718	515524	370146232	26.7955220	8.9545029	.001392758
719	516961	371694959	26.8141754	8.9586581	.001390821

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No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
720	518400	373248000	26.8328157	8.9628095	.001388889
721	519841	374805361	26.8514432	8.9669570	.001386963
722	521284	376367048	26.8700577	8.9711007	.001385042
723	522729	377933067	26.8886593	8.9752406	.001383126
724	524176	379503424	26.9072481	8.9793766	.001381215
725	525625	381078125	26.9258240	8.9835089	.001379310
726	527076	382657176	26.9443872	8.9876373	.001377410
727	528529	384240583	26.9629375	8.9917620	.001377516
728	529984	385828352	26.9814751	8.9958829	.001373626
	531441				
729		387420489	27.0000000	9.0000000	.001371742
730	532900	389017000	27.0185122	9.0041134	.001369863
731	534361	390617891	27.0370117	9.0082229	.001367989
732	535824	392223168	27.0554985	9.0123288	.001366120
733	537289	393832837	27.0739727	9.0164309	.001364256
734	538756	395446904	27.0924344	9.0205293	.001362398
735	540225	397065375	27.1108834	5.0246239	.001360544
736	541696	398688256	27.1293199	9.0287149	.001358696
737	543169	400315553	27.1477439	9.0328021	.001356852
738	544644	401947272	27.1661554	9.0368857	.001355014
739	546121	403583419	27.1845544	9.0409655	.001353180
740	547600	405224000	27.2029410	9.0450417	.001351351
740	549081	406869021	27.2029410 27.2213152	9.0450417	.001349528
741					
	550564	408518488	27.2396769	9.0531831	.001347709
743	552049	410172407	27.2580263	9.0572482	.001345895
744	553536	411830784	27.2763634	9.0613098	.001344086
745	555025	413493625	27.2946881	9.0653677	.001342282
746	556516	415160936	27.3130006	9.0694220	.001340483
747	558009	416832723	27.3313007	9.0734726	.001338688
748	559504	418508992	27.3495887	9.0775197	.001336898
749	561001	420189749	27.3678644	9.0815631	.001335113
750	562500	421875000	27.3861279	9.0856030	.001333333
751	564001	423564751	27.4043792	9.0896392	.001331558
752	565504	425259008	27.4226184	9.0936719	.001329787
753	567009	426957777	27.4408455	9.0977010	.001328021
754	568516	428661064	27.4590604	9.1017265	.001326260
755	570025	430368875	27.4772633	9.1057485	.001324503
756	571536	432081216	27.4954542	9.1097669	.001322751
757	573049	433798093	27.5136330	9.1137818	.001321004
758	574564	435519512	27.5317998	9.1177931	.001319261
759	576081	437245479	27.5499546	9.1218010	.001317523
760	577600	438976000	27.5680975	9.1258053	.001315789
761	579121	440711081	27.5862284	9.1298061	.001314060
762	580644	442450728	27.6043475	9.1338034	.001312336
763	582169	444194947	27.6224546	9.1377971	.001310616
764	583696	445943744	27.6405499	9.1417874	.001308901
765	585225	447697125	27.6586334	9.1457742	.001307190
766	586756	449455096	27.6767050	9.1497576	.001305483
767	588289	451217663	27.6947648	9.1537375	.001303781
768	589824	452984832	27.7128129	9.1577139	.001302083
769	591361	454756609	27.7308492	9.1616869	.001300390
770	592900	456533000	27.7488739	9.1656565	.001298701
771	594441	458314011	27.7668868	9.1696225	.001297017
772	595984	460099648	27.7848880	9.1735852	.001295337
773	597529	461889917	27.8028775	9.1775445	.001293661
774	599076	463684824	27.8208555	9.1815003	.001291990
775	600625	465484375	27.8388218	9.1854527	.001290323
776	602176	467288576	27.8567766	9.1894018	.001288660
777	603729	469097433	27.8747197	9.1933474	.001287001
778	605284	470910952	27.8926514	9.1972897	.001285347
779	606841	472729139	27.9105715	9.2012286	.001283697
	000011	112120100	minoronito	0.2012200	1001200001

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
780	608400	474552000	27.9284801	9.2051641	.001282051
781	609961	476379541	27.9463772	9.2090962	.001280410
782	611524	478211768	27.9642629	9.2130250	.001278772
783	613089	480048687	27.9821372	9.2169505	.001277139
784	614656	481890304	28.0000000	9.2208726	.001275510
785	616225	483736625	28.0178515	9.2247914	.001273885
786	617796	485587656	28.0356915	9.2287068	.001272265
787	619369	487443403	28.0535203	9.2326189	.001270648
788	620944	489303872	28.0713377	9.2365277	.001269036
789	622521	491169069	28.0891438	9.2404333	.001267427
790	624100	493039000	28.1069386	9.2443355	.001265823
791	625681	494913671	28.1247222	9.2482344	.001264223
792	627264	496793088	28.1424946	9.2521300	.001262626
793	628849	498677257	28.1602557	9.2560224	.001261034
794	630436	500566184	28.1780056	9.2599114	.001259446
795	632025	502459875	28.1957444	9.2637973	.001257862
796	633616	504358336	28.2134720	9.2676798	.001256281
797	635209	506261573	28.2311884	9.2715592	.001254705
798	636804	508169592	28.2488938	9.2754352	.001253133
799	638401	510082399	28.2665881	9.2793081	.001251564
800	640000	51200000 <b>0</b>	28.2842712	9.2831777	.001250000
801	641601	513922401	28.3019434	9.2870440	.001248439
802	643204	515849608	28.3196045	9.2909072	.001246883
803	644809	517781627	28.3372546	9.2947671	.001245330
804	646416	519718464	28.3548938	9.2986239	.001243781
805	648025	521660125	28.3725219	9.3024775	.001242236
806	649636	523606616	28.3901391	9.3063278	.001240695
807	651249	525557943	28.4077454	9.3101750	.001239157
808	652864	527514112	28,4253408	9.3140190	.001237624
809	654481	529475129	28.4429253	9.3178599	.001236094
810	656100	531441000	28.4604989	9.3216975	.001234568
811	657721	533411731	28.4780617	9.3255320	.001233046
812	659344	535387328	28.4956137	9.3293634	.001231527
813	660969	537367797	28.5131549	9.3331916	.001230012
814	662596	539353144	28.5306852	9.3370167	.001228501
815	664225	541343375	28.5482048	9.3408386	.001226994
816 817	665856	543338496	28.5657137	9.3446575	.001225490
818	667489 669124	545338513 547343432	28.5832119 28.6006993	9.3484731 9.3522857	.001223990
819	670761	549353259	28.6181760	9.3560952	.001221001
820	672400	551368000	28.6356421	9.3599016	.001219512
821 822	674041 675684	553387661 555412248	28.6530976 28.6705424	9.3637049 9.3675051	.001218027 .001216545
823	677329	557441767	28.6879766	9.3673031 9.3713022	.001216945
824	678976	559476224	28.7054002	9.3750963	.001213592
825	680625	561515625	28.7228132	9.3788873	.001212121
826	682276	563559976	28.7402157	9.3826752	.001212121
827	683929	565609283	28.7576077	9.3864600	.001209190
828	685584	567663552	28.7749891	9.3902419	.001207729
829	687241	569722789	28.7923601	9.3940206	.001206273
830	688900	571787000	28.8097206	9.3977964	.001204819
831	690561	573856191	28.8270706	9.4015691	.001203369
832	692224	575930368	28.8444102	9.4053387	.001201923
833	693889	578009537	28.8617394	9.4091054	.001200480
834	695556	580093704	28.8790582	9.4128690	.001199041
835	697225	582182875	28.8963666	9.4166297	.001197605
836	698896	584277056	28.9136646	9.4203873	.001196172
837	700569	586376253	28.9309523	9.4241420	.001194743
838	702244	588480472	28.9482297	9.4278936	.001193317
839	703921	590589719	28.9654967	9.4316423	.001191895

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No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
0.10	FOECOO	500704000	00 0007505	0.4950000	001100470
840	705600	592704000	28.9827535	9.4353880	.001190476
841	707281	594823321	29.0000000	9.4391307	.001189061
842	708964	596947688	29.0172363	9.4428704	.001187648
843	710649	599077107	29.0344623	9.4466072	
					.001186240
844	712336	601211584	29.0516781	9.4503410	.001184834
845	714025	603351125	29.0688837	9.4540719	.001183432
846	715716	605495736	29.0860791	9.4577999	.001182033
				0.4015040	001102000
847	717409	607645423	29.1032644	9.4615249	.001180638
848	719104	609800192	29.1204396	9.4652470	.001179245
849	720801	611960049	29.1376046	9.4689661	.001177856
850	722500	614125000	29.1547595	9.4726824	.001176471
851	724201	616295051	29.1719043	9.4763957	.001175088
852			20.100000		
	725904	618470208	29.1890390	9.4801061	.001173709
853	727609	620650477	29.2061637	9.4838136	.001172333
854	729316	622835864	29.2232784	9.4875182	.001170960
855	731025	625026375	29.2403830	9.4912200	.001169591
856	732736	627222016	29.2574777	9.4949188	.001168224
857	734449	629422793	29.2745623	9.4986147	.001166861
858	736164	631628712	29.2916370	9.5023078	.001165501
859	737881	633839779	29.3087018	9.5059980	.001164144
860	739600	636056000	29.3257566	9.5096854	.001162791
861	741321	638277381	29.3428015	9.5133699	.001161440
		050211501			
862	743044	640503928	29.3598365	9.5170515	.001160093
863	744769	642735647	29.3768616	9.5207303	.001158749
864	746496	644972544	29.3938769	9.5244063	.001157407
865	748225	647214625	29.4108823	9.5280794	.001156069
866	749956	649461896	29.4278779	9.5317497	.001154734
867	751689	651714363	29.4448637	9.5354172	.001153403
868	753424	653972032	29.4618397	9.5390818	.001152074
869	755161	656234909	29.4788059	9.5427437	.001150748
870	756900	658503000	29.4957624	9.5464027	.001149425
871	758641	660776311	29.5127091	9.5500589	.001148106
872	760384	663054848	29.5296461	9.5537123	.001146789
873	762129	665338617	29.5465734	9.5573630	.001145475
874	763876	667627624	29,5634910	9.5610108	.001144165
875	765625	669921875	29.5803989	9.5646559	.001142857
876	767376	672221376	29.5972972	9.5682982	.001141553
877	769129	674526133	29.6141858	9.5719377	.001140251
878	770884	676836152	29.6310648	9.5755745	.001138952
879	772641	679151439	29.6479342	9.5792085	.001137656
880	774400	681472000	29.6647939	9.5828397	.001136364
881	776161	683797841	29.6816442	9.5864682	.001135074
882	777924	686128968	29.6984848	9.5900939	.001133787
883	779689	688465387	29.7153159	9.5937169	.001132503
884	781456	690807104	29.7321375	9.5973373	.001131222
885	783225	693154125	29.7489496	9.6009548	.001129944
886	784996	695506456	29.7657521	9.6045696	.001128668
887	786769	697864103	29.7825452	9.6081817	.001127396
888	788544	700227072	29.7993289	9,6117911	.001126126
889	790321	702595369	29.8161030	9.6153977	.001124859
890	792100	704969000	29.8328678	9.6190017	.001123596
891			29.8496231	9.6226030	.001122334
	793881	707347971			
892	795664	709732288	29.8663690	9.6262016	.001121076
893	797449	712121957	29.8831056	9.6297975	.001119821
894	799236	714516984	29.8998328	9.6333907	.001118568
895	801025	716917375	29.9165506	9.6369812	.001117318
896	802816	719323136	29.9332591	9.6405690	.001116071
897	804609	721734273	29.9499583	9.6441542	.001114827
898	806404	724150792	29,9666481	9.6477367	.001113586
899	808201	726572699	29.9833287	9.6513166	.001112347

No.   Squares   Cubes   Square Roots   Cube Roots   Recipt	20010
901 811801 781432701 30.0166620 9.6584684 .00114 902 813604 783870808 30.0333148 9.6620403 .00114 903 815409 736314327 30.0499584 9.6656096 .00114 904 817216 788763264 30.0665928 9.6691762 .00114 905 819025 741217625 30.0832179 9.6727403 .00114 907 822649 746142643 30.1164407 9.6798604 .00114 907 822649 746142643 30.1164407 9.6798604 .00114 908 824464 748613812 30.1330383 9.6834166 .00114 909 826281 751059429 30.1496269 9.6869701 .00114 910 828100 753571000 30.1662063 9.6905211 .00104 911 829021 756058081 30.1827765 9.6940894 .00104 912 881744 758550528 30.1998377 9.6976151 .00104 913 833569 761048497 30.2158899 9.7011583 .00105 914 885396 763551944 30.2324329 9.7046989 .00105 915 887225 766069875 30.2459669 9.7082369 .00105 916 839056 768575296 30.2654919 9.71152051 .00107 917 840889 771095213 30.2820079 9.7153051 .00107 918 842724 773620632 30.2985148 9.7183554 .00107 920 846400 778685000 30.33150128 9.7228631 .00107 921 845241 781229961 30.3479818 9.724109 .00107 922 850054 788777448 30.3644529 9.732299 .00107 923 851929 786330467 30.380151 9.7324484 .00107 924 853776 78888904 30.3873683 9.7329809 .00107 925 855625 791458125 30.4185127 9.7444758 .00107 927 859329 7685768 30.445094 9.7569979 .00107 928 866761 8069875 30.445094 9.7569979 .00107 929 863041 801765089 30.4166747 9.7569920 .00107 921 84766 148497 30.585689 9.758950 .00107 922 850064 788777448 30.3644529 9.7329809 .00107 923 861929 768330467 30.3809151 9.7364484 .00107 924 853776 78889094 30.3873683 9.7396894 .00107 925 855625 791458125 30.4138127 9.7434758 .00107 927 859329 96567988 30.4466747 9.759992 .00107 928 866761 8069875 30.5450487 9.7714848 .00107 929 863041 801765089 30.4795014 9.7610941 .00107 931 866761 806985491 30.5157697 9.7784616 .00107 932 868004 804357000 30.4959014 9.7610902 .00107 933 864900 804357000 30.4959014 9.7610902 .00107 934 872356 814780504 30.5614136 9.7749748 .00107 935 879844 82523672 30.625787 9.7889067 .00107 936 879844 82523672 30.625787 9.77854288 .00107 940 88600 8805888 30.6920185 9.8028036 .00107 941 885481 88	cals,
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909         826281         751089429         30.1496269         9.6869701         .00101           910         828100         758571000         30.1662063         9.6905211         .00101           911         829921         756058081         30.1827765         9.6940894         .00101           912         831744         758550528         30.1993377         9.6976151         .00101           913         8335896         761048497         30.2158899         9.7011588         .00101           914         8353966         768575296         30.2489669         9.708369         .00101           916         839056         768575296         30.2654919         9.7117723         .00101           917         840889         771095213         30.2820079         9.7153051         .00101           918         842724         773620632         30.2935148         9.7188354         .0010           920         846400         778688000         30.35150128         9.7225631         .0010           921         848241         781229961         30.3479818         9.7294109         .0010           922         850084         78377448         30.3644529         9.7329809         .0010 <tr< td=""><td></td></tr<>	
910         828100         753571000         30.1662063         9.6905211         ,00101           911         829921         756058031         30.1827765         9.6940694         ,00101           912         831744         758550528         30.1993377         9.6976151         ,00101           913         833589         761048497         30.2158899         9.7011583         ,00101           914         833596         763551944         30.2324329         9.7046989         ,00101           915         837225         766060875         30.24564919         9.7117723         ,00101           916         839056         76857296         30.2654919         9.7117723         ,00101           917         840889         771095213         30.2820079         9.7158051         ,0010           918         842724         773620632         30.2955148         9.7118723         ,0010           918         842724         773620632         30.3150128         9.7223631         ,0010           920         846400         778688000         30.3150128         9.7225631         ,0010           920         846400         778688000         30.3315018         9.723633         ,0010	1322
911         829921         756058081         30.1827765         9.6940694         ,00101           912         831744         758550528         30.1993377         9.6976151         ,00101           913         833569         761048497         30.2158899         9.7011583         ,00101           914         835396         763551944         30.2324329         9.7046989         ,00101           915         837225         766060875         30.2489669         9.7082369         ,00101           916         839056         768575296         30.2654919         9.7117723         ,0010           917         840889         771095213         30.2820079         9.7153051         ,0010           918         842724         773620632         30.2985148         9.718354         ,0010           918         842724         773620632         30.3150128         9.7223631         ,0010           920         846400         778688000         30.3150128         9.7225631         ,0010           921         848241         7817248         30.34478818         9.7294109         ,0010           922         850694         785377448         30.34478918         9.7239609         ,0010	0110
911         829921         756058081         30.1827765         9.6940694         ,00101           912         831744         758550528         30.1993377         9.6976151         ,00101           913         833569         761048497         30.2158899         9.7011583         ,00101           914         835396         763551944         30.2324329         9.7046989         ,00101           915         837225         766060875         30.2489669         9.7082369         ,00101           916         839056         768575296         30.2654919         9.7117723         ,0010           917         840889         771095213         30.2820079         9.7153051         ,0010           918         842724         773620632         30.2985148         9.718354         ,0010           918         842724         773620632         30.3150128         9.7223631         ,0010           920         846400         778688000         30.3150128         9.7225631         ,0010           921         848241         7817248         30.34478818         9.7294109         ,0010           922         850694         785377448         30.34478918         9.7239609         ,0010	2001
912 831744 758550528 30.1993377 9.6976151 .00100 913 833569 761048497 30.2158899 9.7011588 .00100 914 835396 768551944 30.2324329 9.7046989 .00100 915 837225 766660875 30.2489669 9.7082369 .00100 916 839056 768575296 30.2654919 9.7117723 .00100 917 840889 771095213 30.2820079 9.7153051 .00100 918 842724 773620632 30.2985148 9.7128354 .00100 919 844561 776151559 30.3150128 9.7223631 .00100 920 846400 778688000 30.33150128 9.7223631 .00100 921 848241 781229961 30.3479818 9.7294109 .00100 922 850084 788777448 30.3644529 9.7329809 .00100 923 851929 786330467 30.3809151 9.7364484 .00100 924 853776 788889024 30.38793683 9.7399684 .00100 925 855625 791458125 30.4138127 9.7434758 .00100 926 857476 794022776 30.4302481 9.7469857 .00100 927 859329 786597983 30.4466747 9.7504980 .00100 928 861184 789178752 30.4680924 9.7539979 .00100 929 863041 801765089 30.4795018 9.7575002 .00100 931 866761 806954491 30.5122926 9.7644974 .00100 931 866761 806954491 30.5122926 9.7644974 .00100 931 866761 806954491 30.5122926 9.7644974 .00100 931 866761 806954491 30.5122926 9.7644974 .00100 931 866761 806954491 30.5122926 9.7644974 .00100 931 866761 806954491 30.5122926 9.7644974 .00100 931 866761 806954491 30.5122926 9.7644974 .00100 931 866761 806954491 30.5122926 9.7644974 .00100 931 866761 806954491 30.5122926 9.7644974 .00100 931 866761 806954491 30.5122926 9.7644974 .00100 931 866761 806954491 30.5122926 9.7644974 .00100 931 866761 806954491 30.5122926 9.7644974 .00100 931 866761 806954491 30.5122926 9.7644974 .00100 931 866761 806954491 30.5122926 9.7644974 .00100 931 866761 806954491 30.5122926 9.7644974 .00100 931 866761 806954491 30.5122926 9.7644974 .00100 931 866761 806954491 30.5122926 9.7644974 .00100 931 866761 806954491 30.5122926 9.7644974 .00100 931 866761 806954491 30.5122926 9.7644974 .00100 931 866761 806954491 30.5122926 9.7764938 .00100 932 868824 809557568 30.6901859 9.7923861 .00100 934 87364 83589688 30.69021859 9.7923861 .00100 934 87364 83589688 30.6902185 9.8028086 .00100 944 885481 83589688 30.6902185 9.80280	
915         833599         761048497         30.2158899         9.7011588         .00109           914         835396         763551944         30.2324329         9.7046989         .00101           915         837225         766060875         30.2489669         9.7082369         .00101           916         839056         768575296         30.2654919         9.7117723         .00101           917         840889         771095213         30.2820079         9.7153051         .00101           918         842724         773620632         30.2985148         9.71188354         .0010           919         844561         776151559         30.3150128         9.7223631         .0010           920         846400         778688000         30.3150128         9.7258838         .0010           921         848241         781229961         30.3479818         9.7294109         .0010           922         850084         78377448         30.3644529         9.7329809         .0010           923         851929         786330467         30.389151         9.7399684         .0010           924         85376         784889024         30.3978683         9.7399684         .0010	
914 835396 768551944 30.2324329 9.7046989 .00109 915 837225 766060875 30.2489669 9.7082369 .00109 916 839056 768575296 30.2654919 9.7117723 .00109 917 840889 771095213 30.2820079 9.7153051 .00109 918 842724 773620632 30.2985148 9.7188354 .00109 919 844561 776151559 30.3150128 9.7223631 .00109 920 846400 778688000 30.33150128 9.7223631 .00109 921 848241 781229961 30.3479818 9.7294109 .00109 922 850084 768777448 30.3644529 9.7329809 .00109 923 851929 786330467 30.3809151 9.7364484 .00109 924 853776 788880024 30.3978683 9.7399684 .00109 925 855625 791453125 30.4138127 9.7434758 .00109 926 857476 794022776 30.4302481 9.7469857 .00109 927 859329 796597983 30.4466747 9.7504930 .00109 928 861184 799178752 30.4302481 9.7469857 .00109 929 863041 801765089 30.4795013 9.7575002 .00109 930 864900 804357000 30.4959014 9.7610001 .0010931 866761 806954491 30.5122926 9.7644974 .0010931 866761 806954491 30.5122926 9.7644974 .0010932 868624 809557568 30.5286750 9.7679922 .0010934 87285 874225 817400375 30.5777697 9.7784616 .0010934 87285 874825 817400375 30.5777697 9.7784616 .0010936 877609 822656953 30.6104557 9.7854288 .0010938 879844 8225293672 30.5678787 9.7789088 .0010938 879844 8225293672 30.6267857 9.7889087 .0010938 879844 825293672 30.6267857 9.7889087 .0010938 879844 825293672 30.6267857 9.7889087 .0010938 879844 825293672 30.6267857 9.7889087 .0010938 879844 825293672 30.6267857 9.7889087 .0010938 879844 825293672 30.6267857 9.7889087 .0010938 879844 825293672 30.6267857 9.7889087 .0010938 879844 825293672 30.6267857 9.7889087 .0010938 879844 825293672 30.6267857 9.7889087 .0010938 879844 825293672 30.6267857 9.7889087 .0010938 879844 825293672 30.6267857 9.7889087 .0010938 879844 825293672 30.6267857 9.7889087 .0010938 879844 825293672 30.6267857 9.7889087 .0010938 879844 825293672 30.6267857 9.7889087 .0010938 879844 825293672 30.6267857 9.7889087 .00109442 887364 83589688 30.6920185 9.80220386 .00109443 889249 888561807 30.7088051 9.8062711 .0010943 888561807 30.7088051 9.8062711 .0010943	
915 837225 766060875 30.2489669 9.7082369 .0010916 839056 768575296 30.2654919 9.7117723 .0010917 840889 771095213 30.2820079 9.7153051 .0010918 842724 773620632 30.295148 9.7188554 .0010919 844561 776151559 30.3150128 9.7223631 .0010919 844561 776151559 30.3150128 9.7223631 .0010919 844561 776151559 30.3150128 9.7223631 .0010910 .0010911 848241 781229961 30.3479818 9.7294109 .0010911 922 850084 788777448 30.3644529 9.7329309 .0010910 .0010	
916         839056         768575296         30.2654919         9.7117723         .0010           917         840889         771095213         30.2820079         9.7153051         .0010           918         842724         773620632         30.2985148         9.7188354         .0010           919         844561         776151559         30.3150128         9.7223631         .0010           920         846400         778688000         30.3315018         9.7258883         .0010           921         848241         781229961         30.3479818         9.7294109         .0010           922         850984         785777448         30.3644529         9.7329809         .0010           923         851929         786330467         30.3809151         9.7364484         .0010           924         853776         788889024         30.3973683         .7399684         .0010           925         855625         791458125         30.4138127         9.7434758         .0010           926         857476         794022776         30.4302481         9.7469857         .0010           928         861184         799178752         30.466747         9.7504980         .0010           <	4092
916         839056         768575296         30.2654919         9.7117723         .0010           917         840889         771095213         30.2820079         9.7153051         .0010           918         842724         773620632         30.2985148         9.7188354         .0010           919         844561         776151559         30.3150128         9.7223631         .0010           920         846400         778688000         30.3315018         9.7258883         .0010           921         848241         781229961         30.3479818         9.7294109         .0010           922         850084         785777448         30.3644529         9.7329309         .0010           923         851929         786330467         30.3809151         9.7364484         .0010           924         853776         788889024         30.3973683         .7399684         .0010           925         855625         791458125         30.4138127         9.7434758         .0010           926         857476         794022776         30.4302481         9.7469857         .0010           928         861184         799178752         30.466747         9.7504930         .0010           <	2896
917	
918         842724         773620632         30.2985148         9.7188354         .0010           919         844561         776151559         30.3150128         9.7223631         .0010           920         846400         778688000         30.3315018         9.7258883         .0010           921         848241         781229961         30.3479818         9.7294109         .0010           922         850084         783777448         30.3644529         9.7329609         .0010           923         851929         78630467         30.3809151         9.7364484         .0010           924         853776         788889024         30.3978683         9.7396684         .0010           925         855625         791458125         30.4138127         9.7449785         .0010           926         857476         794022776         30.4302481         9.7469857         .0010           927         859329         796597983         30.4466747         9.7539979         .0010           928         861184         799178752         30.4630924         9.7539979         .0010           930         864900         804357000         30.4959014         9.7610001         .0010	
919         844561         776151559         30.3150128         9.7223631         .0010           920         846400         778688000         30.3315018         9.7258883         .0010           921         848241         781229961         30.3479818         9.7294109         .0010           922         850084         78377748         30.3644529         9.7329309         .0010           923         851929         786330467         30.3809151         9.7369399         .0010           924         853776         788889024         30.3978683         9.7399684         .0010           925         855625         791453125         30.4138127         9.7459758         .0010           926         857476         794022776         30.4302481         9.7469857         .0010           927         859329         796597983         30.4466747         9.7504930         .0010           928         861184         799178752         30.4630924         9.7539979         .0010           930         864900         804357000         30.4959014         9.7610001         .0010           931         866761         806954491         30.5122926         9.7644974         .0010	
920         846400         778688000         30.3315018         2.7258883         .0010           921         848241         781229961         30.3479818         9.7294109         .0010           922         850084         783777448         30.3644529         9.7329809         .0010           923         851929         786330467         30.3809151         9.7364484         .0010           924         853776         788889024         30.3973683         9.7399684         .0010           925         855625         791453125         30.4138127         9.7434758         .0010           926         857476         794022776         30.4302481         9.7469857         .0010           927         859329         796597983         30.4466747         9.7504930         .0010           928         861184         799178752         30.4302481         9.7539979         .0010           929         863041         801765089         30.4795018         9.7539979         .0010           930         864900         804357000         30.4959014         9.7610001         .0010           931         866761         806954491         30.5122926         9.7644974         .0010	
921         848241         781229961         30.3479818         9.7294109         .0010           922         850084         783777448         30.3644529         9.7329809         .0010           923         851929         786330467         30.3809151         9.7364484         .0010           924         853776         788889024         30.3973638         .7399684         .0010           925         855625         791458125         30.4138127         9.7434758         .0010           926         857476         794022776         30.4302481         9.7469857         .0010           927         859329         796597983         30.4466747         9.7504930         .0010           928         861184         799178752         30.430924         9.7539979         .0010           930         864900         804357000         30.4959014         9.7610001         .0010           931         866761         806954491         30.5122926         9.7644974         .0010           932         868624         809557568         30.5286750         9.7679922         .0010           933         870489         812166237         30.5450487         9.7714845         .0010           <	
922         850084         783777448         30.3644529         9.7329309         .0010           923         851929         786330467         30.3809151         9.7329309         .0010           924         853776         788889024         30.3978683         9.7399684         .0010           925         855625         791453125         30.4183127         9.7434758         .0010           926         857476         794022776         30.4302481         9.7469857         .0010           927         859329         796597983         30.4466747         9.7504930         .0010           928         861184         799178752         30.4630924         9.7539979         .0010           929         863041         801765089         30.4795013         9.7575002         .0010           930         864900         804357000         30.4959014         9.7610001         .0010           931         866761         806954491         30.5122926         9.7644974         .0010           933         870489         812166237         30.5286750         9.7679922         .0010           934         872356         814780504         30.5614136         9.774943         .0010	
923 851929 786330467 30.3809151 9.7364484 .0010 924 853776 788889024 30.3973683 9.7399684 .0010 925 855625 791458125 30.4138127 9.7454758 .0010 926 857476 794022776 30.4302481 9.7469857 .0010 927 859329 796597983 30.4466747 9.7504930 .0010 928 861184 799178752 30.4630924 9.7539979 .0010 929 863041 801765089 30.4795013 9.7575002 .0010 930 864900 804357000 30.4959014 9.7610001 .0010 931 866761 806954491 30.5122926 9.7644974 .0010 932 868624 809557568 30.5286750 9.7679922 .0010 933 870489 812166237 30.5450487 9.7714845 .0010 934 872356 814780504 30.5614136 9.7749743 .0010 935 874225 817400375 30.5777697 9.7784616 .0010 936 876096 820025856 30.594171 9.7819466 .0010 937 877969 822656953 30.6104557 9.7859087 .0010 938 879844 825293672 30.6267857 9.7889087 .0010 939 881721 827936019 30.6131069 9.7923861 .0010 940 885600 830584000 30.6594194 9.7958611 .0010 941 885481 838237621 30.6757233 9.7993336 .0010 942 887364 835896888 30.6920185 9.8028036 .0010 943 889249 888561807 30.7088051 9.8062711 .0010	5776
923         851929         786330467         30.3809151         9.7364484         .0010           924         853776         788889024         30.3978683         9.7396684         .0010           925         855625         791458125         30.4188127         9.7434758         .0010           926         857476         794022776         30.4302481         9.7469857         .0010           927         859329         796597983         30.4466747         9.7504930         .0010           928         861184         799178752         30.4680924         9.7539979         .0010           929         863041         801765089         30.4795013         9.7519072         .0010           930         864900         804357000         30.4959014         9.7610001         .0010           931         866761         806954491         30.5122926         9.7644974         .0010           933         870489         812166237         30.5450487         9.7714845         .0010           934         872356         814780504         30.514136         9.7749743         .0010           935         874225         817400375         30.5777697         9.7784616         .0010	4599
924         853776         788889024         30.3973683         9,7399684         .0010           925         855625         791453125         30.4138127         9,7434758         .0010           926         857476         794022776         30.4302481         9,7469857         .0010           927         859329         796597983         30.446747         9,7539979         .0010           928         861184         799178752         30.4630924         9,7539979         .0010           929         863041         801765089         30.4795013         9,7575002         .0010           930         864900         804357000         30.4959014         9,7610001         .0010           931         866761         806954491         30.5122926         9,7614974         .0010           932         868624         809557568         30.5286750         9,7679922         .0010           933         870489         812166237         30.5450487         9,7714845         .0010           934         872356         814780504         30.5614136         9,7749743         .0010           935         874225         817400375         30.5777697         9,7784616         .0010	3424
925         855625         791458125         30.4185127         9.7434758         .0010           926         857476         794022776         30.4302481         9.7469857         .0010           927         859329         796597983         30.4466747         9.7504930         .0010           928         861184         799178752         30.460924         9.7539979         .0010           929         863041         801765089         30.4795018         9.7575002         .0010           930         864900         804357000         30.4959014         9.7610001         .0010           931         8666761         806954491         30.5122926         9.7644974         .0010           932         868624         809557568         30.5286750         9.7679922         .0010           933         870489         812166237         30.5450487         9.7714943         .0010           934         872356         814780504         30.5614136         9.7749743         .0010           935         874225         817400375         30.5777697         9.7784616         .0010           937         877969         820656953         30.6104557         9.7889087         .0010	
926         857476         794022776         30.4302481         9.7469857         .0010           927         859329         796597983         30.4466747         9.7504930         .0010           928         861184         799178752         30.4630924         9.7539979         .0010           929         863041         801765089         30.4795018         9.7575002         .0010           930         864900         804357000         30.4959014         9.7610001         .0010           931         866761         806954491         30.5122926         9.7644974         .0010           932         868624         809557568         30.5286750         9.7679922         .0010           933         870489         812166237         30.5450487         9.7714845         .0010           934         872356         814780504         30.5614136         9.7749743         .0010           935         874225         817400375         30.5777697         9.7784616         .0010           937         877969         822656953         30.6104557         9.7854288         .0010           938         879844         825293672         30.6267857         9.7889087         .0010	
927         859329         796597983         30.4466747         9.7504930         .0010           928         861184         799178752         30.4630924         9.7539979         .0010           929         863041         801765089         30.4795013         9.7575002         .0010           930         864900         804357000         30.4959014         9.7610001         .0010           931         866761         806954491         30.5122926         9.7644974         .0010           932         868624         809557568         30.5286750         9.7679922         .0010           933         870489         812166237         30.5450487         9.7714845         .0010           934         872356         814780504         30.5614136         9.7749743         .0010           935         874225         817400375         30.5777697         9.7784616         .0010           936         876096         820025856         30.5941171         9.781466         .0010           935         879844         825293672         30.6267857         9.7889087         .0010           939         881721         827936019         30.6431069         9.7923861         .0010	
928         861184         799178752         30,4630924         9,7539979         .0010           929         863041         801765089         30,4795013         9,7575002         .0010           930         864900         804357000         30,4959014         9,7610001         .0010           931         866761         806954491         30,5122926         9,7644974         .0010           932         868624         809557568         30,5286750         9,7679922         .0010           933         870489         812166237         30,5450487         9,7714845         .0010           934         872356         814780504         30,5614136         9,7749743         .0010           935         874225         817400375         30,5777697         9,7784616         .0010           936         876096         820025856         30,5941171         9,7819466         .0010           937         877969         822656933         30,6104557         9,7889087         .0010           938         879844         825293672         30,6267857         9,7889087         .0010           939         881721         827936019         30,6431069         9,7923861         .0010	
929         863041         801765089         30.4795018         9.7575002         .0010           930         864900         804357000         30.4959014         9.7610001         .0010           931         8666761         806954491         30.5122926         9.7644974         .0010           932         868624         809557568         30.5286750         9.7679922         .0010           933         870489         812166237         30.5450487         9.7714945         .0010           934         872356         814780504         30.5614136         9.7749743         .0010           935         874225         817400375         30.5777697         9.7784616         .0010           936         876096         820025856         30.5941171         9.7819466         .0010           937         877969         822656953         30.6104557         9.7889087         .0010           938         879844         825293672         30.6267857         9.7889087         .0010           939         881721         827936019         30.6431069         9.7923861         .0010           941         885481         838597621         30.6594194         9.7958336         .0010	
930 864900 804357000 30.4959014 9.7610001 .0010 931 866761 806954491 30.5122926 9.7644974 .0010 932 868624 809557568 30.5286750 9.7679922 .0010 938 870489 812166237 30.5450487 9.7714845 .0010 934 872856 814780504 30.5614136 9.7749743 .0010 935 874225 817400375 30.5777697 9.7784616 .0010 936 876096 820025856 30.5941171 9.7819466 .0010 937 877969 822656953 30.6104557 9.7854288 .0010 938 879844 825298672 30.6267857 9.7889087 .0010 939 881721 827936019 30.6431069 9.7923861 .0010 940 883600 830584000 30.6594194 9.7958611 .0010 941 885481 838237621 30.6757233 9.7993336 .0010 942 887364 838896888 30.6920185 9.8028036 .0010 943 889249 888561807 30.7083051 9.8062711 .0010	
931         866761         806954491         30.5122926         9.7644974         .0010           932         868624         809557568         30.5286750         9.76749922         .0010           933         870489         812166237         30.5450487         9.7714845         .0010           934         872356         814780504         30.5614136         9.7749743         .0010           935         874225         817400375         30.5777697         9.7784616         .0010           936         876096         820025856         30.5941171         9.7854288         .0010           937         877969         822656953         30.6104557         9.7854288         .0010           938         879844         825293672         30.627857         9.7889087         .0010           939         881721         827936019         30.6431069         9.7923861         .0010           940         858600         830584000         30.6594194         9.7958611         .0010           941         885481         838597621         30.6757233         9.7993386         .0010           942         887364         835896888         30.6920185         9.8028036         .0010	6426
931         866761         806954491         30.5122926         9.7644974         .0010           932         868624         809557568         30.5286750         9.76749922         .0010           933         870489         812166237         30.5450487         9.7714845         .0010           934         872356         814780504         30.5614136         9.7749743         .0010           935         874225         817400375         30.5777697         9.7784616         .0010           936         876096         820025856         30.5941171         9.7854288         .0010           937         877969         822656953         30.6104557         9.7854288         .0010           938         879844         825293672         30.627857         9.7889087         .0010           939         881721         827936019         30.6431069         9.7923861         .0010           940         858600         830584000         30.6594194         9.7958611         .0010           941         885481         838597621         30.6757233         9.7993386         .0010           942         887364         835896888         30.6920185         9.8028036         .0010	5269
932         868624         809557568         30.5286750         9.7679922         .0010           933         870489         812166237         30.5450487         9.7714845         .0010           934         872356         814780504         30.5614136         9.7749743         .0010           935         874225         817400375         30.5777697         9.7784616         .0010           936         876096         820025856         30.5941171         9.7819466         .0010           937         877969         822656953         30.6104557         9.7854288         .0010           938         879844         825293672         30.6267857         9.7889087         .0010           939         881721         827936019         30.6431069         9.7923861         .0010           940         885600         830584000         30.6594194         9.7958611         .0010           941         885481         838237621         30.6757233         9.7993336         .0010           942         887364         835896888         30.6920185         9.8028036         .0010           943         889249         888561807         30.7088051         9.8062711         .0010	4114
938         870489         812166237         30.5450487         9.7714845         .0010*           934         872356         814780504         30.5614136         9.7749743         .0010*           935         874225         817400375         30.5777697         9.7784616         .0010*           936         876096         820025856         30.5941171         9.7819466         .0010*           937         877969         822656953         30.6104557         9.7854288         .0010*           938         879844         825293672         30.6267857         9.7889087         .0010*           939         831721         827936019         30.6431069         9.7923861         .0010*           940         858600         830584000         30.6594194         9.7958611         .0010*           941         885481         838237621         30.6757233         9.7993336         .0010*           942         887364         835896888         30.6920185         9.8028036         .0010*           943         889249         838561807         30.7088051         9.8062711         .0010*	
934         872356         814780504         30.5614136         9.7749743         .0010'           935         874225         817400375         30.5777697         9.7784616         .0010'           936         876096         820025856         30.5941171         9.7819466         .0010'           937         877969         822656953         30.6104557         9.7854288         .0010'           938         879844         825293672         30.6267857         9.7889087         .0010'           939         881721         827936019         30.6431069         9.7923861         .0010'           940         885600         830584000         30.6594194         9.7958611         .0010'           941         885481         838237621         30.6757233         9.7993336         .0010'           942         887364         835896888         30.6920185         9.8028036         .0010'           943         889249         838561807         30.7088051         9.8062711         .0010'	
935         874225         817400375         30.5777697         9.7784616         .0010           936         876096         820025856         30.5941171         9.7819466         .0010           937         877969         822656953         30.6104557         9.7854288         .0010           938         879844         825293672         30.6267857         9.7889087         .0010           939         881721         827936019         30.6431069         9.7923861         .0010           940         853600         830584000         30.6594194         9.7958611         .0010           941         885481         838237621         30.6757233         9.7993386         .0010           942         887364         838896888         30.6920185         9.8028036         .0010           943         899249         838561807         30.7083051         9.8062711         .0010	
936         876096         820025856         30.5941171         9.7819466         .0010           937         877969         822656953         30.6104557         9.7854288         .0010           938         879844         825293672         30.6267857         9.7889087         .0010           939         881721         827936019         30.6431069         9.7923861         .0010           940         858600         830584000         30.6594194         9.7958611         .0010           941         885481         838237621         30.6757233         9.7993336         .0010           942         887364         835896888         30.6920185         9.8028036         .0010           943         889249         838561807         30.7088051         9.8062711         .0010	
937         877969         822656953         30.6104557         9.7854288         .0010           938         879844         825293672         30.6267857         9.7889087         .0010           939         881721         827936019         30.6431069         9.7923861         .0010           940         885600         830584000         30.6594194         9.7958611         .0010           941         885481         838237621         30.6757233         9.7993336         .0010           942         887364         835896888         30.6920185         9.8028036         .0010           943         889249         838561807         30.7088051         9.8062711         .0010	
938         879844         825293672         30.6267857         9.7889087         .0010           939         881721         827936019         30.6431069         9.7923861         .0010           940         885600         830584000         30.6594194         9.7958611         .0010           941         885481         838237621         30.6757233         9.7993336         .0010           942         887364         835896888         30.6920185         9.8028036         .0010           943         89249         838561807         30.7083051         9.8062711         .0010	
989         881721         827936019         30.6431069         9.7923861         .0010           940         858600         830584000         30.6594194         9.7958611         .0010           941         835481         838237621         30.6757233         9.7993386         .0010           942         887364         835896888         30.6920185         9.8028036         .0010           943         889249         838561807         30.7088051         9.8062711         .0010	
940         8\$3600         8\$0584000         30.6594194         9.7958611         .0010           941         8\$3481         8\$3237621         30.6757233         9.7993336         .0010           942         8\$7364         835896888         30.6920185         9.8028036         .0010           943         8\$9249         8\$8561807         30.7088051         9.8062711         .00100	
941     885481     835237621     30.6757233     9.7993336     .0010       942     887364     835896888     30.6920185     9.8028036     .0010       943     889249     838561807     30.7088051     9.8062711     .0010	4963
941     885481     835237621     30.6757233     9.7993336     .0010       942     887364     835896888     30.6920185     9.8028036     .0010       943     889249     838561807     30.7088051     9.8062711     .0010	3830
942 887364 835896888 30.6920185 9.8028036 .0010 943 889249 838561807 30.7088051 9.8062711 .0010	2699
943 889249 838561807 30.7083051 9.8062711 .0010	
34.1 SULIZE X41757584 SUL7235830 USDUZED INDIE	9322
946 894916 846590536 30.7571130 9.8166591 .00100	
947 896809 849278123 30.7733651 9.8201169 .00103	
948 898704 851971392 30.7896086 9.8235723 .00103	
949 900601 854670349 30.8058436 9.8270252 .00103	3741
950 902500 857375000 30.8220700 9.8304757 .0010	2632
951 904401 860085351 30.8382879 9.8339238 .00103	
952 906304 862801408 30.8544972 9.8373695 .00103	
958 908209 865523177 30.8706981 9.8408127 .0010	
954 910116 868250664 30.8868904 9.8442536 .00104	
955 912025 870983875 30.9030743 9.8476920 .00104	
956 913986 873722816 30.9192497 9.8511280 .00104	
957 915849 876467493 30.9354166 9.8545617 .00104	
958 917764 879217912 30.9515751 9.857992900104	
959 919681 881974079 30,9677251 9.8614218 .0010	2753

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No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
960	921600	884736000	30.9838668	9.8648483	.001041667
961	923521	887503681	31.0000000	9.8682724	.001040583
962	925444	890277128	31.0161248	9.8716941	.001039501
963	927369	893056347	31.0322413	9.8751135	.001038422
964	929296	895841344	31.0483494	9.8785305	.001037344
965	931225	898632125	31.0644491	9.8819451	.001036269
966	933156	901428696	31.0805405	9.8853574	.001035197
967	935089	904231063	31.0966236	9.8887673	.001034126
968	937024	907039232	31.1126984	9.8921749	.001033058
969	938961		31.1120304	9.8955801	.001033033
		909853209			
970	940900	91267300 <b>0</b>	31.1448230	9.8989830	.001030928
971	942841	915498611	31.1608729	9.9023835	.001029866
972	944784	918330048	31.1769145	9.9057817	.001028807
973	946729	921167317	31.1929479	9.9091776	.001027749
974	948676				
		924010424	31.2089731	9.9125712	.001026694
975	950625	926859375	31.2249900	9.9159624	.001025641
976	952576	929714176	31.2409987	9.9193513	.001024590
977	954529	932574833	31.2569992	9.9227379	.001023541
978	956484	935441352	31.2729915	9.9261222	.001022495
979	958441	938313739	31.2889757	9.9295042	.001021450
980	960400	941192000	31.3049517	9.9328839	.001020408
981	962361	944076141	31.3209195	9.9362613	.001019368
982	964324	946966168	31.3368792	9.9396363	.001018330
983	966289	949862087	31.3528308	9.9430092	.001017294
984	968256	952763904	31.3687743	9.9463797	.001016260
985	970225	955671625	31.3847097	9.9497479	.001015228
986	972196	958585256	31.4006369	9.9531138	.001014199
987	974169	961504803	31.4165561		.001013171
				9.9564775	
988	976144	964430272	31.4324673	9.9598389	.001012146
989	978121	967361669	31.4483704	9.9631981	.001011122
990	980100	970299000	31.4642654	9.9665549	.001010101
991	982081	973242271	31.4801525	9.9699095	.001009082
992	984064	976191488	31.4960315	9.9732619	.001008065
993	986049	979146657	31.5119025	9.9766120	.001003003
994	988036	982107784	31.5277655	9.9799599	.001006036
995	990025	985074875	31.5436206	9.9833055	.001005025
996	992016	988047936	31.5594677	9.9866488	.001004016
997	994009	991026973	31.5753068	9.9899900	.001003009
998	996004	994011992	31.5911380	9.9933289	.001002004
999	998001	997002999	31.6069613	9.9966656	.001001001
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1000	1000000	1000000000	31.6227766	10.0000000	.001000000
1001	1002001	1003003001	31.6385840	10.0033322	.0009990010
1002	1004004	1006012008	31.6543836	10.0066622	.0009980040
1003	1006009	1009027027	31.6701752	10.0099899	.0009970090
1004	1008016	1012048064	31.6859590	10.0133155	.0009960159
1005	1010025	1015075125	31.7017349	10.0166389	.0009950249
1006	1012036	1018108216	31.7175030	10.0199601	.0009940358
1007	1014049	1021147343	31.7332633	10.0232791	.0009930487
1008	1016064	1024192512	31.7490157	10.0265958	.0009920635
1009	1018081	1027243729	31.7647603	10.0299104	.0009910803
1010	1020100	1030301000	31.7804972	10.0332228	.0009900990
1011	1022121	1033364331	31.7962262	10.0365330	.0009891197
1012	1024144	1036433728	31.8119474	10.0398410	.0009881423
1013	1026169	1039509197	31.8276609	10.0330410	.0009871668
1014	1028196	1042590744	31.8433666	10.0464506	.0009861933
1015	1030225	1045678375	31.8590646	10.0497521	.0009852217
1016	1032256	1048772096	31.8747549	10.0530514	.0009842520
1017	1034289	1051871913	31.8904374	10.0563485	.0009832842
1018	1036324	1054977832	31.9061123	10.0596435	.0009823183
1019	1088361	1058089859	31.9217794	10.0629364	.0009813543
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#### WEIGHTS AND MEASURES.

#### AVOIRDUPOIS WEIGHT.

UNITED STATES AND BRITISH.

Gra <u>in</u> s.	Drams.	Ounces.	Pounds.	Hundred- weight.	Gross Tons.
1, 27,34375 437,5 7000, 784000, 5680000,	.03657 1, 16. 256. 28672. 573440.	.002286 .0625 1. 16. 1792. 35840.	.000143 .003906 .0625 1. 112. 2240.	.00000128 .00003488 .00055804 .0089286 1. 20.	.000000176 .000001744 .00002790 .0004464 .05

1 pound avoirdupois = 1.215278 pounds troy.

1 net ton = 2000 pounds = .892857 gross ton.

# TROY WEIGHT. UNITED STATES AND BRITISH.

Grains.	Pennyweight.	Ounces.	Pounds.
$\begin{array}{c} 1\\ 24\\ 480\\ 5760 \end{array}$	.041667	.0020833	.0001736
	1.	.05	.0041667
	20.	1.	.0833333
	240.	12.	1.

1 pound troy = .822857 pound avoirdupois. 175 ounces troy = 192 ounces avoirdupois.

# APOTHECARIES' WEIGHT. UNITED STATES AND BRITISH.

Grains.	Scruples.	Drams.	Ounces.	Pounds.
1 20 60 480 5760	.05 1. 3. 24. 288.	.016667 .3333333 1, 8. 96.	.0020833 .0416667 .125 1.	.000173611 .0034722 .0104167 .0833333 1.

The pound, ounce and grain are the same as in troy weight. The avoirdupois grain = troy grain = apothecaries' grain.

#### WEIGHTS AND MEASURES—Continued.

#### LINEAR MEASURE.

#### UNITED STATES AND BRITISH.

Inches.	Feet.	Yards.	Rods.	Furlong.	Miles.
1 12 36 198 7920 63360	.08333 1. 3. 16.5 660. 5280.	.02778 .33333 1. 5.5 220. 1760.	.0050505 .0606061 .1818182 1. 40. 320.	.00012626 .00151515 .00454545 .025 1.	.00001578 .00018939 .00056818 .003125 .125

#### ROPE AND CABLE MEASURE.

- 1 inch = .111111 span = .013889 fathom = .0001157 cable's length.
- 1 span = 9 inches = .125 fathom = .00104167 cable's length.
- 1 fathom = 6 feet = 8 spans = 72 inches = .008333 cable's length.
- 1 cable's length = 120 fathoms = 720 feet = 960 spans = 8640 inches.

#### NAUTICAL MEASURE.

1 nautical mile, as adopted by the United States Coast and Geodetic Survey, equals the length of one minute of arc of a great circle of a sphere whose surface equals that of the earth = 6080.204 feet = 1.1516 statute miles.

1 league = 3 nautical miles = 18240.613 feet.

#### GUNTER'S CHAIN.

- 1 link = 7.92 inches = .01 chain = .000125 mile.
- 1 chain = 100 links = 66 feet = 4 rods = .0125 mile.
- 1 mile = 80 chains = 8000 links.

## SQUARE OR LAND MEASURE. UNITED STATES AND BRITISH.

Square Inches,	Square Feet.	Square Yards.	Square Rods,	Acres.	Square Miles.
$ \begin{array}{r} 1 \\ 144 \\ 1296 \\ 39204 \\ 6272640 \end{array} $	.006944 1. 9.0 272.25 43560. 27878400.	.0007716 .111111 1. 30.25 4840. 3097600.	.03306 1. 160. 102400.		.00000977 .0015625

- 1 square rood = 40 square rods.
- 1 acre = 4 square roods.
- 1 square acre = 208.71 feet square.

#### WEIGHTS AND MEASURES-Continued.

## CUBIC OR SOLID MEASURE.

#### UNITED STATES AND BRITISH,

1 cubic inch = .0005787 cubic foot = .000021433 cubic yard.

1 cubic foot = 1728 cubic inches = .03703704 cubic yard.

1 cubic yard = 27 cubic feet = 46656 cubic inches.

1 cord of wood = 128 cubic feet = 4 feet by 4 feet by 8 feet.

1 perch of masonry =24.75 cubic feet =16.5 feet by 1.5 feet by 1 foot. It is usually taken as 25 cubic feet.

## DRY MEASURE. UNITED STATES ONLY.

Pints.	Quarts.	Gallons.	Pecks,	Bushels.	Cubic Inches.
$1 \\ 2 \\ 8 \\ 16 \\ 64$	.50 1. 4. 8. 32.	.125 .25 1. 2. 8.	.0625 .125 .05 1.	.015625 .03125 .125 .25	33.6003125 67.200625 268.8025 537.605 2150.42

1 heaped bushel = 1.25 struck bushel, and the cone must be not less than 6 inches high.

## LIQUID MEASURE. UNITED STATES ONLY.

Gills.	Pints.	Quarts.	Gallons,	Barrels.	Cubic Inches.
1 4 8 32 2008	.25 1. 2. 8. 252.	.125 .5 1. 4. 126.	.03125 .125 .25 1. 31.5	.000498 .003968 .007937 .031746	7.21875 28.875 57.75 231. 7276.5

The British imperial gallon = 277.274 cubic inches or 10 pounds avoirdupois of pure water at  $62^{\circ}$  F. and barometer at 30 inches.

The British imperial gallon = 1.20032 United States gallons.

1 fluid drachm = 60 minims = .125 fluid ounce = .0078125 pint.

1 fluid ounce = 480 minims = 8 drachms = .0625 pint.

## WEIGHTS AND MEASURES—Concluded. METRIC SYSTEM.

MEASURES OF LENGTH, CAPACITY AND WEIGHT.

LENGTH.	Kilometre.	Hecto- metre.	Decametre.	Metre.	Decimetre.	Centimetre.	Millimetre.
CAPACITY.	Kilolitre or Stere.	Hectolitre or Decistere.	Decalitre or Centistere,	Litre or Millistere,	Decilitre.	Centilitre.	Millilitre.
WEIGHT.	Kilo- gramme.	Hecto- gramme.	Deca- gramme.	Gramme. Decigramm		Centi- gramme.	Milli- gramme.
	1	10	100 10 1	1000 100 10 10 1 .1 .01 .001	10000 1000 100 10 10 1 .1 .01	190000 10000 1000 100 100 10 1	1000000 100000 10000 1000 100 100 10 10

1 myriametre = 10 kilometres = 10000 metres.

1 tonne = 1000 kilogrammes = 100 quintals = 10 myriagrammes.

1 gramme = 1 cubic centimeter of distilled water at its maximum density at sea level in latitude of Paris and barometer at 760 millimetres.

1 litre = 1 cubic decimeter.

## METRIC SYSTEM. SQUARE OR SURFACE MEASURE.

Square Kilometre.	Square Hectometre or Hectare.	Square Decametre or Are.	Square Metre or Centiare.	Square Decimetre.	Square Centimetre.	Square Millimetre.
1	100 1 .01 .0001 .000001	10000 100 1 .01 .0001 .000001	1000000 10000 100 1 .01 .0001 .00001	1000000 10000 100 1 .01 .0001	1000000 10000 100 100 1	1000000 10000 100 100

1 square myriametre = 100 square kilometres = 100 000 000 square metres.

#### METRIC SYSTEM. CUBIC MEASURE.

Cubic Decametre.	Gubic Metre.	Cubic Decimetre.	Cubic Centimetre.	Cubic Millimetre.
.001 .000001 .00000001	1000 1 .001 .000001 .000000001	1000000 1000 1 .001 .000001	1000000000 1000000 1000 1000 1	1000000000 1000000 1000 1000

1 cubic metre = 1 kilolitre = 1 stere.

# TABLES FOR CONVERTING UNITED STATES WEIGHTS AND MEASURES.

#### CUSTOMARY TO METRIC.

#### Weights.

	Grains.	Troy Ounces	Avoirdupois	Avoirdupois	Net Tons of	Gross Tons of
No.	to ··	-to	Ounces	Pounds to	2000 Pounds	2240 Pounds
	Milligrammes.	Grammes.	to Grammes.	Kilogrammes.	to Tonnes.	to Tonnes.
1	64,79892	31.10348	28,34953	.45359	.90718	1.01605
2	129.59784	62.20696	56.69905	.90718	1.81437	2.03209
3	194.39675	93.31044	85.04858	1.36078	2.75155	3.04814
4	259.19567	124.41392	113.39811	1.81437	3.62874	4.06419
5	323.99459	155.51740	141.74763	2.26796	4.53592	5.08024
6	388.79351	186.62088	170.09716	2.72155	5.44311	6.09628
7	453.59243	217.72437	198.44669	3.17515	6.35029	7.11233
8	518.39135	248.82785	226.79621	3.62874	7.25748	8.12838
9	583.19026	279.93133	255.14574	4.08233	8.16466	9.14442

1 Avoirdupois Pound = 453.5924277 Grammes.

#### Linear Measure.

No.	64ths of an	Inches	Feet to	Yards to	Statute Miles	Nautical Miles
	Millimetres.	Centimetres.	Metres.	Metres.	Kilometres.	Kilometres.
1 2 3 4 5 6 7 8	.39688 .79375 1.19063 1.58750 1.98438 2.38125 2.77813 3.17501 3.57188	2.54001 5.08001 7.62002 10.16002 12.70003 15.24003 17.78004 20.32004 22.86005	.304801 .609601 .914402 1.219202 1.524003 1.828804 2.133604 2.438405 2.743205	.914402 1.828804 2.743205 3.657607 4.572009 5.486411 6.400813 7.315215 8.229616	1.60935 3.21869 4.82804 6.43739 8.04674 9.65608 11.26543 12.87478 14.48412	1.85325 3.70650 5.55975 7.41300 9.26625 11.11950 12.97275 14.82600 16.67925

1 Nautical Mile = 1853.25 Metres.

1 Gunter's Chain = 20.1168 Metres.

1 Fathom = 1.829 Metres.

# METRIC TO CUSTOMARY.

## Weights.

	Milligrammes	Grammes	Grammes	Kilogrammes	- Tonnes to	Tonnes to
No.	to	·· to	to Avoirdupois	to Avoirdupois	Net Tons of	Gross Tons of
	Grains.	Troy Ounces.	Ounces.	Pounds.	2000 Pounds.	2240 Pounds.
1	.01543	.03215	.03527	2.20462	1.10231	.98421
2	.03086	.06430	.07055	4.40924	2.20462	1.96841
3	.04630	.09645	.10582	6.61387	3.30693	2.95262
4	.06173	.12860	.14110	8.81849	4.40924	3.93682
5	.07716	.16075	.17637	11.02311	5.51156	4.92103
6	.09259	.19290	.21164	13.22773	6.61387	5.90524
7	.10803	.22506	.24692	15.43236	7.71618	6.88944
8	.12346	.25721	.28219	17.63698	8.81849	7.87365
9	.13889	.28936	.31747	19.84160	9.92080	8.85785

1 Kilogramme = 15432,35639 Grains.

### Linear Measure.

	Millimetres	Centimetres	Metres	Metres	Kilometres	Kilometres
No.	to 64ths of an	to	to	to	to	to
	Inch.	Inches.	Feet.	Yards.	Statute Miles.	Nautical Miles.
1	2,51968	.39370	3,280833	1.093611	.62137	.53959
2	5.03936	.78740	6.561667	2.187222	1.24274	1.07919
3	7.55904	1.18110	9.842500	3.280833	1.86411	1.61878
4 5	10.07872	1.57480	13.123333	4.374444	2.48548	2.15837
5	12.59840	1.96850	16.404167	5.468056	3.10685	2.69796
6	15.11808	2.36220	19.685000	6.561667	3.72822	3.23756
7	17.63776	2.75590	22.965833	7.655278	4.34959	3.77715
8	20.15744	3.14960	26.246667	8.748889	4.97096	4.31674
9	22.67712	3.54330	29.527500	9.842500	5.59233	4.85633

## CUSTOMARY TO METRIC.

## Square Measure.

No.	Square Inches to Square Centimetres.	Square Feet to Square Metres.	Square Yards to Square Metres.	Acres to Hectares.	Square Miles to Square Kilometres.
1 2 3 4 5 6 7 8	6.45163 12.90325 19.35488 25.80650 32.25813 38.70975 45.16138 51.61300 58.06463	.09290 .18581 .27871 .37161 .46452 .55742 .65032 .74323 .83613	.83613 1.67226 2.50839 3.34452 4.18065 5.01679 5.85292 6.68905 7.52518	.40470 .80939 1.21409 1.61879 2.02349 2.42818 2.83288 3.23758 3.64228	2.59000 5.18000 7.77000 10.35999 12.94999 15.53999 18.12999 20.71999 23.30999

<sup>1</sup> Square Statute Mile = 259.00 Hectares.

### Cubic Measure,

	Cubic Inches	Cubic Inches	Cubic Feet	Cubic Yards
No.	to	to	to	to
	Cubic Centimetres.	Cubic Decimetres.	Cubic Metres.	Cubic Metres.
1 2 3 4 5 6 7 8	16.38716 32.77432 49.16148 65.54864 81.93580 98.32296 114.71013 131.09729 147.48445	.01639 .03277 .04916 .06555 .08194 .09832 .11471 .13110	.02832 .05663 .08495 .11327 .14159 .16990 .19822 .22654	.76456 1.52912 2.29368 3.05824 3.82280 4.58736 5.35192 6.11648 6.88104

### METRIC TO CUSTOMARY.

### Square Measure.

No,	Square Centi- metres to Square Inches.	Square Metres to Square Feet.	Square Metres to Square Yards.	Hectares to Acres.	Square Kilo- metres to Square Miles.
1 2 3 4 5 6 7 8	.15500 .31000 .46500 .62000 .77500 .93000 1.08500 1.24000 1.39500	10.76387 21.52773 32.29160 43.05547 53.81934 64.58320 75.34707 86.11094 96.87481	1.19599 2.39197 3.58796 4.78394 5.97993 7.17591 8.37190 9.56788 10.76387	2.47104 4.94209 7.41313 9.88418 12.35522 14.82626 17.29731 19.76835 22.23940	.38610 .77220 1.15830 1.54440 1.93050 2.31660 2.70270 3.08880 3.47490

1 Hectare = .003861 Square Statute Mile.

### Cubic Measure.

No.	Cubic Centimetres to Cubic Inches.	Cubic Decimetres to Cubic Inches.	Cubic Metres to Cubic Feet.	Cubic Metres to Cubic Yards,
1	.06102	61.02338	35.31445	1.30794
2	.12205	122.04676	70.62891	2.61589
3	.18307	183.07013	105.94336	3.92383
4	.24409	244.09351	141.25782	5.23177
5	.30512	305.11689	176.57227	6.53971
6	.36614	366.14027	211.88673	7.84766
7	.42716	427.16365	247.20118	9.15560
8	.48819	488.18702	282.51564	10.46354
9	.54921	549.21040	317.83009	11.77149

## CUSTOMARY TO METRIC.

## Capacity Measures.

No.	Liquid Quarts to Litres.	Gallons to Litres.	Gallons to Cubic Metres.	Bushels to Hectolitres.	Fluid Drachms to Millilitres or Cubic Centimetres.	Fluid Ounces to Millilitres or Cubic Centimetres.
1	.94636	3.78543	.00379	.35239	3.69671	29.57370
2	1.89272	7.57087	.00757	.70479	7.39343	59.14741
3	2.83908	11.35630	.01136	1.05718	11.09014	88.72111
4	3.78543	15.14174	.01514	1.40957	14.78685	118.29482
5	4.73179	18.92717	.01893	1.76196	18.48357	147.86852
6	5.67815	22.71260	.02271	2.11436	22.18028	177.44222
7	6.62451	26.49804	.02650	2.46675	25.87699	207.01593
8	7.57087	30.28347	.03028	2.81914	29.57370	236.58963
9	8.51723	34.06891	.03407	3.17154	33.27042	266.16334

### Miscellaneous.

No.	Pounds per Lineal Foot to Kilogrammes per Lineal Metre.	Pounds per Square Inch to Kilogrammes per Square Centimetre,	Pounds per Square Foot to Kilogrammes per Square Metre.	Pounds per Cubic Foot to Kilogrammes per Cubic Metre,	Foot-Pounds to Kilogramme- Metres.	United States Horsepower to Metric Horsepower.
1 2 3 4 5 6 7 8	1.48816 2.97632 4.46448 5.95264 7.44081 8.92897 10.41713 11.90529 13.39345	.07031 .14061 .21092 .28123 .35153 .42184 .49215 .56245 .63276	4.88241 9.76482 14.64723 19.52963 24.41204 29.29445 34.17686 39.05927 43.94168	16.01837 32.03674 48.05510 64.07348 80.09185 96.11021 112.12858 128.14695 144.16532	.13826 .27651 .41477 .55302 .69128 .82953 .96779 1.10604 1.24430	1.01387 2.02775 3.04162 4.05549 5.06937 6.08324 7.09711 8.11098 9.12486

### METRIC TO CUSTOMARY.

## Capacity Measures.

No.	Litres to Fluid Quarts.	Litres to Gallons,	Cubic Metres to Gallons.	Hectolitres to Bushels	Millilitres or Cubic Centi- metres to Fluid Drachms.	Millilitres or Cubic Centi- metres to Fluid Ounces.
1	1.05668	.26417	264.17047	2.83774	.27051	.03381
2	2.11336	.52834	528.34093	5.67548	.54102	.06763
2	3.17005	.79251	792.51140	8.51323	.81153	.10144
4	4.22673	1.05668	1056,68187	11.35097	1.08204	.13526
5	5.28341	1.32085	1320.85234	14.18871	1.35255	.16907
6	6.34009	1.58502	1585.02280	17.02645	1.62306	.20288
7	7.39677	1.84919	1849.19327	19.86420	1.89357	.23670
8	8.45345	2.11336	2113.36374	22.70194	2.16408	.27051
9	9.51014	2.37753	2377.53420	25.53968	2.43460	.30432

### Miscellaneous.

No.	Kilogrammes per Lineal Metre to Pounds per Lineal Foot.	Kilogrammes per Square Centimetre to Pounds per Square Inch.	Kilogrammes per Square Metre to Pounds per Square Foot.	Kilogrammes per Cubic Metre to Pounds per Cubic Foot.	Kilogramme- Metres to Foot-Pounds,	Metric Horsepower to United States Horsepower.
1	.67197	14.22340	.20482	.06243	7.23300	.98632
2	1.34393	28.44680	.40963	.12486	14.46600	1.97264
3	2.01590	42.67020	.61445	.18728	21.69899	2.95895
4	2.68787	56.89359	.81927	.24971	28.93199	3.94527
5	3.35984	71.11699	1.02408	.31214	36.16499	4.93159
6	4.03180	85.34039	1.22890	.37457	43.39799	5.91791
7	4.70377	99.56379	1.43372	.43700	50.63098	6.90423
8	5.37574	113.78719	1.63854	.49943	57.86398	7.89054
9	6.04770	128.01059	1.84335	.56185	65.09698	8.87686

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